Attachment F

*Information Submitted for the Limestone Generating Station and the W A Parish Electric Generating Station*

Contents:

Part 1: *Submittal Letter from NRG to the TCEQ*

Part 2: *Information on Limestone Generating Station*

Part 3: *Information on W A Parish Electric Generating Station*
Attachment F

*Information Submitted for the Limestone Generating Station and the W A Parish Electric Generating Station*

Part 1:

*Submittal Letter from NRG to the TCEQ*
July 24, 2015

Via Email

David Brymer
Director, Air Quality Division
Texas Commission on Environmental Quality
12100 Park 35 Circle
Austin, TX 78753

Re: NRG Texas Power LLC
Demonstrations of 1-Hour SO2 NAAQS Attainment Status
Limestone and W.A. Parish Power Plants

Dear Mr. Brymer:

NRG Texas Power LLC ("NRG") respectfully offers the attached air quality demonstrations for the Limestone and W.A. Parish facilities regarding EPA’s proposed actions on the 1-hour SO2 National Ambient Air Quality Standard (NAAQS) in Texas.

NRG is a subsidiary of NRG Energy, Inc., a Fortune 250 Company and one of the country’s largest power generation and retail electricity businesses. NRG Energy’s power plants provide about 52,000 megawatts of generation capacity and its retail businesses serve more than 3 million customers throughout the country. In Southeast Texas, NRG owns more than 11,000 MW of generation capacity from nine electric generating stations. NRG supports clean energy resources and technologies critical to our transition to a sustainable, low carbon society.

The attached reports demonstrate that the ambient air around NRG’s Limestone and Parish plants meets the 1-hour SO2 NAAQS. These demonstrations have been made using air dispersion modeling and take into account representative actual emissions from the Limestone and W.A. Parish plants, other nearby SO2 sources, and background SO2 levels. We believe that this information supports Texas’ recommendation that all areas of the state should be designated as attainment or unclassifiable for the 1-hour SO2 NAAQS.

NRG appreciates your consideration of this information. Please contact me at 832-357-5291 or craig.eckberg@nrg.com if you have any questions or require additional information.

Sincerely,

Craig Eckberg
NRG Texas Power LLC
Attachments


Attachment F

*Information Submitted for the Limestone Generating Station*

and the *W A Parish Electric Generating Station*

Part 2:

*Information on Limestone Generating Station*
SO₂ Air Dispersion Modeling
Report for Limestone Generating Station

July 24, 2015

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Farrar, Texas

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# TABLE OF CONTENTS

1.0 **INTRODUCTION**  
1.1 PROJECT OVERVIEW  
1.2 OVERVIEW OF METHODOLOGY  

2.0 **FACILITY DESCRIPTION AND REGULATORY SETTING**  
2.1 FACILITY LOCATION  
2.2 SO₂ ATTAINMENT STATUS  
2.3 SOURCE PARAMETERS AND EMISSION RATES  

3.0 **AIR DISPERSION MODELING ANALYSIS**  
3.1 MODEL SELECTION AND APPLICATION  
3.2 THE 1-HOUR SO₂ NAAQS  
3.3 METEOROLOGICAL DATA  
3.3.1 Meteorological Data Refinements  
3.4 RECEPTOR GRID  
3.5 GOOD ENGINEERING PRACTICE STACK HEIGHT ANALYSIS  
3.6 AMBIENT SO₂ BACKGROUND DATA FOR CUMULATIVE MODELING  
3.7 REVIEW OF NON-FACILITY SOURCES FOR CUMULATIVE INVENTORY  

4.0 **MODELING RESULTS**  
4.1 CONCLUSIONS  

5.0 **REFERENCES**
TABLE OF CONTENTS (Cont’d)

List of Tables

Table 2-1: Limestone Station Point Sources – Stack Parameters
Table 3-1: Characteristics of the Corsicana Municipal Airport Meteorological Data
Table 3-2: Summary of Limestone Station GEP Analysis
Table 3-3: SO₂ Emissions within 50 km of SO₂ Monitors Closest to Limestone
Table 3-4: Seasonal Diurnal Ambient SO₂ Concentrations (µg/m³)
Table 3-5: Major Source Considered for Cumulative Modeling Study
Table 3-6: Cumulative Inventory Source Parameters
Table 4-1: 1-hour SO₂ Modeling Results for Limestone Station (µg/m³)

List of Figures

Figure 1-1: Limestone Station Surroundings and Land Use
Figure 2-1: Limestone Station Site Plan
Figure 2-2: Limestone Station Local Topography
Figure 3-1: Relative Location of Facility and Meteorological Site
Figure 3-2: Three-year Wind Rose (2012-2014): Corsicana Municipal Airport
Figure 3-3: Area Terrain Elevations
Figure 3-4: Corsicana Municipal Airport – 1km Aerial
Figure 3-5: Corsicana Municipal Airport – 1km 1992 NLCD Land Use
Figure 3-6: Limestone Station – 1km Aerial
Figure 3-7: Limestone Station – 1km 1992 NLCD Land Use
Figure 3-8: Limestone Station – 1km 1992 NLCD Land Use – Corrected
Figure 3-9: Example of “Upwind” based on AERSURFACE
Figure 3-10: Example of “Upwind” based on the “Wedge” Approach
Figure 3-11: Near-Field Model Receptors
Figure 3-12: Far-Field Model Receptors
Figure 3-13: Structures Included in the Limestone GEP Analysis
Figure 3-14: SO₂ Sources and Monitors in the Region
Figure 3-15: SO₂ Concentration vs. Wind Direction at Corsicana Monitor
Figure 3-16: SO₂ Concentration vs. Wind Direction at Waco Monitor
Figure 3-17: Relative Location of Limestone and Major Sources in the Region
Figure 4-1: Limestone Station 1-hour SO₂ Impact Contours Including Background
1.0 INTRODUCTION

Environmental Resources Management (ERM), presents this air dispersion modeling report to Baker Botts, L.L.P (Baker Botts) documenting that maximum model-predicted Sulfur Dioxide (SO₂) impacts from NRG’s Limestone Generating Station (Limestone) are in attainment with the 1-hour SO₂ National Ambient Air Quality Standard (NAAQS). This analysis shows that the ambient air quality in the vicinity of Limestone, currently undesignated for the 1-hour SO₂ NAAQS, is below the standard and should be identified as “attainment” status in the next cycle of designations.

This modeling report describes the modeling methodology that was used to evaluate potential impacts of SO₂ emissions from Limestone on ambient air quality.

1.1 PROJECT OVERVIEW

Unlike previous NAAQS attainment demonstrations, EPA has proposed to make 1-hour SO₂ NAAQS attainment determinations using ambient air monitoring data and/or air dispersion modeling. In situations where air modeling is used to make this determination, the approach described in EPA’s proposed “Modeling Technical Assistance Document” (TAD)¹ could be used, which sets forth a significantly different technical approach compared to conventional regulatory modeling prescribed by 40 CFR Part 51, Appendix W (EPA’s Guideline on Air Quality Models). This approach would also be expected to meet EPA’s proposed 1-Hour SO₂ Data Requirements Rule (DRR).

EPA distinguishes the approaches described in the SO₂ Modeling TAD to “reflect a view that designations are intended to address current actual air quality (i.e., modeling simulates a monitor), and thus are unlike attainment plan modeling, which must provide assurances that attainment will occur.” EPA’s proposed approach would utilize several distinctive technical approaches, including but not limited to the following:

- Simulating actual emissions and exhaust conditions (e.g., temperature and flowrate) on an hourly basis reflecting actual operations for a specified historical time period;
- Representing actual stack heights, irrespective of the GEP limitations;
- Limiting modeled ambient air receptors to locations where monitoring could actually take place and locations that would conventionally be considered “ambient air” for regulatory and permitting purposes, by excluding waterways, roadways, railways, restricted access property, and other locations not accessible to the general public or where a monitor could not reasonably be sited; and

¹ [http://epa.gov/oaqps001/sulfurdioxide/pdfs/SO2ModelingTAD.pdf](http://epa.gov/oaqps001/sulfurdioxide/pdfs/SO2ModelingTAD.pdf)
ERM performed a modeling analysis evaluating the impacts on ambient air quality from SO\textsubscript{2} emissions at Limestone. In addition, although the approach for considering cumulative ambient impacts with other SO\textsubscript{2} sources in the region is not specifically covered in the proposed DRR, ERM considered other sources of SO\textsubscript{2} within 50 kilometers for inclusion in the modeling.

As discussed in this report, ERM’s approach to the modeling analysis used those refinements directly addressed in the proposed DRR, i.e. the use of actual hourly emissions, actual stack heights, and seasonal diurnal ambient background concentrations.

As shown in this modeling report, SO\textsubscript{2} impacts from Limestone Generating Station emission sources, when combined with modeled impacts from other large SO\textsubscript{2} sources in the region and ambient air concentrations taken from a representative nearby monitor, are below the 1-hour SO\textsubscript{2} NAAQS.

This first section of this report describes the modeling methodology that was followed. Section 2 provides a description of the facility and the emissions included in the modeling. Model selection and the methodology used in the modeling are described in Section 3. The modeling results are presented in Section 4. References are provided in Section 5.

### OVERVIEW OF METHODOLOGY

ERM’s assessments were conducted in a manner consistent with United States Environmental Protection Agency (EPA) and Texas Commission on Environmental Quality (TCEQ) air quality regulations and modeling guidelines, including the following EPA documents:

- “SO\textsubscript{2} NAAQS Designations Modeling Technical Assistance Document (Draft),” December 2013;
- “SO\textsubscript{2} NAAQS Designations Monitoring Technical Assistance Document (Draft),” December 2013;
- “Data Requirements Rule for the 1-Hour Sulfur Dioxide (SO\textsubscript{2}) Primary National Ambient Air Quality Standard (NAAQS),” Pre-publication proposed rule, April 17, 2014 (published in the Federal Register on May 13, 2014 79FR 27446); and
- “Guidance for 1-hour SO\textsubscript{2} Nonattainment Area SIP Submissions,” April 23, 2014.
As well as:


The steps that were undertaken by ERM to conduct the air dispersion modeling analyses are summarized below:

- Compiled information on the parameters and characteristics for all sources of SO\textsubscript{2} emissions at Limestone including the 2 main EGU’s.
- Developed a comprehensive receptor grid to capture the maximum off-site impacts from Limestone sources.
- Reviewed regional ambient background monitors to determine the most appropriate ambient background concentration data for SO\textsubscript{2} to represent sources not explicitly included in the modeling runs.
- Developed 3 years (2012-2014) of meteorological data using surface observations from Corsicana Municipal Airport in Corsicana, TX with upper air data from Fort Worth, TX using the most recent version (v.14134) of AERMET, the meteorological data processor for AERMOD, and its two preprocessors: AERSURFACE (v.13016) and AERMINUTE (v.14237).
- Reviewed sources of SO\textsubscript{2} within 50 kilometers of Limestone for possible inclusion in the cumulative modeling analysis using the 2011 National Emission Inventory Database\textsuperscript{2}, based on guidance included in the SO\textsubscript{2} Modeling TAD. Sources above the proposed DRR threshold were included in the cumulative modeling analysis.
- Conducted an air dispersion modeling analysis using the most recent version of EPA’s regulatory dispersion model, AERMOD (v.14134) and 3 years of actual emissions data (2012-2014) from Limestone Sources and other large SO\textsubscript{2} sources in the region, consistent with the methodology described in the proposed SO\textsubscript{2} Data Requirements Rule and SO\textsubscript{2} Modeling TAD.
- Summarized the results and compared them with the 1-hour SO\textsubscript{2} NAAQS to determine a recommended attainment designation for the vicinity of Limestone.

Figure 1-1 depicts the location of the Limestone Station and surrounding land use.

\textsuperscript{2} http://www.epa.gov/ttnchie1/net/2011inventory.html
Figure 1-1: Limestone Station Surroundings and Land Use
2.0 FACILITY DESCRIPTION AND REGULATORY SETTING

2.1 FACILITY LOCATION

The Limestone Generating Station is located in the town of Farrar, TX. The station is located about 98 miles south-southwest of downtown Dallas, TX and 126 miles north-northwest of Houston, TX. The site is accessed by Texas Rt. 39. Approximate site coordinates are 31.423° North Latitude, 96.253° West Longitude. The Universal Transverse Mercator (“UTM”) coordinates of the facility are 761,111 Easting and 3,479,736 Northing (using North American Datum of 1983 - NAD83) in UTM Zone 14. The base elevation of the facility is 450’ (137.2m) above sea level. A full scale site plan of Limestone is shown in Figure 2-1, and Figure 2-2 shows the site location marked on a United States Geological Survey (“USGS”) 7.5-minute topographic map.

