garza emc

GENERATIONAL PROPERTIES

6900 West Parmer Lane Austin, Travis County/Williamson County, Texas

SEWAGE COLLECTION SYSTEM (SCS) AND LIFT STATION REPORT

Prepared For:

APPLE INC. 12545 Riata Vista Circle, MS 522-EHS Austin, Texas 78727

Prepared by:

GARZA EMC, LLC. 7708 Rialto Blvd., Suite 125 Austin, Texas 78735 TBPE Registration No. F-14629

FEBRUARY 2024

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TBPE Registration No. F-14629

FEBRUARY 2024





March 13, 2024

Texas Commission on Environmental Quality Edwards Aquifer Protection Program 12100 Park 35 Circle, Building A Austin, Texas 78753

RE: TCEQ Modification Application Memo Capstone 6900 W. Parmer Lane Austin, Texas 78729

Dear Reviewer,

The purpose of this memo is to explain the proposed modifications to our previously approved Sewage Collection System (SCS) application.

All previously approved SCS infrastructure is detailed in the additional tables' pages immediately after the SCS application form. The tables in the SCS application form itself only contain new SCS infrastructure proposed with this modification. We are now proposing a lift station with 185 feet of 4" force main pipe and an additional 743 feet of 8" wastewater pipe connecting the lift station system to existing, previously approved, SCS infrastructure (Table 1). This table also lists 23 feet of 6" wastewater pipe and 134 feet of 8" wastewater pipe which has been added with changes to building services throughout the site. Table 1 on the SCS application form and the fee table on the Application Fee form only list the new, proposed SCS pipe which has a total length of 1,085 feet. Both the Modification of a Previously Approved Plan form and the Edwards Aquifer Application Cover Page list the previously approved SCC pipe length plus the new proposed SCS pipe length which now has a total length of 6,488 feet.

Furthermore, the previously approved SCS infrastructure listed on the additional tables' pages following the SCS application form reference sheet numbers of the now expired City of Austin Site Development Permit, SP-2018-0602C(R2) which was what the original SCS was approved under. The project is currently under review for a new City of Austin Site Development Permit, SP-0223-0292C which will replace the expired permit. This permit shows all the installed infrastructure from the expired permit as existing with the under construction and future phases being shown as new. The tables for new and revised SCS infrastructure reference sheets from the

GarzaEMC, LLC 7708 Rialto Blvd. Suite 125 Austin, Texas 78735 o: 512.298.3284 f: 512.298.2592

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new, under review, permit. The new under review permit has been included to be consistent with the tables. There are six new manholes proposed with this SCS pipe (Table 2). Utility sheets showing these new improvements are included with this application's submittal.

The City of Austin Service Extension Request (SER) was updated to include the expansion property. The new approved SER and the new SER's calculations are included as attachments with the modified SCS application.

As mentioned previously, we are now proposing a lift station and have included a Lift Station Application form and its required attachments with this application's submittal. The original TCEQ WPAP and SCS application's approval letter, as well as the approval letters from previous modifications, are included with this submittal.

Sincerely,

John Pelham, P.E. Senior Vice Presiden



Texas Commission on Environmental Quality Edwards Aquifer Application Cover Page

Our Review of Your Application

The Edwards Aquifer Program staff conducts an administrative and technical review of all applications. The turnaround time for administrative review can be up to 30 days as outlined in 30 TAC 213.4(e). Generally administrative completeness is determined during the intake meeting or within a few days of receipt. The turnaround time for technical review of an administratively complete Edwards Aquifer application is 90 days as outlined in 30 TAC 213.4(e). Please know that the review and approval time is directly impacted by the quality and completeness of the initial application that is received. In order to conduct a timely review, it is imperative that the information provided in an Edwards Aquifer application include final plans, be accurate, complete, and in compliance with <u>30 TAC 213</u>.

Administrative Review

1. <u>Edwards Aquifer applications</u> must be deemed administratively complete before a technical review can begin. To be considered administratively complete, the application must contain completed forms and attachments, provide the requested information, and meet all the site plan requirements. The submitted application and plan sheets should be final plans. Please submit one full-size set of plan sheets with the original application, and half-size sets with the additional copies.

To ensure that all applicable documents are included in the application, the program has developed tools to guide you and web pages to provide all forms, checklists, and guidance. Please visit the below website for assistance: <u>http://www.tceq.texas.gov/field/eapp</u>.

- 2. This Edwards Aquifer Application Cover Page form (certified by the applicant or agent) must be included in the application and brought to the administrative review meeting.
- 3. Administrative reviews are scheduled with program staff who will conduct the review. Applicants or their authorized agent should call the appropriate regional office, according to the county in which the project is located, to schedule a review. The average meeting time is one hour.
- 4. In the meeting, the application is examined for administrative completeness. Deficiencies will be noted by staff and emailed or faxed to the applicant and authorized agent at the end of the meeting, or shortly after. Administrative deficiencies will cause the application to be deemed incomplete and returned.

An appointment should be made to resubmit the application. The application is re-examined to ensure all deficiencies are resolved. The application will only be deemed administratively complete when all administrative deficiencies are addressed.

- 5. If an application is received by mail, courier service, or otherwise submitted without a review meeting, the administrative review will be conducted within 30 days. The applicant and agent will be contacted with the results of the administrative review. If the application is found to be administratively incomplete, it can be retrieved from the regional office or returned by regular mail. If returned by mail, the regional office may require arrangements for return shipping.
- 6. If the geologic assessment was completed before October 1, 2004 and the site contains "possibly sensitive" features, the assessment must be updated in accordance with the *Instructions to Geologists* (TCEQ-0585 Instructions).

Technical Review

- 1. When an application is deemed administratively complete, the technical review period begins. The regional office will distribute copies of the application to the identified affected city, county, and groundwater conservation district whose jurisdiction includes the subject site. These entities and the public have 30 days to provide comments on the application to the regional office. All comments received are reviewed by TCEQ.
- 2. A site assessment is usually conducted as part of the technical review, to evaluate the geologic assessment and observe existing site conditions. The site must be accessible to our staff. The site boundaries should be

clearly marked, features identified in the geologic assessment should be flagged, roadways marked and the alignment of the Sewage Collection System and manholes should be staked at the time the application is submitted. If the site is not marked the application may be returned.

- 3. We evaluate the application for technical completeness and contact the applicant and agent via Notice of Deficiency (NOD) to request additional information and identify technical deficiencies. There are two deficiency response periods available to the applicant. There are 14 days to resolve deficiencies noted in the first NOD. If a second NOD is issued, there is an additional 14 days to resolve deficiencies. If the response to the second notice is not received, is incomplete or inadequate, or provides new information that is incomplete or inadequate, the application must be withdrawn or will be denied. Please note that because the technical review is underway, whether the application is withdrawn or denied **the application fee will be forfeited**.
- 4. The program has 90 calendar days to complete the technical review of the application. If the application is technically adequate, such that it complies with the Edwards Aquifer rules, and is protective of the Edwards Aquifer during and after construction, an approval letter will be issued. Construction or other regulated activity may not begin until an approval is issued.

Mid-Review Modifications

It is important to have final site plans prior to beginning the permitting process with TCEQ to avoid delays.

Occasionally, circumstances arise where you may have significant design and/or site plan changes after your Edwards Aquifer application has been deemed administratively complete by TCEQ. This is considered a "Mid-Review Modification". Mid-Review Modifications may require redistribution of an application that includes the proposed modifications for public comment.

If you are proposing a Mid-Review Modification, two options are available:

- If the technical review has begun your application can be denied/withdrawn, your fees will be forfeited, and the plan will have to be resubmitted.
- TCEQ can continue the technical review of the application as it was submitted, and a modification application can be submitted at a later time.

If the application is denied/withdrawn, the resubmitted application will be subject to the administrative and technical review processes and will be treated as a new application. The application will be redistributed to the affected jurisdictions.

Please contact the regional office if you have questions. If your project is located in Williamson, Travis, or Hays County, contact TCEQ's Austin Regional Office at 512-339-2929. If your project is in Comal, Bexar, Medina, Uvalde, or Kinney County, contact TCEQ's San Antonio Regional Office at 210-490-3096

Please fill out all required fields below and submit with your application.

1. Regulated Entity Name: Generational Properties				2. Regulated Entity No.: RN110792173					
3. Customer Name: Apple Inc.				4. Customer No.: CN603691783					
5. Project Type: (Please circle/check one)	New		Modification		Extension		Exception		
6. Plan Type: (Please circle/check one)	WPAP	CZP	SCS	UST AST EX		EXP	EXT	Technical Clarification	Optional Enhanced Measures
7. Land Use: (Please circle/check one) Residentia		ntial	Non-residential		8. Sit		e (acres):	126.7	
9. Application Fee: \$650.00 10. Permanent		nent I	BMP(s	s):					
11. SCS (Linear Ft.):	6,664		12. AST/UST (No			o. Tanks):			
13. County: Travis/Willi 14. Watershed: amson				Rattan Creek					

Application Distribution

Г

Instructions: Use the table below to determine the number of applications required. One original and one copy of the application, plus additional copies (as needed) for each affected incorporated city, county, and groundwater conservation district are required. Linear projects or large projects, which cross into multiple jurisdictions, can require additional copies. Refer to the "Texas Groundwater Conservation Districts within the EAPP Boundaries" map found at:

http://www.tceq.texas.gov/assets/public/compliance/field_ops/eapp/EAPP%20GWCD%20map.pdf

For more detailed boundaries, please contact the conservation district directly.

Ausun Region							
County:	Hays	Travis	Williamson				
Original (1 req.) Region (1 req.)		_					
		_					
County(ies)							
Groundwater Conservation District(s)	Edwards Aquifer Authority Barton Springs/ Edwards Aquifer Hays Trinity Plum Creek	_√_Barton Springs/ Edwards Aquifer	NA				
City(ies) Jurisdiction	Austin Buda Dripping Springs Kyle Mountain City San Marcos Wimberley Woodcreek	_√_Austin Bee Cave Pflugerville Rollingwood Round Rock Sunset Valley West Lake Hills	_√_Austin Cedar Park Florence Georgetown Jerrell Leander Liberty Hill Pflugerville Round Rock				

San Antonio Region						
County:	Bexar	Comal	Kinney	Medina	Uvalde	
Original (1 req.)						
Region (1 req.)						
County(ies)						
Groundwater Conservation District(s)	Edwards Aquifer Authority Trinity-Glen Rose	Edwards Aquifer Authority	Kinney	EAA Medina	EAA Uvalde	
City(ies) Jurisdiction	Castle Hills Fair Oaks Ranch Helotes Hill Country Village Hollywood Park San Antonio (SAWS) Shayano Park	Bulverde Fair Oaks Ranch Garden Ridge New Braunfels Schertz	NA	San Antonio ETJ (SAWS)	NA	

Austin Region

I certify that to the best of my knowledge, that the application is complete and accurate. This application is hereby submitted to TCEQ for administrative review and technical review.

John Pelhapy P.E. Print Name of Oustomer/Authorized Agent

Signature of Customer/Authorized Agent

04/02/2024 Date

FOR TCEQ INTERNAL USE ONLY					
Date(s)Reviewed:	e(s)Reviewed: Date Administratively Complete:				
Received From:		Correct Number of Copies:			
Received By:		Distribution Date:			
EAPP File Number:		Complex:			
Admin. Review(s) (No.):		No. AR Rounds:			
Delinquent Fees (Y/N):		Review Time Spent:			
Lat./Long. Verified:	SOS Customer Verification:				
Agent Authorization Complete/Notarized (Y/N):	gent Authorization omplete/Notarized (Y/N):		/N):		
Core Data Form Complete (Y/N):		Check: Signed (Y/N):			
Core Data Form Incomplete Nos.:		Less than 90 days old (Y/N):			

General Information Form

Texas Commission on Environmental Quality

For Regulated Activities on the Edwards Aquifer Recharge and Transition Zones and Relating to 30 TAC §213.4(b) & §213.5(b)(2)(A), (B) Effective June 1, 1999

To ensure that the application is administratively complete, confirm that all fields in the form are complete, verify that all requested information is provided, consistently reference the same site and contact person in all forms in the application, and ensure forms are signed by the appropriate party.

Note: Including all the information requested in the form and attachments contributes to more streamlined technical reviews.

Signature

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This **General Information Form** is hereby submitted for TCEQ review. The application was prepared by:

Print Name of Customer/Agent: John Pelham, P.E.

Date: 04/02/2024

Signature of Customer/Agent:

Project Information

- 1. Regulated Entity Name: Generational Properties
- 2. County: <u>Travis/Williamson</u>
- 3. Stream Basin: Brazos River Rattan Creek
- 4. Groundwater Conservation District (If applicable): _____
- 5. Edwards Aquifer Zone:

\times	Recharge Zone
	Transition Zone

6. Plan Type:

WPAP	AST
scs	🔲 UST
Modification	Exception Request

7. Customer (Applicant):

Contact Person: <u>Dani Sattman</u> Entity: <u>Apple Inc.</u> Mailing Address: <u>12545 Riata Vista Circle, MS 522-EHS</u> City, State: <u>Austin, TX</u> Zip: <u>78727</u> Telephone: <u>512-674-8221</u> FAX: _____ Email Address: <u>dsattman598@apple.com</u>

8. Agent/Representative (If any):

Contact Person: John Pelham, P.E.Entity: GarzaEMC,LLCMailing Address: 7708 Rialto Blvd Suite 125City, State: AustinTelephone: 512-298-3284Email Address: jpelham@garzaemc.com

9. Project Location:

The project site is located inside the city limits of <u>Austin</u>.

The project site is located outside the city limits but inside the ETJ (extra-territorial jurisdiction) of ______.

The project site is not located within any city's limits or ETJ.

10. The location of the project site is described below. The description provides sufficient detail and clarity so that the TCEQ's Regional staff can easily locate the project and site boundaries for a field investigation.

<u>The east side of West Parmer Lane located between its intersections with McNeil Drive</u> and Anderson Mill Road, across from the intersection of Dallas Drive, with the centerline of Rattan Creek being the north boundary of the site, and south boundary near the mid-way point between Rattan Creek and McNeil Drive.</u>

- 11. Attachment A Road Map. A road map showing directions to and the location of the project site is attached. The project location and site boundaries are clearly shown on the map.
- 12. Attachment B USGS / Edwards Recharge Zone Map. A copy of the official 7 ½ minute USGS Quadrangle Map (Scale: 1" = 2000') of the Edwards Recharge Zone is attached. The map(s) clearly show:

Project site boundaries.

USGS Quadrangle Name(s).

Boundaries of the Recharge Zone (and Transition Zone, if applicable).

Drainage path from the project site to the boundary of the Recharge Zone.

13. The TCEQ must be able to inspect the project site or the application will be returned. Sufficient survey staking is provided on the project to allow TCEQ regional staff to locate the boundaries and alignment of the regulated activities and the geologic or manmade features noted in the Geologic Assessment.

- Survey staking will be completed by this date: _____
- 14. Attachment C Project Description. Attached at the end of this form is a detailed narrative description of the proposed project. The project description is consistent throughout the application and contains, at a minimum, the following details:
 - Area of the site
 Offsite areas
 Impervious cover
 Permanent BMP(s)
 - Proposed site use
 - Site history
 - Previous development
 - Area(s) to be demolished
- 15. Existing project site conditions are noted below:
 - Existing commercial site
 - Existing industrial site
 - Existing residential site
 - Existing paved and/or unpaved roads
 - Undeveloped (Cleared)
 - Undeveloped (Undisturbed/Uncleared)
 - Other: Site is currently under construction

Prohibited Activities

- 16. I am aware that the following activities are prohibited on the Recharge Zone and are not proposed for this project:
 - (1) Waste disposal wells regulated under 30 TAC Chapter 331 of this title (relating to Underground Injection Control);
 - (2) New feedlot/concentrated animal feeding operations, as defined in 30 TAC §213.3;
 - (3) Land disposal of Class I wastes, as defined in 30 TAC §335.1;
 - (4) The use of sewage holding tanks as parts of organized collection systems; and
 - (5) New municipal solid waste landfill facilities required to meet and comply with Type I standards which are defined in §330.41(b), (c), and (d) of this title (relating to Types of Municipal Solid Waste Facilities).
 - (6) New municipal and industrial wastewater discharges into or adjacent to water in the state that would create additional pollutant loading.
- 17. I am aware that the following activities are prohibited on the Transition Zone and are not proposed for this project:

- (1) Waste disposal wells regulated under 30 TAC Chapter 331 (relating to Underground Injection Control);
- (2) Land disposal of Class I wastes, as defined in 30 TAC §335.1; and
- (3) New municipal solid waste landfill facilities required to meet and comply with Type I standards which are defined in §330.41 (b), (c), and (d) of this title.

Administrative Information

18. The fee for the plan(s) is based on:

- For a Water Pollution Abatement Plan or Modification, the total acreage of the site where regulated activities will occur.
- For an Organized Sewage Collection System Plan or Modification, the total linear footage of all collection system lines.
- For a UST Facility Plan or Modification or an AST Facility Plan or Modification, the total number of tanks or piping systems.
- A request for an exception to any substantive portion of the regulations related to the protection of water quality.
- A request for an extension to a previously approved plan.
- 19. Application fees are due and payable at the time the application is filed. If the correct fee is not submitted, the TCEQ is not required to consider the application until the correct fee is submitted. Both the fee and the Edwards Aquifer Fee Form have been sent to the Commission's:

 Austin Regional Office (for projects in Hays, Travis, and Williamson Counties)
 San Antonio Regional Office (for projects in Bexar, Comal, Kinney, Medina, and Uvalde Counties)

- 20. Submit one (1) original and one (1) copy of the application, plus additional copies as needed for each affected incorporated city, groundwater conservation district, and county in which the project will be located. The TCEQ will distribute the additional copies to these jurisdictions. The copies must be submitted to the appropriate regional office.
- 21. No person shall commence any regulated activity until the Edwards Aquifer Protection Plan(s) for the activity has been filed with and approved by the Executive Director.

ATTACHMENT A – ROAD MAP

A road map is included with this application





V:\113799-00002\Civil\00-CAD\EXHBITS\Drainage Report - Site Location Map.dwg modified by hhumes on Jun 27, 23 12:51 PM

ATTACHMENT B – USGS / EDWARDS RECHARHE ZONE MAP

A USGS / Edwards recharge zone map is included with this application





(103452-0009)Civil(00-CAD/EXHIBITS)SDP EXHIBITS/Edward Aquifer Map.dwg modified by hhumes on Nov 7, 23 9:53 AM

ATTACHMENT C – PROJECT DESCRIPTION

The proposed development consists of approximately 3,000,000 square feet of office and R&D space, parking garages providing approximately 9,092 parking spaces, two central utility plants, and water, wastewater, storm sewer, and other dry utility infrastructure. In addition, there are site circulation roads, landscape and hardscape improvements, and a previously approved biofiltration pond for water quality treatment with a stacked detention pond. The project is proposed to be constructed in three phases.

The project site is approximately 126.7 acres in total area. Approximately 83.3 acres is developable area, with the remaining area proposed as Open Space. The north property boundary is the centerline of Rattan Creek, and the west boundary is West Parmer Lane. Currently the site is partially developed with a large number of existing trees.

The entirety of the site is located within Austin City Limits under Limited Purpose Jurisdiction. The site is also located within the Desired Development Zone as defined by the City of Austin and is currently partially developed. The proposed development is located within the Robinson Ranch PUD, per zoning case number C814-04-0066.

The project is located within the Rattan Creek Watershed which is classified as a suburban Watershed by the City of Austin's Comprehensive Watershed ordinance (CWO). The maximum allowable impervious cover for commercial uses in a suburban Watershed within the Robinson Ranch PUD is 90% under the MXD Major Land Use Category, as identified in the PUD Site Development Standards. Since the site is located within the Edwards Aquifer Recharge Zone, permanent Best Management Practices will be employed through biofiltration.



Modification of a Previously Approved Plan

Texas Commission on Environmental Quality

for Regulated Activities on the Edwards Aquifer Recharge Zone and Transition Zone and Relating to 30 TAC 213.4(j), Effective June 1, 1999

To ensure that the application is administratively complete, confirm that all fields in the form are complete, verify that all requested information is provided, consistently reference the same site and contact person in all forms in the application, and ensure forms are signed by the appropriate party.

Note: Including all the information requested in the form and attachments contributes to more streamlined technical reviews.

Signature

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This request for a **Modification of a Previously Approved Plan** is hereby submitted for TCEQ review and executive director approval. The request was prepared by:

Print Name of Customer/Agent: John Pelham, P.E.

Date: 04/02/2024 Signature of Customer/Agent:

Project Information

 Current Regulated Entity Name: <u>Generational Properties</u> Original Regulated Entity Name: <u>Generational Properties</u> Regulated Entity Number(s) (RN): <u>110792173</u>

Edwards Aquifer Protection Program ID Number(s): <u>11001603</u>, <u>11001604</u>

The applicant has not changed and the Customer Number (CN) is: <u>603691783</u>

The applicant or Regulated Entity has changed. A new Core Data Form has been provided.

2. Attachment A: Original Approval Letter and Approved Modification Letters. A copy of the original approval letter and copies of any modification approval letters are attached.

3. A modification of a previously approved plan is requested for (check all that apply):

Physical or operational modification of any water pollution abatement structure(s)
including but not limited to ponds, dams, berms, sewage treatment plants, and
diversionary structures;

Change in the nature or character of the regulated activity from that which was originally approved or a change which would significantly impact the ability of the plan to prevent pollution of the Edwards Aquifer;

Development of land previously identified as undeveloped in the original water pollution abatement plan;

Physical modification of the approved organized sewage collection system;

] Physical modification of the approved underground storage tank system;

Physical modification of the approved aboveground storage tank system.

4. Summary of Proposed Modifications (select plan type being modified). If the approved plan has been modified more than once, copy the appropriate table below, as necessary, and complete the information for each additional modification.

WPAP Modification	Approved Project	Proposed Modification
Summary		
Acres		
Type of Development		
Number of Residential		
Lots		
Impervious Cover (acres)		
Impervious Cover (%		
Permanent BMPs		
Other		
SCS Modification	Approved Project	Proposed Modification
Summary		
Linear Feet	<u>5,579</u>	<u>6664</u>
Pipe Diameter	<u>6",8",10",12" and 15"</u>	4",6",8",10",12" and 15"
Other		

AST Modification	Approved Project	Proposed Modification
Summary		
Number of ASTs		
Volume of ASTs		
Other		
UST Modification	Approved Project	Proposed Modification
UST Modification Summary	Approved Project	Proposed Modification
UST Modification Summary Number of USTs	Approved Project	Proposed Modification
UST Modification Summary Number of USTs Volume of USTs	Approved Project	Proposed Modification

- 5. Attachment B: Narrative of Proposed Modification. A detailed narrative description of the nature of the proposed modification is attached. It discusses what was approved, including any previous modifications, and how this proposed modification will change the approved plan.
- 6. Attachment C: Current Site Plan of the Approved Project. A current site plan showing the existing site development (i.e., current site layout) at the time this application for modification is attached. A site plan detailing the changes proposed in the submitted modification is required elsewhere.
 - The approved construction has not commenced. The original approval letter and any subsequent modification approval letters are included as Attachment A to document that the approval has not expired.
 - The approved construction has commenced and has been completed. Attachment C illustrates that the site was constructed as approved.
 - The approved construction has commenced and has been completed. Attachment C illustrates that the site was **not** constructed as approved.

The approved construction has commenced and has **not** been completed. Attachment C illustrates that, thus far, the site was constructed as approved.

- The approved construction has commenced and has **not** been completed. Attachment C illustrates that, thus far, the site was **not** constructed as approved.
- 7. The acreage of the approved plan has increased. A Geologic Assessment has been provided for the new acreage.
 - Acreage has not been added to or removed from the approved plan.
- 8. Submit one (1) original and one (1) copy of the application, plus additional copies as needed for each affected incorporated city, groundwater conservation district, and county in which the project will be located. The TCEQ will distribute the additional copies to these jurisdictions. The copies must be submitted to the appropriate regional office.