2.2 SO₂ ATTAINMENT STATUS

In July 2013, EPA issued a rule designating 29 counties or partial counties as non-attainment for 1-hour SO₂. However, the vast majority of the country was not designated by EPA at that time. Neither Limestone County, where Limestone is located, nor any of the surrounding counties have been classified as attainment or non-attainment for 1-hour SO₂ NAAQS.
Figure 2-1: Limestone Station Site Plan
2.3 SOURCE PARAMETERS AND EMISSION RATES

For this 1-hour SO\textsubscript{2} NAAQS modeling demonstration, all major sources of SO\textsubscript{2} at the facility were included in the modeling. Per the proposed 1-hour SO\textsubscript{2} Data Requirements Rule and SO\textsubscript{2} Modeling TAD, the most recent 3 years of actual emissions data, along with the actual stack heights of all sources, were used in the modeling. The following provides a description of all Limestone SO\textsubscript{2} emission sources represented in the model. Table 2-1 summarizes the characteristics of the emissions sources that were included in the modeling. The actual emissions data used in the modeling are described below:

- Units No. 1 and No. 2 (Source ID’s: LMS1 and LMS2). These units are lignite/coal fired utility boilers that produce steam for the generation of electricity. For these units, three years (2012-2014) of actual hourly emissions, stack temperature, and exhaust flow rate data were input into the model. These data were provided by NRG based on CEMS data collected at each source. As per the proposed 1-hour SO\textsubscript{2} Data Requirements Rule, the actual height of each stack was represented in the model for each source.

- Other sources at the site include emergency engines and fire pumps. These sources are used exclusively in emergency situations except for approximately one hour/week testing. Therefore, in accordance with USEPA guidance for intermittent sources, the emergency generator and fire pump engine were not included in the modeling demonstration for the 1-hour SO\textsubscript{2} NAAQS.

| Table 2-1: Limestone Station Point Sources – Stack Parameters |

<table>
<thead>
<tr>
<th>Description</th>
<th>Model Source</th>
<th>Stack Height</th>
<th>Exit Temperature</th>
<th>Exit Velocity</th>
<th>Stack Diameter</th>
</tr>
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<tbody>
<tr>
<td></td>
<td></td>
<td>(ft)</td>
<td>(m)</td>
<td>(F)</td>
<td>(K)</td>
</tr>
<tr>
<td>Unit 1 Boiler\textsuperscript{1}</td>
<td>LMS1</td>
<td>565</td>
<td>172.21</td>
<td>---</td>
<td>---</td>
</tr>
<tr>
<td>Unit 2 Boiler\textsuperscript{1}</td>
<td>LMS2</td>
<td>565</td>
<td>172.21</td>
<td>---</td>
<td>---</td>
</tr>
</tbody>
</table>

\textsuperscript{1} For the 2 main boilers, exit temperature and exit velocity varied on an hourly basis based on CEMS data.
3.0 AIR DISPERSION MODELING ANALYSIS

ERM conducted the modeling analysis for Limestone to quantify ambient impacts of SO$_2$ relative to the 1-hour NAAQS following the proposed approach described in the SO$_2$ Modeling TAD.

3.1 MODEL SELECTION AND APPLICATION

The latest version of USEPA’s AERMOD model (v.14134) was used for predicting ambient impacts for 1-hour SO$_2$. Regulatory default options were used in the analysis. Model predicted impacts were combined with an ambient background concentration and compared to the 1-hour SO$_2$ NAAQS to determine the recommended attainment status of the area in the vicinity of the facility.

3.2 THE 1-HOUR SO$_2$ NAAQS

This study focuses on the maximum model-predicted 1-hour SO$_2$ impacts of Limestone and compares them to the 1-hour SO$_2$ NAAQS. The new standard came into effect in August, 2010. The form of the standard is the $99^{th}$ percentile of the 3-year average 1-hour daily maximum concentration, and the standard was set to 75 ppb (196.5 µg/m$^3$).

3.3 METEOROLOGICAL DATA

Guidance for regulatory air quality modeling recommends the use of one year of on-site meteorological data or five years of representative off-site meteorological data. The SO$_2$ Modeling TAD however, specifies that 3 years of meteorological data concurrent to the actual emissions data being input into the model be used. Since on-site data are not available for the Limestone site, meteorological data available from the National Weather Service (NWS) were used in this analysis.

Three years (2012-2014) of surface observations from the NWS tower at Corsicana Municipal Airport in Corsicana, TX (WBAN No. 53912) and concurrent upper air data from Fort Worth, TX (WBAN No. 03990) were provided by TCEQ and further refined as described in Section 3.3.1. The meteorological data were processed with the most recent version of AERMET (v.14134) the meteorological preprocessor for AERMOD, along with the two preprocessors to AERMET: AERSURFACE (v.13016) and AERMINUTE (v.14237). AERMET was applied to create the two meteorological data files required for input to AERMOD.

The data characteristics of Corsicana Municipal Airport are shown in Table 3-1. Figure 3-1 shows the relative location of the airport and Limestone, and Figure 3-2 shows the 3-year wind rose for Corsicana Municipal Airport.
Table 3-1: Characteristics of the Corsicana Municipal Airport Meteorological Data

<p>| | |</p>
<table>
<thead>
<tr>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td>Distance from Limestone Station</td>
<td>42.8 miles</td>
</tr>
<tr>
<td>Average Wind Speed</td>
<td>4.25 m/s</td>
</tr>
<tr>
<td>Percent Calm Hours</td>
<td>1.83%</td>
</tr>
<tr>
<td>Data Completeness</td>
<td>98.72%</td>
</tr>
</tbody>
</table>

Figure 3-1: Relative Location of Facility and Meteorological Site
Figure 3-2: Three-year Wind Rose (2012-2014): Corsicana Municipal Airport

<table>
<thead>
<tr>
<th>WIND ROSE PLOT:</th>
<th>DISPLAY:</th>
</tr>
</thead>
<tbody>
<tr>
<td>3-Year Wind Rose: Corsicana Municipal Airport</td>
<td>Wind Speed Direction (blowing from)</td>
</tr>
<tr>
<td>2012-2014</td>
<td></td>
</tr>
</tbody>
</table>

**Wind Speed (m/s):**

- >= 11.10
- 8.80 - 11.10
- 5.70 - 8.80
- 3.60 - 5.70
- 2.00 - 3.60
- 0.50 - 2.00
- Calm: 1.83%

**Comments:**

<table>
<thead>
<tr>
<th>DATA PERIOD:</th>
<th>COMPANY NAME:</th>
</tr>
</thead>
<tbody>
<tr>
<td>Start Date: 1/1/2012 - 00:00</td>
<td>ERM</td>
</tr>
<tr>
<td>End Date: 12/31/2014 - 23:00</td>
<td></td>
</tr>
</tbody>
</table>

**Modeler:**

R. Hamel

**Calm Winds:**

1.83%

**Total Count:**

25968 hrs.

**Avg. Wind Speed:**

4.25 m/s

**Date:**

7/22/2015

**Project No.:**

ERM View - Lakes Environmental Software
3.3.1 Meteorological Data Refinements

EPA and TCEQ guidelines recommend that meteorological data from a representative measurement station be used in modeling analyses to address ambient impacts. This section discusses the representativeness of data collected at the Corsicana Municipal Airport, and also describes how these data were processed to generate AERMOD-ready input files. AERMET is the recommended processor for developing inputs to AERMOD. AERMET requires, at a minimum, hourly surface data and once-daily (morning) upper air sounding profiles. The processing program produces two files for input to AERMOD: a surface file containing calculated micrometeorological variables (heat flux, stability, and turbulence parameters) that represent the dispersive potential of the atmosphere, and a profile file that provides vertical profiles of wind speed, wind direction, and temperature. In the case of meteorological data files developed from NWS data, the profiles contain only one level (the surface level) and a meteorological interface within AERMOD generates vertical profiles of wind, temperature, and turbulence from the input data files. It is important to consider the full set of processing steps, including the profiling done within AERMOD, when evaluating the representativeness of a measurement site for application at a particular location such as the Limestone Station.

Meteorological representativeness is a function of a number of factors, including distance between the measurement and application site, and land use and terrain near the measurement site compared to land use and terrain in the vicinity of the application site. Differences are expected between airport land use and land use surrounding almost any application site, and frequently there are differences in terrain between measurement and application sites. Neither EPA nor TCEQ have established quantitative criteria for assessing whether differences are significant; therefore, this comparison is made based on a qualitative assessment and consideration of the importance of the land use and terrain differences to the analysis.

Terrain

Figure 3-1 displayed the relative locations of the airport and Limestone Station; as noted previously, the airport is approximately 43 miles (69 kilometers) north of the Station. Figure 3-3 provides a depiction of terrain elevations surrounding the airport and the Station. This part of Texas is relatively flat; the airport is only about 5 meters lower in elevation than the Station, and as Figure 3-3 shows there are no intervening elevated terrain features that could significantly affect wind flow. Figure 3-2 displayed a wind rose based on measurements at the airport; the predominant south to south-southeast flow, with secondary northerly flow, is typical of many locations in East Texas and is thus indicative that the winds measured at the airport are representative of a large area.
Land Use

Three parameters that represent land use characteristics around a measurement site are the Bowen ratio, noon-time albedo, and surface roughness. The Bowen ratio is an indicator of surface moisture and the albedo is a measure of the reflectivity of the land surface – together they are used by AERMET to estimate heat flux and other boundary layer parameters such as the convective mixing height and indicators of the stability of the atmosphere. The surface roughness is related to the heights of obstacles to the wind flow, and is used to parameterize other surface stability indicators in AERMET and is a factor in determining the strength of mechanical turbulence, and hence the degree of plume dispersion, in AERMOD. The focus of representativeness based on land use is on the three parameters Bowen ratio, albedo, and surface roughness.

The Bowen ratio and albedo associated with land use characteristics are calculated in AERSURFACE within an area 10km by 10km centered on the site being evaluated. Land use within an area this size surrounding the Corsicana Municipal Airport (reference Figure 3-1) contains roughly the same amount of developed areas as the area surrounding Limestone, and both sites have light wooded areas to the north. Most of the development around Corsicana is in the form of small residential neighborhoods, while most of the area surrounding Limestone is characterized by gas and oil extraction, which, while somewhat
industrialized, results in very few large structures in the area. Since there are no heavily industrialized or urbanized areas around the airport or power plant, it is expected that the Bowen ratio and albedo values for the two sites are similar. This is borne out by using AERSURFACE to determine these parameters for both sites. The albedo values produced by AERSURFACE for both sites are nearly identical – 0.15 to 0.18. The Bowen ratio values produced by AERSURFACE for the airport range from 0.42 to 0.80; and almost identical – 0.44 to 0.80 – at the Limestone site. These differences are not significant in terms of the overall effect on AERMET computations for boundary layer parameters and subsequent use in AERMOD.

Surface roughness is calculated by AERMET as a function of land use characteristics within a circle centered on the site being evaluated, with a recommended radius of 1 km. The current version of AERSURFACE utilizes the USGS NLCD 1992 land use data set as the source of land use information. To compare land use as it relates to surface roughness, ERM first evaluated whether significant changes have occurred since 1992 in the vicinity of the airport and the Limestone site, and evaluated on a qualitative basis the characteristics surrounding the airport anemometer compared to characteristics surrounding Limestone.

Figure 3-4 is current aerial view of the area within 1 km of the Corsicana anemometer. The NLCD 1992 land use data base identifies land use categories in 30 m cells as of 1992. The land use categories extracted from NLCD 1992 have been superimposed on the aerial image in Figure 3-5. As shown in the aerial image, the majority of the area surrounding the anemometer is relatively flat with occasional obstructions and developed areas, and forested areas to the north and northeast. The NLCD 1992 land use categories shown in Figure 3-5 display a similar pattern, that indicates that the 1992 data set adequately represents the area surrounding the anemometer, but with less developed areas. Figure 3-6 displays the area within 1 km of Limestone on a current aerial image, and Figure 3-7 displays the 1992 land use characteristics superimposed on the current aerial view of the area around Limestone. A qualitative evaluation of Figure 3-7 reveals that there are significant differences between the 1992 land use data and the actual site; it appears as though the 1992 data does not include the Limestone station at all. Because of these errors, ERM undertook an effort to correct the land us characterizations for Limestone, essentially replacing incorrect land use codes with corrected codes that better represent the land use throughout the 1 km circle. Figure 3-8 displays the corrected land use values surrounding Limestone.
Figure 3-4: Corsicana Municipal Airport – 1km Aerial

Figure 3-5: Corsicana Municipal Airport – 1km 1992 NLCD Land Use
Figure 3-6: Limestone Station – 1km Aerial

Figure 3-7: Limestone Station – 1km 1992 NLCD Land Use
An examination of the figures presented here reveals some differences and some similarities between land use surrounding the airport and land use surrounding the Limestone site. Since in particular some of the “Commercial Industrial Transportation” categories at the airport represent the runways, there is less to contribute to larger values of the roughness length at the airport than at the Limestone site. For some important reasons, however, the corrected land use values surrounding Limestone were used to characterize surface roughness for input to AERMET. The first is to capture directional differences between the airport and Limestone, consistent with the goal of the TAD to reproduce “what a monitor would measure” in mind. The second reason is related to the fact that the important dispersion regime for the stacks being modeled at Limestone is above the surface layer – with an average plume rise of approximately 150 meters, total plume height for the Limestone sources is in the range of 300 meters above the ground. Surface values of turbulence for these plumes are considerably less important than turbulence values determined for the layer several hundred meters above the surface. Since turbulence levels at plume height depend strongly on the roughness length (in addition to the stability parameters), a roughness length more representative of the site provides a more realistic, and ultimately more accurate, estimate of turbulence at plume level and therefore a more accurate depiction of “what a monitor would see” than roughness length values determined for the airport.
ERM calculated roughness length values on a seasonal and direction-specific basis, assigning roughness length values for each land use cell based on the values contained in Table A-3 of the AERSURFACE users’ guide (EPA, 2008). Effective roughness was calculated in a manner entirely consistent with AERSURFACE, namely as the distance-weighted geometric mean of all land use cells upwind of the sources being modeled, with the following formula:

\[
z_0 \text{effective} = \exp\left(\frac{\sum \ln(z_{0xy})}{\sum 1/d_{xy}}\right)
\]

AERSURFACE is not a required tool in the set of related AERMOD processing programs. ERM took a different approach than AERSURFACE in terms of determining which cells are “upwind” for a particular wind. This different approach is appropriate for situations where the stacks being modeled are separated by up to a few hundred meters, as it more accurately defines “upwind” as not based on a single point. An illustration of the difference between the AERSURFACE approach and the modified “wedge” approach used by ERM is illustrated in Figure 3-9 and Figure 3-10.