ATTACHMENT A – ORIGINAL APPROVAL LETTER AND MODIFICATION APPROVAL LETTERS

The original approval letter and approved modification letters are included with this application



Jon Niermann, Chairman Emily Lindley, Commissioner Toby Baker, Executive Director



TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

August 29, 2019

Mr. Scott Sidlow Apple, Inc. 1 Infinite Loop, MS:47-2 RE Cupertino, CA 95014-2083

Re: Edwards Aquifer, Williamson County

NAME OF PROJECT: Generational Properties; located east of Dallas Dr. and Parmer Ln., Austin Texas

TYPE OF PLAN: Request for Approval of a Water Pollution Abatement Plan (WPAP) & Organized Sewage Collection System Plan (SCS) 30 Texas Administrative Code (TAC) Chapter 213 Edwards Aquifer

Edwards Aquifer Protection Program ID No. 11001603 and 11001604; Regulated Entity No. RN110792173

Dear Mr. Sidlow:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the WPAP and SCS applications for the referenced project submitted to the Austin Regional Office on behalf of Apple, Inc. by Garza EMC, LLC on June 11, 2019. Final review of the WPAP and SCS was completed after additional material was received on August 20, 2019 and August 28, 2019. As presented to the TCEQ, the Temporary and Permanent Best Management Practices (BMPs) were selected and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213. These planning materials were sealed, signed and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

WPAP PROJECT DESCRIPTION

The proposed project will have an area of approximately 126.7 acres. It will include the construction of an office complex with multiple buildings, parking garages, drives, sidewalks, utility plants, water quality facilities, utilities, and associated appurtenances. The impervious cover will be 56.64 acres (45 percent).

TCEQ Region 11 • P.O. Box 13087 • Austin, Texas 78711-3087 • 512-339-2929 • Fax 512-339-3795

Mr. Scott Sidlow Page 2 August 29, 2019

PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, a biofiltration water quality basin, designed using the City of Austin <u>Environmental Criteria Manual (2019)</u>, will be constructed to treat stormwater runoff.

SCS PROJECT_DESCRIPTION

The proposed SCS will provide disposal service for the development. The system will consist of 3,691 linear feet of 6-inch diameter SDR-26 ASTM D3034 PVC pipe, 706 linear feet of 8-inch diameter SDR-26 ASTM D3034 PVC pipe, 517 linear feet of 10-inch diameter SDR-26 ASTM D3034 PVC pipe, 488 linear feet of 12-inch diameter SDR-26 ASTM D3034 PVC pipe, and 1,730 linear feet of 15-inch diameter SDR-26 ASTM D3034 PVC pipe.

The system will be connected to the existing Walnut Creek Wastewater Treatment Plant for treatment and disposal. The project is located within the City of Austin and will conform to all applicable codes, ordinances, and requirements of the City of Austin.

GEOLOGY

According to the Geologic Assessment included with the application, the site is underlain by Edwards Limestone. The soils are described as Fairlie clay, Georgetown stony clay, and Speck stony clay. Five sensitive features (F-1, F-3, F-4, F-5, and F-7) were identified in the Geologic Assessment. No regulated activities (such as construction or soil disturbing activities) will take place within the natural buffers. The size of the natural buffers is generally based on the drainage area for each sensitive feature and is depicted in the plan. No sensitive features were identified within 50 feet of the proposed SCS. The TCEQ site assessment conducted on August 1, 2019 revealed the site to be generally as described.

SPECIAL CONDITIONS

- I. All permanent pollution abatement measures shall be operational prior to occupancy of the facility.
- II. All sediment and/or media removed from the water quality basin during maintenance activities shall be properly disposed of according to 30 TAC 330 or 30 TAC 335, as applicable.
- III. It is emphasized that where wastewater lines must bridge faults, caverns, sinkholes, or solution features the lines shall be constructed in a manner that will maintain the structural integrity of the pipe. When such sensitive features area encountered, 30 TAC §213.5(f)(2) requires that all regulated activities near the feature must be immediately suspended and the owner/developer shall immediately notify the Austin Regional Office. Additionally, when such geologic features are encountered which are bridged by construction, the location and extend of those features must be assessed by a geologist and must be reported to the Austin Regional Office in writing within two working days of discovery as required by 30 TAC §213.5(c)(3)(K). Construction may not resume in the area of the feature until the executive director has reviewed and approved the methods proposed to protect the aquifer from any potential adverse impacts. See Standard Condition 12 below.

STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

Prior to Commencement of Construction:

- 4. Within 60 days of receiving written approval of an Edwards Aquifer Protection Plan, the applicant must submit to the Austin Regional Office, proof of recordation of notice in the county deed records, with the volume and page number(s) of the county deed records of the county in which the property is located. A description of the property boundaries shall be included in the deed recordation in the county deed records. A suggested form (Deed Recordation Affidavit, TCEQ-0625) that you may use to deed record the approved WPAP is enclosed.
- 5. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved WPAP, SCS and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 6. Modification to the activities described in the referenced WPAP and SCS applications following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.
- 7. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the Austin Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the date on which the regulated activity will commence, the name of the approved plan and program ID number for the regulated activity, and the name of the prime contractor with the name and telephone number of the contact person. The executive director will use the notification to determine if the approved plan is eligible for an extension.
- 8. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved WPAP, must be installed prior to construction and inspected, maintained and repaired during construction. Temporary E&S controls may be removed when vegetation is established and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.
- 9. All borings with depths greater than or equal to 20 feet must be plugged with non-shrink grout from the bottom of the hole to within three (3) feet of the surface. The remainder of the hole must be backfilled with cuttings from the boring. All borings less than 20 feet must be backfilled with cuttings from the boring. All borings must be backfilled or plugged within four (4) days of completion of the drilling operation. Voids may be filled with gravel.

Mr. Scott Sidlow Page 4 August 29, 2019

During Construction:

- 10. During the course of regulated activities related to this project, the applicant or agent shall comply with all applicable provisions of 30 TAC Chapter 213 and Chapter 217, Edwards Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.
- 11. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 6, above.
- 12. If any sensitive feature (caves, solution cavities, sink holes, etc.) is discovered during construction, all regulated activities near the feature must be suspended immediately. The applicant or his agent must immediately notify the Austin Regional Office of the discovery of the feature. Regulated activities near the feature may not proceed until the executive director has reviewed and approved the methods proposed to protect the feature and the aquifer from potentially adverse impacts to water quality. The plan must be sealed, signed, and dated by a Texas Licensed Professional Engineer.
- 13. All water wells including injection, dewatering, and monitoring wells must be in compliance with the requirements of the Texas Department of Licensing and Regulation under Title 16 TAC Chapter 76 (relating to Water Well Drillers and Pump Installers) and all other locally applicable rules, as appropriate.
- 14. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50 percent. Litter, construction debris, and construction chemicals shall be prevented from becoming stormwater discharge pollutants.
- 15. Discharges of sediment laden water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices.
- 16. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 17. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.
- 18. No part of the system shall be used as a holding tank for a pump-and-haul operation.

After Completion of Construction:

- 19. Owners of permanent BMPs and measures must insure that the BMPs and measures are constructed and function as designed. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the Austin Regional Office within 30 days of site completion.
- 20. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. Such entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is

transferred. A copy of the transfer of responsibility must be filed with the executive director through the Austin Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.

- 21. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 22. Certification by a Texas Licensed Professional Engineer of the testing of sewage collection systems required by 30 TAC Chapter 213 and Chapter 217 shall be submitted to the Austin Regional Office within 30 days of test completion and prior to the new sewage collection system being put into service. The certification should include the project name as it appeared on the approved application, the program ID number, and two copies of a site plan sheet(s) indicating the wastewater lines that were tested and are being certified as complying with the appropriate regulations.
- 23. Every five years after the initial certification, the sewage collection system shall be retested. Any lines that fail the test must be repaired and retested. Certification that the system continues to meet the requirements of 30 TAC Chapter 213 and Chapter 217 shall be submitted to the Austin Regional Office. The certification should include the project name as it appeared on the approved application, the program ID number and two copies of a site plan sheet(s) indicating the wastewater lines that were tested and are being certified as complying with the appropriate regulations. Should any test result fail to meet passing test criteria, and then subsequently pass testing, the result(s) and an explanation of what repair, adjustment, or other means were taken to facilitate a subsequent passing result shall be provided.
- 24. If ownership of this organized sewage collection system is legally transferred (e.g., developer to city or Municipal Utility District), the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 25. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.
- 26. An Edwards Aquifer protection plan approval or extension will expire and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new Edwards Aquifer protection plan must be submitted to the Austin Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.

This action is taken under authority delegated by the Executive Director of the Texas Commission on Environmental Quality. If you have any questions or require additional information, please contact James "Bo" Slone, P.G. of the Edwards Aquifer Protection Program of the Austin Regional Office at (512) 339-2929.

Sincerely,

Robert Sadlier, Section Manager Edwards Aquifer Protection Program Texas Commission on Environmental Quality

Mr. Scott Sidlow Page 6 August 29, 2019

RCS/jcs

Enclosure:Deed Recordation Affidavit, Form TCEQ-0625Change in Responsibility for Maintenance of Permanent BMPs, Form TCEQ-10263

Deed Recordation Affidavit Edwards Aquifer Protection Plan

THE STATE OF TEXAS §

County of _____ §

BEFORE ME, the undersigned authority, on this day personally appeared ______ who, being duly sworn by me, deposes and says:

- (1) That my name is ______and that I own the real property described below.
- (2) That said real property is subject to an EDWARDS AQUIFER PROTECTION PLAN which was required under the 30 Texas Administrative Code (TAC) Chapter 213.
- (3) That the EDWARDS AQUIFER PROTECTION PLAN for said real property was approved by the Texas Commission on Environmental Quality (TCEQ) on _______.

A copy of the letter of approval from the TCEQ is attached to this affidavit as Exhibit A and is incorporated herein by reference.

(4) The said real property is located in _____ County, Texas, and the legal description of the property is as follows:

LANDOWNER-AFFIANT

SWORN AND SUBSCRIBED TO before me, on this _ day of _____, ____.

NOTARY PUBLIC

THE STATE OF _____ §

County of _____ §

BEFORE ME, the undersigned authority, on this day personally appeared ______ known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that (s)he executed same for the purpose and consideration therein expressed.

GIVEN under my hand and seal of office on this _ day of _____, ____,

NOTARY PUBLIC

Typed or Printed Name of Notary

MY COMMISSION EXPIRES: _____

Change in Responsibility for Maintenance on Permanent Best Management Practices and Measures

The applicant is no longer responsible for maintaining the permanent best management practice (BMP) and other measures. The project information and the new entity responsible for maintenance is listed below.

,,,,
D:

Signature of New Responsible Party

Date

I acknowledge and understand that I am assuming full responsibility for maintaining all permanent best management practices and measures approved by the TCEQ for the site, until another entity assumes such obligations in writing or ownership is transferred.

If you have questions on how to fill out this form or about the Edwards Aquifer protection program, please contact us at 210/490-3096 for projects located in the San Antonio Region or 512/339-2929 for projects located in the Austin Region.

Individuals are entitled to request and review their personal information that the agency gathers on its forms. They may also have any errors in their information corrected. To review such information, contact us at 512/239-3282.

TCEQ-10263 (10/01/04)

Jon Niermann, Chairman Emily Lindley, Commissioner Bobby Janecka, Commissioner Toby Baker, Executive Director



TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

April 9, 2020

Ms. Dani Sattman Apple, Inc. 5505 W. Parmer Ln., Bldg 4, EHS-578 Austin, Texas 78727

Re: Edwards Aquifer, Williamson County

NAME OF PROJECT: Generational Properties; located E. of Dallas Dr. and W. Parmer Ln., Austin Texas

TYPE OF PLAN: Request for Modification of a Previously Approved Water Pollution Abatement Plan (WPAP) & Organized Sewage Collection System Plan (SCS) 30 Texas Administrative Code (TAC) Chapter 213 Edwards Aquifer

Edwards Aquifer Protection Program (EAPP) ID Nos. 11001930 and 11001931; Regulated Entity No. RN110792173

Dear Ms. Sattman:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the WPAP and SCS Modifications for the referenced project submitted to the Austin Regional Office on behalf of Apple, Inc. by Garza EMC, LLC on February 11, 2020. Final review of the WPAP and SCS was completed after additional material was received on April 1, 2020 and April 2, 2020. As presented to the TCEQ, the Temporary and Permanent Best Management Practices (BMPs) were selected and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213. These planning materials were sealed, signed and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

BACKGROUND

WPAP and SCS applications were approved by letter dated August 29, 2019 (EAPP ID Nos. 11001603 and 11001604). The letter approved the development of a 126.7-acre office complex with 56.64 acres of impervious cover.

TCEQ Region 11 • P.O. Box 13087 • Austin, Texas 78711-3087 • 512-339-2929 • Fax 512-339-3795

Ms. Dani Sattman Page 2 April 9, 2020

WPAP PROJECT DESCRIPTION

The proposed project will have an area of approximately 126.7 acres. It will include the construction of an office complex with multiple buildings, parking garages, drives, sidewalks, utility plants, water quality facilities, utilities, and associated appurtenances. The impervious cover will be 56.1 acres (44 percent).

PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, a biofiltration water quality basin, designed using the City of Austin <u>Environmental Criteria Manual (2019)</u>, will be constructed to treat stormwater runoff.

SCS PROJECT DESCRIPTION

The proposed SCS will provide disposal service for the development. The system will consist of 1,403.49 linear feet of 6-inch diameter SDR-26 ASTM D3034 PVC pipe, 999.80 linear feet of 8-inch diameter SDR-26 ASTM D3034 PVC pipe, 737.77 linear feet of 10-inch diameter SDR-26 ASTM D3034 PVC pipe, 847.07 linear feet of 12-inch diameter SDR-26 ASTM D3034 PVC pipe, and 1,259.46 linear feet of 15-inch diameter SDR-26 ASTM D3034 PVC pipe. Additionally, the system will include 160 linear feet of 6-inch diameter SDR-21 ASTM D2241 PVC pipe, 40 linear feet of 8-inch diameter SDR-21 ASTM D2241 PVC pipe, and 20 linear feet of 12-inch diameter SDR-21 ASTM D2241 PVC pipe for wastewater line/water line crossings.

The system will be connected to the existing Walnut Creek Wastewater Treatment Plant for treatment and disposal. The project is located within the City of Austin and will conform to all applicable codes, ordinances, and requirements of the City of Austin.

GEOLOGY

According to the Geologic Assessment included with the application, the site is underlain by Edwards Limestone. The soils are described as Fairlie clay, Georgetown stony clay, and Speck stony clay. Five sensitive features (F-1, F-3, F-4, F-5, and F-7) were identified in the Geologic Assessment. No regulated activities (such as construction or soil disturbing activities) will take place within the natural buffers. The size of the natural buffers is generally based on the drainage area for each sensitive feature and is depicted in the plan. No sensitive features were identified within 50 feet of the proposed SCS. The TCEQ site assessment was conducted on August 1, 2019 in association with the EAPP ID Nos. 11001603 and 11001604 applications. The site assessment revealed the site to be generally as described.

SPECIAL CONDITIONS

- I. All permanent pollution abatement measures shall be operational prior to occupancy of the facility.
- II. All sediment and/or media removed from the water quality basin during maintenance activities shall be properly disposed of according to 30 TAC 330 or 30 TAC 335, as applicable.

STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

Prior to Commencement of Construction:

- 4. Within 60 days of receiving written approval of an Edwards Aquifer Protection Plan, the applicant must submit to the Austin Regional Office, proof of recordation of notice in the county deed records, with the volume and page number(s) of the county deed records of the county in which the property is located. A description of the property boundaries shall be included in the deed recordation in the county deed records. A suggested form (Deed Recordation Affidavit, TCEQ-0625) that you may use to deed record the approved WPAP is enclosed.
- 5. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved WPAP, SCS and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 6. Modification to the activities described in the referenced WPAP and SCS applications following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.
- 7. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the Austin Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the date on which the regulated activity will commence, the name of the approved plan and program ID number for the regulated activity, and the name of the prime contractor with the name and telephone number of the contact person. The executive director will use the notification to determine if the approved plan is eligible for an extension.
- 8. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved WPAP, must be installed prior to construction and inspected, maintained and repaired during construction. Temporary E&S controls may be removed when vegetation is established and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.
- 9. All borings with depths greater than or equal to 20 feet must be plugged with non-shrink grout from the bottom of the hole to within three (3) feet of the surface. The remainder of the hole must be backfilled with cuttings from the boring. All borings less than 20 feet must be backfilled with cuttings from the boring. All borings must be backfilled or plugged within four (4) days of completion of the drilling operation. Voids may be filled with gravel.

During Construction:

10. During the course of regulated activities related to this project, the applicant or agent shall comply with all applicable provisions of 30 TAC Chapter 213 and Chapter 217, Edwards

Ms. Dani Sattman Page 4 April 9, 2020

Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.

- 11. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 6, above.
- 12. If any sensitive feature (caves, solution cavities, sink holes, etc.) is discovered during construction, all regulated activities near the feature must be suspended immediately. The applicant or his agent must immediately notify the Austin Regional Office of the discovery of the feature. Regulated activities near the feature may not proceed until the executive director has reviewed and approved the methods proposed to protect the feature and the aquifer from potentially adverse impacts to water quality. The plan must be sealed, signed, and dated by a Texas Licensed Professional Engineer.
- 13. All water wells including injection, dewatering, and monitoring wells must be in compliance with the requirements of the Texas Department of Licensing and Regulation under Title 16 TAC Chapter 76 (relating to Water Well Drillers and Pump Installers) and all other locally applicable rules, as appropriate.
- 14. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50 percent. Litter, construction debris, and construction chemicals shall be prevented from becoming stormwater discharge pollutants.
- 15. Discharges of sediment laden water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices.
- 16. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 17. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.
- 18. No part of the system shall be used as a holding tank for a pump-and-haul operation.

After Completion of Construction:

- 19. Owners of permanent BMPs and measures must ensure that the BMPs and measures are constructed and function as designed. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the Austin Regional Office within 30 days of site completion.
- 20. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. Such entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred. A copy of the transfer of responsibility must be filed with the executive director through the Austin Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.
- 21. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence

Ms. Dani Sattman Page 5 April 9, 2020

- any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director.
 Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 22. Certification by a Texas Licensed Professional Engineer of the testing of sewage collection systems required by 30 TAC Chapter 213 and Chapter 217 shall be submitted to the Austin Regional Office within 30 days of test completion and prior to the new sewage collection system being put into service. The certification should include the project name as it appeared on the approved application, the program ID number, and two copies of a site plan sheet(s) indicating the wastewater lines that were tested and are being certified as complying with the appropriate regulations.
- 23. Every five years after the initial certification, the sewage collection system shall be retested. Any lines that fail the test must be repaired and retested. Certification that the system continues to meet the requirements of 30 TAC Chapter 213 and Chapter 217 shall be submitted to the Austin Regional Office. The certification should include the project name as it appeared on the approved application, the program ID number and two copies of a site plan sheet(s) indicating the wastewater lines that were tested and are being certified as complying with the appropriate regulations. Should any test result fail to meet passing test criteria, and then subsequently pass testing, the result(s) and an explanation of what repair, adjustment, or other means were taken to facilitate a subsequent passing result shall be provided.
- 24. If ownership of this organized sewage collection system is legally transferred (e.g., developer to city or Municipal Utility District), the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 25. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.

An Edwards Aquifer protection plan approval or extension will expire and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new Edwards Aquifer protection plan must be submitted to the Austin Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.

This action is taken under authority delegated by the Executive Director of the Texas Commission on Environmental Quality. If you have any questions or require additional information, please contact James "Bo" Slone, P.G. of the Edwards Aquifer Protection Program of the Austin Regional Office at (512) 339-2929.

Sincerely,

Robert Sadlier, Section Manager Edwards Aquifer Protection Program Texas Commission on Environmental Quality

RCS/jcs

Enclosure: Deed Recordation Affidavit, Form TCEQ-0625

Change in Responsibility for Maintenance of Permanent BMPs, Form TCEQ-10263

Deed Recordation Affidavit Edwards Aquifer Protection Plan

THE STATE OF TEXAS 5 County of _____ § BEFORE ME, the undersigned authority, on this day personally appeared ______ who, being duly sworn by me, deposes and says: That my name is ______and that I own the real property described below. (1)That said real property is subject to an EDWARDS AQUIFER PROTECTION PLAN which was required (2)under the 30 Texas Administrative Code (TAC) Chapter 213. That the EDWARDS AQUIFER PROTECTION PLAN for said real property was approved by the Texas (3)Commission on Environmental Quality (TCEQ) on _____ A copy of the letter of approval from the TCEQ is attached to this affidavit as Exhibit A and is incorporated herein by reference. The said real property is located in _____ County, Texas, and the legal description of (4)the property is as follows: LANDOWNER-AFFIANT SWORN AND SUBSCRIBED TO before me, on this __ day of _____, ____. NOTARY PUBLIC THE STATE OF _____§ County of _____ § BEFORE ME, the undersigned authority, on this day personally appeared __ known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that (s)he executed same for the purpose and consideration therein expressed. GIVEN under my hand and seal of office on this _ day of _____, ____, NOTARY PUBLIC Typed or Printed Name of Notary MY COMMISSION EXPIRES: _____

Change in Responsibility for Maintenance on Permanent Best Management Practices and Measures

The applicant is no longer responsible for maintaining the permanent best management practice (BMP) and other measures. The project information and the new entity responsible for maintenance is listed below.

Customer:			;		
Regulated Entity Name	•				
Site Address:					
City, Texas, Zip:		<u> </u>			
County:		æ .			
Approval Letter Date:					
BMPs for the project:					
New Responsible Party	/:				,
Name of contact:					
Mailing Address:		16			
City, State:				Zip:	
Telephone:			FAX	×	

Signature of New Responsible Party

Date

I acknowledge and understand that I am assuming full responsibility for maintaining all permanent best management practices and measures approved by the TCEQ for the site, until another entity assumes such obligations in writing or ownership is transferred.

If you have questions on how to fill out this form or about the Edwards Aquifer protection program, please contact us at 210/490-3096 for projects located in the San Antonio Region or 512/339-2929 for projects located in the Austin Region.

Individuals are enlitled to request and review their personal information that the agency gathers on its forms. They may also have any errors in their information corrected. To review such information, contact us at 512/239-3282.

TCEQ-10263 (10/01/04)
Jon Niermann, *Chairman* Emily Lindley, *Commissioner* Bobby Janecka, *Commissioner* Toby Baker, *Executive Director*



TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

November 16, 2022

Ms. Dani Sattman Apple, Inc. 5505 W. Parmer Ln. Bldg. 4, EHS-578 Austin, Texas 78727

Re: Edwards Aquifer, Williamson County

NAME OF PROJECT: Generational Properties; located east of Dallas Dr. and West Parmer Lane; Austin, Texas

TYPE OF PLAN: Request for Modification of an approved Water Pollution Abatement Plan (WPAP-MOD) & an approved Organized Sewage Collection System (SCS-MOD) Plan; 30 Texas Administrative Code (TAC) Chapter 213 Edwards Aquifer

Edwards Aquifer Protection Program ID No. 11003239 (WPAP-MOD) and 11003240 (SCS-MOD); Regulated Entity No. RN110792173

Dear Mr. Sidlow:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the WPAP-MOD and SCS-MOD applications for the above-referenced project submitted to the Austin Regional Office by Garza EMC, LLC. on behalf of Apple, Inc. on September 09, 2022. Final review of the WPAP-MOD and SCS-MOD Applications was completed after additional material was received on November 4, 2022. As presented to the TCEQ, the Temporary and Permanent Best Management Practices (BMPs) were selected, and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213 and Chapter 217. These planning materials were sealed, signed and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

BACKGROUND

A WPAP application and a SCS application were approved by letter dated August 29, 2019 (EAPP ID Nos. 11001603 and 11001604). The WPAP included the construction of a biofiltration basin. A WPAP-MOD application and a SCS-MOD application were approved by letter dated April 9, 2020 (EAPP ID Nos. 11001930 and 11001931). A WPAP Exception application was approved by letter dated November 12, 2020 (EAPP ID No. 11002205).

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WPAP PROJECT DESCRIPTION

The proposed project will have an area of approximately 126.7 acres. It will include the construction of an office complex with multiple buildings, parking garages, drives, sidewalks, utility plants, water quality facilities, utilities, and associated appurtenances. The impervious cover will be 49.8 acres (39.3 percent).

PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, a biofiltration water quality basin (EAPP ID No. 11001603), designed using the City of Austin <u>Environmental Criteria Manual</u> (2019), will be used to treat stormwater runoff.

SCS PROJECT DESCRIPTION

The proposed sewage collection system will provide disposal service for the development. The 5,819 linear feet gravity SCS will be composed of 1,219 linear feet of 6-inch PVC-SDR 26 ASTM D3034 pipe, 1,503 linear feet of 8-inch PVC-SDR 26 ASTM D3034 pipe, 722 linear feet of 10-inch PVC-SDR 26 ASTM D3034 pipe, 876 linear feet of 12-inch PVC-SDR 26 ASTM D3034 pipe, and 1,259 linear feet of 15-inch PVC-SDR 26 ASTM D3034 pipe. Additionally, the system will include 160 linear feet of 6-inch PVC-SDR 26 ASTM D2241 pipe, 40 linear feet of 8-inch PVC-SDR 26 ASTM D2241 pipe, and 20 linear feet of 12-inch PVC-SDR 26 ASTM D2241 pipe, and 20 linear feet of 12-inch PVC-SDR 26 ASTM D2241 pipe. The system will be connected to the existing Walnut Creek Wastewater Treatment Plant for treatment and disposal. The project is located within the City of Austin and will conform to all applicable codes, ordinances, and requirements of the City of Austin.

GEOLOGY

According to the Geologic Assessment included with the application, the site is underlain by Edwards Limestone. The soils are described as Fairlie clay, Georgetown stony clay, and Speck stony clay. Five sensitive features (F-1, F-3, F-4, F-5, and F-7) were identified in the Geologic Assessment. No regulated activities (such as construction or soil disturbing activities) will take place within the natural buffers. The size of the natural buffers is generally based on the drainage area for each sensitive feature and is depicted in the plan. No sensitive features were identified within 50 feet of the proposed SCS. The TCEQ site assessment, conducted during a review for a previous application on August 1, 2019, revealed the site to be generally as described.

STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

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Prior to Commencement of Construction:

- 4. Within 60 days of receiving written approval of an Edwards Aquifer Protection Plan, the applicant must submit to the Austin Regional Office, proof of recordation of notice in the county deed records, with the volume and page number(s) of the county deed records of the county in which the property is located. A description of the property boundaries shall be included in the deed recordation in the county deed records. A suggested form (Deed Recordation Affidavit, TCEQ-0625) that you may use to deed record the approved WPAP is enclosed.
- 5. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved WPAP and SCS and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 6. Modification to the activities described in the referenced WPAP and SCS applications following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.
- 7. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the Austin Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the date on which the regulated activity will commence, the name of the approved plan and program ID number for the regulated activity, and the name of the prime contractor with the name and telephone number of the contact person. The executive director will use the notification to determine if the approved plan is eligible for an extension.
- 8. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved WPAP, must be installed prior to construction and inspected, maintained and repaired during construction. Temporary E&S controls may be removed when vegetation is established and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.
- 9. All borings with depths greater than or equal to 20 feet must be plugged with non-shrink grout from the bottom of the hole to within three (3) feet of the surface. The remainder of the hole must be backfilled with cuttings from the boring. All borings less than 20 feet must be backfilled with cuttings from the boring. All borings must be backfilled or plugged within four (4) days of completion of the drilling operation. Voids may be filled with gravel.

During Construction:

- 10. During the course of regulated activities related to this project, the applicant or agent shall comply with all applicable provisions of 30 TAC Chapter 213 and Chapter 217, Edwards Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.
- 11. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 6, above.
- 12. If any sensitive feature (caves, solution cavities, sink holes, etc.) is discovered during construction, all regulated activities near the feature must be suspended immediately. The applicant or his agent must immediately notify the Austin Regional Office of the discovery of the feature. Regulated activities near the feature may not proceed until the executive director has reviewed and approved the methods proposed to protect the feature and the

aquifer from potentially adverse impacts to water quality. The plan must be sealed, signed, and dated by a Texas Licensed Professional Engineer.

- 13. All water wells including injection, dewatering, and monitoring wells must be in compliance with the requirements of the Texas Department of Licensing and Regulation under Title 16 TAC Chapter 76 (relating to Water Well Drillers and Pump Installers) and all other locally applicable rules, as appropriate.
- 14. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50 percent. Litter, construction debris, and construction chemicals shall be prevented from becoming stormwater discharge pollutants.
- 15. Discharges of sediment laden water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices.
- 16. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 17. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.
- 18. No part of the system shall be used as a holding tank for a pump-and-haul operation.

After Completion of Construction:

- 19. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the Austin Regional Office within 30 days of site completion.
- 20. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. The regulated entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred. A copy of the transfer of responsibility must be filed with the executive director through Austin Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.
- 21. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 22. Certification by a Texas Licensed Professional Engineer of the testing of sewage collection systems required by 30 TAC Chapter 213 and Chapter 217 shall be submitted to the Austin Regional Office within 30 days of test completion and prior to the new sewage collection system being put into service. The certification should include the project name as it appeared on the approved application, the program ID number, and two copies of a site plan sheet(s) indicating the wastewater lines that were tested and are being certified as complying with the appropriate regulations.

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> Every five years after the initial certification, the sewage collection system shall be retested. Any lines that fail the test must be repaired and retested. Certification that the system continues to meet the requirements of 30 TAC Chapter 213 and Chapter 217 shall be submitted to the Austin Regional Office. The certification should include the project name as it appeared on the approved application, the program ID number and two copies of a site plan sheet(s) indicating the wastewater lines that were tested and are being certified as complying with the appropriate regulations. Should any test result fail to meet passing test criteria, and then subsequently pass testing, the result(s) and an explanation of what repair, adjustment, or other means were taken to facilitate a subsequent passing result shall be provided.

- 23. If ownership of this organized sewage collection system is legally transferred (e.g., developer to city or Municipal Utility District), the new owner(s) is required to comply with all terms of the approved Edwards Aquifer protection plan. If the new owner intends to commence any new regulated activity on the site, a new Edwards Aquifer protection plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 24. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.
- 25. An Edwards Aquifer protection plan approval or extension will expire and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new Edwards Aquifer protection plan must be submitted to the Austin Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.

This action is taken under authority delegated by the Executive Director of the Texas Commission on Environmental Quality. If you have any questions or require additional information, please contact James "Bo" Slone, P.G. of the Edwards Aquifer Protection Program of the Austin Regional Office at (512) 339-2929.

Sincerely,

Lillian Butter

Lillian Butler, Section Manager Edwards Aquifer Protection Program Texas Commission on Environmental Quality

LIB/jcs

Enclosures: Deed Recordation Affidavit, Form TCEQ-0625

CC Mr. John D. Pelham, P.E., Garza Emc, LLC

Deed Recordation Affidavit Edwards Aquifer Protection Plan

THE STATE OF TEXAS §

County of _____ §

BEFORE ME, the undersigned authority, on this day personally appeared ______ who, being duly sworn by me, deposes and says:

- (1) That my name is ______and that I own the real property described below.
- (2) That said real property is subject to an EDWARDS AQUIFER PROTECTION PLAN which was required under the 30 Texas Administrative Code (TAC) Chapter 213.
- (3) That the EDWARDS AQUIFER PROTECTION PLAN for said real property was approved by the Texas Commission on Environmental Quality (TCEQ) on _____.

A copy of the letter of approval from the TCEQ is attached to this affidavit as Exhibit A and is incorporated herein by reference.

(4) The said real property is located in _____ County, Texas, and the legal description of the property is as follows:

LANDOWNER-AFFIANT

SWORN AND SUBSCRIBED TO before me, on this __ day of _____, ____.

NOTARY PUBLIC

THE STATE OF ______ §

County of _____ §

BEFORE ME, the undersigned authority, on this day personally appeared ______ known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that (s)he executed same for the purpose and consideration therein expressed.

GIVEN under my hand and seal of office on this _ day of _____, ____.

NOTARY PUBLIC

Typed or Printed Name of Notary

MY COMMISSION EXPIRES:

Attachment B- Narrative of Proposed Modification

This narrative addresses changes associated with the proposed modification to the previously approved Sewage Collection System (SCS). The changes associated with the previously approved SCS plan are as follow:

<u>Site Plan</u>

• Revised drives and Building locations

Grading effects:

- Grading has been revised to reflect the site plan revision
- Changes to temporary stormwater erosion and sedimentation controls to accommodate grading changes

<u>Storm</u>

• Revised storm water routing to reflect site plan changes

<u>Water</u>

• Revised water utility route to reflect site plan changes

<u>Wastewater</u>

- Revised wastewater utility route to reflect site plan changes
- A lift station and associated force main pipe has been added
- Revised F-0582 Application Table 1 Pipe Description

All the changes associated with this modification are reflected in the attached site plans. See Attachment C.

ATTACHMENT C – CURRENT SITE PLAN OF THE APPROVED PROJECT

Currently approved construction documents are included with this application



Organized Sewage Collection System Application

Texas Commission on Environmental Quality

For Regulated Activities on the Edwards Aquifer Recharge Zone and Relating to 30 TAC §213.5(c), Effective June 1, 1999

To ensure that the application is administratively complete, confirm that all fields in the form are complete, verify that all requested information is provided, consistently reference the same site and contact person in all forms in the application, and ensure forms are signed by the appropriate party.

Note: Including all the information requested in the form and attachments contributes to more streamlined technical reviews.

Regulated Entity Name: Generational Properties

 Attachment A – SCS Engineering Design Report. This Engineering Design Report is provided to fulfill the requirements of 30 TAC Chapter 217, including 217.10 of Subchapter A, §§217.51 – 217.70 of Subchapter C, and Subchapter D as applicable, and is required to be submitted with this SCS Application Form.

Customer Information

 The entity and contact person responsible for providing the required engineering certification of testing for this sewage collection system upon completion (including private service connections) and every five years thereafter to the appropriate TCEQ region office pursuant to 30 TAC §213.5(c) is:

Contact Person: <u>Dani Sattman</u> Entity: <u>Apple Inc.</u> Mailing Address: <u>12545 Riata Vista Circle, MS 522-EHS</u> City, State: <u>Austin, TX</u> Zip: <u>78727</u> Telephone: <u>512-674-8221</u> Fax: _____ Email Address: <u>dsattman598@apple.com</u> The appropriate regional office must be informed of any changes in this information within 30 days of the change.

3. The engineer responsible for the design of this sewage collection system is:

Contact Person: John Pelham, P.E. Texas Licensed Professional Engineer's Number: <u>98294</u> Entity: <u>GarzaEMC, LLC</u> Mailing Address: <u>7708 Rialto Blvd Suite 125</u> City, State:<u>Austin, TX</u> Telephone:<u>512 298 3284</u> Email Address:<u>ipelham@garzaemc.com</u>

Project Information

4. Anticipated type of development to be served (estimated future population to be served, plus adequate allowance for institutional and commercial flows):

	Residential: Number of single-family lots:
	Multi-family: Number of residential units:
\times	Commercial
	Industrial
	Off-site system (not associated with any development)
	Other:

5. The character and volume of wastewater is shown below:

<u>0</u> % Domestic	<u>296,640</u> gallons/day
<u>0</u> % Industrial	<u>0</u> gallons/day
<u>100</u> % Commingled	<u>0</u> gallons/day
Total gallons/day: <u>296,640</u>	

- 6. Existing and anticipated infiltration/inflow is <u>62,475</u> gallons/day. This will be addressed by: <u>Pipe sizing adjustments</u>.
- 7. A Water Pollution Abatement Plan (WPAP) is required for construction of any associated commercial, industrial or residential project located on the Recharge Zone.

The WPAP application for this development was approved by letter dated <u>8/29/2019</u>, <u>4/9/2020</u>, and <u>11/16/2022</u>. A copy of the approval letter is attached.

The WPAP application for this development was submitted to the TCEQ on _____, but has not been approved.

A WPAP application is required for an associated project, but it has not been submitted. There is no associated project requiring a WPAP application.

8. Pipe description:

Table 1 - Pipe Description

Pipe			
Diameter(Inches)	Linear Feet (1)	Pipe Material (2)	Specifications (3)
4	184.50	PVC SDR 26	ASTM D 2241
6	22.65	PVC SDR 26	ASTM D 3034
8	877.75	PVC SDR 26	ASTM D 3034
Prev approved at end			

Total Linear Feet: 1085

- (1) Linear feet Include stub-outs and double service connections. Do not include private service laterals.
- (2) Pipe Material If PVC, state SDR value.
- (3) Specifications ASTM / ANSI / AWWA specification and class numbers should be included.

9. The sewage collection system will convey the wastewater to the <u>Walnut Creek</u> (name) Treatment Plant. The treatment facility is:

\times	Existing
	Proposed

10. All components of this sewage collection system will comply with:



- 11. No force main(s) and/or lift station(s) are associated with this sewage collection system.
 - A force main(s) and/or lift station(s) is associated with this sewage collection system and the Lift Station/Force Main System Application form (TCEQ-0624) is included with this application.

Alignment

- 12. There are no deviations from uniform grade in this sewage collection system without manholes and with open cut construction.
- 13. There are no deviations from straight alignment in this sewage collection system without manholes.

Attachment B - Justification and Calculations for Deviation in Straight Alignment without Manholes. A justification for deviations from straight alignment in this sewage collection system without manholes with documentation from pipe manufacturer allowing pipe curvature is attached.

For curved sewer lines, all curved sewer line notes (TCEQ-0596) are included on the construction plans for the wastewater collection system.

Manholes and Cleanouts

14. Manholes or clean-outs exist at the end of each sewer line(s). These locations are listed below: (Please attach additional sheet if necessary)

Line	Shown on Sheet	Station	Manhole or Clean- out?
СВС	151 Of 235	10+74.51	MH
СВС	151 Of 235	11+20.80	MH
CBC	151 Of 235	11+62.98	CO
CBC	151 Of 235	12+15.63	CO
AC09 GREASE WASTE	151 Of 235	11+22.26	MH
AC09 GREASE WASTE	148 Of 235	11+99.27	MH
AC09 GREASE WASTE	148 Of 235	16.21+88	MH

Table 2 - Manholes and Cleanouts

Line	Shown on Sheet	Station	Manhole or Clean- out?
CBC-GT 11	148 Of 235	11+84.50	MH
	Of		
Prev approved at end	Of		

- 15. Manholes are installed at all Points of Curvature and Points of Termination of a sewer line.
- 16. The maximum spacing between manholes on this project for each pipe diameter is no greater than:

Pipe Diameter (inches)	Max. Manhole Spacing (feet)
6 - 15	500
16 - 30	800
36 - 48	1000
≥54	2000

- Attachment C Justification for Variance from Maximum Manhole Spacing. The maximum spacing between manholes on this project (for each pipe diameter used) is greater than listed in the table above. A justification for any variance from the maximum spacing is attached, and must include a letter from the entity which will operate and maintain the system stating that it has the capability to maintain lines with manhole spacing greater than the allowed spacing.
- 17. 🛛 All manholes will be monolithic, cast-in-place concrete.

The use of pre-cast manholes is requested for this project. The manufacturer's specifications and construction drawings, showing the method of sealing the joints, are attached.

Site Plan Requirements

Items 18 - 25 must be included on the Site Plan.

18. \square The Site Plan must have a minimum scale of 1" = 400'.

Site Plan Scale: 1" = <u>30</u>'.

- 19. The Site Plan must include the sewage collection system general layout, including manholes with station numbers, and sewer pipe stub outs (if any). Site plan must be overlain by topographic contour lines, using a contour interval of not greater than ten feet and showing the area within both the five-year floodplain and the 100-year floodplain of any drainage way.
- 20. Lateral stub-outs:
 - \boxtimes The location of all lateral stub-outs are shown and labeled.
 -] No lateral stub-outs will be installed during the construction of this sewer collection system.

- 21. Location of existing and proposed water lines:
 - The entire water distribution system for this project is shown and labeled.
 - If not shown on the Site Plan, a Utility Plan is provided showing the entire water and sewer systems.
 - There will be no water lines associated with this project.

22. 100-year floodplain:

- After construction is complete, no part of this project will be in or cross a 100-year floodplain, either naturally occurring or manmade. (Do not include streets or concrete-lined channels constructed above of sewer lines.)
- After construction is complete, all sections located within the 100-year floodplain will have water-tight manholes. These locations are listed in the table below and are shown and labeled on the Site Plan. (Do not include streets or concrete-lined channels constructed above sewer lines.)

Table 3 - 100-Year Floodplain

Line	Sheet	Station
	of	to

23. 5-year floodplain:

- After construction is complete, no part of this project will be in or cross a 5-year floodplain, either naturally occurring or man-made. (Do not include streets or concrete-lined channels constructed above sewer lines.)
- After construction is complete, all sections located within the 5-year floodplain will be encased in concrete or capped with concrete. These locations are listed in the table below and are shown and labeled on the Site Plan. (Do not include streets or concrete-lined channels constructed above sewer lines.)

|--|

Line	Sheet	Station
	of	to

- 24. \square Legal boundaries of the site are shown.
- 25. The *final plans and technical specifications* are submitted for the TCEQ's review. Each sheet of the construction plans and specifications are dated, signed, and sealed by the Texas Licensed Professional Engineer responsible for the design on each sheet.

Items 26 - 33 must be included on the Plan and Profile sheets.

26. All existing or proposed water line crossings and any parallel water lines within 9 feet of sewer lines are listed in the table below. These lines must have the type of pressure rated pipe to be installed shown on the plan and profile sheets. Any request for a variance from the required pressure rated piping at crossings must include a variance approval from 30 TAC Chapter 290.

There will be no water line crossings.

There will be no water lines within 9 feet of proposed sewer lines.

Table 5 - Water Line Crossings

Line	Station or Closest Point	Crossing or Parallel	Horizontal Separation Distance	Vertical Separation Distance
Prev approved at end				

27. Vented Manholes:

No part of this sewer line is within the 100-year floodplain and vented manholes are not required by 30 TAC Chapter 217.

A portion of this sewer line is within the 100-year floodplain and vented manholes will be provided at less than 1500 foot intervals. These water-tight manholes are listed in the table below and labeled on the appropriate profile sheets.

A portion of this sewer line is within the 100-year floodplain and an alternative means of venting shall be provided at less than 1500 feet intervals. A description of the alternative means is described on the following page.

A portion of this sewer line is within the 100-year floodplain; however, there is no interval longer than 1500 feet located within. No vented manholes will be used.

Table 6 - Vented Manholes

Line	Manhole	Station	Sheet

Line	Manhole	Station	Sheet
Prev approved at end			

28. Drop manholes:

There are no drop manholes associated with this project.

Sewer lines which enter new or existing manholes or "manhole structures" higher than 24 inches above the manhole invert are listed in the table below and labeled on the appropriate profile sheets. These lines meet the requirements of 30 TAC §217.55(I)(2)(H).

Table 7 - Drop Manholes

Line	Manhole	Station	Sheet
WW-A	EXISTING MH CB-C	31+31.82	151

29. Sewer line stub-outs (For proposed extensions):

The placement and markings of all sewer line stub-outs are shown and labeled.

No sewer line stub-outs are to be installed during the construction of this sewage collection system.

30. Lateral stub-outs (For proposed private service connections):

The placement and markings of all lateral stub-outs are shown and labeled.

No lateral stub-outs are to be installed during the construction of this sewage collection system.

31. Minimum flow velocity (From Appendix A)

Assuming pipes are flowing full; all slopes are designed to produce flows equal to or greater than 2.0 feet per second for this system/line.

32. Maximum flow velocity/slopes (From Appendix A)

Assuming pipes are flowing full, all slopes are designed to produce maximum flows of less than or equal to 10 feet per second for this system/line.

Attachment D – Calculations for Slopes for Flows Greater Than 10.0 Feet per Second. Assuming pipes are flowing full, some slopes produce flows which are greater than 10 feet per second. These locations are listed in the table below. Calculations are attached.

Line	Profile Sheet	Station to Station	FPS	% Slope	Erosion/Shock Protection

Table 8 - Flows Greater Than 10 Feet per Second

33. Assuming pipes are flowing full, where flows are ≥ 10 feet per second, the provisions noted below have been made to protect against pipe displacement by erosion and/or shock under 30 TAC §217.53(I)(2)(B).

Concrete encasement shown on appropriate Plan and Profile sheets for the locations listed in the table above.

Steel-reinforced, anchored concrete baffles/retards placed every 50 feet shown on appropriate Plan and Profile sheets for the locations listed in the table above.
 N/A

Administrative Information

- 34. The final plans and technical specifications are submitted for TCEQ review. Each sheet of the construction plans and specifications are dated, signed, and sealed by the Texas Licensed Professional Engineer responsible for the design on each sheet.
- 35. Standard details are shown on the detail sheets, which are dated, signed, and sealed by the Texas Licensed Professional Engineer, as listed in the table below:

Standard Details	Shown on Sheet
Lateral stub-out marking [Required]	164 of 235
Manhole, showing inverts comply with 30 TAC §217.55(I)(2) [Required]	163 of 235
Alternate method of joining lateral to existing SCS line for potential future connections [Required]	164 of 235
Typical trench cross-sections [Required]	163 of 235
Bolted manholes [Required]	163 of 235
Sewer Service lateral standard details [Required]	164 of 235
Clean-out at end of line [Required, if used]	161 of 235
Baffles or concrete encasement for shock/erosion protection [Required, if flow velocity of any section of pipe >10 fps]	161 of 235
Detail showing Wastewater Line/Water Line Crossing [Required, if crossings are proposed]	164 of 235
Mandrel detail or specifications showing compliance with 30 TAC §217.57(b) and (c) [Required, if Flexible Pipe is used]	164 of 235

Table 9 - Standard Details

Standard Details	Shown on Sheet
Drop manholes [Required, if a pipe entering a manhole is more than 24 inches above manhole invert]	164 of 235

- 36. All organized sewage collection system general construction notes (TCEQ-0596) are included on the construction plans for this sewage collection system.
- 37. All proposed sewer lines will be sufficiently surveyed/staked to allow an assessment prior to TCEQ executive director approval. If the alignments of the proposed sewer lines are not walkable on that date, the application will be deemed incomplete and returned.

Survey staking was completed on this date: _____

- 38. Submit one (1) original and one (1) copy of the application, plus additional copies as needed for each affected incorporated city, groundwater conservation district, and county in which the project will be located. The TCEQ will distribute the additional copies to these jurisdictions. The copies must be submitted to the appropriate regional office.
- 39. Any modification of this SCS application will require TCEQ approval, prior to construction, and may require submission of a revised application, with appropriate fees.

Signature

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This **Organized Sewage Collection System Application** is hereby submitted for TCEQ review and executive director approval. The system was designed in accordance with the requirements of 30 TAC §213.5(c) and 30 TAC §217 and prepared by:

Print Name of Licensed Professional Engineer: John Pelham, P.E.



Appendix A-Flow Velocity Table

Flow Velocity (Flowing Full) All gravity sewer lines on the Edwards Aquifer Recharge Zone shall be designed and constructed with hydraulic slopes sufficient to give a velocity when flowing full of not less than 2.0 feet per second, and not greater than 10 feet per second. The grades shown in the following table are based on Manning's formula and an n factor of 0.013 and shall be the minimum and maximum acceptable slopes unless provisions are made otherwise.