**Figure 3-9: Example of “Upwind” based on AERSURFACE**
Land use files were created based on this approach and combining the roughness length determinations with the Bowen ratio/albedo values generated by AERSURFACE. AERMINUTE was used to develop speed and direction values for low-wind hours. Upper air profiles were generated and filled in for the Fort Worth, TX upper air sounding station, and AERMET was run to create 3 years (2012-2014) of meteorological files used in AERMOD.

3.4 RECEPTOR GRID

A comprehensive Cartesian receptor grid extending out to approximately 20 kilometers (km) from Limestone was used in the AERMOD modeling analysis to assess maximum ground-level 1-hour SO$_2$ concentrations. The Modeling TAD states that the receptor grid must be sufficient to determine ambient air quality in the vicinity of the source being studied. The 20-kilometer receptor grid is more than sufficient to resolve the maximum 1-hour SO$_2$ impacts, and it clearly illustrates decreasing SO$_2$ concentration gradients in relation to the plant. Further, the receptor grid used in the modeling is consistent with the guidelines provided by the TCEQ for regulatory applications.

Specifically, the Cartesian receptor grid consisted of the following receptor spacing:

- 50-meter spacing along the facility fence line;
- 100-meter spacing extending from the fence line to 3 kilometers;
- 200-meter spacing extending from 3 to 5 kilometers;
• 500-meter spacing extending from 5 to 10 kilometers; and
• 1,000-meter spacing extending from 10 to 20 kilometers.

The above receptor data was used without modification in the modeling. Per the 1-hour SO$_2$ Modeling TAD, receptors located over areas where monitors could not reasonably be sited could be excluded from the modeling, but these receptors were retained in this analysis as a measure of conservatism.

Terrain elevations from National Elevation Data (“NED”) from USGS were processed using the most recent version of AERMAP (v.11103) to develop the receptor terrain elevations required by AERMOD. NED data files contain profiles of terrain elevations, which in conjunction with receptor locations are used to generate receptor height scales. The height scale is the terrain elevation in the vicinity of a receptor that has the greatest influence on dispersion at that location and is used for model computations in complex terrain areas. The near-field (within 5 kilometers) and far-field (full grid) receptor grids are shown in Figure 3-11 and Figure 3-12, respectively.
Figure 3-11: Near-Field Model Receptors
Figure 3-12: Far-Field Model Receptors
GOOD ENGINEERING PRACTICE STACK HEIGHT ANALYSIS

Good engineering practice ("GEP") stack height is defined as the stack height necessary to ensure that emissions from the stack do not result in excessive concentrations of any air pollutant as a result of atmospheric downwash, wakes, or eddy effects created by the source, nearby structures, or terrain features.

A GEP stack height analysis was performed for each stack using the Building Profile Input Program (BPIP) in accordance with USEPA’s guidelines (USEPA 1985). Per the guidelines, the physical GEP height, \( H_{\text{GEP}} \), is determined from the dimensions of all buildings which are within the region of influence using the following equations, depending on the construction data of the stack:

For stacks in existence on January 12, 1979 and for which the owner or operator had obtained all applicable permits or approvals required,

\[
H_{\text{GEP}} = 2.5H,
\]

provided the owner or operator produces evidence that this equation was actually relied on in establishing an emission limitation;

(1) For all other stacks:

\[
H_{\text{GEP}} = H + 1.5L
\]

where:

\[
H = \text{height of the structure within 5L of the stack which maximizes } H_{\text{GEP}};
\]

and

\[
L = \text{lesser dimension (height or projected width) of the structure.}
\]

For a squat structure, i.e., height less than projected width, the formula reduces to:

\[
H_{\text{GEP}} = 2.5H
\]

In the absence of influencing structures, a "default" GEP stack height is creditable up to 65 meters (213 feet).

A summary of the GEP stack height analyses is presented in Table 3-2. As described in the \( \text{SO}_2 \) Modeling TAD, when modeling actual emissions in order to determine the attainment status of the facility when compared to the 1-hour \( \text{SO}_2 \) NAAQS, the full height of all stacks is allowed in the modeling regardless of their GEP Formula Heights. Both stacks at Limestone are below their respective GEP heights so application of the \( \text{SO}_2 \) Modeling TAD did not affect the stack height assumptions for Limestone. The locations of all structures and sources included in the GEP analysis are shown in Figure 3-13. The output from BPIP
was input into AERMOD to represent aerodynamic downwash caused by structures around the stacks.

**Figure 3-13: Structures Included in the Limestone GEP Analysis**
Table 3-2: Summary of Limestone Station GEP Analysis

<table>
<thead>
<tr>
<th>Emission Source</th>
<th>Stack Height (m)</th>
<th>Controlling Buildings / Structures</th>
<th>Building Height (m)</th>
<th>Projected Width (m)</th>
<th>GEP Formula Height (m)</th>
</tr>
</thead>
<tbody>
<tr>
<td>LMS1</td>
<td>172.21</td>
<td>Unit 2 Boiler Bldg.</td>
<td>85.04</td>
<td>68.73</td>
<td>188.13</td>
</tr>
<tr>
<td>LMS2</td>
<td>172.21</td>
<td>Unit 1 Boiler Bldg.</td>
<td>85.04</td>
<td>69.07</td>
<td>188.64</td>
</tr>
</tbody>
</table>

1. In the absence of influencing structures, a “default” GEP stack height is creditable up to 65 meters (213 feet).

3.6 AMBIENT SO$_2$ BACKGROUND DATA FOR CUMULATIVE MODELING

In addition to assessing impacts from Limestone Station sources, the impact from other sources of SO$_2$ in the region were considered in order to demonstrate that the air quality in the region is in attainment with the NAAQS. Other sources of SO$_2$ in the vicinity of Limestone that were explicitly included in the modeling are discussed in Section 3.7. In order to account for other minor sources of SO$_2$ in the area an ambient background concentration was added to model-predicted impacts from Limestone and the other sources for comparison to the NAAQS.

The criteria for determining the monitor best suited to characterize air quality at a given location include:

- Stations with similar influencing SO$_2$ sources as the source being modeled (not necessarily the closest).
- Avoid stations influenced by the source being modeled to prevent double-counting impacts.
- Avoid stations influenced by sources not likely to interact with the source being modeled.
- Consider predicted concentration patterns for source being modeled, along with wind frequency, to assist in selection.

Figure 3-14 shows the location of the ambient monitors in the vicinity of Limestone Station, as well as the location of all other SO$_2$ sources in the region that emitted more than 1000 tons of SO$_2$ according to the 2011 EPA National Emissions Inventory. The figure shows that there are two sources that emitted over 1000 tons of SO$_2$ in 2011 within 50 km. Additionally, all of the monitors sited in the region are located to the north of Limestone, approaching the Dallas-Ft. Worth area.
ERM evaluated 3 monitors to determine their representativeness: Corsicana (Monitor ID# 48-349-1051) to the north of Limestone, Waco (Monitor ID# 48-309-1037), located west northwest of Limestone, and Italy (Monitor ID# 48-139-1044), located northwest of Limestone.

The first monitor evaluated was the Corsicana monitor. This monitor is the closest to Limestone in terms of proximity, located 69.5 km to the north. A review of the most recent (2012-2014) years of hourly concentrations at the monitor vs. the wind direction at the time the concentration was reported, shown in Figure 3-15, shows that virtually all of the highest concentrations at the monitor occur when the wind is blowing from the direction of Limestone, Big Brown Generating Station, or Streetman Glass towards the monitor.

Because the monitor is strongly influenced by impacts from Limestone, using the Corsicana monitor would result in “double counting” the impacts from the station. Additionally, Big Brown Generating Station was also explicitly included in the modeling and therefore impacts from that station on the monitor would be “double counting sources already included in the modeling. Lastly, Streetman Glass is much closer to the monitor than it is to Limestone Station and therefore is having a greater impact on the monitor than any source in the vicinity of
Limestone would have. Thus, the monitor is not useful to represent non-facility related impacts in the region.

**Figure 3-15: SO$_2$ Concentration vs. Wind Direction at Corsicana Monitor**

The next monitor reviewed was the Waco monitor, located 82.2 km northwest of Limestone, and oriented in a downwind direction from Limestone such that impacts from Limestone itself are no longer noteworthy. As shown in Figure 3-16, the concentrations recorded at the monitor do not appear to be highly influenced by any large sources, as would be the case near Limestone, and the only two large sources within 50 km of Limestone: Big Brown Generating Station and Oak Grove Station are explicitly included in the modeling as described in Section 3.7.

Sources that do not meet the 1,000 tons/year level were also considered. The TAD recommends that smaller sources be reviewed to determine the total magnitude of emissions and whether the smaller sources can be considered to be accounted for by background concentrations and whether they are clustered in areas where collectively the total magnitude may reach or exceed the 1,000 ton level. Table 3-3 provides a summary of the total SO$_2$ emissions (with and without 1,000 ton sources) within certain distance ranges of Limestone, and a summary of the total SO$_2$ emissions (with and without 1,000 ton sources) within certain distance ranges of the monitors closest to Limestone. Based on this analysis, the Waco monitor most closely matches the SO$_2$ emissions in the area around Limestone.
Lastly, in the initial screening modeling for Limestone the highest impacts were to the north of the plant. Thus any interaction with other sources would have to come from the south of Limestone, and the Waco monitor is more representative than Corsicana in representing ambient impacts coming from that direction. The Italy monitor was also considered, but the monitor is farther away from Limestone than Waco, and the pattern of SO$_2$ emissions is less similar to that of Limestone than Waco. For all of the reasons described here, Waco was chosen as the monitor most representative of the ambient air quality in the area around Limestone.

### Table 3-3: SO$_2$ Emissions within 50 km of SO$_2$ Monitors Closest to Limestone

<table>
<thead>
<tr>
<th>Monitor i.d.</th>
<th>Name</th>
<th>City</th>
<th>Kilometers from Limestone</th>
</tr>
</thead>
<tbody>
<tr>
<td>48-139-1044 Italy</td>
<td>Not_in_a_city</td>
<td>0, 4, 898</td>
<td>-59.82, 81.91, 101.43</td>
</tr>
<tr>
<td>48-309-1037 Waco</td>
<td>Waco</td>
<td>0, 1,020, 387</td>
<td>-77.58, 23.81, 81.15</td>
</tr>
<tr>
<td>48-349-1051 Corsicana</td>
<td>Corsicana</td>
<td>225, 0, 374</td>
<td>-15.36, 66.99, 68.72</td>
</tr>
</tbody>
</table>

### Figure 3-16: SO$_2$ Concentration vs. Wind Direction at Waco Monitor

EPA guidance allows simulation of background values that vary by season and hour of day that could simulate a lower value than the 99th percentile. The modeling was performed with a set of seasonal diurnal values developed using the methodology described in the USEPA March 1st, 2011 Clarification Memorandum for 1-hour NO$_2$ Modeling. Though this memorandum primarily addresses NO$_2$ modeling, page 20 describes the process for developing seasonal...
diurnal background values for SO₂ as well. The seasonal diurnal values used are shown in Table 3-4.