Pipe Diameter(Inches)	% Slope required for minimum flow velocity of 2.0 fps	% Slope which produces flow velocity of 10.0 fps
6	0.50	12.35
8	0.33	8.40
10	0.25	6.23
12	0.20	4.88
15	0.15	3.62
18	0.11	2.83
21	0.09	2.30
24	0.08	1.93
27	0.06	1.65
30	0.055	1.43
33	0.05	1.26
36	0.045	1.12
39	0.04	1.01
>39	*	*

Table 10 - Slope Velocity

*For lines larger than 39 inches in diameter, the slope may be determined by Manning's formula (as shown below) to maintain a minimum velocity greater than 2.0 feet per second when flowing full and a maximum velocity less than 10 feet per second when flowing full.

$$v = \frac{1.49}{n} \times R_h^{0.67} \times \sqrt{S}$$

Figure 1 - Manning's Formula

Where:

v = velocity (ft/sec)
n = Manning's roughness coefficient
(0.013)
Rh = hydraulic radius (ft)
S = slope (ft/ft)

Table 1				
Pipe				
Diameter		Pipe		
(Inches)	Linear Feet (1)	Material (2)	Specification (3)	
6	1219	PVC SDR 26	ASTM D3034	
8	1504	PVC SDR 26	ASTM D3034	
10	722	PVC SDR 26	ASTM D3034	
12	876	PVC SDR 26	ASTM D3034	
15	1259	PVC SDR 26	ASTM D3034	
6	160	PVC SDR 26	ASTM D2241	
8	40	PVC SDR 26	ASTM D2241	
10	20	PVC SDR 26	ASTM D2241	
12	20	PVC SDR 26	ASTM D2241	

(Previously Approved) (Previously Approved)

Table 2			
Line	Shown on Sheet	Station	Manhole or Cleanout
А	152 Of 239	10+00.00	MH EXISTING
А	152 Of 239	10+30.31	MH
А	152 Of 239	10+73.51	MH
А	152 Of 239	14+76.81	MH
А	152 Of 239	17+02.73	MH
А	153 Of 239	21+72.11	MH
А	153 Of 239	22+59.45	MH
А	153 Of 239	23+52.88	MH
А	153 Of 239	24+84.15	MH
А	153 Of 239	27+33.06	MH
Α	153 Of 239	29+29.98	MH
А	153 Of 239	31+31.82	MH
А	154 Of 239	33+27.31	MH
А	154 Of 239	34+98.24	MH
А	154 Of 239	35+28.36	MH
А	154 Of 239	36+87.72	MH
А	154 Of 239	39+12.13	MH
А	154 Of 239	39+96.08	MH
А	154 Of 239	41+86.85	MH
А	155 Of 239	44+28.06	MH
А	155 Of 239	46+77.65	MH
А	155 Of 239	47+24.14	CO
В	155 Of 239	10+00.00	MH
В	155 Of 239	10+59.27	MH
В	155 Of 239	11+12.12	MH
В	155 Of 239	13+55.50	MH
В	156 Of 239	14+92.44	MH
В	156 Of 239	16+26.70	MH
В	156 Of 239	17+81.02	MH
В	156 Of 239	18+43.88	MH
В	156 Of 239	19+82.50	MH
В	156 Of 239	20+92.03	MH
B6	154 Of 239	11+44.77	MH
B6	154 Of 239	12+80.85	MH
PG2-G2	147 Of 235	10+00.00	CO
PG2-G2	147 Of 235	10+01.82	СО

(Previously Approved) (Previously Approved)

PG2-G2	147 Of 235	10+08.79	CO
RD2-1	147 Of 235	10+09.30	CO

	Table 5					
	Station or Closest	Crossing or	Horizontal Separation	Vertical Separation		
Line	Point	Parallel	Distance	Distance(FT)		
А	22+45.53	Crossing		23.1'		
А	23+04.11	Crossing		21.4		
А	29+68.78	Crossing		3.8'		
А	39+25.63	Crossing		3.4'		
А	41+61.49	Crossing		2.4'		
А	47+16.45	Crossing		2.6'		
В	10+44.85	Crossing		5.1'		
В	15+66.23	Crossing		4.1'		
В	18+06.27	Crossing		5.8'		
В	20+09.55	Crossing		7.8'		

(Previously Approved) (Previously Approved)

		Table 7		
	Sheet	Station	Manhole	Line
(Previously Approved)	153 of 239	22+59.45		А
(Previously Approved)	153 of 239	23+52.88		А
(Previously Approved)	153 of 239	31+31.82		А
(Previously Approved)	154 of 239	33+27.31		А
(Previously Approved)	155 of 239	10+00.00		В
(Previously Approved)	155 of 239	11+12.12		В
(Previously Approved)	155 of 239	13+55.50		В
(Previously Approved)	156 of 239	16+26.70		В
(Previously Approved)	156 of 239	18+43.88		В
(Previously Approved)	156 of 239	20+92.03		В

ATTACHMENT A – SCS ENGINEERING DESIGN REPORT

A SCS engineering design report is included with this application



Engineering Design Report

For

Generational Properties

Organized Sewage Collection System

December 2023

Prepared By: Garza EMC 7708 Rialto Blvd, Suite 125 Austin, Texas 78735 TBPE Registration Number F14629

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PVC PIPE STANDARDS

The American Society for Testing and Materials (ASTM) also known as ASTM International (Reference: www.astm.org) governs the manufacturing specifications for Polyvinyl Chloride (PVC) pipes, including the dimension ratio and water pressure allowable for use of each pipe, through its D-3034 standard. ASTM D-3034 lists its pipe dimensions and pipe classes using the "SDR" mark up, such as SDR-13.5, SDR-21, SDR-26 and SDR-41. The SDR refers to the standard dimension ratio (SDR) of the outside pipe diameter and the wall thickness. This project specifies the use of SDR-26 PVC pipe, which are to meet the ASTM pressure rating of 160 psi and fall in the size category listed below. ASTM D-3034 standards must be meticulously adhered to by all PVC pipe manufacturers and is recognized as the standard during PVC pressure pipe testing and quality checks. Other in-depth information can be found published in <u>Thermoplastic Pressure Pipe Design and Selection</u> UNI-TR-7, by the Uni-Bell PVC Pipe Association.

SDR 26 Pipe Size Matrix (Per ASTM D-3034)			
Size (in)	O.D. (in)	Avg I.D. (in)	Thickness (in)
4	4.125	3.891	0.162
6	6.275	5.793	0.241
8	8.4	7.754	0.323
10	10.5	9.692	0.404
12	12.5	11.538	0.481
15	15.3	14.124	0.588

PROPOSED TYPE OF PIPE (6")

(6")

Type I, Grade I, Polyvinyl Chloride (PVC) Specifications: Size of Pipe: <u>6.00</u> in.

SDR 26 Properties	
Pipe Compliance:	ASTM D-3034
Joint Compliance:	ASTM D-3139
Cell Classification:	12454
Minimum Tensile Strength (psi):	7,000
Minimum Modulus of Elasticity (psi):	400,000
Average Inner Diameter (inch):	6.084
Average Outer Diameter inch):	6.625
Wall Thickness (inch):	0.255
Approximate Trenching Width (feet):	2.00
Minimum Pipe Depth (Cover) used (feet):	2.41
Maximum Pipe Depth (Cover) used (feet):	13.85

FLOW/CAPACITY ANALYSIS

For the Proposed Project:

Proposed Waste Water Usage:	<u>296,640</u> GPD

 Q_{max} (As determined in Attachment A) = 0.199 CFS

$$Q_{full} = \frac{1.486}{n} \times A \times R^{\frac{2}{3}} \times \sqrt{S}$$

For the Specified Pipe at the Minimum Design Slope, the full flow is

$$Q_{full} = 0.582$$
 CFS

0.199 < 0.582 Design meets TCEQ Guidelines

PROPOSED TYPE OF PIPE (8")

(8")

Type I, Grade I, Polyvinyl Chloride (PVC) Specifications: Size of Pipe: 8.00 in.

SDR 26 Properties

Pipe Compliance:	ASTM D-3034
Joint Compliance:	ASTM D-3139
Cell Classification:	12454
Minimum Tensile Strength (psi):	7,000
Minimum Modulus of Elasticity (psi):	400,000
Average Inner Diameter (inch):	7.921
Average Outer Diameter inch):	8.625
Wall Thickness (inch):	0.332
Approximate Trenching Width (feet):	2.25
Minimum Pipe Depth (Cover) used (feet):	2.76
Maximum Pipe Depth (Cover) used (feet):	4.74

FLOW/CAPACITY ANALYSIS

For the Proposed Project:

Proposed Waste Water Usage:	<u>296,640</u> GPD
-----------------------------	--------------------

 Q_{max} (As determined in Attachment A) = 0.673 CFS

$$Q_{full} = \frac{1.486}{n} \times A \times R^{\frac{2}{3}} \times \sqrt{S}$$

For the Specified Pipe at the Minimum Design Slope, the full flow is

$$Q_{full} = 1.177$$
 CFS

0.673 < 1.177 Design meets TCEQ Guidelines

PROPOSED TYPE OF PIPE (10") (10")

Type I, Grade I, Polyvinyl Chloride (PVC) Specifications: Size of Pipe: 10.00 in.

SDR 26 Properties	
Pipe Compliance:	ASTM D-3034
Joint Compliance:	ASTM D-3139
Cell Classification:	12454
Minimum Tensile Strength (psi):	7,000
Minimum Modulus of Elasticity (psi):	400,000
Average Inner Diameter (inch):	9.874
Average Outer Diameter inch):	10.75
Wall Thickness (inch):	0.413
Approximate Trenching Width (feet):	2.40
Minimum Pipe Depth (Cover) used (feet):	7.95
Maximum Pipe Depth (Cover) used (feet):	14.27

FLOW/CAPACITY ANALYSIS

For the Proposed Project:

Proposed Waste Water Usage:	<u>296,640</u> GPD
-----------------------------	--------------------

 Q_{max} (As determined in Attachment A) = 1.057 CFS

$$Q_{full} = \frac{1.486}{n} \times A \times R^{\frac{2}{3}} \times \sqrt{S}$$

For the Specified Pipe at the Minimum Design Slope, the full flow is

$$Q_{full} = 1.498$$
 CFS

1.057 < 1.498 Design meets TCEQ Guidelines

PROPOSED TYPE OF PIPE (12")

(12")

Type I, Grade I, Polyvinyl Chloride (PVC) Specifications: Size of Pipe: 12.00 in.

SDR 26 Properties	
Pipe Compliance:	ASTM D-3034
Joint Compliance:	ASTM D-3139
Cell Classification:	12454
Minimum Tensile Strength (psi):	7,000
Minimum Modulus of Elasticity (psi):	400,000
Average Inner Diameter (inch):	11.711
Average Outer Diameter inch):	12.75
Wall Thickness (inch):	0.49
Approximate Trenching Width (feet):	2.60
Minimum Pipe Depth (Cover) used (feet):	8.07
Maximum Pipe Depth (Cover) used (feet):	26.78

FLOW/CAPACITY ANALYSIS

For the Proposed Project:

Proposed Waste Water Usage:	<u>296,640</u> GPD
-----------------------------	--------------------

 Q_{max} (As determined in Attachment A) = 1.770 CFS

$$Q_{full} = \frac{1.486}{n} \times A \times R^{\frac{2}{3}} \times \sqrt{S}$$

For the Specified Pipe at the Minimum Design Slope, the full flow is

$$Q_{full} = 2.361$$
 CFS

1.770 < 2.361 Design meets TCEQ Guidelines

PROPOSED TYPE OF PIPE (15")

(15")

Type I, Grade I, Polyvinyl Chloride (PVC) Specifications: Size of Pipe: 15.00 in.

SDR 26 Properties	
Pipe Compliance:	ASTM D-3034
Joint Compliance:	ASTM D-3139
Cell Classification:	12454
Minimum Tensile Strength (psi):	7,000
Minimum Modulus of Elasticity (psi):	400,000
Average Inner Diameter (inch):	14.124
Average Outer Diameter inch):	15.3
Wall Thickness (inch):	0.588
Approximate Trenching Width (feet):	2.80
Minimum Pipe Depth (Cover) used (feet):	7.44
Maximum Pipe Depth (Cover) used (feet):	24.90

FLOW/CAPACITY ANALYSIS

For the Proposed Project:

Proposed Waste Water Usage:	<u>296,640</u> GPD
-----------------------------	--------------------

 Q_{max} (As determined in Attachment A) = 2.660 CFS

$$Q_{full} = \frac{1.486}{n} \times A \times R^{\frac{2}{3}} \times \sqrt{S}$$

For the Specified Pipe at the Minimum Design Slope, the full flow is

$$Q_{full} = 3.891$$
 CFS

2.660 < 3.891 Design meets TCEQ Guidelines

MINIMUM AND MAXIMUM GRADES FOR PIPES (30 TAC §217.53(l)(2)(A)) (6")

Minimum and Maximum Pipe Slopes		
Size of Pipe	Minimum Slope (%)	Maximum Slope (%)
6	0.5	12.35
8	0.33	8.4
10	0.25	6.23
12	0.2	4.88
15	0.15	3.62
18	0.11	2.83
21	0.09	2.3
24	0.08	1.93
27	0.06	1.65
30	0.055	1.43
33	0.05	1.26
36	0.045	1.12
39	0.04	1.01
>39	*	*
* For pipes larger than 39 inches in diameter, the slope is determined by Manning's formula to maintain a velocity greater than 2.0 feet per second and less than 10.0 feet per second when flowing full.		

MINIMUM AND MAXIMUM VELOCITY FOR THE PROPOSED SYSTEM: (6")

<u>1.00</u>

	So, using 6.00 inch PVC	Pipe:	
$V = \frac{1.49}{8} \times R_{\cdot}^{0.67} \times \sqrt{S}$	V = velocity (ft/sec)	=	(solve)
	n = Manning's coefficient	=	0.013
n	$R_h = hydraulic radius$	=	0.127
	S = slope (ft/ft)		

$V_{min} =$		<u>2.89</u> ft/sec	$V_{max} =$		<u>5.01</u> ft/sec
2.89	>	2.00 ft/sec	5.01	<	10.00 ft/sec

Design meets TCEQ Guidelines

Minimum Slope Used (%):

Design meets TCEQ Guidelines

Maximum Slope Used (%):

<u>3.00</u>

MINIMUM AND MAXIMUM GRADES FOR PIPES (30 TAC §217.53(l)(2)(A)) (8")

Minimum and Maximum Pipe Slopes					
Size of Pipe	Minimum Slope (%)	Maximum Slope (%)			
6	0.5	12.35			
8	0.33	8.4			
10	0.25	6.23			
12	0.2	4.88			
15	0.15	3.62			
18	0.11	2.83			
21	0.09	2.3			
24	0.08	1.93			
27	0.06	1.65			
30	0.055	1.43			
33	0.05	1.26			
36	0.045	1.12			
39	0.04	1.01			
>39	*	*			
* For pipes larger than 39 inches in diameter, the slope is determined by Manning's formula to maintain a velocity greater than 2.0 feet per second and less than 10.0 feet per second when flowing full.					

MINIMUM AND MAXIMUM VELOCITY FOR THE PROPOSED SYSTEM: (8")

<u>1.00</u>

	So, using 8.00 inch PVC	Pipe:	
$V = \frac{1.49}{8} \times R_{\cdot}^{0.67} \times \sqrt{S}$	V = velocity (ft/sec)	=	(solve)
	n = Manning's coefficient	=	0.013
n	$R_h = hydraulic radius$	=	0.165
	S = slope (ft/ft)		

$V_{min} =$		<u>3.45</u> ft/sec	$V_{max} =$		<u>7.90</u> ft/sec
3.45	>	2.00 ft/sec	7.90	<	10.00 ft/sec

Design meets TCEQ Guidelines

Minimum Slope Used (%):

Design meets TCEQ Guidelines

Maximum Slope Used (%):

<u>5.26</u>

MINIMUM AND MAXIMUM GRADES FOR PIPES (30 TAC §217.53(l)(2)(A)) (10")

Minimum and Maximum Pipe Slopes					
Size of Pipe	Minimum Slope (%)	Maximum Slope (%)			
6	0.5	12.35			
8	0.33	8.4			
10	0.25	6.23			
12	0.2	4.88			
15	0.15	3.62			
18	0.11	2.83			
21	0.09	2.3			
24	0.08	1.93			
27	0.06	1.65			
30	0.055	1.43			
33	0.05	1.26			
36	0.045	1.12			
39	0.04	1.01			
>39	*	*			
* For pipes larger than 39 inches in diameter, the slope is determined by Manning's formula to maintain a velocity greater than 2.0 feet per second and less than 10.0 feet per second when flowing full.					

MINIMUM AND MAXIMUM VELOCITY FOR THE PROPOSED SYSTEM: (10")

		So, using 10.00 inch PVC	Pipe:	
1.10		V = velocity (ft/sec)	=	(solve)
$V = \frac{1.49}{1.49} \times R_{10.67} \times \sqrt{R_{10.67}}$	\overline{S}	n = Manning's coefficient	=	0.013
n	-	$R_h = hydraulic radius$	=	0.206
		S = slope (ft/ft)		
Minimum Slope Used (%):	<u>0.50</u>	Maximum Slope Us	ed (%):	<u>1.00</u>

$V_{min} =$		<u>2.82</u> ft/sec	$V_{max} =$		<u>3.99</u> ft/sec
2.82	>	2.00 ft/sec	3.99	<	10.00 ft/sec

Design meets TCEQ Guidelines

Design meets TCEQ Guidelines

MINIMUM AND MAXIMUM GRADES FOR PIPES (30 TAC §217.53(l)(2)(A)) (12")

Minimum and Maximum Pipe Slopes					
Size of Pipe	Minimum Slope (%)	Maximum Slope (%)			
6	0.5	12.35			
8	0.33	8.4			
10	0.25	6.23			
12	0.2	4.88			
15	0.15	3.62			
18	0.11	2.83			
21	0.09	2.3			
24	0.08	1.93			
27	0.06	1.65			
30	0.055	1.43			
33	0.05	1.26			
36	0.045	1.12			
39	0.04	1.01			
>39	*	*			
* For pipes larger than 39 inches in diameter, the slope is determined by Manning's formula to maintain a velocity greater than 2.0 feet per second and less than 10.0 feet per second when flowing full.					

MINIMUM AND MAXIMUM VELOCITY FOR THE PROPOSED SYSTEM: (12")

Minimum Slope Used (%):	<u>0.50</u>	Maximum Slope Us	ed (%):	<u>0.50</u>
		S = slope (ft/ft)		
n		$R_h = hydraulic radius$	=	0.244
$V = \frac{1.49}{2} \times R_{L}^{0.67} \times \sqrt{S}$	\overline{S}	n = Manning's coefficient	=	0.013
1 40		V = velocity (ft/sec)	=	(solve)
		So, using 12.00 inch PVC	Pipe:	

$V_{min} =$		<u>3.16</u> ft/sec	$V_{max} =$		<u>3.16</u> ft/sec
3.16	>	2.00 ft/sec	3.16	<	10.00 ft/sec

Design meets TCEQ Guidelines

Design meets TCEQ Guidelines

MINIMUM AND MAXIMUM GRADES FOR PIPES (30 TAC §217.53(l)(2)(A)) (15")

Minimum and Maximum Pipe Slopes					
Size of Pipe	Minimum Slope (%)	Maximum Slope (%)			
6	0.5	12.35			
8	0.33	8.4			
10	0.25	6.23			
12	0.2	4.88			
15	0.15	3.62			
18	0.11	2.83			
21	0.09	2.3			
24	0.08	1.93			
27	0.06	1.65			
30	0.055	1.43			
33	0.05	1.26			
36	0.045	1.12			
39	0.04	1.01			
>39	*	*			
* For pipes larger than 39 inches in diameter, the slope is determined by Manning's formula to maintain a velocity greater than 2.0 feet per second and less than 10.0 feet per second when flowing full.					

MINIMUM AND MAXIMUM VELOCITY FOR THE PROPOSED SYSTEM: (15")

$V = \frac{1.49}{n} \times R_h^{0.67} \times \sqrt{S}$		So, using 15.00 inch PVC V = velocity (ft/sec) n = Manning's coefficient $R_h =$ hydraulic radius	? Pipe: = = =	(solve) 0.013 0.294	
Minimum Slope Used (%):	<u>0.50</u>	S = slope (ft/ft) Maximum Slope Us	sed (%):	<u>1.00</u>	

$V_{min} =$		<u>3.58</u> ft/sec	$V_{max} =$		<u>5.07</u> ft/sec
3.58	>	2.00 ft/sec	5.07	<	10.00 ft/sec

Design meets TCEQ Guidelines

Design meets TCEQ Guidelines

AVERAGE VALUES OF MODULUS OF SOIL REACTION, E'

	E for Degree of Compaction of Bedding, in pounds per square inch				
Soil type-pipe bedding material (Unified Classification System)	Dumped	Slight <85% Proctor, <40% relative density	Moderate 85%-95% Proctor, 40%-70% relative density	High, >95% Proctor, >70% relative density	
(1)	(2)	(3)	(4)	(5)	
Fine-grained Soils (LL>50₅) Soils with medium to high plasticity CH, MH, CH-MH	No data available; consult a competent soils engineer; Otherwise use E'=0				
Fine-grained Soils (LL<50) Soils with medium to no plasticity, CL, ML, ML-CL,with less than 25% coarse-grained particles	50	200	400	1000	
Fine-grained Soils (LL<50) Soils with medium to no plasticity, CL, ML, ML-CL,with more than 25% coarse-grained particles Coarse-grained Soils with Fines GM, GC, SM, SC ^c contains more than 12% fines	100	400	1000	2000	
Coarse-grained Soils with Little or no Fines GW, GP, SW, SP ^e contains less than 12% fines	200	1000	2000	3000	
Crushed Rock	1000	3000	3000	3000	
Accuracy in Terms of Percentage Deflection	± 2	± 2	± 1	± 0.5	

Taken from: Howard, Amster K. "Soil Reaction for Buried Flexible Pipe" U.S. Bureau of Reclamation, Denver, CO and the American Society of Civil Engineers.

Modulus of Soil Reaction for the in-situ soil is determined to be = 2000 psi

PIPE BEDDING CLASS

Taken from the American Society for Testing and Material (ASTM) D 2321 and American Association of State Highway and Transportation Officials (AASHTO) M43, and as published on Table 7, in <u>Deflection: The Pipe/Soil Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association, Pg 24.

Pipe Embedment Material				E', psi (kPa) for Degree of Embedment Compaction							
A Class	STM D 2321* Description	/ Notation	ASTM D 2487 Description	AASHTO M43 Notation	Min. Std. Proctor Density (%)	Lift Placement Depth	Dumped	Slightly < 85%	Moderate 85% - 95%	High > 95%	
IA	Open-graded, clean manu- factured aggregates	N/A	Angular crushed stone or rock, crushed gravel, crushed slag; large voids with little or no fines	5 56	5 Dumped 56	Dumped	18" (0.45 m)	1000 (6,900)	3000 (20,700)	3000 (20,700)	3000 (20,700)
IB	Dense-graded, clean manu- factured, processed aggregates	N/A	Angular crushed stone or other Class IA material and stone/sand mixtures; little or no fines								
11	Clean, coarse- grained soils	GW	Well-graded gravel, gravel/sand mixtures; little or no fines	57 6 67	85%	12* (0.30 m)	N/R	1000 (6,900)	2000 (13,800)	3000 (20,700)	
		GP	Poorly graded gravel, gravel/sand mixtures; little or no fines								
		SW	Well-graded sands, gravelly sands; little or no fines								
		SP	Poorly graded sands, gravelly sands; little or no fines								
Ш	Coarse-grained soils with fines	GM	Silty gravels, gravel/sand/silt mixtures	Gravel and sand with <10% fines	Gravel and 90% sand with <10% fines	9* (0.20 m)	N/R	N/R	1000 (6,900)	2000 (13,800)	
		GC	Clayey gravels, gravel/sand/clay mixtures								
		SM	Silty sands, sand/ silt mixtures								
		SC	Clayey sands, sand/clay mixtures	1							

NOTE:

Per TCEQ guidelines, a contractor is allowed to use ASTM D 2321 Bedding Class 1A, 1B, II, or III at no less than 85% percent compaction. To grant the contractor its ability to make the proper judgment of which bedding class to use, the calculations provided in this Engineering Design Report reflect the use of **Bedding Class III, at 85%-95%** compaction, with an E' value of 1000 psi. This provides the "worst case" scenario for the SCS line. All other Bedding Class options will provide an improved value for the zeta factor as well as pipe deflection.

```
For Bedding Class III, 85%-95% Compaction, E_b = 1000 psi
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PIPE BEDDING ANGLE

As Published on Figure 8 and Table 5, in <u>Deflection: The Pipe/Soil Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association, Pgs 18-19.



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Bedding Angle, degrees	Bedding Constant
0	0.110
30	0.108
45	0.105
60	0.102
90	0.096
120	0.090
180	0.083

Bedding Constant Values

LIVE LOAD DETERMINATION

Source: AASHTO H20 and E80 Loads and as Published on Table 4, in <u>Deflection: The</u> <u>Pipe/Soil Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association, Pg 14.

Height	Live Load Transferred to Pipe, lb/in ²			Height	Live Load T	ransferred to	Pipe, lb/in ²
Cover (ft)	Highway H20 ¹	Railway E80 ²	Airport	Cover (ft)	Highway H20 ¹	Railway E80 ²	Airport
1	12.50			14	*	4.17	3.06
2	5.56	26.39	13.14	16	*	3.47	2.29
3	4.17	23.61	12.28	18	*	2.78	1.91
4	2.78	18.40	11.27	20	*	2.08	1.53
5	1.74	16.67	10.09	22	*	1.91	1.14
6	1.39	15.63	8.79	24	*	1.74	1.05
7	1.22	12.15	7.85	26	*	1.39	*
8	0.69	11.11	6.93	28	*	1.04	*
10	*	7.64	6.09	30	*	0.69	*
12	*	5.56	4.76	35	*	*	*
				40	*	*	*

¹ Simulates 20 ton truck + impact

² Simulates 80,000 lb/ft railway load + impact

³ 180,000 lbs. dual tandem gear assembly. 26 inch spacing between tires and 66 inch

center-to-center spacing between fore and aft tires under a rigid pavement 12 inches thick + impact.

* Negligible live load influence

PRISM LOAD DETERMINATION

Also referred to as the 'dead' load, the prism load is the pressure acting on the pipe by the weight of the soil column above a given section of the pipe. The following prism load columns are industry standards as referenced from Table 3, <u>Deflection: The Pipe/Soil</u> <u>Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association, Pg 13.

Height of Cover (ft) Soil Unit Weight (lb/ft*) 1 0.69 0.76 0.83 0.87 0.90 2 1.39 1.53 1.67 1.74 1.81 3 2.08 2.29 2.50 2.60 2.71 4 2.78 3.06 3.33 3.47 3.61 5 3.47 3.82 4.17 4.34 4.51 6 4.17 4.58 5.00 5.21 5.42 7 4.86 5.35 5.83 6.08 6.33 8 5.56 6.11 6.67 6.94 7.22 9 6.25 6.88 7.50 7.81 8.13 10 6.94 7.64 8.33 8.68 9.03 11 7.64 8.40 9.17 9.55 9.93
Height of Cover (ft) 100 110 120 125 130 1 0.69 0.76 0.83 0.87 0.90 2 1.39 1.53 1.67 1.74 1.81 3 2.08 2.29 2.50 2.60 2.71 4 2.78 3.06 3.33 3.47 3.61 5 3.47 3.82 4.17 4.34 4.51 6 4.17 4.58 5.00 5.21 5.42 7 4.86 5.35 5.83 6.08 6.32 8 5.56 6.11 6.67 6.94 7.22 9 6.25 6.88 7.50 7.81 8.13 10 6.94 7.64 8.33 8.68 9.03 11 7.64 8.40 9.17 9.55 9.93
$\begin{array}{cccccccccccccccccccccccccccccccccccc$
12 8.33 9.17 10.00 10.42 10.83 13 9.03 9.93 10.83 11.28 11.74 14 9.72 10.69 11.67 12.15 12.64 15 10.42 11.46 12.50 13.02 13.44 17 11.81 12.99 14.17 14.76 15.35 18 12.50 13.75 15.00 15.63 16.25 19 13.19 14.51 15.83 16.49 17.15 20 13.89 15.28 16.67 17.36 18.06 21 14.58 16.04 17.50 18.23 18.06 22 15.28 16.81 18.33 19.10 19.83 21.67 23 15.97 17.57 19.17 19.97 22.57 26 18.06 19.86 21.67 22.57 23.47 27

Note that the Prism Loads are calculated based upon the Marston Theory of Loads, developed by Professor Anson Marston, circa 1913, and is calculated using the formula:

$$P = \frac{\gamma_s * H}{144}$$

This formula determines the earth load on a flexible pipe and is regarded as a conservative approach to determining the dead load placed upon a buried flexible pipe.

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Where:

q_a	=	Allowable buckling pressure (psi)			
h	=	Height of soil surface above top of pipe (in)			
Н	=	Depth of burial, feet, from ground	surface to	top of pipe	
Β'	=	Empirical coefficient of elastic sup	port		
E _b	=	Modulus of soil reaction for the be	dding mate	erial (psi)	
E	=	Modulus of elasticity of the pipe m	aterial (ps	i)	
Ι	=	Moment of inertia of the pipe, per	linear inch	of pipe (in ³)
t	=	Pipe wall thickness (in)			
D	=	Mean pipe diameter, inner (in)	D =	6.084	

Solving for the Empirical coefficient of elastic support, given by Luscher in 1966, as referenced on Pg 113 of Moser, A.P., <u>Buried Pipe Design</u>. 2nd Ed., McGraw-Hill:

$$B' = \frac{4(h^2 + Dh)}{1.5(2h + D)^2}$$

$$B' = \frac{1104.34}{1712.04} = 0.645$$

Using the Allowable Buckling Pressure Equation as shown in Moser, A.P., <u>Buried Pipe</u> <u>Design</u>. 2nd Ed., McGraw-Hill, Pg 112, and an initial factor of safety (SF) of 2.5, the Allowable Buckling Pressure is then:

$$q_{a} = \frac{1}{FS} * \sqrt{32 * R_{w}} * B' * E_{b} * \left(E * \frac{I}{D^{3}}\right)$$
$$q_{a} = \frac{1}{2.5} \sqrt{\left[32\right] \left[1\right] \left[0.645\right] \left[1000\right] \left[400000 \frac{0.001}{225.20}\right]}$$

90.03

psi

 $q_a =$

(8'')

Where:

\mathbf{q}_{a}	=	Allowable buckling pressure (psi)
h	=	Height of soil surface above top of pipe (in)
Н	=	Depth of burial, feet, from ground surface to top of pipe
Β'	=	Empirical coefficient of elastic support
E _b	=	Modulus of soil reaction for the bedding material (psi)
Е	=	Modulus of elasticity of the pipe material (psi)
Ι	=	Moment of inertia of the pipe, per linear inch of pipe (in ³)
t	=	Pipe wall thickness (in)
D	=	Mean pipe diameter, inner (in) $D = 7.921$

Solving for the Empirical coefficient of elastic support, given by Luscher in 1966, as referenced on Pg 113 of Moser, A.P., <u>Buried Pipe Design</u>. 2nd Ed., McGraw-Hill:

$$B' = \frac{4(h^2 + Dh)}{1.5(2h + D)^2}$$

$$B' = \frac{240.053}{454.192} = 0.529$$

Using the Allowable Buckling Pressure Equation as shown in Moser, A.P., <u>Buried Pipe</u> <u>Design</u>. 2nd Ed., McGraw-Hill, Pg 112, and an initial factor of safety (SF) of 2.5, the Allowable Buckling Pressure is then:

$$q_{a} = \frac{1}{FS} * \sqrt{32 * R_{w} * B' * E_{b} * \left(E * \frac{I}{D^{3}}\right)}$$

$$q_{a} = \frac{1}{2.5} \sqrt{\left[32\right] \left[1\right] \left[0.529\right] \left[1000\right] \left[400000 \frac{0.003}{496.98}\right]}$$

$$q_{a} = 81.50 \text{ psi}$$

(10'')
Where:

q_a	=	Allowable buckling pressure (psi)				
h	=	Height of soil surface above top of pipe (in)				
Н	=	Depth of burial, feet, from ground	Depth of burial, feet, from ground surface to top of pipe			
Β'	=	Empirical coefficient of elastic support				
E _b	=	Modulus of soil reaction for the bedding material (psi)				
E	=	Modulus of elasticity of the pipe m	naterial (p	si)		
Ι	=	Moment of inertia of the pipe, per	linear incl	h of pipe (in	3)	
t	=	Pipe wall thickness (in)				
D	=	Mean pipe diameter, inner (in)	D =	9.874		

Solving for the Empirical coefficient of elastic support, given by Luscher in 1966, as referenced on Pg 113 of Moser, A.P., Buried Pipe Design. 2nd Ed., McGraw-Hill:

$$B' = \frac{4(h^2 + Dh)}{1.5(2h + D)^2}$$

$$B' = \frac{1378.14}{2213.45} = 0.623$$

Using the Allowable Buckling Pressure Equation as shown in Moser, A.P., Buried Pipe Design. 2nd Ed., McGraw-Hill, Pg 112, and an initial factor of safety (SF) of 2.5, the Allowable Buckling Pressure is then:

$$q_{a} = \frac{1}{FS} * \sqrt{32 * R_{w} * B' * E_{b} * \left(E * \frac{I}{D^{3}}\right)}$$

$$q_{a} = \frac{1}{2.5} \sqrt{\left[32\right] \left[1\right] \left[0.623\right] \left[0\right] \left[400000 \frac{0.006}{962.67}\right]}$$

$$q_{a} = 88.18 \text{ psi}$$

psi

(12'')
Where:

\mathbf{q}_{a}	=	Allowable buckling pressure (psi)			
h	=	Height of soil surface above top of pipe (in)			
Н	=	Depth of burial, feet, from ground surface to top of pipe			
B'	=	Empirical coefficient of elastic support			
E _b	=	Modulus of soil reaction for the bedding material (psi)			
Е	=	Modulus of elasticity of the pipe material (psi)			
Ι	=	Moment of inertia of the pipe, per linear inch of pipe (in ³)			
t	=	Pipe wall thickness (in)			
D	=	Mean pipe diameter, inner (in) $D = 11.711$			

Solving for the Empirical coefficient of elastic support, given by Luscher in 1966, as referenced on Pg 113 of Moser, A.P., Buried Pipe Design. 2nd Ed., McGraw-Hill:

$$B' = \frac{4(h^2 + Dh)}{1.5(2h + D)^2}$$

$$B' = \frac{4123.16}{6390.46} = 0.645$$

Using the Allowable Buckling Pressure Equation as shown in Moser, A.P., Buried Pipe Design. 2nd Ed., McGraw-Hill, Pg 112, and an initial factor of safety (SF) of 2.5, the Allowable Buckling Pressure is then:

$$q_{a} = \frac{1}{FS} * \sqrt{32 * R_{w} * B' * E_{b} * \left(E * \frac{I}{D^{3}}\right)}$$

$$q_{a} = \frac{1}{2.5} \sqrt{\left[32\right] \left[1\right] \left[0.645\right] \left[0\right] \left[400000 \frac{0.010}{1606.13}\right]}$$

$$q_{a} = 89.81 \text{ psi}$$

psi

(15'')
Where:

\mathbf{q}_{a}	=	Allowable buckling pressure (psi)			
h	=	Height of soil surface above top of pipe (in)			
Н	=	Depth of burial, feet, from ground surface to top of pipe			
Β'	=	Empirical coefficient of elastic support			
E _b	=	Modulus of soil reaction for the bedding material (psi)			
E	=	Modulus of elasticity of the pipe material (psi)			
Ι	=	Moment of inertia of the pipe, per linear inch of pipe (in ³			
t	=	Pipe wall thickness (in)			
D	=	Mean pipe diameter, inner (in) $D = 14.124$			

Solving for the Empirical coefficient of elastic support, given by Luscher in 1966, as referenced on Pg 113 of Moser, A.P., <u>Buried Pipe Design</u>. 2nd Ed., McGraw-Hill:

$$B' = \frac{4(h^2 + Dh)}{1.5(2h + D)^2}$$

$$B' = \frac{3886.79}{6129.42} = 0.634$$

Using the Allowable Buckling Pressure Equation as shown in Moser, A.P., <u>Buried Pipe</u> <u>Design</u>. 2nd Ed., McGraw-Hill, Pg 112, and an initial factor of safety (SF) of 2.5, the Allowable Buckling Pressure is then:

$$q_{a} = \frac{1}{FS} * \sqrt{32 * R_{w} * B' * E_{b} * \left(E * \frac{I}{D^{3}}\right)}$$

$$q_{a} = \frac{1}{2.5} \sqrt{\left[32\right] \left[1\right] \left[0.634\right] \left[0\right] \left[400000 \frac{0.017}{2817.56}\right]}$$

$$q_{a} = 88.37 \text{ psi}$$

(6'')

Where:	q_P	=	Pressure applied to pipe under installed conditions (psi)
	$\gamma_{\rm W}$	=	Specific Weight of Water = 0.0361 (pci)
	$\gamma_{\rm S}$	=	Specific Weight of Soil (pcf)
	W _c	=	Vertical Soil Load on the pipe per unit length (lb/in)
	L_L	=	Live load as determined from chart

Standard industry vertical soil load (W_c) calculation (lb/in) developed from empirical data:

$$W_c = \gamma_s * H * \left(\frac{D+t}{144}\right)$$

Where: $\gamma_{\rm S} = 130$ D = 6.084 t = 0.255 $W_C = \begin{bmatrix} 130 \end{bmatrix} \begin{bmatrix} 13.85 \end{bmatrix} \begin{bmatrix} 6.084 + 0.255 \\ 144 \end{bmatrix}$ $W_C = 79.26$ lb/in

Using the Equation on Pg 114 of Moser, A.P., <u>Buried Pipe Design</u>. 2nd Ed., McGraw-Hill, Pressure Applied to Pipe under installed conditions at its deepest installed depth (Note, hw = 0, therefore Rw = 1) is calculated to be:

$$q_{p} = \gamma_{w}h_{w} + R_{w}\left(\frac{W_{c} + L_{L}}{D}\right)$$

$$q_{P} = 62.4 \times 0 + 1 \times \left(\frac{79.26}{6.084}\right)$$

$$q_{P} = 26.06 \text{ psi}$$

(8'')

Where:	$q_{\rm P}$	=	Pressure applied to pipe under installed conditions (psi)
	$\gamma_{ m W}$	=	Specific Weight of Water = 0.0361 (pci)
	$\gamma_{\rm S}$	=	Specific Weight of Soil (pcf)
	W _c	=	Vertical Soil Load on the pipe per unit length (lb/in)
	L_L	=	Live load as determined from chart

Standard industry vertical soil load (W_c) calculation (lb/in) developed from empirical data:

$$W_c = \gamma_s * H * \left(\frac{D+t}{144}\right)$$

Where: $\gamma_{\rm S} = 130$ D = 7.921 t = 0.332 $W_C = \begin{bmatrix} 130 \end{bmatrix} \begin{bmatrix} 4.74 \end{bmatrix} \begin{bmatrix} 7.921 + 0.332 \\ 144 \end{bmatrix}$ $W_C = 35.32$ lb/in

Using the Equation on Pg 114 of Moser, A.P., <u>Buried Pipe Design</u>. 2nd Ed., McGraw-Hill, Pressure Applied to Pipe under installed conditions at its deepest installed depth (Note, hw = 0, therefore Rw = 1) is calculated to be:

$$q_{p} = \gamma_{w}h_{w} + R_{w}\left(\frac{W_{c} + L_{L}}{D}\right)$$

$$q_{P} = 62.4 \times 0 + 1 \times \left(\frac{35.32}{7.921}\right)$$

$$q_{P} = 8.92 \text{ psi}$$

(10")

Where:	q_P	=	Pressure applied to pipe under installed conditions (psi)
	$\gamma_{\rm W}$	=	Specific Weight of Water = 0.0361 (pci)
	$\gamma_{\rm S}$	=	Specific Weight of Soil (pcf)
	W _c	=	Vertical Soil Load on the pipe per unit length (lb/in)
	L_L	=	Live load as determined from chart

Standard industry vertical soil load (W_c) calculation (lb/in) developed from empirical data:

$$W_c = \gamma_s * H * \left(\frac{D+t}{144}\right)$$

Where: $\gamma_{\rm S} = 130$ D = 9.874 t = 0.413 $W_C = \begin{bmatrix} 130 \end{bmatrix} \begin{bmatrix} 14.27 \end{bmatrix} \begin{bmatrix} 9.874 + 0.413 \\ 144 \end{bmatrix}$ $W_C = 132.52$ lb/in

Using the Equation on Pg 114 of Moser, A.P., <u>Buried Pipe Design</u>. 2nd Ed., McGraw-Hill, Pressure Applied to Pipe under installed conditions at its deepest installed depth (Note, hw = 0, therefore Rw = 1) is calculated to be:

$$q_{p} = \gamma_{w}h_{w} + R_{w}\left(\frac{W_{c} + L_{L}}{D}\right)$$

$$q_{P} = 62.4 \times 0 + 1 \times \left(\frac{132.52}{9.874}\right)$$

$$q_{P} = 26.84 \text{ psi}$$

(12")

Where:	$q_{\rm P}$	=	Pressure applied to pipe under installed conditions (psi)
	$\gamma_{\rm W}$	=	Specific Weight of Water = 0.0361 (pci)
	$\gamma_{\rm S}$	=	Specific Weight of Soil (pcf)
	W_{c}	=	Vertical Soil Load on the pipe per unit length (lb/in)
	L_L	=	Live load as determined from chart

Standard industry vertical soil load (W_c) calculation (lb/in) developed from empirical data:

$$W_c = \gamma_s * H * \left(\frac{D+t}{144}\right)$$

Where: $\gamma_{\rm S} = 130$ D = 11.711 t = 0.49 $W_C = \begin{bmatrix} 130 \end{bmatrix} \begin{bmatrix} 26.78 \end{bmatrix} \begin{bmatrix} 11.711 + 0.49 \\ 144 \end{bmatrix}$ $W_C = 294.98$ lb/in

Using the Equation on Pg 114 of Moser, A.P., <u>Buried Pipe Design</u>. 2nd Ed., McGraw-Hill, Pressure Applied to Pipe under installed conditions at its deepest installed depth (Note, hw = 0, therefore Rw = 1) is calculated to be:

$$q_{p} = \gamma_{w}h_{w} + R_{w}\left(\frac{W_{c} + L_{L}}{D}\right)$$

$$q_{P} = 62.4 \times 0 + 1 \times \left(\frac{294.98}{11.711}\right)$$

$$q_{P} = 50.38 \text{ psi}$$

(15")

Where:	$q_{\rm P}$	=	Pressure applied to pipe under installed conditions (psi)
	$\gamma_{\rm W}$	=	Specific Weight of Water = 0.0361 (pci)
	$\gamma_{\rm S}$	=	Specific Weight of Soil (pcf)
	W_{c}	=	Vertical Soil Load on the pipe per unit length (lb/in)
	L_L	=	Live load as determined from chart

Standard industry vertical soil load (W_c) calculation (lb/in) developed from empirical data:

$$W_c = \gamma_s * H * \left(\frac{D+t}{144}\right)$$

Where: $\gamma_{\rm S} = 130$ D = 14.124 t = 0.588 $W_C = \begin{bmatrix} 130 \end{bmatrix} \begin{bmatrix} 24.90 \end{bmatrix} \begin{bmatrix} 14.124 + 0.588 \\ 144 \end{bmatrix}$ $W_C = 330.71$ lb/in

Using the Equation on Pg 114 of Moser, A.P., <u>Buried Pipe Design</u>. 2nd Ed., McGraw-Hill, Pressure Applied to Pipe under installed conditions at its deepest installed depth (Note, hw = 0, therefore Rw = 1) is calculated to be:

$$q_{p} = \gamma_{w}h_{w} + R_{w}\left(\frac{W_{c} + L_{L}}{D}\right)$$

$$q_{P} = 62.4 \times 0 + 1 \times \left(\frac{330.71}{14.124}\right)$$

$$q_{P} = 46.83 \text{ psi}$$

WALL CRUSHING CALCULATION

(6	••)
· -		/

Where:	D _o	=	outside pipe diameter, in. $=$ 6.625 in
	P _c	=	Compressive stress or hydrostatic design basis (HDB). For
			typical PVC pipe assume 4,000 psi. For any other pipe
			material the HDB must be supplied by the pipe manufacturer.
	А	=	surface area of the pipe wall, in. ² /ft = $0.255 \text{ in.}^2/\text{ft}$
	γs	=	specific weight of soil, pcf, = 130 pcf
	Н	=	Depth of burial (ft) from ground surface to crown of pipe

Using the Wall Crushing and Wall Thrust equations, as referenced in <u>Plastic Pipe Design</u> <u>Manual</u> published by Vylon Pipe, Pg 14 the Wall Crushing due to compressive stress can be found using the following:

$$P_c = \frac{T}{A}$$
 where T, Thrust, is calculated as $T = \frac{P_y D}{2}$

Substituting the Thrust equation into the Wall Crushing equation:

$$P_c = \frac{\frac{P_y D}{2}}{A} = \frac{P_y D}{2A}$$

From the Marston Equation determining the Prism Load Calculation (See previous section on Prism Load), substitute the equation for P_v :

$$P_{c} = \frac{\frac{\gamma_{s} * H}{144}D}{2A}$$
 Rearranging this equation, it becomes: $2AP_{c} = \frac{\gamma_{s} * H}{144}D$
And simplifies to: $288AP_{c} = \gamma_{s}HD$

Note that the Surface Area of the Pipe Wall, A, is per unit length in inches² per foot, a conversion factor (from feet to inches) of 12 must be applied, therefore,

$$24AP_c = \gamma_s HD$$

Solving for H, the equation becomes:

$$H = \frac{24 * P_c * A}{\gamma_s * D_o}$$

(*Continued on next page*)

Using this equation, and converting all units, solve for "height" of the soil column, or in other words, the depth of burial of the PVC pipe:

$$H = \frac{24 4000 0.255 \times 12}{130 \times 6.625} = 341.09$$

Note: The resulting Wall Crushing will occur at a greater depth than the deepest burial depth of the proposed SCS lines, therefore pipe design is acceptable.

WALL CRUSHING CALCULATION

(8'')

Where:	D _o	=	outside pipe diameter, in. $=$ 8.625 in
	P _c	=	Compressive stress or hydrostatic design basis (HDB). For
			typical PVC pipe assume 4,000 psi. For any other pipe
			material the HDB must be supplied by the pipe manufacturer.
	А	=	surface area of the pipe wall, in. ² /ft = 0.332 in. ² /ft
	γ_{S}	=	specific weight of soil, pcf, = 130 pcf
	Н	=	Depth of burial (ft) from ground surface to crown of pipe

Using the Wall Crushing and Wall Thrust equations, as referenced in <u>Plastic Pipe Design</u> <u>Manual</u> published by Vylon Pipe, Pg 14 the Wall Crushing due to compressive stress can be found using the following:

$$P_c = \frac{T}{A}$$
 where T, Thrust, is calculated as $T = \frac{P_y D}{2}$

Substituting the Thrust equation into the Wall Crushing equation:

$$P_c = \frac{\frac{P_y D}{2}}{A} = \frac{P_y D}{2A}$$

From the Marston Equation determining the Prism Load Calculation (See previous section on Prism Load), substitute the equation for P_v :

$$P_{c} = \frac{\frac{\gamma_{s} * H}{144}D}{2A}$$
 Rearranging this equation, it becomes: $2AP_{c} = \frac{\gamma_{s} * H}{144}D$
And simplifies to: $288AP_{c} = \gamma_{s}HD$

Note that the Surface Area of the Pipe Wall, A, is per unit length in inches² per foot, a conversion factor (from feet to inches) of 12 must be applied, therefore,

$$24AP_c = \gamma_s HD$$

Solving for H, the equation becomes:

$$H = \frac{24 * P_c * A}{\gamma_s * D_o}$$

(Continued on next page)

Using this equation, and converting all units, solve for "height" of the soil column, or in other words, the depth of burial of the PVC pipe:

$$H = \frac{[24] [4000] [0.332 \times 12]}{130 \times 8.625} = 341.11$$

$$H = 341.11$$
 feet

Note: The resulting Wall Crushing will occur at a greater depth than the deepest burial depth of the proposed SCS lines, therefore pipe design is acceptable.

WALL CRUSHING CALCULATION

(1	0'	')
<u>(</u> -		

Where:	D _o	=	outside pipe diameter, in. $=$ 10.75 in
	P _c	=	Compressive stress or hydrostatic design basis (HDB). For
			typical PVC pipe assume 4,000 psi. For any other pipe
			material the HDB must be supplied by the pipe manufacturer.
	А	=	surface area of the pipe wall, in. ² /ft = $0.413 \text{ in.}^2/\text{ft}$
	$\gamma_{\rm S}$	=	specific weight of soil, pcf , = 130 pcf
	Н	=	Depth of burial (ft) from ground surface to crown of pipe

Using the Wall Crushing and Wall Thrust equations, as referenced in <u>Plastic Pipe Design</u> <u>Manual</u> published by Vylon Pipe, Pg 14 the Wall Crushing due to compressive stress can be found using the following:

$$P_c = \frac{T}{A}$$
 where T, Thrust, is calculated as $T = \frac{P_y D}{2}$

Substituting the Thrust equation into the Wall Crushing equation:

$$P_c = \frac{\frac{P_y D}{2}}{A} = \frac{P_y D}{2A}$$

From the Marston Equation determining the Prism Load Calculation (See previous section on Prism Load), substitute the equation for P_v :

$$P_{c} = \frac{\frac{\gamma_{s} * H}{144}D}{2A}$$
 Rearranging this equation, it becomes: $2AP_{c} = \frac{\gamma_{s} * H}{144}D$
And simplifies to: $288AP_{c} = \gamma_{s}HD$

Note that the Surface Area of the Pipe Wall, A, is per unit length in inches² per foot, a conversion factor (from feet to inches) of 12 must be applied, therefore,