Table 3-4: Seasonal Diurnal Ambient SO₂ Concentrations (µg/m³)

<table>
<thead>
<tr>
<th>Hour</th>
<th>Winter</th>
<th>Spring</th>
<th>Summer</th>
<th>Fall</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>3.05</td>
<td>3.23</td>
<td>3.40</td>
<td>4.80</td>
</tr>
<tr>
<td>2</td>
<td>2.70</td>
<td>2.88</td>
<td>3.75</td>
<td>9.60</td>
</tr>
<tr>
<td>3</td>
<td>2.97</td>
<td>2.97</td>
<td>3.32</td>
<td>9.07</td>
</tr>
<tr>
<td>4</td>
<td>4.01</td>
<td>1.83</td>
<td>3.32</td>
<td>6.98</td>
</tr>
<tr>
<td>5</td>
<td>1.83</td>
<td>1.66</td>
<td>2.36</td>
<td>2.53</td>
</tr>
<tr>
<td>6</td>
<td>2.18</td>
<td>1.40</td>
<td>2.36</td>
<td>2.70</td>
</tr>
<tr>
<td>7</td>
<td>1.92</td>
<td>1.48</td>
<td>2.01</td>
<td>3.23</td>
</tr>
<tr>
<td>8</td>
<td>1.83</td>
<td>1.40</td>
<td>1.83</td>
<td>2.62</td>
</tr>
<tr>
<td>9</td>
<td>2.70</td>
<td>2.09</td>
<td>4.19</td>
<td>3.75</td>
</tr>
<tr>
<td>10</td>
<td>4.01</td>
<td>4.19</td>
<td>7.33</td>
<td>7.77</td>
</tr>
<tr>
<td>11</td>
<td>11.34</td>
<td>5.32</td>
<td>6.54</td>
<td>13.44</td>
</tr>
<tr>
<td>12</td>
<td>13.26</td>
<td>3.40</td>
<td>4.80</td>
<td>9.07</td>
</tr>
<tr>
<td>13</td>
<td>2.74</td>
<td>3.14</td>
<td>5.24</td>
<td>7.68</td>
</tr>
<tr>
<td>14</td>
<td>12.13</td>
<td>4.28</td>
<td>5.06</td>
<td>8.99</td>
</tr>
<tr>
<td>15</td>
<td>7.07</td>
<td>4.01</td>
<td>4.01</td>
<td>7.15</td>
</tr>
<tr>
<td>16</td>
<td>8.73</td>
<td>4.19</td>
<td>3.66</td>
<td>7.33</td>
</tr>
<tr>
<td>17</td>
<td>8.64</td>
<td>3.75</td>
<td>4.10</td>
<td>6.81</td>
</tr>
<tr>
<td>18</td>
<td>6.81</td>
<td>3.66</td>
<td>3.40</td>
<td>7.07</td>
</tr>
<tr>
<td>19</td>
<td>7.77</td>
<td>3.49</td>
<td>3.75</td>
<td>6.81</td>
</tr>
<tr>
<td>20</td>
<td>4.54</td>
<td>6.63</td>
<td>4.80</td>
<td>9.34</td>
</tr>
<tr>
<td>21</td>
<td>4.54</td>
<td>4.45</td>
<td>8.81</td>
<td>7.33</td>
</tr>
<tr>
<td>22</td>
<td>3.05</td>
<td>4.89</td>
<td>6.02</td>
<td>6.20</td>
</tr>
<tr>
<td>23</td>
<td>3.75</td>
<td>5.93</td>
<td>4.36</td>
<td>5.50</td>
</tr>
<tr>
<td>24</td>
<td>2.88</td>
<td>3.58</td>
<td>3.66</td>
<td>8.46</td>
</tr>
</tbody>
</table>

1. Hours in AERMOD are defined as hour-ending, i.e., Hour 1 is the period from midnight through 1 AM, etc.
3.7 REVIEW OF NON-FACILITY SOURCES FOR CUMULATIVE INVENTORY

Section 4.1 of the SO$_2$ Modeling TAD discusses the criteria for the addition of major SO$_2$ sources in the region for cumulative modeling purposes when determining the recommended attainment status of the area surrounding a facility as described in the 1-hour SO$_2$ Data Requirements Rule. The TAD describes sources that should be included in the modeling as those expected to have an impact on the air quality in the vicinity of the source being studied, in this case Limestone Station. Additionally, the TAD states that except in cases where numerous smaller sources are close together in the study area, consideration of sources to include should begin at sources with emissions in excess of the threshold selected in the Data Requirements Rule. For purposes of this analysis, ERM assumed not only that the lowest threshold described in the proposed final rule will be the one selected, but also that there would be no differentiation between low- and high-population areas in the final rule.

The 2011 EPA National Emissions Inventories (NEI) was reviewed to determine candidate major sources. For the purpose of this study, all major sources of SO$_2$ within 50 kilometers of Limestone that had at least 1000 tons (the lowest possible threshold in the proposed final Data Requirements Rule) of SO$_2$ emissions were considered for inclusion in the modeling. Two facilities were identified in the NEI search: Big Brown Generating Station, located 47.9 kilometers to the north-northeast, and Oak Grove Generating Station located 34.9 kilometers to the southwest. Table 3-5 presents the emissions, distance, and bearing for each facility. The locations of the facility relative to the location of Limestone are shown in Figure 3-17.

Table 3-5: Major Source Considered for Cumulative Modeling Study

<table>
<thead>
<tr>
<th>Facility Name</th>
<th>Distance (km)</th>
<th>Bearing from Limestone Station (deg)</th>
<th>SO$_2$ Emissions (tpy)$^1$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>2011</td>
</tr>
<tr>
<td>Big Brown</td>
<td>47.9</td>
<td>23</td>
<td>64,198</td>
</tr>
<tr>
<td>Oak Grove</td>
<td>34.9</td>
<td>220</td>
<td>4,911</td>
</tr>
</tbody>
</table>

1. Emissions data from EPA Clear Air Markets Database. (http://www.epa.gov/airmarkets/)

Cumulative Sources for 1-hour NO$_2$ and SO$_2$ NAAQS Modeling:

On Page 16 of the 1 March 2011 USEPA Memorandum “Additional Clarification Regarding Application of Appendix W Modeling Guidance for the 1-hour NO$_2$ Ambient Air Quality Standard” (USEPA 2011)$^3$, the following statement is made regarding the focus area for consideration for 1-hour NO$_2$ cumulative modeling:

“...Even accounting for some terrain influences on the location and gradients of maximum 1-hour concentrations, these considerations suggest that the emphasis

$^3$ http://www.epa.gov/scram001/guidance/clarification/Additional_Clarifications_AppendixW_Hourly-NO2-NAAQS_FINAL_03-01-2011.pdf
on determining which nearby sources to include in the modeling analysis should focus on the area within about 10 kilometers of the project location in most cases. The routine inclusion of all sources within 50 kilometers of the project location, the nominal distance for which AERMOD is applicable, is likely to produce an overly conservative result in most cases.”

While the memo specifically refers to NO\textsubscript{2} modeling, the similarity in the form of the 1-hour NO\textsubscript{2} and SO\textsubscript{2} standards and their probabilistic nature suggest that the same approach would be appropriate for identifying major sources for inclusion in a SO\textsubscript{2} cumulative modeling exercise as well.

Despite the above EPA memorandum and the considerable distance of Big Brown and Oak Grove from Limestone Station, for conservatism both sources were included in the modeling. Hourly emissions data for each EGU at both stations were downloaded from the Clean Air Markets database for use in the modeling, and stack parameters for each unit were provided by TCEQ via email on July 16, 2015. Table 3-6 shows the stack parameters for each source located at Big Brown Station and Oak Grove Station. Based on the review of SO\textsubscript{2} emissions from smaller sources described in Section 3.6, the measured background concentration accounts for all other SO\textsubscript{2} sources in the area surrounding Limestone.

Table 3-6: Cumulative Inventory Source Parameters

<table>
<thead>
<tr>
<th>Description</th>
<th>Model Source</th>
<th>Stack Height</th>
<th>Exit Temperature</th>
<th>Exit Velocity</th>
<th>Stack Diameter</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>(ft)</td>
<td>(F)</td>
<td>(ft/sec)</td>
<td>(ft.)</td>
</tr>
<tr>
<td><strong>Big Brown Generating Station</strong></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Unit 1</td>
<td>BB1</td>
<td>400</td>
<td>121.92</td>
<td>250.0</td>
<td>27.0</td>
</tr>
<tr>
<td>Unit 2</td>
<td>BB2</td>
<td>400</td>
<td>121.92</td>
<td>250.0</td>
<td>27.0</td>
</tr>
<tr>
<td><strong>Oak Grove Generating Station</strong></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Unit 1 Boiler</td>
<td>OG1</td>
<td>450</td>
<td>137.16</td>
<td>138.0</td>
<td>32.61</td>
</tr>
<tr>
<td>Unit 2 Boiler</td>
<td>OG2</td>
<td>450</td>
<td>137.16</td>
<td>132.8</td>
<td>33.99</td>
</tr>
</tbody>
</table>

1. Hourly SO\textsubscript{2} emissions from each unit were downloaded from the EPA Clean Air Markets Database
Figure 3-17: Relative Location of Limestone and Major Sources in the Region
4.0 **MODELING RESULTS**

The modeling results are shown in Table 4-1 below. The modeled design value represents the modeled 3-year average of the 99th percentile, maximum daily 1-hour average impact for Limestone. The predicted impacts when the seasonal diurnal background is added are then shown and compared to the NAAQS to demonstrate attainment.

Contours of the predicted impacts, as well as the location of the maximum predicted impact of 176.6 \( \mu g/m^3 \) for the cumulative NAAQS modeling including emissions from Limestone, Big Brown, Oak Grove, along with the ambient background concentration, are shown in Figure 4-1. The table shows that Limestone emissions, when modeled using the most recent three years of actual emissions data and combined with impacts from other nearby sources, the maximum design value is within the level of the 1-hour SO\(_2\) NAAQS.

<table>
<thead>
<tr>
<th>Source</th>
<th>Limestone Station Only</th>
<th>Cumulative Impacts</th>
<th>1-hr. SO(_2) NAAQS</th>
<th>Below NAAQS?</th>
</tr>
</thead>
<tbody>
<tr>
<td>Limestone Station</td>
<td>170.1</td>
<td>176.6</td>
<td>196.5</td>
<td>Yes</td>
</tr>
</tbody>
</table>

**Table 4-1: 1-hour SO\(_2\) Modeling Results for Limestone Station (\(\mu g/m^3\))**

4.1 **CONCLUSIONS**

The air dispersion modeling performed as described in this report shows that the SO\(_2\) emissions from Limestone Generating Station, when combined with the impacts from other major sources and ambient background monitoring data, result in maximum predicted impacts below the 1-hour SO\(_2\) National Ambient Air Quality Standard and therefore an attainment designation for the vicinity of Limestone Generating Station is recommended.
Figure 4-1: Limestone Station 1-hour SO$_2$ Impact Contours Including Background
5.0 REFERENCES


U.S. Environmental Protection Agency. (USEPA 2014) “Data Requirements Rule for the 1-Hour Sulfur Dioxide (SO₂) Primary National Ambient Air Quality Standard (NAAQS),” Pre-publication proposed rule, April 17, 2014.

Attachment F

Information Submitted for the Limestone Generating Station
and the W A Parish Electric Generating Station

Part 3:

Information on W A Parish Electric Generating Station
Baker Botts, L.L.P.

SO₂ Air Dispersion Modeling
Report for W. A. Parish Generating Station

July 2015

Project No. 0266075

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# TABLE OF CONTENTS

1.0 INTRODUCTION ................................................................. 1
   1.2 PROJECT OVERVIEW ................................................. 1
   1.3 OVERVIEW OF METHODOLOGY ................................... 2

2.0 FACILITY DESCRIPTION AND REGULATORY SETTING ............... 5
   2.1 FACILITY LOCATION ............................................... 5
   2.2 SO\textsubscript{2} ATTAINMENT STATUS ......................... 5
   2.3 SOURCE PARAMETERS AND EMISSION RATES ..................... 8

3.0 AIR DISPERSION MODELING ANALYSIS .................................. 10
   3.1 MODEL SELECTION AND APPLICATION ........................... 10
   3.2 THE 1-HOUR SO\textsubscript{2} NAAQS ............................... 10
   3.3 METEOROLOGICAL DATA ......................................... 10
      3.3.1 Meteorological Data Refinements .......................... 13
   3.4 RECEPTOR GRID .................................................. 20
   3.5 GOOD ENGINEERING PRACTICE STACK HEIGHT ANALYSIS ...... 24
   3.6 AMBIENT SO\textsubscript{2} BACKGROUND DATA FOR CUMULATIVE
        MODELING ......................................................... 27
   3.7 REVIEW OF NON-FACILITY SOURCES FOR CUMULATIVE
        INVENTORY ...................................................... 33

4.0 MODELING RESULTS ...................................................... 36
   4.1 CONCLUSIONS ........................................................ 36

5.0 REFERENCES .............................................................. 38
TABLE OF CONTENTS (Cont’d)

List of Tables

2-1 Parish Station Point Sources – Stack Parameters

3-1 Characteristics of the Sugar Land Regional Airport Meteorological Data
3-2 Summary of Parish Station GEP Analysis
3-3 SO₂ Emissions within 50 km of Texas SO₂ Monitors
3-4 Seasonal Diurnal Ambient SO₂ Concentrations for the Italy Monitor (µg/m³)
3-5 Major Source Considered for Cumulative Modeling Study
3-6 Directional Wind Frequency between Parish Station and Rhodia Houston Plant

4-1 1-hour SO₂ Modeling Results for Parish Station and background (µg/m³)

List of Figures

1-1 Parish Station Surroundings and Land Use

2-1 Parish Station Site Plan
2-2 Parish Station Local Topography

3-1 Relative Location of Facility and Meteorological Site
3-2 Three-year Wind Rose (2012-2014): Sugar Land Regional Airport
3-3 Area Terrain Elevations
3-4 Sugar Land Airport – 1km Aerial
3-5 Sugar Land Airport – 1km 1992 NLCD Land Use
3-6 Parish Station – 1km Aerial
3-7 Parish Station – 1km 1992 NLCD Land Use
3-8 Parish Station – 1km 1992 NLCD Land Use – Corrected
3-9 Example of “Upwind” based on AERSURFACE
3-10 Example of “Upwind” based on the “Wedge” Approach
3-11 Near-Field Model Receptors
3-12 Far-Field Model Receptors
3-13 Structures Included in the Parish GEP Analysis (Units 1-4 area)
3-14 Structures Included in the Parish GEP Analysis (Units 5-8 area)
3-15 SO₂ Sources and Monitors in the Region
3-16 SO₂ Concentration vs. Wind Direction at Croquet Monitor
3-17 SO₂ Concentration vs. Wind Direction at North Wayside Monitor

4-1 Parish Station 1-hour SO₂ Impact Contours
1.0 INTRODUCTION

Environmental Resources Management (ERM), presents this air dispersion modeling report to Baker Botts, L.L.P (Baker Botts) documenting that maximum model-predicted Sulfur Dioxide (SO2) impacts from NRG’s W. A. Parish Generating Station (Parish) are in attainment with the 1-hour SO2 National Ambient Air Quality Standard (NAAQS). This analysis shows that the ambient air quality in the vicinity of Parish, currently undesignated for the 1-hour SO2 NAAQS, is within the standard and should be identified as “attainment” in the next cycle of designations.

This modeling report describes the modeling methodology that was used to evaluate potential impacts of SO2 emissions from Parish on ambient air quality.

1.2 PROJECT OVERVIEW

Unlike previous NAAQS attainment demonstrations, EPA has proposed to make 1-hour SO2 NAAQS attainment determinations using ambient air monitoring data and/or air dispersion modeling. In situations where air modeling is used to make this determination, the approach described in EPA’s proposed “Modeling Technical Assistance Document” (TAD)1, which sets forth a significantly different technical approach compared to conventional regulatory modeling prescribed by 40 CFR Part 51, Appendix W (EPA’s Guideline on Air Quality Models) could be used. This approach would also be expected to meet EPA’s proposed 1-Hour SO2 Data Requirements Rule (DRR).

EPA distinguishes the approaches described in the SO2 Modeling TAD to “reflect a view that designations are intended to address current actual air quality (i.e., modeling simulates a monitor), and thus are unlike attainment plan modeling, which must provide assurances that attainment will occur.” EPA’s proposed approach would utilize several distinctive technical approaches, including but not limited to the following:

Simulating actual emissions and exhaust conditions (e.g., temperature and flowrate) on an hourly basis reflecting actual operations for a specified historical time period:

- Representing actual stack heights, irrespective of the GEP limitations;
- Limiting modeled ambient air receptors to locations where monitoring could actually take place and locations that would conventionally be considered “ambient air” for regulatory and permitting purposes, by excluding waterways, roadways, railways, restricted access property, and other locations not accessible to the general public or where a monitor could not reasonably be sited; and

1 http://epa.gov/oaqps001/sulfurdioxide/pdfs/SO2ModelingTAD.pdf
Simulating a three-year period of meteorological and background monitoring data, concurrent with the actual operating conditions and emissions, to meet EPA’s objective that “modeling simulates monitoring” in this context.

ERM performed a modeling analysis evaluating the impacts on ambient air quality from SO2 emissions at Parish. In addition, although the approach for considering cumulative ambient impacts with other SO2 sources in the region is not specifically covered in the proposed DRR, ERM considered other sources of SO2 within 50 kilometers for inclusion in the modeling.

As discussed in this report, ERM’s approach to the modeling analysis used those refinements directly addressed in the proposed DRR, i.e. the use of actual hourly emissions, actual stack heights, and seasonal diurnal ambient background concentrations.

As shown in this modeling report, SO2 impacts from W. A. Parish Station emission sources, when combined with ambient air concentrations taken from a representative monitor, are below the 1-hour SO2 NAAQS.

This first section of this report describes the modeling methodology that was followed. Section 2 provides a description of the facility and the emissions included in the modeling. Model selection and the methodology used in the modeling are described in Section 3. The modeling results are presented in Section 4. References are provided in Section 5.

1.3 OVERVIEW OF METHODOLOGY

ERM’s assessments were conducted in a manner consistent with United States Environmental Protection Agency (EPA) and Texas Commission on Environmental Quality (TCEQW) air quality regulations and modeling guidelines, including the following EPA documents:

- AERMOD Implementation Guide, Revised March 19, 2009;
- “SO2 NAAQS Designations Modeling Technical Assistance Document (Draft),” December 2013;
- “SO2 NAAQS Designations Monitoring Technical Assistance Document (Draft),” December 2013;
- “Data Requirements Rule for the 1-Hour Sulfur Dioxide (SO2) Primary National Ambient Air Quality Standard (NAAQS),” Pre-publication proposed rule, April 17, 2014 (published in the Federal Register on May 13, 2014 79FR 27446); and
As well as:


The steps that were undertaken by ERM to conduct the air dispersion modeling analyses are summarized below:

- Compiled information on the parameters and characteristics for sources of SO\textsubscript{2} emissions at Parish including the 8 main EGU’s, the auxiliary boiler, and the gas turbine.

- Developed a comprehensive receptor grid to capture the maximum off-site impacts from Parish sources using AERMAP (v.11103).

- Reviewed regional ambient background monitors to determine the most appropriate ambient background concentration data for SO\textsubscript{2} to represent sources not explicitly included in the modeling runs.

- Developed 3 years (2012-2014) of meteorological data using surface observations from Sugar Land Regional Airport in Sugar Land, TX with upper air data from Lake Charles, LA using the most recent version (v.14134) of AERMET, the meteorological data processor for AERMOD, and its two preprocessors: AERSURFACE (v.13016) and AERMINUTE (v.14237).

- Reviewed all major sources of SO\textsubscript{2} within 50 kilometers of Parish for possible inclusion in the cumulative modeling analysis using the 2011 National Emission Inventory Database\textsuperscript{2}, based on guidance included in the SO\textsubscript{2} Modeling TAD.

- Conducted an air dispersion modeling analysis using the most recent version of EPA’s regulatory dispersion model, AERMOD (v.14134) and 3 years (2012-2014) of actual emissions data from Parish Sources, consistent with the methodology described in the proposed SO\textsubscript{2} Data Requirements Rule and SO\textsubscript{2} Modeling TAD.

- Summarized the results and compared them with the 1-hour SO\textsubscript{2} NAAQS to determine a recommended attainment designation for the vicinity of Parish.

\textsuperscript{2} http://www.epa.gov/ttnchie1/net/2011inventory.html
FIGURE 1-1: Parish Station Surroundings and Land Use
2.0 FACILITY DESCRIPTION AND REGULATORY SETTING

2.1 FACILITY LOCATION

The W. A. Parish Generating Station is located in the town of Thompsons, Texas. The station is located about 25 miles southwest of downtown Houston, Texas. The site is accessed by FM 762 off Interstate 69. Approximate site coordinates are 29.477° North Latitude, 95.635° West Longitude. The Universal Transverse Mercator (“UTM”) coordinates of the facility are 244,480 Easting and 3,263,763 Northing (using North American Datum of 1983 - NAD83) in UTM Zone 15. The base elevation of the facility is 71’ (21.6m) above sea level. A full scale site plan of Parish is shown in Figure 2.1, and Figure 2.2 shows the site location marked on a United States Geological Survey (“USGS”) 7.5-minute topographic map.

2.2 SO₂ ATTAINMENT STATUS

In July 2013, EPA issued a rule designating 29 counties or partial counties as non-attainment for 1-hour SO₂. However, the vast majority of the country was not designated by EPA at that time. None of the counties surrounding Parish, including Fort Bend, the county in which Parish is located, have been designated as attainment or non-attainment for the 1-hour SO₂ NAAQS.
FIGURE 2-1: Parish Station Site Plan
FIGURE 2-2: Parish Station Local Topography
2.3 SOURCE PARAMETERS AND EMISSION RATES

For this 1-hour SO₂ NAAQS modeling demonstration, all major sources of SO₂ at the facility were included in the modeling. Per the proposed 1-hour SO₂ Data Requirements Rule and SO₂ Modeling TAD, the most recent 3 years of actual emissions data, along with the actual stack heights of all sources, were used in the modeling. The following provides a description of all Parish SO₂ emission sources represented in the model. Table 2-1 summarizes the characteristics of the emissions sources that were included in the modeling.

**TABLE 2-1: Parish Station Point Sources – Stack Parameters**

<table>
<thead>
<tr>
<th>Description</th>
<th>Model Source</th>
<th>Stack Height (ft)</th>
<th>Exit Temperature (F)</th>
<th>Exit Velocity (ft/sec)</th>
<th>Stack Diameter (ft)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Unit 1 Boiler¹</td>
<td>UNIT1A, UNIT 1B</td>
<td>168</td>
<td>---</td>
<td>---</td>
<td>10.5</td>
</tr>
<tr>
<td>Unit 2 Boiler¹</td>
<td>UNIT2A, UNIT 2B</td>
<td>167.6</td>
<td>---</td>
<td>---</td>
<td>10.5</td>
</tr>
<tr>
<td>Unit 3 Boiler¹</td>
<td>UNIT3A, UNIT 3B</td>
<td>181</td>
<td>55.17</td>
<td>---</td>
<td>12.5</td>
</tr>
<tr>
<td>Unit 4 Boiler¹</td>
<td>UNIT4</td>
<td>182</td>
<td>55.47</td>
<td>---</td>
<td>18.0</td>
</tr>
<tr>
<td>Unit 5 Boiler¹</td>
<td>UNIT5</td>
<td>600</td>
<td>182.88</td>
<td>---</td>
<td>24.0</td>
</tr>
<tr>
<td>Unit 6 Boiler¹</td>
<td>UNIT6</td>
<td>600</td>
<td>182.88</td>
<td>---</td>
<td>24.0</td>
</tr>
<tr>
<td>Unit 7 Boiler¹</td>
<td>UNIT7</td>
<td>500</td>
<td>152.40</td>
<td>---</td>
<td>24.0</td>
</tr>
<tr>
<td>Unit 8 Boiler¹</td>
<td>UNIT8</td>
<td>500</td>
<td>152.50</td>
<td>---</td>
<td>22.5</td>
</tr>
<tr>
<td>Auxiliary Boiler²</td>
<td>AUXBOIL</td>
<td>45</td>
<td>13.72</td>
<td>450</td>
<td>4.5</td>
</tr>
<tr>
<td>Gas Turbine²</td>
<td>GASTURB</td>
<td>28</td>
<td>8.53</td>
<td>975</td>
<td>9.5</td>
</tr>
</tbody>
</table>

1. For the 8 main boilers, exit temperature and exit velocity varied on an hourly basis based on CEMS data.
2. For the auxiliary boiler and gas turbine, exit velocity varied on an hourly basis based on CEMS data

The actual emissions data used in the modeling are described below:

- Units No. 1 through No. 4 (Source ID’s: UNIT1A, UNIT1B, UNIT2A, UNIT2B, UNIT3A, UNIT3B, and UNIT4). These units are gas-fired utility boilers that produce steam for the generation of electricity. For these units, three years (2012-2014) of actual hourly emissions, stack temperature, and exhaust flow rate data were input into the model. These data were provided by NRG based on CEMS data collected at each source. As per the proposed 1-hour SO₂ Data Requirements Rule, the actual height of each stack was represented in the model for each source.

- Units No. 5 through No. 8 (Source ID’s UNIT5, UNIT6, UNIT7, and UNIT8). These units are coal and gas-fired utility boilers that produce steam for the generation of electricity and are the primary focus of this analysis. For these units, three years (2012-2014) of actual hourly emissions, stack temperature, and exhaust flow rate data were input into the model. These data were
provided by NRG based on CEMS data collected at each source. As per the proposed 1-hour SO$_2$ Data Requirements Rule, the actual height of each stack was represented in the model for each source.

- **Auxiliary Boiler (Source ID: AUXBOIL).** The auxiliary boiler provides steam for the startup of gas-fired Unit’s 1, 2, and 4. The auxiliary boiler was also modeled using actual hourly emissions data and exhaust flow data provided by NRG based on CEMS data collected at the source. For this source, however, hourly exhaust temperature data was not available, so for all hours the exit temperature was set to the values located in the facility’s operating permit.

- **Gas Turbine (Source ID: GASTURB).** The station also has a gas turbine that is available to supply electricity in emergency situations. The gas turbine was also modeled using actual hourly emissions data and exhaust flow data provided by NRG based on CEMS data collected at the source. For this source, hourly exhaust temperature data was not available, so for all hours the exit temperature was set to the values located in the facility’s operating permit.

- **Other sources at the site include emergency engines and fire pumps.** These sources are used exclusively in emergency situations except for approximately one hour/week testing. Therefore, in accordance with USEPA guidance for intermittent sources, the emergency generator and fire pump engine were not included in the modeling demonstration for the 1-hour SO$_2$ NAAQS.
3.0 AIR DISPERSION MODELING ANALYSIS

ERM conducted the modeling analysis for Parish to quantify ambient impacts of SO₂ relative to the 1-hour NAAQS following the proposed approach described in the SO₂ Modeling TAD.

3.1 MODEL SELECTION AND APPLICATION

The latest version of USEPA’s AERMOD model (v.14134) was used for predicting ambient impacts for 1-hour SO₂. Regulatory default options were used in the analysis. Model predicted impacts were combined with an ambient background concentration and compared to the 1-hour SO₂ NAAQS to determine the recommended attainment status of the area in the vicinity of the facility.

3.2 THE 1-HOUR SO₂ NAAQS

This study focuses on the maximum model-predicted 1-hour SO₂ impacts of Parish and compares them to the 1-hour SO₂ NAAQS. The new standard came into effect in August, 2010. The form of the standard is the 99th percentile of the 3-year average 1-hour daily maximum concentration, and the standard was set to 75 ppb (196.5 µg/m³).

3.3 METEOROLOGICAL DATA

Guidance for regulatory air quality modeling recommends the use of one year of on-site meteorological data or five years of representative off-site meteorological data. The SO₂ Modeling TAD however, specifies that 3 years of meteorological data concurrent to the actual emissions data being input into the model be used. Since on-site data are not available for the Parish site, meteorological data available from the National Weather Service (NWS) were used in this analysis.