$$24AP_c = \gamma_s HD$$

Solving for H, the equation becomes:

$$H = \frac{24 * P_c * A}{\gamma_s * D_o}$$

(Continued on next page)

Using this equation, and converting all units, solve for "height" of the soil column, or in other words, the depth of burial of the PVC pipe:

$$H = \frac{[24] [4000] [0.413 \times 12]}{130 \times 10.75} = 340.45$$

Note: The resulting Wall Crushing will occur at a greater depth than the deepest burial depth of the proposed SCS lines, therefore pipe design is acceptable.

WALL CRUSHING CALCULATION

(1	2'	•)
· ·			/

Where:	D _o	=	outside pipe diameter, in. $=$ 12.75 in
	P _c	=	Compressive stress or hydrostatic design basis (HDB). For
			typical PVC pipe assume 4,000 psi. For any other pipe material the HDB must be supplied by the pipe manufacturer.
	А	=	surface area of the pipe wall, in. ² /ft = $0.49 \text{ in.}^{2}/\text{ft}$
	γ_{S}	=	specific weight of soil, pcf, = 130 pcf
	Н	=	Depth of burial (ft) from ground surface to crown of pipe

Using the Wall Crushing and Wall Thrust equations, as referenced in <u>Plastic Pipe Design</u> <u>Manual</u> published by Vylon Pipe, Pg 14 the Wall Crushing due to compressive stress can be found using the following:

$$P_c = \frac{T}{A}$$
 where T, Thrust, is calculated as $T = \frac{P_y D}{2}$

Substituting the Thrust equation into the Wall Crushing equation:

$$P_c = \frac{\frac{P_y D}{2}}{A} = \frac{P_y D}{2A}$$

From the Marston Equation determining the Prism Load Calculation (See previous section on Prism Load), substitute the equation for P_v :

$$P_{c} = \frac{\frac{\gamma_{s} * H}{144}D}{2A}$$
 Rearranging this equation, it becomes: $2AP_{c} = \frac{\gamma_{s} * H}{144}D$
And simplifies to: $288AP_{c} = \gamma_{s}HD$

Note that the Surface Area of the Pipe Wall, A, is per unit length in inches² per foot, a conversion factor (from feet to inches) of 12 must be applied, therefore,

$$24AP_c = \gamma_s HD$$

Solving for H, the equation becomes:

$$H = \frac{24 * P_c * A}{\gamma_s * D_o}$$

(Continued on next page)

Using this equation, and converting all units, solve for "height" of the soil column, or in other words, the depth of burial of the PVC pipe:

$$H = \frac{[24] [4000] [0.49 \times 12]}{130 \times 12.75} = 340.56$$

Note: The resulting Wall Crushing will occur at a greater depth than the deepest burial depth of the proposed SCS lines, therefore pipe design is acceptable.

WALL CRUSHING CALCULATION

(1	5'	•)
· ·			/

Where:	D _o	=	outside pipe diameter, in. $=$ 15.3 in
	P _c	=	Compressive stress or hydrostatic design basis (HDB). For
			typical PVC pipe assume 4,000 psi. For any other pipe
			material the HDB must be supplied by the pipe manufacturer.
	А	=	surface area of the pipe wall, in. ² /ft = $0.588 \text{ in.}^2/\text{ft}$
	$\gamma_{\rm S}$	=	specific weight of soil, pcf , = 130 pcf
	Н	=	Depth of burial (ft) from ground surface to crown of pipe

Using the Wall Crushing and Wall Thrust equations, as referenced in <u>Plastic Pipe Design</u> <u>Manual</u> published by Vylon Pipe, Pg 14 the Wall Crushing due to compressive stress can be found using the following:

$$P_c = \frac{T}{A}$$
 where T, Thrust, is calculated as $T = \frac{P_y D}{2}$

Substituting the Thrust equation into the Wall Crushing equation:

$$P_c = \frac{\frac{P_y D}{2}}{A} = \frac{P_y D}{2A}$$

From the Marston Equation determining the Prism Load Calculation (See previous section on Prism Load), substitute the equation for P_v :

$$P_{c} = \frac{\frac{\gamma_{s} * H}{144}D}{2A}$$
 Rearranging this equation, it becomes: $2AP_{c} = \frac{\gamma_{s} * H}{144}D$
And simplifies to: $288AP_{c} = \gamma_{s}HD$

Note that the Surface Area of the Pipe Wall, A, is per unit length in inches² per foot, a conversion factor (from feet to inches) of 12 must be applied, therefore,

$$24AP_c = \gamma_s HD$$

Solving for H, the equation becomes:

$$H = \frac{24 * P_c * A}{\gamma_s * D_o}$$

(Continued on next page)

Using this equation, and converting all units, solve for "height" of the soil column, or in other words, the depth of burial of the PVC pipe:

$$H = \frac{[24] [4000] [0.588 \times 12]}{130 \times 15.3} = 340.56$$

Note: The resulting Wall Crushing will occur at a greater depth than the deepest burial depth of the proposed SCS lines, therefore pipe design is acceptable.

(6'')

The Leonhardt's Zeta Factor Equation can be calculated using Equation 9 of Buczala and Cassady in <u>Buried Plastic Pipe Technology</u>, Pgs 196-197

Where:	D	=	Pipe Outer Diameter, in =	6.625
	В	=	Trench Width, in, =	24
	E _b	=	Modulus of soil reaction for	the bedding material (psi)
	E _{'n}	=	Modulus of soil reaction for	the in-situ soil (psi)

$$zeta = \frac{1.662 + 0.639 \left(\frac{B}{D-1}\right)}{\frac{B}{D-1} + \left[1.662 + 0.361 \left(\frac{B}{D}\right) - 1\right] \left[\frac{E_b}{E'_n}\right]}$$

The Leonhardt Zeta factor is then determined as:

$$zeta = \frac{1.662 + 0.639 \times \left(\frac{24}{5.625}\right)}{\frac{24}{5.625} \left[1.662 + 0.361 \times \left(\frac{24}{6.625}\right) - 1\right] \left(\frac{1000}{2000}\right)}$$

(8'')

The Leonhardt's Zeta Factor Equation can be calculated using Equation 9 of Buczala and Cassady in <u>Buried Plastic Pipe Technology</u>, Pgs 196-197

Where:	D	=	Pipe Outer Diameter, in =	8.625
	В	=	Trench Width, in, =	27
	E _b	=	Modulus of soil reaction for the	e bedding material (psi)
	E_{n}	=	Modulus of soil reaction for the	e in-situ soil (psi)

$$zeta = \frac{1.662 + 0.639 \left(\frac{B}{D-1}\right)}{\frac{B}{D-1} + \left[1.662 + 0.361 \left(\frac{B}{D}\right) - 1\right] \left[\frac{E_b}{E'_n}\right]}$$

The Leonhardt Zeta factor is then determined as:

$$zeta = \frac{1.662 + 0.639 \times \left[\frac{27}{7.625}\right]}{\frac{27}{7.625} \left[1.662 + 0.361 \times \left[\frac{27}{8.625}\right] - 1\right] \left[\frac{1000}{2000}\right]}$$

(10'')

The Leonhardt's Zeta Factor Equation can be calculated using Equation 9 of Buczala and Cassady in <u>Buried Plastic Pipe Technology</u>, Pgs 196-197

Where:	D	=	Pipe Outer Diameter, in $=$ 10.75
	В	=	Trench Width, in, = 28.8
	E _b	=	Modulus of soil reaction for the bedding material (psi)
	E_{n}	=	Modulus of soil reaction for the in-situ soil (psi)

$$zeta = \frac{1.662 + 0.639 \left(\frac{B}{D-1}\right)}{\frac{B}{D-1} + \left[1.662 + 0.361 \left(\frac{B}{D}\right) - 1\right] \left[\frac{E_b}{E'_n}\right]}$$

The Leonhardt Zeta factor is then determined as:

$$zeta = \frac{1.662 + 0.639 \times \left[\frac{28.8}{9.75}\right]}{\frac{28.8}{9.75} \left[1.662 + 0.361 \times \left[\frac{28.8}{10.75}\right] - 1\right] \left[\frac{1000}{2000}\right]}$$

Leonhardt's zeta factor = 0.942

(12'')

The Leonhardt's Zeta Factor Equation can be calculated using Equation 9 of Buczala and Cassady in <u>Buried Plastic Pipe Technology</u>, Pgs 196-197

Where:	D	=	Pipe Outer Diameter, in	=	12.75
	В	=	Trench Width, in, =		31.2
	E_b	=	Modulus of soil reaction f	for th	e bedding material (psi)
	E_{n}	=	Modulus of soil reaction f	for th	e in-situ soil (psi)

$$zeta = \frac{1.662 + 0.639 \left(\frac{B}{D-1}\right)}{\frac{B}{D-1} + \left[1.662 + 0.361 \left(\frac{B}{D}\right) - 1\right] \left[\frac{E_b}{E'_n}\right]}$$

The Leonhardt Zeta factor is then determined as:

$$zeta = \frac{1.662 + 0.639 \times \left[\frac{31.2}{11.75}\right]}{\frac{31.2}{11.75} \left[1.662 + 0.361 \times \left[\frac{31.2}{12.75}\right] - 1\right] \left[\frac{1000}{2000}\right]}$$

$$Leonhardt's zeta factor = 0.980$$

(15'')

The Leonhardt's Zeta Factor Equation can be calculated using Equation 9 of Buczala and Cassady in <u>Buried Plastic Pipe Technology</u>, Pgs 196-197

D	=	Pipe Outer Diameter, in $=$ 15.3
В	=	Trench Width, in, = 33.6
E _b	=	Modulus of soil reaction for the bedding material (psi)
E_{n}	=	Modulus of soil reaction for the in-situ soil (psi)
	D B E _b E'n	$\begin{array}{llllllllllllllllllllllllllllllllllll$

$$zeta = \frac{1.662 + 0.639 \left(\frac{B}{D-1}\right)}{\frac{B}{D-1} + \left[1.662 + 0.361 \left(\frac{B}{D}\right) - 1\right] \left[\frac{E_b}{E'_n}\right]}$$

The Leonhardt Zeta factor is then determined as:

$$zeta = \frac{1.662 + 0.639 \times \boxed{\begin{array}{c} 33.6 \\ 14.3 \end{array}}}{33.6 \left[1.662 + 0.361 \times \boxed{\begin{array}{c} 33.6 \\ 15.3 \end{array}} \right] - 1 \left[\begin{array}{c} 1000 \\ 2000 \end{array} \right]}$$

Leonhardt's zeta factor = 1.028

(6'')

Using Equation B.1, as directed in 30 TAC §217.53(k)(3), to Calculate the Pipe Stiffness:

$$PS = C \times RSC \times (\frac{8.337}{D})$$

Where: PS		=	Pipe Stiffness in pounds per square	re inch (psi)
	С	=	Conversion factor = 0.8	
	RSC	=	Ring Stiffness Constant	
	D	=	Mean Pipe Diameter, Inner =	6.084 in

The RSC can be supplied by the manufacturer or otherwise calculated using Equation 4 of Resistance to Ring Bending – Pipe Stiffness (PS), Ring Stiffness Constant (RSC) and Flexibility Factor (FF) for Buried Gravity Flow Pipes TN-19/2005, Pg 6 published by the Plastics Pipe Institute:

$$RSC = 6.44 \times \frac{EI}{D^2}$$

$$I = \left(\frac{t^3}{12}\right) * \left(\frac{inches^3}{in_{linear}}\right) = 0.001$$

$$RSC = 6.44 \times \frac{552.713}{37.015} = 96.1627$$

$$PS = 0.8 \times 96.163 \times \frac{8.337}{6.084}$$

(8'')

Using Equation B.1, as directed in 30 TAC §217.53(k)(3), to Calculate the Pipe Stiffness:

$$PS = C \times RSC \times (\frac{8.337}{D})$$

Where: PS		=	Pipe Stiffness in pounds per squa	re inch (psi)
	С	=	Conversion factor = 0.8	
	RSC	=	Ring Stiffness Constant	
	D	=	Mean Pipe Diameter, Inner =	7.921 in

The RSC can be supplied by the manufacturer or otherwise calculated using Equation 4 of Resistance to Ring Bending – Pipe Stiffness (PS), Ring Stiffness Constant (RSC) and Flexibility Factor (FF) for Buried Gravity Flow Pipes TN-19/2005, Pg 6 published by the Plastics Pipe Institute:

$$RSC = 6.44 \times \frac{EI}{D^2}$$

$$I = \left(\frac{t^3}{12}\right) * \left(\frac{inches^3}{in_{linear}}\right) = 0.003$$

$$RSC = 6.44 \times \frac{1219.812}{62.742} = 125.204$$

$$PS = 0.8 \times 125.204 \times \frac{8.337}{7.921}$$

$$PS = 105.42 \text{ psi}$$

(10'')

Using Equation B.1, as directed in 30 TAC §217.53(k)(3), to Calculate the Pipe Stiffness:

$$PS = C \times RSC \times (\frac{8.337}{D})$$

Where: PS		=	Pipe Stiffness in pounds per squa	re inch (psi)
	С	=	Conversion factor = 0.8	
	RSC	=	Ring Stiffness Constant	
	D	=	Mean Pipe Diameter, Inner =	9.874 in

The RSC can be supplied by the manufacturer or otherwise calculated using Equation 4 of <u>Resistance to Ring Bending – Pipe Stiffness (PS), Ring Stiffness Constant (RSC) and</u> <u>Flexibility Factor (FF) for Buried Gravity Flow Pipes TN-19/2005, Pg 6 published by the</u> <u>Plastics Pipe Institute:</u>

$$RSC = 6.44 \times \frac{EI}{D^2}$$

$$I = \left(\frac{t^3}{12}\right) * \left(\frac{inches^3}{in_{linear}}\right) = 0.006$$

$$RSC = 6.44 \times \frac{2348.167}{97.496} = 155.106$$

$$PS = 0.8 \times 155.106 \times \frac{8.337}{9.874}$$

(12")

Using Equation B.1, as directed in 30 TAC §217.53(k)(3), to Calculate the Pipe Stiffness:

$$PS = C \times RSC \times (\frac{8.337}{D})$$

Where:	Vhere: PS		Pipe Stiffness in pounds per squa	are inch (psi)
	С	=	Conversion factor = 0.8	
	RSC	=	Ring Stiffness Constant	
	D	=	Mean Pipe Diameter, Inner =	11.711 in

The RSC can be supplied by the manufacturer or otherwise calculated using Equation 4 of Resistance to Ring Bending – Pipe Stiffness (PS), Ring Stiffness Constant (RSC) and Flexibility Factor (FF) for Buried Gravity Flow Pipes TN-19/2005, Pg 6 published by the Plastics Pipe Institute:

$$RSC = 6.44 \times \frac{EI}{D^2}$$

$$I = \left(\frac{t^3}{12}\right) * \left(\frac{inches^3}{in_{linear}}\right) = 0.010$$

$$RSC = 6.44 \times \frac{3921.633}{137.148} = 184.147$$

$$PS = 0.8 \times 184.147 \times \frac{8.337}{11.711}$$

$$PS = 104.87 psi$$

(15'')

Using Equation B.1, as directed in 30 TAC §217.53(k)(3), to Calculate the Pipe Stiffness:

$$PS = C \times RSC \times (\frac{8.337}{D})$$

Where: PS		=	Pipe Stiffness in pounds per squ	are inch (psi)
	С	=	Conversion factor = 0.8	
	RSC	=	Ring Stiffness Constant	
	D	=	Mean Pipe Diameter, Inner =	14.124 in

The RSC can be supplied by the manufacturer or otherwise calculated using Equation 4 of <u>Resistance to Ring Bending – Pipe Stiffness (PS), Ring Stiffness Constant (RSC) and</u> <u>Flexibility Factor (FF) for Buried Gravity Flow Pipes TN-19/2005, Pg 6 published by the</u> <u>Plastics Pipe Institute:</u>

$$RSC = 6.44 \times \frac{EI}{D^2}$$

$$I = \left(\frac{t^3}{12}\right) * \left(\frac{inches^3}{in_{linear}}\right) = 0.017$$

$$RSC = 6.44 \times \frac{6776.582}{199.487} = 218.767$$

$$PS = 0.8 \times 218.767 \times \frac{8.337}{14.124}$$

$$PS = 103.31 \text{ psi}$$

(6'')

. ,			
Where:	PS	=	Pipe Stiffness (psi) = 105.42 psi
	E _b	=	Modulus of soil reaction for the bedding material (psi)
	zeta	=	Leonhardt's Zeta factor = 0.836
	SSF	=	Soil stiffness factor $(0.061 \times zeta \times E_b)$

The Soil Stiffness Factor is calculated using Equation 10 referenced by Buczala and Cassady, <u>Buried Plastic Pipe Technology</u>, Pg 198, where:

$$SSF = 0.6 * zeta * E_b$$

$$\frac{PS}{SSF} = \frac{PS}{0.6*zeta*E_b}$$

$$\frac{PS}{SSF} = \frac{105.42}{501.38} = 0.21$$

(**8''**) Where:

:	PS	=	Pipe Stiffness (psi) = 105.42 psi
	E _b	=	Modulus of soil reaction for the bedding material (psi)
	zeta	=	Leonhardt's Zeta factor = 0.885
	SSF	=	Soil stiffness factor $(0.061 \times zeta \times E_b)$

The Soil Stiffness Factor is calculated using Equation 10 referenced by Buczala and Cassady, <u>Buried Plastic Pipe Technology</u>, Pg 198, where:

$$SSF = 0.6 * zeta * E_b$$

$$\frac{PS}{SSF} = \frac{PS}{0.6 * zeta * E_b}$$

$$\frac{PS}{SSF} = \frac{105.42}{530.72} = 0.20$$

 $\begin{array}{rcl} \textbf{(10'')} \\ \text{Where:} & PS & = & Pipe \ Stiffness \ (psi) = & 104.77 \ psi \\ E_b & = & Modulus \ of \ soil \ reaction \ for \ the \ bedding \ material \ (psi) \\ zeta & = & Leonhardt's \ Zeta \ factor = & 0.942 \\ SSF & = & Soil \ stiffness \ factor \ (0.061 \times zeta \times E_b) \end{array}$

The Soil Stiffness Factor is calculated using Equation 10 referenced by Buczala and Cassady, <u>Buried Plastic Pipe Technology</u>, Pg 198, where:

 $SSF = 0.6 * zeta * E_b$

$$\frac{PS}{SSF} = \frac{PS}{0.6 * zeta * E_b}$$

$$\frac{PS}{SSF} = \frac{104.77}{565.15} = 0.19$$

 $\begin{array}{rcl} \textbf{(12'')} \\ \text{Where:} & PS & = & Pipe \ Stiffness \ (psi) = & 104.87 \ psi \\ E_b & = & Modulus \ of \ soil \ reaction \ for \ the \ bedding \ material \ (psi) \\ zeta & = & Leonhardt's \ Zeta \ factor = & 0.980 \\ SSF & = & Soil \ stiffness \ factor \ (0.061 \times zeta \times E_b) \end{array}$

The Soil Stiffness Factor is calculated using Equation 10 referenced by Buczala and Cassady, Buried Plastic Pipe Technology, Pg 198, where:

 $SSF = 0.6 * zeta * E_b$

$$\frac{PS}{SSF} = \frac{PS}{0.6 * zeta * E_b}$$

$$\frac{PS}{SSF} = \frac{104.87}{587.88} = 0.18$$
PIPE STIFFNESS TO SOIL STIFFNESS FACTOR

 $\begin{array}{rcl} \textbf{(15'')} \\ \text{Where:} & PS & = & Pipe \ Stiffness \ (psi) = & 103.31 \ psi \\ E_b & = & Modulus \ of \ soil \ reaction \ for \ the \ bedding \ material \ (psi) \\ zeta & = & Leonhardt's \ Zeta \ factor = & 1.028 \\ SSF & = & Soil \ stiffness \ factor \ (0.061 \times zeta \times E_b) \end{array}$

The Soil Stiffness Factor is calculated using Equation 10 referenced by Buczala and Cassady, <u>Buried Plastic Pipe Technology</u>, Pg 198, where:

$$SSF = 0.6 * zeta * E_b$$

Therefore,

$$\frac{PS}{SSF} = \frac{PS}{0.6 * zeta * E_b}$$

$$\frac{PS}{SSF} = \frac{103.31}{616.84} = 0.17$$

(6'')

Using the Modified Iowa Equation, referenced and published by the Uni-Bell PVC Pipe association and found at http://www.uni-bell.org/faq.html, and Equation 14 of <u>Deflection: The Pipe/Soil Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association Pgs 17, the predicted pipe deflection can be calculated.

Where:	$\Delta Y/D$	=	Predicted % vertical deflection under load
	Р	=	Prism Load, psi
	Κ	=	Bedding angle constant, Assumed to = 0.083
	W'	=	Live Load, psi , = 0
	DR	=	Dimension Ratio= 26
	Е	=	Modulus of tensile elasticity of the pipe material, psi
	E'	=	Modulus of Soil Reaction, psi
	D_L	=	Deflection Lag Factor $= 1.5$

And using the Modified Iowa Equation:

$$(\%)\frac{\Delta Y}{D} = \frac{(D_L KP + KW') \times 100}{[2E/(3(DR-1)^3)] + 0.061E'}$$

Where, Prism Load,
$$P = \frac{\gamma_s * H}{144}$$

and/or from previous chart, prism load = 12.50 psi

The Predicted Deflection is determined as:

$$(\%)\frac{\Delta Y}{D} = \frac{\left[\left[1.5 \times 1.03779\right] + 0\right] \times 100}{\left[\frac{800000}{46875}\right] + \left[0.061 \times 1000\right]} = 1.99\%$$

NOTE: 1.99% < 5%, therefore pipe design is acceptable

(8'')

Using the Modified Iowa Equation, referenced and published by the Uni-Bell PVC Pipe association and found at http://www.uni-bell.org/faq.html, and Equation 14 of <u>Deflection: The Pipe/Soil Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association Pgs 17, the predicted pipe deflection can be calculated.

Where:	$\%\Delta Y/D$	=	Predicted % vertical deflection under load
	Р	=	Prism Load, psi
	Κ	=	Bedding angle constant, Assumed to $=$ 0.110
	W'	=	Live Load, psi , = 0
	DR	=	Dimension Ratio= 26
	Е	=	Modulus of tensile elasticity of the pipe material, psi
	E'	=	Modulus of Soil Reaction, psi
	D_L	=	Deflection Lag Factor = 1.5

And using the Modified Iowa Equation:

$$(\%)\frac{\Delta Y}{D} = \frac{(D_L KP + KW') \times 100}{[2E/(3(DR - 1)^3)] + 0.061E'}$$

Where, Prism Load,
$$P = \frac{\gamma_s * H}{144}$$

and/or from previous chart, prism load = 4.28 psi

The Predicted Deflection is determined as:

$$(\%)\frac{\Delta Y}{D} = \frac{\left[1.5 \times 0.47071\right] + 0 \times 100}{\left[\frac{800000}{46875}\right] + \left[0.061 \times 1000\right]} = 0.90\%$$

NOTE: 0.90% < 5%, therefore pipe design is acceptable

(10")

Using the Modified Iowa Equation, referenced and published by the Uni-Bell PVC Pipe association and found at http://www.uni-bell.org/faq.html, and Equation 14 of <u>Deflection:</u> <u>The Pipe/Soil Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association Pgs 17, the predicted pipe deflection can be calculated.

Where:	$\%\Delta Y/D$	=	Predicted % vertical deflection under load
	Р	=	Prism Load, psi
	Κ	=	Bedding angle constant, Assumed to $=$ 0.083
	W'	=	Live Load, psi , = 0
	DR	=	Dimension Ratio= 26
	E	=	Modulus of tensile elasticity of the pipe material, psi
	E'	=	Modulus of Soil Reaction, psi
	D_L	=	Deflection Lag Factor $= 1.5$

And using the Modified Iowa Equation:

$$(\%)\frac{\Delta Y}{D} = \frac{(D_L KP + KW') \times 100}{[2E/(3(DR-1)^3)] + 0.061E'}$$

Where, Prism Load,
$$P = \frac{\gamma_s * H}{144}$$

and/or from previous chart, prism load = 12.88 psi

The Predicted Deflection is determined as:

$$(\%)\frac{\Delta Y}{D} = \frac{\left[1.5 \times 1.06926\right] + 0 \times 100}{\left[\frac{800000}{46875}\right] + \left[0.061 \times 1000\right]} = 2.05\%$$

NOTE: 2.05% < 5%, therefore pipe design is acceptable

(12")

Using the Modified Iowa Equation, referenced and published by the Uni-Bell PVC Pipe association and found at http://www.uni-bell.org/faq.html, and Equation 14 of <u>Deflection:</u> <u>The Pipe/Soil Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association Pgs 17, the predicted pipe deflection can be calculated.

Where:	$\Delta Y/D$	=	Predicted % vertical deflection under load
	Р	=	Prism Load, psi
	Κ	=	Bedding angle constant, Assumed to $=$ 0.090
	W'	=	Live Load, psi , = 0
	DR	=	Dimension Ratio= 26
	Е	=	Modulus of tensile elasticity of the pipe material, psi
	E'	=	Modulus of Soil Reaction, psi
	D_L	=	Deflection Lag Factor $= 1.5$

And using the Modified Iowa Equation:

$$(\%)\frac{\Delta Y}{D} = \frac{(D_L KP + KW') \times 100}{[2E/(3(DR - 1)^3)] + 0.061E'}$$

Where, Prism Load,
$$P = \frac{\gamma_s * H}{144}$$

and/or from previous chart, prism load = 24.18 psi

The Predicted Deflection is determined as:

$$(\%)\frac{\Delta Y}{D} = \frac{\left[1.5 \times 2.17588\right] + 0 \times 100}{\left[\frac{800000}{46875}\right] + \left[0.061 \times 1000\right]} = 4.18\%$$

NOTE: 4.18% < 5%, therefore pipe design is acceptable

(15")

Using the Modified Iowa Equation, referenced and published by the Uni-Bell PVC Pipe association and found at http://www.uni-bell.org/faq.html, and Equation 14 of <u>Deflection: The Pipe/Soil Mechanism</u> UNI-TR-1-97, Uni-Bell PVC Pipe Association Pgs 17, the predicted pipe deflection can be calculated.

Where:	$\Delta Y/D$	=	Predicted % vertical deflection under load
	Р	=	Prism Load, psi
	Κ	=	Bedding angle constant, Assumed to $=$ 0.083
	W'	=	Live Load, psi, = 0
	DR	=	Dimension Ratio= 26