Three years (2012-2014) of surface observations from the NWS tower at Sugar Land Regional Airport in Sugar Land, TX (WBAN No. 12977) and concurrent upper air data from Lake Charles, LA (WBAN No. 03937) were provided by TCEQ and further refined as described in Section 3.3.1. The meteorological data were processed with the most recent version of AERMET (v.14134) the meteorological preprocessor for AERMOD, along with the two pre-processors to AERMET: AERSURFACE (v.13016) and AERMINUTE (v.14237). AERMET was applied to create the two meteorological data files required for input to AERMOD.

The data characteristics of Sugar Land Regional Airport are shown in Table 3-1. Figure 3-1 shows the relative location of the airport and Parish Station, and Figure 3-2 shows the 3-year wind rose for Sugar Land Regional Airport.
TABLE 3-1: Characteristics of the Sugar Land Regional Airport Meteorological Data

<p>| | |</p>
<table>
<thead>
<tr>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Distance from Parish Station</strong></td>
<td>10.0 miles</td>
</tr>
<tr>
<td><strong>Average Wind Speed</strong></td>
<td>3.73 m/s</td>
</tr>
<tr>
<td><strong>Percent Calm Hours</strong></td>
<td>0.97%</td>
</tr>
<tr>
<td><strong>Data Completeness</strong></td>
<td>99.86%</td>
</tr>
</tbody>
</table>

FIGURE 3-1: Relative Location of Facility and Meteorological Site
FIGURE 3-2: Three-year Wind Rose (2012-2014): Sugar Land Regional Airport
3.3.1 Meteorological Data Refinements

EPA and TCEQ guidelines recommend that meteorological data from a representative measurement station be used in modeling analyses to address ambient impacts. This section discusses the representativeness of data collected at the Sugar Land Airport, and also describes how these data were processed to generate AERMOD-ready input files. AERMET is the recommended processor for developing inputs to AERMOD. AERMET requires, at a minimum, hourly surface data and once-daily (morning) upper air sounding profiles. The processing program produces two files for input to AERMOD: a surface file containing calculated micrometeorological variables (heat flux, stability, and turbulence parameters) that represent the dispersive potential of the atmosphere, and a profile file that provides vertical profiles of wind speed, wind direction, and temperature. In the case of meteorological data files developed from NWS data, the profiles contain only one level (the surface level) and a meteorological interface within AERMOD generates vertical profiles of wind, temperature, and turbulence from the input data files. It is important to consider the full set of processing steps, including the profiling done within AERMOD, when evaluating the representativeness of a measurement site for application at a particular location such as the W.A. Parish Station.

Meteorological representativeness is a function of a number of factors, including distance between the measurement and application site, and land use and terrain near the measurement site compared to land use and terrain in the vicinity of the application site. Differences are expected between airport land use and land use surrounding almost any application site, and frequently there are differences in terrain between measurement and application sites. Neither EPA nor TCEQ have established quantitative criteria for assessing whether differences are significant; therefore, this comparison is made based on a qualitative assessment and consideration of the importance of the land use and terrain differences to the analysis.

Terrain

Figure 3-1 displayed the relative locations of the airport and Parish Station; as noted previously, the airport is approximately 10 miles (15 kilometers) north of the Station. Figure 3-3 provides a depiction of terrain elevations surrounding the airport and the Station. This part of Texas is flat; the airport is only about 3 meters higher in elevation than the Station, and as Figure 3-3 shows there are no intervening terrain features that could significantly affect wind flow. Figure 3-2 displayed a wind rose based on measurements at the airport; the predominant south to south-southeast flow, with secondary northerly flow, is typical of many locations in East Texas and is thus indicative that the winds measured at the airport are representative of a large area.
FIGURE 3-3: Area Terrain Elevations

Land Use

Three parameters that represent land use characteristics around a measurement site are the Bowen ratio, noon-time albedo, and surface roughness. The Bowen ratio is an indicator of surface moisture and the albedo is a measure of the reflectivity of the land surface – together they are used by AERMET to estimate heat flux and other boundary layer parameters such as the convective mixing height and indicators of the stability of the atmosphere. The surface roughness is related to the heights of obstacles to the wind flow, and is used to parameterize other surface stability indicators in AERMET and is a factor in determining the strength of mechanical turbulence, and hence the degree of plume dispersion, in AERMOD. The focus of representativeness based on land use is on the three parameters Bowen ratio, albedo, and surface roughness.

The Bowen ratio and albedo associated with land use characteristics are calculated in AERSURFACE within an area 10km by 10km centered on the site being evaluated. Land use within an area this size surrounding the Sugar Land Regional Airport (reference Figure 3-1) contains more developed areas than an area this size surrounding the Parish station. Most of the development around the airport is in the form of residential neighborhoods, while most of the area surrounding Parish is undeveloped farmland or water (Smithers Lake). Since there are no heavily industrialized or urbanized areas around the airport, it is expected that the Bowen ratio and albedo values for the two sites are similar.
This is borne out by using AERSURFACE to determine these parameters for both sites. The albedo values produced by AERSURFACE for both sites are nearly identical – 0.17 to 0.18. The Bowen ratio values produced by AERSURFACE for the airport range from 0.44 to 0.77; and somewhat lower – 0.33 to 0.53 – at the Parish site. These differences are not significant in terms of the overall effect on AERMET computations for boundary layer parameters and subsequent use in AERMOD.

Surface roughness is calculated by AERMET as a function of land use characteristics within a circle centered on the site being evaluated, with a recommended radius of 1 km. The current version of AERSURFACE utilizes the USGS NLCD 1992 land use data set as the source of land use information. To compare land use as it relates to surface roughness, ERM first evaluated whether significant changes have occurred since 1992 in the vicinity of the airport and the Parish site, and evaluated on a qualitative basis the characteristics surrounding the airport anemometer compared to characteristics surrounding Parish.

Figure 3-4 is a current aerial view of the area within 1 km of the Sugar Land Airport anemometer. The NLCD 1992 land use data base identifies land use categories in 30 m cells as of 1992. The land use categories extracted from NLCD 1992 have been superimposed on the image in Figure 3-5. As shown in the aerial image, the majority of the area surrounding the anemometer is relatively flat with occasional obstructions and forested areas to the northwest. The NLCD 1992 land use categories shown in Figure 3-5 display a similar pattern that indicates that the 1992 data set adequately represents the area surrounding the anemometer, but with much less of a forested area to the northwest. Figure 3-6 displays the area within 1 km of Parish, and Figure 3-7 displays the 1992 land use characteristics superimposed on the current aerial view of the area around Parish. A qualitative evaluation of Figure 3-7 reveals that there are areas where the 1992 land use data is not correct for the site – most significantly, the coal pile is coded as “wetlands” and there are several water cells scattered throughout the plant site. Because of these errors, ERM undertook an effort to correct the land use characterizations for Parish, essentially replacing incorrect land use codes with corrected codes that better represent the land use throughout the 1 km circle. Figure 3-8 displays the corrected land use values surrounding Parish.
FIGURE 3-4: Sugar Land Airport – 1km Aerial

FIGURE 3-5: Sugar Land Airport – 1km 1992 NLCD Land Use
FIGURE 3-6: Parish Station – 1km Aerial

FIGURE 3-7: Parish Station – 1km 1992 NLCD Land Use
An examination of the figures presented here reveals some differences and some similarities between land use surrounding the airport and land use surrounding the Parish site. Since in particular some of the “Commercial Industrial Transportation” categories at the airport represent the runways, there is less to contribute to larger values of the roughness length at the airport than at the Parish site. For some important reasons, however, the corrected land use values surrounding Parish were used to characterize surface roughness for input to AERMET. The first is to capture directional differences between the airport and Parish, consistent with the goal of the TAD to reproduce “what a monitor would measure” in mind. The second reason is related to the fact that the important dispersion regime for the stacks being modeled at Parish is above the surface layer - with an average plume rise of approximately 150 meters, total plume height for the Parish sources is in the range of 300 meters above the ground. Surface values of turbulence for these plumes are considerably less important than turbulence values determined for the layer several hundred meters above the surface. Since turbulence levels at plume height depend strongly on the roughness length (in addition to the stability parameters), a roughness length more representative of the site provides a more realistic, and ultimately more accurate, estimate of turbulence at plume level and therefore a more accurate depiction of “what a monitor would see” than roughness length values determined for the airport.
ERM calculated roughness length values on a seasonal and direction-specific basis, assigning roughness length values for each land use cell based on the values contained in Table A-3 of the AERSURFACE users’ guide (EPA, 2008). Effective roughness was calculated in a manner entirely consistent with AERSURFACE, namely as the distance-weighted geometric mean of all land use cells upwind of the sources being modeled, with the following formula:

$$z_0 \text{ effective} = \exp^\left(\frac{\sum \ln(z_{0,xy})}{\sum 1/d_{xy}}\right)$$

AERSURFACE is not part of the AERMOD system; rather it is a recommended, but not required, tool in the set of related AERMOD processing programs. ERM took a different approach than AERSURFACE in terms of determining which cells are “upwind” for a particular wind direction (note that). This different approach is appropriate for situations where the stacks being modeled are separated by up to a few hundred meters, as it more accurately defines “upwind” as not based on a single point. An illustration of the difference between the AERSURFACE approach and the modified “wedge” approach used by ERM is illustrated in Figures 3-9 and 3-10.

**FIGURE 3-9: Example of “Upwind” based on AERSURFACE**
Land use files were created based on this approach and combining the roughness length determinations with the Bowen ratio/albedo values generated by AERSURFACE. AERMINUTE was used to develop speed and direction values for low-wind hours. Upper air profiles were generated and filled in for the Lake Charles, LA upper air sounding station, and AERMET was run to create 3 years (2012-2014) of meteorological files used in AERMOD.

3.4 RECEPTOR GRID

A comprehensive Cartesian receptor grid extending out to approximately 20 kilometers (km) from Parish was used in the AERMOD modeling analysis to assess maximum ground-level 1-hour SO2 concentrations. The Modeling TAD states that the receptor grid must be sufficient to determine ambient air quality in the vicinity of the source being studied. The 20-kilometer receptor grid is more than sufficient to resolve the maximum 1-hour SO2 impacts, and it clearly illustrates decreasing SO2 concentration gradients in relation to the plant. Further, the receptor grid used in the modeling is consistent with the guidelines provided by the TCEQ for regulatory applications.
Specifically, the Cartesian receptor grid consisted of the following receptor spacing:

- 50-meter spacing along the facility fence line;
- 100-meter spacing extending from the fence line to 3 kilometers;
- 200-meter spacing extending from 3 to 5 kilometers;
- 500-meter spacing extending from 5 to 10 kilometers; and
- 1,000-meter spacing extending from 10 to 20 kilometers.

The above receptor data was used without modification in the modeling. Per the 1-hour SO₂ Modeling TAD, receptors located over areas where monitors could not reasonably be sited could be excluded from the modeling, but these receptors were retained in this analysis as a measure of conservatism.

Terrain elevations from National Elevation Data (‘NED’) from USGS were processed using the most recent version of AERMAP (v.11103) to develop the receptor terrain elevations required by AERMOD. NED data files contain profiles of terrain elevations, which in conjunction with receptor locations are used to generate receptor height scales. The height scale is the terrain elevation in the vicinity of a receptor that has the greatest influence on dispersion at that location and is used for model computations in complex terrain areas. The near-field (within 5 kilometers) and far-field (full grid) receptor grids are shown in Figures 3-11 and 3-12, respectively.
FIGURE 3-11: Near-Field Model Receptors
FIGURE 3-12: Far-Field Model Receptors
3.5 GOOD ENGINEERING PRACTICE STACK HEIGHT ANALYSIS

Good engineering practice ("GEP") stack height is defined as the stack height necessary to ensure that emissions from the stack do not result in excessive concentrations of any air pollutant as a result of atmospheric downwash, wakes, or eddy effects created by the source, nearby structures, or terrain features.

A GEP stack height analysis was performed for all stacks using the Building Profile Input Program (BPIP) in accordance with USEPA’s guidelines (USEPA 1985). Per the guidelines, the physical GEP height, \( H_{GEP} \), is determined from the dimensions of all buildings which are within the region of influence using the following equations, depending on the construction data of the stack:

1. For stacks in existence on January 12, 1979 and for which the owner or operator had obtained all applicable permits or approvals required,
   \[ H_{GEP} = 2.5H, \]
   provided the owner or operator produces evidence that this equation was actually relied on in establishing an emission limitation;

2. For all other stacks:
   \[ H_{GEP} = H + 1.5L \]

where:

\( H = \) height of the structure within 5L of the stack which maximizes \( H_{GEP} \);
   and
\( L = \) lesser dimension (height or projected width) of the structure.

For a squat structure, i.e., height less than projected width, the formula reduces to:

\[ H_{GEP} = 2.5H \]

In the absence of influencing structures, a “default” GEP stack height is creditable up to 65 meters (213 feet).

A summary of the GEP stack height analyses is presented in Table 3-2. As described in the SO\(_2\) Modeling TAD, when modeling actual emissions in order to determine the attainment status of the facility when compared to the 1-hour SO\(_2\) NAAQS, the full height of all stacks is allowed in the modeling regardless of their GEP Formula Heights. All stacks at Parish are below their respective GEP heights so application of the SO\(_2\) Modeling TAD did not affect the stack height assumptions for Parish. The locations of all structures and sources included in the GEP analysis are shown in Figure 3-13 (Units 1-4 and ancillary sources) and Figure 3-14 (Units 5-8). The output from BPIP was input into AERMOD to represent aerodynamic downwash caused by structures around the stacks.
FIGURE 3-13: Structures Included in the Parish GEP Analysis (Units 1-4 area)
FIGURE 3-14: Structures Included in the Parish GEP Analysis (Units 5-8 area)
### TABLE 3-2: Summary of Parish Station GEP Analysis

<table>
<thead>
<tr>
<th>Emission Source</th>
<th>Stack Height (m)</th>
<th>Controlling Buildings / Structures</th>
<th>Building Height (m)</th>
<th>Projected Width (m)</th>
<th>GEP Formula Height (m)¹</th>
</tr>
</thead>
<tbody>
<tr>
<td>UNIT 1A</td>
<td>51.08</td>
<td>Unit 3 Boiler Bldg.</td>
<td>21.34</td>
<td>21.90</td>
<td>52.66</td>
</tr>
<tr>
<td>UNIT 1B</td>
<td>51.08</td>
<td>Unit 3 Boiler Bldg.</td>
<td>21.34</td>
<td>21.90</td>
<td>52.66</td>
</tr>
<tr>
<td>UNIT 2A</td>
<td>51.21</td>
<td>Unit 2 Boiler Bldg.</td>
<td>21.34</td>
<td>21.37</td>
<td>53.15</td>
</tr>
<tr>
<td>UNIT 2B</td>
<td>51.21</td>
<td>Unit 1 Boiler Bldg.</td>
<td>21.34</td>
<td>21.35</td>
<td>53.15</td>
</tr>
<tr>
<td>UNIT 3A</td>
<td>55.17</td>
<td>Unit 4 Boiler Bldg.</td>
<td>21.34</td>
<td>33.22</td>
<td>53.73</td>
</tr>
<tr>
<td>UNIT 3B</td>
<td>55.17</td>
<td>Unit 4 Boiler Bldg.</td>
<td>21.34</td>
<td>33.22</td>
<td>53.73</td>
</tr>
<tr>
<td>UNIT 4</td>
<td>55.47</td>
<td>Unit 4 Boiler Bldg.</td>
<td>21.34</td>
<td>25.93</td>
<td>53.35</td>
</tr>
<tr>
<td>UNIT 5</td>
<td>182.88</td>
<td>Unit 8 Boiler Bldgs.</td>
<td>75.59</td>
<td>82.87</td>
<td>188.36</td>
</tr>
<tr>
<td>UNIT 6</td>
<td>182.88</td>
<td>Unit 8 Boiler Bldgs.</td>
<td>75.59</td>
<td>84.84</td>
<td>188.36</td>
</tr>
<tr>
<td>UNIT 7</td>
<td>152.40</td>
<td>Unit 7 Boiler Bldgs.</td>
<td>75.59</td>
<td>75.79</td>
<td>188.66</td>
</tr>
<tr>
<td>UNIT 8</td>
<td>152.40</td>
<td>Unit 7 Boiler Bldgs.</td>
<td>75.59</td>
<td>80.51</td>
<td>188.66</td>
</tr>
<tr>
<td>AUXBOIL</td>
<td>13.72</td>
<td>Unit 4 Boiler Bldg.</td>
<td>21.34</td>
<td>39.08</td>
<td>53.68</td>
</tr>
<tr>
<td>GASTURB</td>
<td>8.53</td>
<td>Unit 1 Boiler Bldg.</td>
<td>21.34</td>
<td>21.75</td>
<td>53.15</td>
</tr>
</tbody>
</table>

¹. In the absence of influencing structures, a “default” GEP stack height is creditable up to 65 meters (213 feet).

### 3.6 AMBIENT SO₂ BACKGROUND DATA FOR CUMULATIVE MODELING

In addition to assessing impacts from Parish Station sources, the impact from other sources of SO₂ in the region were considered to demonstrate that the air quality in the region is in attainment with the NAAQS. While there are no sources of SO₂ in the vicinity of Parish that warranted explicit inclusion in the modeling as discussed in Section 3.7, in order to account for other minor sources of SO₂ in the area an ambient background concentration was added to model-predicted impacts from Parish for comparison to the NAAQS.

The criteria for determining the monitor best suited to characterize air quality at a given location include:

- Stations with similar influencing SO₂ sources as the source being modeled (not necessarily the closest).
- Avoid stations influenced by the source being modeled to prevent double-counting impacts.
- Avoid stations influenced by sources not likely to interact with the source being modeled.
- Consider predicted concentration patterns for source being modeled, along with wind frequency, to assist in selection.

Figure 3-15 shows the location of the ambient monitors in the vicinity of Parish Station and the 1-hour SO$_2$ design value, as well as the location of all other SO$_2$ sources in the region that emitted more than 1,000 tons of SO$_2$ according to the 2011 EPA National Emissions Inventory. The figure shows that there are no significant sources of SO$_2$ near Parish, but there are several 1,000 ton sources concentrated around the Houston Ship Channel 50 km to the northeast, only one of which is within 50 km. Additionally, all of the monitors sited in the region are located in the Houston metropolitan area or Galveston. It should also be noted that the design value of all monitors is less than 35% of the 1-hour SO$_2$ NAAQS, and that the design value decreases significantly with distance from these larger sources.

*FIGURE 3-15: SO$_2$ Sources and Monitors in the Region*
ERM initially evaluated 3 monitors to determine their representativeness: Croquet (Monitor ID# 48-201-0051) and North Wayside (Monitor ID# 48-201-0046), both located northeast of Parish in Greater Houston, and the TCEQ monitor in Freeport, TX (Monitor ID# 48-039-1012), located 60 km south-southeast of Parish.

The first monitor evaluated was the Croquet monitor. This monitor is the closest to Parish in terms of proximity, located 22.4 km north-northeast of Parish. A review of the most recent (2012-2014) years of hourly concentrations at the monitor vs. the wind direction relative to Parish at the time the monitor was reported, shown in Figure 3-16, shows that virtually all of the highest concentrations at the monitor occur when the wind is blowing from Parish Station towards the monitor. Additional higher impacts occur when the wind is blowing from the direction of the Houston Ship Channel, which is much closer to the monitor than to Parish. Additional higher impacts occur when the wind is blowing from the direction of the Houston Ship Channel, which is much closer to the monitor than to Parish.

Because the monitor is strongly influenced by impacts from Parish Station, using the Croquet monitor would result in “double counting” the impacts from the station. Therefore the station is not useful to represent non-facility related impacts in the region. It should be noted however that when the monitor is being impacted by Parish Station, the concentrations never approach the standard, and are less than one-third of the standard the vast majority of the time.

**FIGURE 3-16: SO2 Concentration vs. Wind Direction at Croquet Monitor**
The next monitor reviewed was the North Wayside monitor, located 51.4 km north-northeast of Parish, far enough away that impacts from Parish itself are no longer noteworthy. At North Wayside however, the highest concentrations are all associated with Houston Ship Channel and other metropolitan Houston sources, as shown in Figure 3-17. These impacts again are not representative of the types of sources located in close proximity to Parish, and therefore North Wayside was also dismissed as being unrepresentative of ambient air conditions near Parish.

FIGURE 3-17: $SO_2$ Concentration vs. Wind Direction at North Wayside Monitor

The last monitor in the same approximate area as Parish Station reviewed was the Freeport, TX monitor (CAMS 1012). This monitor, located 60 km south-southeast of Parish, was discounted for two reasons: First, the TCEQ website notes that “Data from this instrument does not meet EPA quality assurance criteria and cannot be used for regulatory purposes”3. Secondly, the monitor is sited in a heavily industrialized area between two large chemical manufacturing facilities. Because of the data quality issues and the siting of the monitor in an area far more industrialized than the area around Parish Station, this monitor was also eliminated from consideration.

With the monitors in the same general region as Parish determined to not be representative of air quality around Parish, all monitors in Texas were reviewed and the total tons of \( \text{SO}_2 \) from all sources emitted within 50 km of the monitor per the 2011 NEI were compared to the total tons emitted around Parish Station as shown in Table 3-3:

**TABLE 3-3: \( \text{SO}_2 \) Emissions within 50 km of Texas \( \text{SO}_2 \) Monitors**

<table>
<thead>
<tr>
<th>Monitor i.d.</th>
<th>Name</th>
<th>City</th>
<th>City</th>
<th>SO2 TPY (NEI 2011) within distance shown</th>
<th>Kilometers from Parish</th>
</tr>
</thead>
<tbody>
<tr>
<td>48-029-0059</td>
<td>Calaveras_Lake</td>
<td>San_Antonio</td>
<td>23,269</td>
<td>0-10 km 10-25 km 25-50 km</td>
<td>5</td>
</tr>
<tr>
<td>48-139-0016</td>
<td>Midlothian</td>
<td>Midlothian</td>
<td>6,704</td>
<td>5,673</td>
<td>0</td>
</tr>
<tr>
<td>48-167-0005</td>
<td>Texas_City</td>
<td>Texas_City</td>
<td>1,046</td>
<td>9,121</td>
<td>-257.61 -26.98 259.02</td>
</tr>
<tr>
<td>48-183-0001</td>
<td>Longview</td>
<td>Not_in_a_city</td>
<td>37</td>
<td>76,339 852</td>
<td>76.41 332.72 332.61</td>
</tr>
<tr>
<td>48-201-0046</td>
<td>North_Wayside</td>
<td>Houston</td>
<td>194</td>
<td>10,056 2,257</td>
<td>32.42 39.91 51.42</td>
</tr>
<tr>
<td>48-201-0051</td>
<td>Croquet</td>
<td>Houston</td>
<td>1</td>
<td>53,864 8,130</td>
<td>14.97 16.72 22.44</td>
</tr>
<tr>
<td>48-201-0062</td>
<td>Monrope</td>
<td>Houston</td>
<td>87</td>
<td>10,140 52,911</td>
<td>34.77 17.61 39.72</td>
</tr>
<tr>
<td>48-201-0416</td>
<td>Park_Place</td>
<td>Houston</td>
<td>1,915</td>
<td>6,278 49,874</td>
<td>35.32 29.57 48.06</td>
</tr>
<tr>
<td>48-201-1035</td>
<td>Clinton</td>
<td>Houston</td>
<td>5,103</td>
<td>7,097 13,86</td>
<td>47.95 22.95 53.36</td>
</tr>
<tr>
<td>48-201-1050</td>
<td>Seabrook</td>
<td>Seabrook</td>
<td>49</td>
<td>8,419 4,930</td>
<td>59.15 13.72 60.72</td>
</tr>
<tr>
<td>48-245-0009</td>
<td>Beaumont</td>
<td>Beaumont</td>
<td>1,065</td>
<td>10,756 6,830</td>
<td>147.69 67.46 162.37</td>
</tr>
<tr>
<td>48-245-0011</td>
<td>Port_Arthur</td>
<td>Port_Arthur</td>
<td>10,459</td>
<td>1,361 6,832</td>
<td>156.03 52.45 164.62</td>
</tr>
<tr>
<td>48-245-1050</td>
<td>Beaumont</td>
<td>Beaumont</td>
<td>1,065</td>
<td>1,081 16,506</td>
<td>145.64 70.77 161.93</td>
</tr>
<tr>
<td>48-257-0005</td>
<td>Kaufman</td>
<td>Kaufman</td>
<td>0</td>
<td>152 474</td>
<td>-74.01 339.61 347.58</td>
</tr>
<tr>
<td>48-309-1037</td>
<td>Waco</td>
<td>Waco</td>
<td>0</td>
<td>1,020 387</td>
<td>-142.44 237.32 276.78</td>
</tr>
<tr>
<td>48-349-1051</td>
<td>Corsicana</td>
<td>Corsicana</td>
<td>225</td>
<td>3,506 64,572</td>
<td>-80.22 280.5 291.74</td>
</tr>
<tr>
<td>48-355-0025</td>
<td>Corpus_Christi_West</td>
<td>Corpus_Christi_West</td>
<td>818</td>
<td>155 35</td>
<td>-170.59 -193.23 257.76</td>
</tr>
<tr>
<td>48-355-0026</td>
<td>Corpus_Christi_Tuloso</td>
<td>Corpus_Christi_Tuloso</td>
<td>323</td>
<td>624 61</td>
<td>-182.56 -185.97 260.6</td>
</tr>
<tr>
<td>48-355-0032</td>
<td>Corpus_Christi_Huisache</td>
<td>Corpus_Christi_Huisache</td>
<td>933</td>
<td>40 35</td>
<td>-170.39 -188.89 254.38</td>
</tr>
<tr>
<td>48-453-0014</td>
<td>Austin</td>
<td>Austin</td>
<td>9</td>
<td>1,938 1,438</td>
<td>-205.73 92.81 275.7</td>
</tr>
<tr>
<td>48-113-0069</td>
<td>Dallas_Hinton</td>
<td>Dallas_Hinton</td>
<td>275</td>
<td>422 8,000</td>
<td>-125.1 366.71 387.46</td>
</tr>
</tbody>
</table>

Based on the table, the monitor with the closest emissions pattern relative to Parish was the Italy, TX monitor. Although physically located a long distance from Parish (320.7 km), the pattern of emissions near the monitor was very close: limited emissions within 25 km, but over 5000 tons \( \text{SO}_2 \) emitted at a distance of between 25 and 50 km. Therefore, though still slightly conservative, Italy was determined to be the most representative ambient background monitor for use in the cumulative modeling.