	E	=	Modulus of tensile elasticity of the pipe material, psi
	E'	=	Modulus of Soil Reaction, psi
	D_{L}	=	Deflection Lag Factor = 1.5

And using the Modified Iowa Equation:

$$(\%) \frac{\Delta Y}{D} = \frac{(D_L KP + KW') \times 100}{[2E/(3(DR - 1)^3)] + 0.061E'}$$

Where, Prism Load,
$$P = \frac{\gamma_s * H}{144}$$

and/or from previous chart, prism load = 22.48 psi

The Predicted Deflection is determined as:

$$(\%) \frac{\Delta Y}{D} = \frac{\left[1.5 \times 1.86577 \right] + 0 \right] \times 100}{\left[\frac{800000}{46875} \right] + \left[0.061 \times 2000 \right]} = 2.01\%$$

NOTE: 2.01% < 5%, therefore pipe design is acceptable

*Please see SHT 160 of construction drawings for note on pipe embedment material and bedding classes on pipe with >34.5 feet depth of bury.

(6'')

Pipe strain is also known as the elongation of the pipe over the original length of the pipe. Under normal loading conditions of the PVC pipe, the variable that affects the elongation or straining of the pipe stems from the either the flexure or deflection (i.e.. bending) of the pipe within the bedding material (i.e. increased or excessive pipe deflection causing the pipe to elongate) or hoop stress within the pipe wall. Please note that pipe strain is not generally known to be the limiting performance factor during pipe failure. For this system, pipe deflection is limited to 5% for a SDR 26 pipe. This 5% deflection value is the industry accepted value placing the pipe within its straining limits. Therefore, as the calculated deflection above is shown to be less than 5%, the pipe and bedding class used in this system is within the acceptable straining limits for this pipe.

However, total Pipe strain is calculated as the combination of the before mentioned hoop stress and the maximum strain due to deflection. Both items are calculated below using Equations 15 and 16 found in <u>Deflection: the Pipe/Soil Mechanism</u>, UNI-TR-1-97, Published by the Uni-Bell PVC Pipe Association (Pgs 28-30):

Where:	\in_{h}	=	Maximum Pipe Strain due to Hoop Stress, in/in
	Р	=	Pressure on the pipe (Live + Prism Loads), psi
	Е	=	Modulus of Elasticity of the Pipe, psi
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in

$$\in_h = \frac{PD}{2tE}$$

Using the maximum cover for both live loads and prism loads as well as the previous unit weight of the soil:

$$\in_{h} = \frac{\left[0.00 + 12.50 \right] \times 6.625}{2 \times 0.255 \times 400,000} = 4.061E-04 \frac{\text{in}}{\text{in}}$$

\in_{f}	=	Maximum Pipe Strain due to Ring Deflection, in/in
ΔY	=	Change in vertical pipe diameter under load, in, (numerator in
		the deflection equation, but in decimal form)
t	=	Pipe Wall thickness, in
D	=	Pipe Diameter, Average Outer, in
DR	=	Dimension Ratio= 26
	$\epsilon_{\rm f}$ ΔY t D DR	$\begin{array}{ll} \displaystyle \in_{\rm f} & = \\ \Delta {\rm Y} & = \\ \\ \displaystyle t & = \\ \\ \displaystyle D & = \\ \\ \displaystyle D R & = \end{array}$

$$\in_{f} = \frac{t}{D} \left[\frac{3\Delta Y / D}{1 - 2\Delta Y / D} \right] = \frac{1}{DR} \left[\frac{3\Delta Y}{D - 2\Delta Y} \right]$$

$$\in_f = 0.038 \times \frac{4.670}{6.625 - 3.113} = 0.0511 \frac{\text{in}}{\text{in}}$$

$$\in_{total}$$
 = 5.1555E-02 $\frac{\text{in}}{\text{in}}$

(8'')

Pipe strain is also known as the elongation of the pipe over the original length of the pipe. Under normal loading conditions of the PVC pipe, the variable that affects the elongation or straining of the pipe stems from the either the flexure or deflection (i.e.. bending) of the pipe within the bedding material (i.e. increased or excessive pipe deflection causing the pipe to elongate) or hoop stress within the pipe wall. Please note that pipe strain is not generally known to be the limiting performance factor during pipe failure. For this system, pipe deflection is limited to 5% for a SDR 26 pipe. This 5% deflection value is the industry accepted value placing the pipe within its straining limits. Therefore, as the calculated deflection above is shown to be less than 5%, the pipe and bedding class used in this system is within the acceptable straining limits for this pipe.

However, total Pipe strain is calculated as the combination of the before mentioned hoop stress and the maximum strain due to deflection. Both items are calculated below using Equations 15 and 16 found in <u>Deflection: the Pipe/Soil Mechanism</u>, UNI-TR-1-97, Published by the Uni-Bell PVC Pipe Association (Pgs 28-30):

Where:	\in_{h}	=	Maximum Pipe Strain due to Hoop Stress, in/in
	Р	=	Pressure on the pipe (Live + Prism Loads), psi
	E	=	Modulus of Elasticity of the Pipe, psi
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in

$$\epsilon_h = \frac{PD}{2tE}$$

Using the maximum cover for both live loads and prism loads as well as the previous unit weight of the soil:

$$\in_{h} = \frac{\left[\begin{array}{cccc} 0.00 + 4.28 \end{array}\right] \times 8.625}{2 \times 0.332 \times 400,000} = 1.390\text{E-04} \quad \frac{\text{in}}{\text{in}}$$

Where:	\in_{f}	=	Maximum Pipe Strain due to Ring Deflection, in/in
	ΔY	=	Change in vertical pipe diameter under load, in, (numerator in
			the deflection equation, but in decimal form)
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in
	DR	=	Dimension Ratio= 26

$$\in_{f} = \frac{t}{D} \left[\frac{3\Delta Y / D}{1 - 2\Delta Y / D} \right] = \frac{1}{DR} \left[\frac{3\Delta Y}{D - 2\Delta Y} \right]$$

$$\epsilon_f = 0.038 \times \frac{2.118}{8.625 - 1.412} = 0.0113 \frac{\text{in}}{\text{in}}$$

$$\in_{total}$$
 = 1.1434E-02 $\frac{\text{in}}{\text{in}}$

(10")

Pipe strain is also known as the elongation of the pipe over the original length of the pipe. Under normal loading conditions of the PVC pipe, the variable that affects the elongation or straining of the pipe stems from the either the flexure or deflection (i.e., bending) of the pipe within the bedding material (i.e. increased or excessive pipe deflection causing the pipe to elongate) or hoop stress within the pipe wall. Please note that pipe strain is not generally known to be the limiting performance factor during pipe failure. For this system, pipe deflection is limited to 5% for a SDR 26 pipe. This 5% deflection value is the industry accepted value placing the pipe within its straining limits. Therefore, as the calculated deflection above is shown to be less than 5%, the pipe and bedding class used in this system is within the acceptable straining limits for this pipe.

However, total Pipe strain is calculated as the combination of the before mentioned hoop stress and the maximum strain due to deflection. Both items are calculated below using Equations 15 and 16 found in <u>Deflection: the Pipe/Soil Mechanism</u>, UNI-TR-1-97, Published by the Uni-Bell PVC Pipe Association (Pgs 28-30):

Where:	\in_{h}	=	Maximum Pipe Strain due to Hoop Stress, in/in
	Р	=	Pressure on the pipe (Live + Prism Loads), psi
	E	=	Modulus of Elasticity of the Pipe, psi
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in

$$\in_h = \frac{PD}{2tE}$$

Using the maximum cover for both live loads and prism loads as well as the previous unit weight of the soil:

$$\in_{h} = \frac{\left[\begin{array}{ccc} 0.00 + 12.88 \end{array}\right] \times 10.75}{2 \times 0.413 \times 400,000} = 4.192 \text{E-04} \quad \frac{\text{in}}{\text{in}}$$

Where:	\in_{f}	=	Maximum Pipe Strain due to Ring Deflection, in/in
	ΔY	=	Change in vertical pipe diameter under load, in, (numerator in
			the deflection equation, but in decimal form)
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in
	DR	=	Dimension Ratio= 26

$$\in_{f} = \frac{t}{D} \left[\frac{3\Delta Y / D}{1 - 2\Delta Y / D} \right] = \frac{1}{DR} \left[\frac{3\Delta Y}{D - 2\Delta Y} \right]$$

$$\in_f = 0.038 \times \frac{4.812}{10.75 - 3.208} = 0.0245 \frac{\text{in}}{\text{in}}$$

$$\in_{total}$$
 = 2.4956E-02 $\frac{\text{in}}{\text{in}}$

(12")

Pipe strain is also known as the elongation of the pipe over the original length of the pipe. Under normal loading conditions of the PVC pipe, the variable that affects the elongation or straining of the pipe stems from the either the flexure or deflection (i.e., bending) of the pipe within the bedding material (i.e. increased or excessive pipe deflection causing the pipe to elongate) or hoop stress within the pipe wall. Please note that pipe strain is not generally known to be the limiting performance factor during pipe failure. For this system, pipe deflection is limited to 5% for a SDR 26 pipe. This 5% deflection value is the industry accepted value placing the pipe within its straining limits. Therefore, as the calculated deflection above is shown to be less than 5%, the pipe and bedding class used in this system is within the acceptable straining limits for this pipe.

However, total Pipe strain is calculated as the combination of the before mentioned hoop stress and the maximum strain due to deflection. Both items are calculated below using Equations 15 and 16 found in <u>Deflection: the Pipe/Soil Mechanism</u>, UNI-TR-1-97, Published by the Uni-Bell PVC Pipe Association (Pgs 28-30):

Where:	\in_{h}	=	Maximum Pipe Strain due to Hoop Stress, in/in
	Р	=	Pressure on the pipe (Live + Prism Loads), psi
	E	=	Modulus of Elasticity of the Pipe, psi
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in

$$\in_h = \frac{PD}{2tE}$$

Using the maximum cover for both live loads and prism loads as well as the previous unit weight of the soil:

$$\in_{h} = \frac{[0.00 + 24.18] \times 12.75}{2 \times 0.49 \times 400,000} = 7.863E-04 \frac{\text{in}}{\text{in}}$$

Where:	\in_{f}	=	Maximum Pipe Strain due to Ring Deflection, in/in
	ΔY	=	Change in vertical pipe diameter under load, in, (numerator in
			the deflection equation, but in decimal form)
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in
	DR	=	Dimension Ratio= 26

$$\in_{f} = \frac{t}{D} \left[\frac{3\Delta Y / D}{1 - 2\Delta Y / D} \right] = \frac{1}{DR} \left[\frac{3\Delta Y}{D - 2\Delta Y} \right]$$

$$\epsilon_f = 0.038 \times \frac{9.791}{12.75 - 6.528} = 0.0605 \frac{\text{in}}{\text{in}}$$

$$\in_{total} = 6.1309 \text{E-02} \quad \frac{\text{in}}{\text{in}}$$

(15")

Pipe strain is also known as the elongation of the pipe over the original length of the pipe. Under normal loading conditions of the PVC pipe, the variable that affects the elongation or straining of the pipe stems from the either the flexure or deflection (i.e., bending) of the pipe within the bedding material (i.e. increased or excessive pipe deflection causing the pipe to elongate) or hoop stress within the pipe wall. Please note that pipe strain is not generally known to be the limiting performance factor during pipe failure. For this system, pipe deflection is limited to 5% for a SDR 26 pipe. This 5% deflection value is the industry accepted value placing the pipe within its straining limits. Therefore, as the calculated deflection above is shown to be less than 5%, the pipe and bedding class used in this system is within the acceptable straining limits for this pipe.

However, total Pipe strain is calculated as the combination of the before mentioned hoop stress and the maximum strain due to deflection. Both items are calculated below using Equations 15 and 16 found in <u>Deflection: the Pipe/Soil Mechanism</u>, UNI-TR-1-97, Published by the Uni-Bell PVC Pipe Association (Pgs 28-30):

Where:	\in_{h}	=	Maximum Pipe Strain due to Hoop Stress, in/in
	Р	=	Pressure on the pipe (Live + Prism Loads), psi
	E	=	Modulus of Elasticity of the Pipe, psi
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in

$$\in_h = \frac{PD}{2tE}$$

Using the maximum cover for both live loads and prism loads as well as the previous unit weight of the soil:

$$\in_{h} = \frac{[0.00 + 22.48] \times 15.3}{2 \times 0.588 \times 400,000} = 7.311E-04 \frac{\text{in}}{\text{in}}$$

Where:	\in_{f}	=	Maximum Pipe Strain due to Ring Deflection, in/in
	ΔY	=	Change in vertical pipe diameter under load, in, (numerator in
			the deflection equation, but in decimal form)
	t	=	Pipe Wall thickness, in
	D	=	Pipe Diameter, Average Outer, in
	DR	=	Dimension Ratio= 26

$$\in_{f} = \frac{t}{D} \left[\frac{3\Delta Y / D}{1 - 2\Delta Y / D} \right] = \frac{1}{DR} \left[\frac{3\Delta Y}{D - 2\Delta Y} \right]$$

$$\in_f = 0.038 \times \frac{8.396}{15.3 - 5.597} = 0.0333 \frac{\text{in}}{\text{in}}$$

$$\epsilon_{total} = 3.4013 \text{E-02} \quad \frac{\text{in}}{\text{in}}$$

TCEQ PIPE BEDDING AND TRENCHING REQUIREMENTS (30 TAC 217.54)

These notes are provided in the Construction Documents on Sheet 4

- a. Pipe Embedment
 - A rigid pipe must be laid with the adequate bedding, haunching, and initial backfill to support the anticipated load. The bedding classes that are allowed are A, B, or C, as described in American Society for Testing and Materials (ASTM) C 12, American National Standards Institute (ANSI) A 106.2, Water Environment Federation Manual of Practice No. 9 or American Society of Civil Engineers (ASCE) MOP 37.
 - 2. A flexible pipe must be laid with the adequate bedding, haunching, and initial backfill to support the anticipated load. The bedding classes that are allowed are IA, IB, II, or III, as described in ASTM D-2321 or ANSI K65.171.
 - 3. Debris, large clods, or stones that are greater than six inches in diameter, organic matter, or other unstable materials are prohibited as bedding, haunching, or initial backfill.
 - 4. Backfill must not disturb the alignment of a collection system pipe.
 - 5. If trenching encounters significant fracture, fault zones, caves, or solutional modification to the rock strata, an owner must halt construction until an engineer prepares a written report detailing how construction will accommodate these site conditions.

b. Compaction.

- 1. Compaction of an embedment envelope must meet the manufacturer's recommendations for the collection system pipe used in a project.
- 2. Compaction of an embedment envelope must provide the modulus of soil reaction for the bedding material necessary to ensure a wastewater collection system pipe's structural integrity as required by §217.53 of this title (relating to Pipe Design).
- 3. The placement of the backfill above a pipe must not affect the structural integrity of a pipe.
- c. Envelope Size.
 - 1. A minimum clearance of 6.0 inches below and on each side of the bell of all pipes to the trench walls and floor is required.
 - 2. The embedment material used for haunching and initial backfill must be installed to a minimum depth of 12 inches above the crown of a pipe.

d. Trench Width.

- 1. The width of a trench must allow a pipe to be laid and jointed properly and must allow the backfill to be placed and compacted as needed.
- 2. The maximum and minimum trench width needed for safety and a pipe's structural integrity must be included in the report.
- 3. The width of a trench must be sufficient to properly and safely place and compact haunching materials.
- 4. The space between a pipe and a trench wall must be wider than the compaction equipment used in the pipe zone.

TRENCH CROSS-SECTION (30 TAC 217.54)



NOTE:

Trenching Details along with 30 TAC 217.54 are annotated in the Construction Documents/Plan Sheets on Sheet 4

MANHOLE SPECIFICATIONS

30 TAC 217.55 Requirements with design comments:

- a. An owner must include manholes in a wastewater collection system at:
 - 1. All points of change in alignment, grade, or size;
 - 2. At the intersection of all pipes; and
 - 3. At the end of all pipes that may be extended at a future date. (Self explanatory, the SCS line will not be extended therefore no stub-outs
- b. Manholes placed at the end of a wastewater collection system pipe that may be extended in the future must include pipe stub outs with plugs. (Self explanatory, see item a above)
- c. A clean-out with watertight plugs may be installed in lieu of a manhole at the end of a wastewater collection system pipe if no extensions are anticipated. (Self explanatory, clean outs not used in-lieu of manholes)
- d. Cleanout installations must pass all applicable testing requirements outlined for gravity collection pipes in §217.57 of this title (relating to Testing Requirements for Installation of Gravity Collection System Pipes). (Self explanatory, see Item d above)
- e. A manhole must be made of monolithic, cast-in-place concrete, fiberglass, pre-cast concrete, high-density polyethylene, or equivalent material that provides adequate structural integrity. See the Pre-Cast Manhole Details following these construction notes)
- f. The use of bricks to adjust a manhole cover to grade or construct a manhole is prohibited. (Self explanatory, See Details following these notes)
- g.

Manholes may be spaced no further apart than the distances specified in the following table for a wastewater collection system with straight alignment and uniform grades, unless a variance based on the availability of cleaning equipment that is capable of servicing greater distances is granted by the executive director. (Self explanatory and maintained throughout the design of the SCS)

Table C.2 Maximum Manhole Spacing						
Pipe Diameter	Maximum Manhole					
6-15	500					
18-30	800					
36-48	1000					
54 or larger	2000					

h. Tunnels are exempt from manhole spacing requirements because of construction constraints. (Self explanatory and not applicable)

- i. An intersection of three or more collection pipes must have a manhole. (Self explanatory and maintained throughout the design of the SCS)
- j. A manhole must not be located in the flow path of a watercourse, or in an area where ponding of surface water is probable. (Self explanatory and maintained throughout the design of the SCS)
- k. The inside diameter of a manhole must be no less than 48 inches. A manhole diameter must be sufficient to allow personnel and equipment to enter, exit, and work in the manhole and to allow proper joining of the collection system pipes in the manhole wall. (See Manhole Details following these notes)
- 1. Manholes must meet the following requirements for covers, inlets, and bases.
 - 1. Manhole Covers
 - A.
 - A manhole where personnel entry is anticipated requires at least a 30 inch diameter clear opening. (Covers to have 32" Openings see Manhole Details)
 - B. A manhole located within a 100-year flood plain must have a means of preventing inflow. (Self explanatory and maintained throughout the design of the SCS)
 - C. A manhole cover construction must be constructed of impervious material. (Self explanatory, See Manhole Details following these construction notes)
 - D. A manhole cover that is located in a roadway must meet or exceed the American Association of State Highways and Transportation Officials standard M-306 for load bearing. (Self explanatory, See Manhole Details)
 - 2. Manhole Inverts
 - A. The bottom of a manhole must contain a U-shaped channel that is a smooth continuation of the inlet and outlet pipes. (Self explanatory, see Manhole Details)
 - B.

A manhole connected to a pipe less than 15 inches in diameter must have a channel depth equal to at least half the largest pipe's diameter (**Self explanatory, see Manhole Details**)

- C. A manhole connected to a pipe at least 15 inches in diameter but not more than 24 inches in diameter must have a channel depth equal to at least three-fourths of the largest pipe's diameter (Self explanatory, but not applicable for this project)
- D. A manhole connected to a pipe greater than 24 inches in diameter must have a channel depth equal to at least the largest pipe's diameter (**Self explanatory, but not applicable for this project**).

- E. A manhole with pipes of different sizes must have the tops of the pipes at the same elevation and flow channels in the invert sloped on an even slope from pipe to pipe. (Self explanatory and maintained throughout the design of the SCS)
- F. A bench provided above a channel must slope at a minimum of 0.5 inch per foot. (Self Explanatory)
- G.

An invert must be filleted to prevent solids from being deposited if a wastewater collection system pipe enters a manhole higher than 24 inches above a manhole invert. (Self Explanatory, see manhole details for a drop manhole)

H.

A wastewater collection system pipe entering a manhole more than 24 inches above an invert must have a drop pipe. (**Self Explanatory, see Manhole Details**)

- m. The inclusion of steps in a manhole is prohibited. (Self Explanatory, see Manhole Details)
- n.

Connections. A manhole-pipe connection must use watertight, size-on-size resilient connectors that allow for differential settlement and must conform to American Society for Testing and Materials C-923. (Self Explanatory, see Manhole Details)