EPA guidance allows simulation of background values that vary by season and hour of day that could simulate a lower value than the 99th percentile. The modeling was performed with a set of seasonal diurnal values developed using the methodology described in the USEPA March 1st, 2011 Clarification Memorandum for 1-hour \( \text{NO}_2 \) Modeling. Though this memorandum primarily addresses \( \text{NO}_2 \) modeling, page 20 describes the process for developing seasonal...
diurnal background values for SO$_2$ as well. The seasonal diurnal values used are shown in Table 3-4.

**TABLE 3-4: Seasonal Diurnal Ambient SO$_2$ Concentrations for the Italy Monitor ($\mu$g/m$^3$)**

<table>
<thead>
<tr>
<th>Hour(^1)</th>
<th>Winter</th>
<th>Spring</th>
<th>Summer</th>
<th>Fall</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>3.66</td>
<td>2.70</td>
<td>3.23</td>
<td>3.05</td>
</tr>
<tr>
<td>2</td>
<td>2.62</td>
<td>2.27</td>
<td>2.18</td>
<td>2.88</td>
</tr>
<tr>
<td>3</td>
<td>2.53</td>
<td>2.44</td>
<td>2.36</td>
<td>3.32</td>
</tr>
<tr>
<td>4</td>
<td>2.62</td>
<td>2.18</td>
<td>2.09</td>
<td>3.66</td>
</tr>
<tr>
<td>5</td>
<td>2.18</td>
<td>1.75</td>
<td>1.48</td>
<td>2.97</td>
</tr>
<tr>
<td>6</td>
<td>2.27</td>
<td>1.66</td>
<td>1.40</td>
<td>3.32</td>
</tr>
<tr>
<td>7</td>
<td>2.18</td>
<td>1.57</td>
<td>1.75</td>
<td>2.18</td>
</tr>
<tr>
<td>8</td>
<td>2.36</td>
<td>2.36</td>
<td>3.05</td>
<td>4.01</td>
</tr>
<tr>
<td>9</td>
<td>3.58</td>
<td>3.32</td>
<td>3.66</td>
<td>6.37</td>
</tr>
<tr>
<td>10</td>
<td>4.71</td>
<td>6.20</td>
<td>6.02</td>
<td>10.38</td>
</tr>
<tr>
<td>11</td>
<td>7.33</td>
<td>5.24</td>
<td>6.98</td>
<td>9.77</td>
</tr>
<tr>
<td>12</td>
<td>8.73</td>
<td>4.54</td>
<td>6.28</td>
<td>16.93</td>
</tr>
<tr>
<td>13</td>
<td>9.16</td>
<td>5.85</td>
<td>5.06</td>
<td>10.30</td>
</tr>
<tr>
<td>14</td>
<td>7.42</td>
<td>5.76</td>
<td>5.06</td>
<td>9.77</td>
</tr>
<tr>
<td>15</td>
<td>7.33</td>
<td>5.76</td>
<td>6.02</td>
<td>8.20</td>
</tr>
<tr>
<td>16</td>
<td>9.07</td>
<td>4.36</td>
<td>4.28</td>
<td>8.73</td>
</tr>
<tr>
<td>17</td>
<td>6.46</td>
<td>3.75</td>
<td>3.66</td>
<td>13.26</td>
</tr>
<tr>
<td>18</td>
<td>8.38</td>
<td>4.28</td>
<td>5.24</td>
<td>8.20</td>
</tr>
<tr>
<td>19</td>
<td>4.89</td>
<td>3.58</td>
<td>5.67</td>
<td>4.89</td>
</tr>
<tr>
<td>20</td>
<td>13.00</td>
<td>4.19</td>
<td>8.55</td>
<td>6.54</td>
</tr>
<tr>
<td>21</td>
<td>4.01</td>
<td>2.62</td>
<td>6.72</td>
<td>6.02</td>
</tr>
<tr>
<td>22</td>
<td>2.79</td>
<td>2.53</td>
<td>5.15</td>
<td>4.54</td>
</tr>
<tr>
<td>23</td>
<td>2.27</td>
<td>3.32</td>
<td>2.88</td>
<td>5.06</td>
</tr>
<tr>
<td>24</td>
<td>2.36</td>
<td>2.79</td>
<td>2.88</td>
<td>4.62</td>
</tr>
</tbody>
</table>

1. Hours in AERMOD are defined as hour-ending. i.e., Hour 1 is the period from midnight through 1 AM, etc.
3.7 REVIEW OF NON-FACILITY SOURCES FOR CUMULATIVE INVENTORY

Section 4.1 of the SO$_2$ Modeling TAD discusses the criteria for the addition of major SO$_2$ sources in the region for cumulative modeling purposes when determining the recommended attainment status of the area surrounding a facility as described in the proposed 1-hour SO$_2$ Data Requirements Rule. The TAD describes sources that should be included in the modeling as those expected to have an impact on the air quality in the vicinity of the source being studied, in this case Parish Station. Additionally, the TAD states that except in cases where numerous smaller sources are close together in the study area, consideration of sources to include should begin at sources with emissions in excess of the threshold selected in the Data Requirements Rule. For purposes of this analysis, ERM assumed not only that the lowest threshold described in the proposed final rule will be the one selected, but also that there would be no differentiation between low- and high-population areas in the final rule.

The 2011 EPA National Emissions Inventories (NEI) was reviewed to determine candidate major sources. For the purpose of this study, all major sources of SO$_2$ within 50 kilometers of Parish that had at least 1000 tons (the lowest possible threshold in the proposed final Data Requirements Rule) of SO$_2$ emissions were considered for inclusion in the modeling. Only one facility was identified in the NEI search: the Rhodia Chemical Plant in Houston, located 44.6 kilometers to the northeast of Parish. Table 3-6 presents the emissions, distance, and bearing for this facility. The locations of the facility relative to the location of Parish were shown in Figure 3-13.

<table>
<thead>
<tr>
<th>Facility Name</th>
<th>Distance (km)</th>
<th>Bearing from Parish Station (deg)</th>
<th>2011 NEI SO$_2$ Emissions (tpy)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Rhodia Houston Plant</td>
<td>44.6</td>
<td>53</td>
<td>3755</td>
</tr>
</tbody>
</table>

TABLE 3-5: Major Source Considered for Cumulative Modeling Study

Once the candidate facility was identified, a number of factors were reviewed to determine whether or not the impacts from the Rhodia plant were likely to have significant crossover of impacts with Parish, and thus needed to be included in the cumulative modeling analysis. The factors reviewed included:

- Distance from Parish.
- Direction upwind and downwind of Parish and frequency that the wind blows in those directions.
- The presence of a significant concentration gradient in the direction of the sources being considered.

Based on this review the Rhodia Houston Plant was not included in the cumulative modeling for the following reasons:
**Wind Frequency**

For the modeled impacts of two facilities not immediately proximate to each other to intersect, the receptors in question must be on a line drawn through the two sources. Further, in 1-hour modeling periods, for both sources to impact the same receptor simultaneously the receptor must be downwind of both facilities, since AERMOD holds the winds constant for the entire hour. To review the frequency at which the winds were blowing on a line intersecting both facilities, the 3 most recent years of meteorological data from Sugar Land Regional Airport (2012-2014) were reviewed to assess the frequency of winds in a 30 degree arc centered on each facility: For potential cumulative impacts from Parish and Rhodia, winds blowing from the arcs of 38-68 degrees (towards Parish from Rhodia) and 218- 248 degrees (towards Rhodia from Parish) were considered. Additionally, for hours falling within those 30-degree arcs, the speed of the wind was examined to assess whether an emission from one source could reach the other source in that hour. Table 3-7 shows the frequency of occurrence of winds capable of transporting the emission plumes from one source to the other.

**TABLE 3-6: Directional Wind Frequency between Parish Station and Rhodia Houston Plant**

<table>
<thead>
<tr>
<th>Direction of Travel</th>
<th>30 degree arc</th>
<th>Number of hours</th>
<th>% Hours</th>
<th>Hours that reach source</th>
<th>% Hours</th>
</tr>
</thead>
<tbody>
<tr>
<td>Towards Parish</td>
<td>38-68</td>
<td>1621</td>
<td>6.2%</td>
<td>0</td>
<td>0%</td>
</tr>
<tr>
<td>Towards Rhodia</td>
<td>218-248</td>
<td>990</td>
<td>3.8%</td>
<td>0</td>
<td>0%</td>
</tr>
</tbody>
</table>

1. Minimum speed for wind to travel from Parish Station to Rhodia in one hour is 12.33 m/s.

As shown in the table above, the winds only blow between the locations of Rhodia and Parish Station 10% of the time, and during those hours the wind is never strong enough to transport a parcel from one location to the other in an hour.

**Cumulative Sources for 1-hour NO2 and SO2 NAAQS Modeling:**

On Page 16 of the 1 March 2011 USEPA Memorandum “Additional Clarification Regarding Application of Appendix W Modeling Guidance for the 1-hour NO2 Ambient Air Quality Standard” (USEPA 2011), the following statement is made regarding the focus area for consideration for 1-hour NO2 cumulative modeling:

“..Even accounting for some terrain influences on the location and gradients of maximum 1-hour concentrations, these considerations suggest that the emphasis on determining which nearby sources to include in the modeling analysis should focus on the area within about 10 kilometers of the project location in most cases.

---

4http://www.epa.gov/scram001/guidance/clarification/Additional_Clarifications_AppendixW_Hourly-NO2-NAAQS_FINAL_03-01-2011.pdf
The routine inclusion of all sources within 50 kilometers of the project location, the nominal distance for which AERMOD is applicable, is likely to produce an overly conservative result in most cases.”

While the memo specifically refers to NO\textsubscript{2} modeling, the similarity in the form of the 1-hour NO\textsubscript{2} and SO\textsubscript{2} standards and their probabilistic nature suggest that the same approach would be appropriate for identifying major sources for inclusion in a SO\textsubscript{2} cumulative modeling exercise as well.

Because the Rhodia Houston Plant is more than four times the distance away from Parish as recommended by USEPA in the guidance memorandum, and because during the rare (10\%) of the time that the wind blows roughly from one plant to the other it is never strong enough to transport the plume from one facility to the other in one hour the predictive impacts from the Rhodia Houston Plant are not expected to significantly intersect with the Parish emissions such that the cumulative predicted impacts would exceed the NAAQS.

**Concentration Gradient:**

Figure 4-1 shows impacts contours of the modeling with seasonal diurnal ambient background added for Parish sources only. As shown in the figure, the maximum predicted impact occurs approximately 3.2 km due west of Parish Station. The predicted impacts remain above 100 µg/m\textsuperscript{3} (or approximately 50\% of the standard) as far as 14 km to the west and south, and 12 km to the east and north. The concentration gradient then decreases on a steady slope in all directions, with predicted impacts to the west being slightly higher than in the other directions. Predicted impacts fall off steadily to the northeast, supporting the conclusion that impacts from Parish should not significantly interact with those from Rhodia, or for that matter the combined impacts of all sources in the Houston Ship Channel area. This is further demonstrated in the discussion of ambient background monitors in Section 3.6, where it was shown that the Croquet monitor, roughly halfway to Houston from Parish Station is impacted by emissions from Parish, but the North Wayside monitor, which is much closer to the sources around the Houston Ship Channel, shows no discernable impact from Parish Station at all. Additionally, it should be noted that there are several ambient SO\textsubscript{2} monitors sited in the Houston area, which is far more industrial than the area around Parish, and none of those monitors show ambient concentrations greater than the one hour NAAQS.

For the reasons above, the Rhodia Houston Plant was therefore not explicitly modeled in the 1-hour SO\textsubscript{2} cumulative modeling analyses.
4.0 MODELING RESULTS

The modeling results are shown in Table 4-1 below. The modeled design value represents the modeled 3-year average of the 99th percentile, maximum daily 1-hour average impact for Parish. The predicted impacts when the seasonal diurnal background is added are then shown and compared to the NAAQS to demonstrate attainment.

Contours of the predicted impacts, as well as the location of the maximum predicted impact of 168.6 µg/m³ for the seasonal diurnal background modeling, are shown in Figure 4-1. The table shows that Parish Station emissions, when modeled using the most recent three years of actual emissions data, are below the level of the 1-hour SO₂ NAAQS.

TABLE 4-1: 1-hour SO₂ Modeling Results for Parish Station and background (µg/m³)

<table>
<thead>
<tr>
<th>Source</th>
<th>Parish Station Only</th>
<th>Parish and Background</th>
<th>1-hr.SO₂ NAAQS</th>
<th>Below NAAQS?</th>
</tr>
</thead>
<tbody>
<tr>
<td>Parish Station</td>
<td>163.2</td>
<td>168.6</td>
<td>196.5</td>
<td>Yes</td>
</tr>
</tbody>
</table>

4.1 CONCLUSIONS

The air dispersion modeling analysis performed as described in this report shows that the SO₂ emissions from W. A. Parish Station, when added to representative background values result in maximum predicted impacts below the 1-hour SO₂ National Ambient Air Quality Standard and therefore an attainment designation for Fort Bend County is recommended.
FIGURE 4-1: Parish Station 1-hour SO\textsubscript{2} Impact Contours
5.0 REFERENCES


U.S. Environmental Protection Agency. (USEPA 2014) “Data Requirements Rule for the 1-Hour Sulfur Dioxide (SO2) Primary National Ambient Air Quality Standard (NAAQS),” Pre-publication proposed rule, April 17, 2014; and