venting. An owner must use an alternate means of venting if manholes are at more than 1,500 foot intervals and gasketed manhole covers are required for more than three manholes in sequence. Vents must meet the following requirements: (Self Explanatory, but not applicable for this project)

- 1. Vent design must minimize inflow;
- 2. Vents must be located above a 100-year flood event elevation; and
- 3. Tunnels must be vented in compliance with this subsection.
- p. Cleanouts. The size of a cleanout must be equal to the size of the wastewater collection system main. (Self Explanatory)

Precast Manhole Information:

Hanson Pipe and Precast

Hanson Building Products West 300 E John Carpenter Freeway 11th floor Irving, TX 75062 972.653.5500

San Antonio Metro Area Contact: 210.661.2351 866.426.7661









ATTACHMENT A WASTEWATER / SEWAGE CALCULATIONS

Revised Building Name (Building name from original SERs)	Phase Group	Phase	Estimated Occupancy Date	Gross Area (sf)*	Building Construction Type	LUE Use	Lue Conversion	LUE	Population (persons)	Average Dry Weather Flow (gpm) "F"	PFF	Peak Hour Demand (gpm)	Peak Day Demand (gpm)	Peak Dry Weather Flow (gpm)	Fire Flow Demand (gpm)	Fire Flow Demand (gpm)**
NWUB	1	1	EXISTING	2,880	IIB	Office Warehouse	1 LUE/ 4000 sq ft	0.7	2.5	0.1	4.0	1.6	0.9	0.5	6,000	1,500
PG4 (UPG2)	1	2	EXISTING	353,347	IB	Parking	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	6,000	1,500
CENTRAL PLANT (CPW)	1	3	EXISTING	30,000	IIB	Cooling Plant (Office)	1 LUE/ 3000 sq ft	10.0	35.0	1.7	3.9	22.0	13.0	6.6	3,750	1,500
PG1	1	4	EXISTING	495,681	IB	Parking	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	6,000	1,500
B2/ KITCHEN	1	5	EXISTING	318,111	IB	R&D (Office)	1 LUE/ 3000 sq ft	106.0	371.1	18.0	3.1	233.3	137.8	55.2	6,000	1,500
B1/CONF	1	6	EXISTING	270,608	IB	Office	1 LUE/ 3000 sq ft	90.2	315.7	15.3	3.1	198.4	117.3	48.0	5,500	1,500
RD1	1	7	EXISTING	208,602	IB	R&D (Office)	1 LUE/ 3000 sq ft	69.5	243.4	11.8	3.2	153.0	90.4	38.3	5,000	1,500
							PHASE 1 TOTAL	276.5	967.7	46.9		608.3	359.4	148.6		
G2 (PG2)	2	8	(Jan 23) 2026	1,109,180	IB	Parking	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	6,000	1,500
AC03 (B3)	2	9	(Jan 15) 2026	368,726	IB	Office	1 LUE/ 3000 sq ft	122.9	430.2	20.9	3.0	270.4	159.8	62.7	5,750	1,500
AC09 (CBC)	2	10	(Apr 06) 2026	70,945	IB	Office	1 LUE/ 3000 sq ft	23.6	82.8	4.0	3.6	52.0	30.7	14.6	3,000	1,500
AC09 (CBC)	2	10	(Apr 06) 2026	30,000	IB	Restaurant	1 LUE/ 200 sq ft	150.0	525.0	25.5	2.9	330.0	195.0	74.3	5,000	1,500
AC09 (CBC)	2	10	(Apr 06) 2026	31,489	IB	Retail	1 LUE/ 1660 sq ft	19.0	66.4	3.2	3.7	41.7	24.7	11.9	1,750	1,500
AC09 (CBC)	2	10	(Apr 06) 2026	25,464	IB	Retail	1 LUE/ 1660 sq ft	15.3	53.7	2.6	3.8	33.7	19.9	9.8	1,750	1,500
AC08 (RD2)	2	11	(Jan 21) 2026	289,326	IB	R&D (Office)	1 LUE/ 3000 sq ft	96.4	337.5	16.4	3.1	212.2	125.4	50.9	5,750	1,500
AC07 (RD3)	2	12	(Feb 23) 2026	215,600	IB	R&D (Office)	1 LUE/ 3000 sq ft	71.9	251.5	12.2	3.2	158.1	93.4	39.4	5,000	1,500
AC12-CHILD CARE (CDB) ***	2	13	(Jan 26) 2026	32,947	5B	Childcare	1 LUE/ 15 students	60.0	210.0	10.2	3.3	132.0	78.0	33.6	5,000	1,500
M4 - OFFICE (CWB)	2	14	(June 04) 2026	1,200	5B	Office	1 LUE/ 3000 sq ft	0.4	1.4	0.1	4.0	0.9	0.5	0.3	1,500	1,500
M4 - CENTRAL WASTE (CWB)	2	14	(June 04) 2026	16,312	5B	Office Warehouse	1 LUE/ 4000 sq ft	4.1	14.3	0.7	4.0	9.0	5.3	2.8	3,500	1,500
M5 - OFFICE	2	15	(Sept 1) 2026	1,200	IB	Office	1 LUE/ 3000 sq ft	0.4	1.4	0.1	4.0	0.9	0.5	0.3	1,500	1,500
M5 - WASTEWATER TREATMENT PLANT	2	15	(Sept 1) 2026	22,300	IB	Office Warehouse	1 LUE/ 4000 sq ft	5.6	19.5	0.9	4.0	12.3	7.2	3.8	1,500	1,500
							PHASE 2 TOTAL	569.6	1,993.7	96.6		1,253.2	740.5	304.4	í'	
G3 (PG3)	3	16	(Sept 1) 2028	930,866	IB	Parking	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	6,000	1,500
B4	3	17	(Sept 1) 2028	265,616	IB	Office	1 LUE/ 3000 sq ft	88.5	309.9	15.0	3.1	194.8	115.1	47.2	5,000	1,500
B5	3	18	(Sept 1) 2028	258,171	IB	Office	1 LUE/ 3000 sq ft	86.1	301.2	14.6	3.2	189.3	111.9	46.1	5,000	1,500
B6/BMR	3	19	(June 1) 2028	290,989	IB	Office	1 LUE/ 3000 sq ft	97.0	339.5	16.5	3.1	213.4	126.1	51.1	5,250	1,500
HOTEL	3	20	(Sept 1) 2028	199,175	IB	Hotel	0.5 LUE/ room	96.0	336.0	16.3	3.1	211.2	124.8	50.7	4,750	1,500
B7	3	21	(Dec 1) 2028	11,500	IB	Amenity for Offices	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1,500	1,500
B8	3	21	(Dec 1) 2028	11,500	IB	Amenity for Offices	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1,500	1,500
B9	3	21	(Dec 1) 2028	11,500	IB	Amenity for Offices	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	1,500	1,500
							PHASE 3 TOTAL	367.6	1,286.6	62.4		808.7	477.9	195.1		
						F	PHASES 1,2,&3 TOTAL	1,214	4,248	206	0	2,670	1,578	648		

*BUILDING S.F. ARE APPROXIMATE

** BASED ON 75% FIRE CODE REDUCTION

***LUE CONVERSION BASED ON 60 EMPLOYEES AND A STUDENT EMPLOYEE RATIO OF 15:1

TOTAL OFFICE	2,559,094	SF
TOTAL CENTRAL PLANT	30,000	SF
TOTAL OFFICE WAREHOUSE	41,492	SF
TOTAL RESTAURANT	30,000	SF
TOTAL HOTEL	199,175	SF
TOTAL RETAIL	56,953	SF
TOTAL AMENITY	34,500	SF
TOTAL BUILDING	2,951,214	SF
TOTAL PARKING	2,891,954	SF



SER Calculations

Project:	Capstone SER 4339 & SER 4340 Revision
Phase:	Phase Group 2 (indivdual phases 8-15)
Date:	6/23/2023
Area:	29.5 acres (approximately)

Proposed Building Use	Square Feet*	LUE Conversion	LUEs
Total Office Building	946,997	1 LUE/3,000 SF	316
Total Restaurant	30,000	1 LUE/200 SF	150
Total Retail	56,953	1 LUE/1660 SF	34
Total Office Warehouse	38,612	1 LUE/4000 SF	10
Total Childcare**	32,947	1 LUE/ 15 STUDENTS	60
Total S.F.	1,033,950	Total LUEs	570



* Building S.F. are approximate

Wastewater Design

Population	=	LUEs X 3.5	/LUE	06
	=	569.6	X 3.5 persons/LUE	· · · · · · · · · · · · · · · · · · ·
	=	1,993.70	persons	
Average Dry Weather Flow (F)	=	(70gpd/pe	rsons/day) X (population / 1440)	
	=	96.92	gpm	
PFF	=	[18+(0.020)6 X F)^0.5]/[4+(0.0206 X F)^0.5] ,	Maximum = 4
	=	3.59		
Peak Dry Weather Flow	=	Average D	ry Weather Flow X PFF	
	=	347.58	gpm	
Peak Wet Flow	=	Peak Dry F	low + Inflow/Infiltration	
	=	347.58	+ (750 gpd/acre) X (acres/1440)	
	=	362.96	gpm	
Water Design				
Population	=	LUEs X 3.5	/LUE	
	=	569.63	X 3.5 persons/LUE	
	=	1,993.70	persons	
Peak Hour Demand	=	900 gallon 1. 246.06	s/person/day*persons*1 day/144	0 minutes
		1,2 10100	86	
Peak Day Demand	=	530 gallon	s/person/day*persons*1 day/144	0 minutes
		/33./9	ghu	
Fire Flow	_	1 100 190	ca ft	
	=	1,109,180	sqii	
Construction Type	=	IB		
Buidling Required Fire Flow	=	6000	gpm	
Reduced Building Required Fire Flow*	=	1500	gpm	
Total Peak Day Demand + Reduced Fire Flow	=	2,234	gpm	

*Assumed 75% credit for Automatic Sprinkler System

SER Calculations

Project:	Capstone SER 4339 & SER 4340 Revision
Phase:	Phase Group 3 (individual phases 16-21)
Date:	6/23/2023
Area:	60.0 acres (approximately)

Proposed Building Use Square Feet* LUE Conversion LUEs Total Office Building 814,776 1 LUE/3,000 SF 272 Total Hotel 192 rooms 0.5 LUE/ ROOM 96 Total Hotel 192 rooms 0.5 LUE/ ROOM 96 * Building S.F. are approximate 368 0000 actes (application actes) Wastewater Design Population = LUEs X 3.5/LUE 368 Average Dry Weather Flow (F) = (70gpd/persons/day) X (population / 1440) 67.24 E 3.73 Peak Dry Weather Flow = Average Dry Weather Flow = 3.73 Peak Dry Weather Flow = Average Dry Weather Flow X PFF = 233.05 gpm Peak Wet Flow = Peak Dry Flow + Inflow/Infiltration = 233.05 (26.31) Water Design = LUEs X 3.5/LUE = 1,286.57 persons/LUE 1,286.57 Peak Ury Weather Flow = Average Dry Weather Flow X PFF = 233.05 gpm Peak Wet Flow = Peak Dry Flow + Inflow/Infiltration = 264.31 gpm Peak	Date:		6/23/2023		covimatoly)			1 Au
Proposed Building Use Square Feet* LUE Conversion LUEs Total Office Building 814,776 1 LUE/3,000 SF 272 Total Hotel 192 rooms 0.5 LUE/ ROOM 96 Total Hotel 192 rooms 0.5 LUE/ ROOM 96 Total S.F. 1,013,951 Total LUEs 368 John D. * Building S.F. are approximate 367.6 X 3.5/LUE 367.6 X 3.5 persons/LUE Wastewater Design Population = LUEs X 3.5/LUE 06.71 Average Dry Weather Flow (F) = (70gpd/persons/day) X (population / 1440) 62.54 gpm PFF = [18+(0.0206 X F)^0.5]/[4+(0.0206 X F)^0.5], Maximum = 4 3.73 Peak Dry Weather Flow = Average Dry Weather Flow X PFF = 233.05 gpm Peak Wet Flow Peak Dry Flow + Inflow/Infiltration = 233.05 gpm Peak Wet Flow Peak Day Demand = 367.59 X 3.5 persons/LUE = 1,286.57 persons 1440) = 1,286.57 persons 1440)	Aled.		00.0 at	ries (appi	Uximately)			Hall
Total Office Building 814,776 1 LUE/3,000 SF 272 Total Hotel 192 rooms 0.5 LUE/ ROOM 96 Total S.F. 1,013,951 Total LUEs 368 * Building S.F. are approximate Wastewater Design Population = LUEs X 3.5/LUE = 367.6 X 3.5 persons/LUE 1,286.57 persons Average Dry Weather Flow (F) = (70gpd/persons/day) X (population / 1440) = 62.54 gpm PFF = [184(0.0206 X F)^0.5]/[4+(0.0206 X F)^0.5], Maximum = 4 Average Dry Weather Flow = Average Dry Weather Flow X PFF = 233.05 gpm Peak Dry Weather Flow = Average Dry Flow + Inflow/Inflitration = 233.05 # (750 gpd/acre) X (acres/1440) = 264.31 gpm Water Design Peak Hour Demand = 900 gallons/person/day*persons*1 day/1440 minutes Average Dry Weather Flow Peak Hour Demand = 900 gallons/person/day*persons*1 day/1440	Proposed Build	ling Use	Square Feet	*	LUE Co	onversion	LUEs	
Total Hotel 192 rooms 0.5 LUE/ ROOM 96 Total S.F. 1,013,951 Total LUEs 368 Joint D. * Building S.F. are approximate Wastewater Design Population = LUEs X 3.5/LUE 368 06727 Average Dry Weather Flow (F) = (70gpd/persons/day) X (population / 1440) 62.54 gpm PFF = (18+(0.0206 X F)^0.5]/(4+(0.0206 X F)^0.5] , Maximum = 4 3.73 Peak Dry Weather Flow = Average Dry Weather Flow X = 233.05 gpm Peak Dry Weather Flow = Average Dry Weather Flow X = 233.05 gpm Peak Dry Weather Flow = Average Dry Weather Flow X PFF = 233.05 gpm Peak Wet Flow = Peak Dry Flow + Inflow/Infiltration = 233.05 + (750 gpd/acre) X (acres/1440) = 232.05 + (750 gpd/acre) X (acres/1440) = 1,286.57 persons Water Design Peak Hour Demand = 900 gallons/person/day*persons*1 day/1440 minutes 804.11 gpm Peak Day Demand = 530 gallons/person/day*persons*1 day/1440 minu	Total Office B	uilding	814,776		1 LUE/	/3,000 SF	272	TE OF TEL
Total S.F. 1,013,951 Total LUEs 368 Joint Design * Building S.F. are approximate Wastewater Design = LUEs X 3.5/LUE = 06/27 addresses addresses = 1,286.57 persons 06/27 Average Dry Weather Flow (F) = (70gpd/persons/day) X (population / 1440) = 06/27 Average Dry Weather Flow (F) = (70gpd/persons/day) X (population / 1440) = 06/27 Pere Provide The Provide	Total Hot	tel	192 rooms		0.5 LU	E/ ROOM	96	5. 5
Total UEs 368 JOHN D. * Building S.F. are approximate 960 Wastewater Design 367.6 X 3.5, persons/LUE 960 a Verage Dry Weather Flow (F) = LUEs X 3.5/LUE 967.21, 1286.57 Average Dry Weather Flow (F) = (70gpd/persons/day) X (population / 1440) 967.21, 1286.57 Average Dry Weather Flow (F) = (70gpd/persons/day) X (population / 1440) 967.21, 1286.57 Pers = (18+(0.0206 X F)^0.5]/[4+(0.0206 X F)^0.5], Maximum = 4 97.3 Peak Dry Weather Flow = Average Dry Weather Flow X PFF = 233.05 gpm Peak Wet Flow = Peak Dry Flow + Inflow/Infiltration = 233.05 gpm Peak Wet Flow = 263.31 gpm Water Design Population = LUEs X 3.5/LUE = 367.59 X 3.5 persons/LUE = 1,286.57 persons Peak Hour Demand = 900 gallons/person/day*persons*1 day/1440 minutes 804.11 gpm Peak Day Demand = 530 gallons/person/day*persons*1 day/1440 minutes 473.53 gpm Building Required Footage					_			
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 Fire Flow Fire Flow Fire Flow Fire Flow Fire Flow Largest Building Square Footage Fire Flow Largest Building Square Footage Fire Flow Fire Flow<!--</td--><td></td><td>Average Drv</td><td>Weather Flow (F)</td><td>=</td><td>(70gpd/pe</td><td>ersons/day) X (po</td><td>opulation / 144</td><td>.0)</td>		Average Drv	Weather Flow (F)	=	(70gpd/pe	ersons/day) X (po	opulation / 144	.0)
PFF = [18+(0.0206 X F)^0.5]/[4+(0.0206 X F)^0.5], Maximum = 4 = 3.73 Peak Dry Weather Flow = Average Dry Weather Flow X PFF = 233.05 gpm Peak Wet Flow = Peak Dry Flow + Inflow/Infiltration = 233.05 + (750 gpd/acre) X (acres/1440) = 264.31 gpm Water Design Population = LUEs X 3.5/LUE = 367.59 X 3.5 persons/LUE = 1,286.57 persons Peak Hour Demand = 900 gallons/person/day*persons*1 day/1440 minutes 804.11 gpm Peak Day Demand = 530 gallons/person/day*persons*1 day/1440 minutes 473.53 gpm Fire Flow Largest Building Square Footage = 930866 sq ft Construction Type = IB Buidling Required Fire Flow = 6000 gpm				=	62.54	gpm		-,
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Fire Flow = 233.05 gpm Peak Wet Flow = Peak Dry Flow + Inflow/Infiltration = 233.05 + (750 gpd/acre) X (acres/1440) = 264.31 gpm Water Design = LUEs X 3.5/LUE = 367.59 X 3.5 persons/LUE = 1,286.57 persons Peak Hour Demand = 900 gallons/person/day*persons*1 day/1440 minutes 804.11 gpm Peak Day Demand = 530 gallons/person/day*persons*1 day/1440 minutes 473.53 gpm Fire Flow = 930866 sq ft Building Required Fire Flow = 6000 gpm		Poak ()ry Weather Flow	_	Average D	ry Westher Flow		
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Largest Building Square Footage = 930866 sq ft Construction Type = IB Buidling Required Fire Flow = 6000 gpm	Fire Flow							
Construction Type = IB Buidling Required Fire Flow = 6000 gpm		Largest Buildin	g Square Footage	=	930866	sq ft		
Buidling Required Fire Flow = 6000 gpm		- (Construction Type	=	IB	-		
Buidling Required Fire Flow = 6000 gpm								
	- ·	Buidling R	equired Fire Flow	=	6000	gpm		
Reduced Building Required Fire Flow* = 1500 gpm	Reduc	ed Building Re	quired Fire Flow*	=	1500	gpm		
Total Peak Day Demand + Reduced Fire Flow = 1,974 gpm	Total Peak D	ay Demand + F	educed Fire Flow	=	1,974	gpm		

*Assumed 75% credit for Automatic Sprinkler System

<u>ATTACHMENT B</u> WASTEWATER UTILITY SERVICE AGREEMENT

WATER AND WASTEWATER SERVICE EXTENSION REQUEST FOR CONSIDERATION

Name: Parmer & McNeil (Revised)		Servis	ce Requested: Wastewater				
SER-4340R	Infor (IPS) Service Request ?	Number: 1255001	Date Received: 06/27/20)23			
Location: 6900 W PARMER LN AUS	TIN TX 78729						
Acres: 174.32	Land Use: MIXED		LUE: 1214				
Alt. Utility Service or S.E.R. Number:	City of Austin Water SER-4339	R					
Quad(s): J37 J38	Reclaimed Pressure Zone: N/	A	DDZ: YES				
Drainage Basin: WALNUT	Pressure Zone: NORTHWES	ΤA	DWPZ: NO				
Flow (Estimated Peak Wet Weather): 8	51 GPM		ו				
Cost Participation: \$0	% Within	City Limits: 100	% Within Limited Purpo	15e: 0			
270592) at the location shown on the attached map. Applicant shall also dedicate an 80-foot wastewater easement for the future Rattan Creek Lower Interceptor along the approximate alignment shown on the attached map. <u>Phase Groups 2 and 3 (278 to 1.214 LUEs)</u> Applicant shall upgrade the vortex flow insert located within the Rattan Creek Shaft (Unit ID #270527) when development on the subject tract exceeds 1,000 LUEs or when the average dry weather flow entering the Rattan Creek Shaft exceeds 0.6 MGD. The upgraded vortex flow insert shall have a design capacity of 4.0 MGD, unless otherwise directed by Austin Water's Systems Planning Division. Applicant shall coordinate with Austin Water to initiate flow monitoring to verify existing flows into the Rattan Creek Shaft and to determine the need for the vortex flow insert upgrade. NOTES: 1) Wastewater flow based on engineering calculations received from John D. Pelham, P.E. of GarzaEMC, LLC on 6/27/2023, 2) At the							
time of the approval of this SEEC, the FI	and croup I wasternater impro-	entens have an early been con-	a orige				
 Approval of this Service Extension Request is subject to completion and acceptance of the improvements described above and the conditions set forth below: 1) Construction of all Service Extensions is subject to all environmental and planning ordinances. 2) Service Extensions are subject to the guidelines established in the Land Development Code, Chapter 25-9, Water and Wastewater Utility Service. 3) An approved Service Extension is not a reservation of capacity in the system, but it is an acknowledgment of the intent to serve. Available capacity shall be confirmed at the time a development application is submitted. 4) The level of service approved by this document does not imply commitment for land use. 5) Public utility mains must meet City of Austin Design and Construction Criteria and must be approved by Austin Water Engineering Review. Actual length and location of staff proposed utility mains shall be finalized during the plan review process. 6) Proposed public wastewater improvements will be dedicated to the City of Austin for ownership, operation, and maintenance. 7) Proposed public wastewater improvements will be dedicated to the City of Austin for ownership, operation, and maintenance. 8) The approved Service Extension will automatically expire 180 days after date of approval unless a development application has been accepted by the Development Services Department. The Service Extension expires on the date the development expires, or if approved, on the date the development application approval expires. 							
Ole Himser, Utility Development S	Services Date 11/6/23 Date 11/09/2023 Date	Supervisor, Unility Develop Director, Austin Walter	Unit ment Services Paralson	11/7/23 Date 11/12/2023 Date			



This product is for informational purposes and may not have been prepared for or be suitable for legal, engineering, or surveying purposes. It does not represent an on-five-ground servey and represents only the approximate relative location of the property boundaries. This product has been produced by the City of Austin for the sole purpose of geographic reference. No warranty is made by the City of Austin regarding specific accuracy or completeness.

<u>ATTACHMENT C</u> LOCAL SANITARY SEWER CONSTRUCTION NOTES

STANDARD CONSTRUCTION NOTES

October 1, 2021

THE CITY STANDARD CONSTRUCTION SPECIFICATIONS CURRENT AT THE TIME OF BIDDING SHALL COVER MATERIALS AND METHODS USED TO DO THIS WORK.
 CONTRACTOR MUST OBTAIN A 30W PERMIT FROM AUSTIN TRANSPORTATION DEPT. RIGHT OF WAY MANAGEMENT DIVISION BEFORE BEGINNING CONSTRUCTION WITH

 CONTRACTOR MJST OBTAIN A ROW PERMIT FROM AUSTIN TRANSPORTATION DEPT, RIGHT OF WAY MANAGEMENT DIVISION BEFORE BEGINNING CONSTRUCTION WITHIN THE RIGHT-OF-WAY OF A PUBLIC STREET OR ALLEY. ACTIVITY WITHIN RIGHT-OF-WAY SHALL COMPLY WITH APPROVED TCP.
 AT LEAST 43 HOURS PRIOR TO BEGINNING ANY UTILITY CONSTRUCTION ACTIVITY IN FUBLIC ROW OR PUBLIC EASEMENT, THE CONTRACTOR SHALL NOTIFY THE

3. AT LEAST 43 HOURS PRIOR TO BEGINNING ANY UTILITY CONSTRUCTION ACTIVITY IN FUBLIC ROW OR PUBLIC EASEMENT, THE CONTRACTOR SHALL NOTIFY THE APPLICABLE CITY OF AUSTIN INSPECTION GROUP (AUSTIN TRANSPORTATION, DEVELOPMENT SERVICES, OR PUBLIC WORKS). SEE CURRENT NOTIFICATION REQUIREMENTS AT WWW.AUSTINTEXAS.GOV.

4. THE CONTRACTOR SHALL CONTACT THE AUSTIN AREA "ONE CALL" SYSTEM AT 1-800-344-4377 FOR EXISTING UTILITY LOCATIONS PRIOR TO ANY EXCAVATION IN ADVANCE OF CONSTRUCTION. THE CONTRACTOR SHALL VER FY THE LOCATIONS OF ALL UTILITIES TO BE EXTENDED, THE TO, OR ALTERED, OR SUBJECT TO DAMAGE/INCONVENIENCE BY THE CONSTRUCTION OPERATIONS. THE CITY OF AUSTIN WATER AND WASTEWATER MAINTENANCE RESPONSIBILITY ENDS AT R.O.W.JEASEMENT LINES.

5. NO OTHER UTILITY SERVICE/APPURTENANCES SHALL BE PLACED NEAR THE PROPERTY LINE, OR OTHER ASSIGNED LOCATION DESIGNATED FOR WATER AND WASTEWATER UTILITY SERVICE THAT WOULD INTERFERE WITH THE WATER AND WASTEWATER SERVICES.

 MINIMUM TRENCH SAFETY MEASURES SHALL BE PROVIDED, AS REQUIRED BY OSHA, CITY SPECIFICATION 509S, AND CITY/COUNTY CONSTRUCTION INSPECTORS.
 ALL MATERIALS TESTS ORDERED BY THE OWNER FOR QUALITY ASSURANCE PURPOSES, SHALL BE CONDUCTED BY AN INDEPENDENT LABORATORY AND FUNDED BY THE OWNER IN ACCORDANCE WITH CITY STANDARD SPECIFICATION ITEM 1804S.04.

8. PRESSURE TAPS SHALL BE ALLOWED ON A CASE BY CASE BASIS, AS DETERMINED BY THE DIRECTOR'S DESIGNEE. NORMALLY PRESSURE TAPS 4 INCHES AND LARGER SHALL BE ALLOWED IN THE FOLLOWING CASES: A) A TEST SHUT OUT INDICATES AN ADEQUATE SHUT OUT TO PERFORM THE WORK IS NOT FEASIBLE B) MORE THAN 30 CUSTOMERS OR A SINGLE CRITICAL CUSTOMER (AS DEFINED BY AUSTIN WATER) WOULD BE IMPACTED BY THE SHUT OUT OR C) THE EXISTING WATER LINE WARRANTS IT.

9. WATER LINE TESTING AND STERILIZATION SHALL BE PERFORMED IN ACCORDANCE WITH CITY STANDARD SPECIFICATION ITEMS 510.3 (27)-(29). FORCE MAIN PRESSURE TESTING SHALL BE CONDUCTED AND FALL UNDER THE SPECIFICATIONS AS WATER LINES (PRESSURE PIPE) OR AT THE PRESSURES SHOWN ON THE APPROVED PLANS. 10. ALL MATERIAL USED ON THIS PROJECT MUST BE LISTED ON THE STANDARD PRODUCTS LISTING. ANY MATERIAL NOT LISTED HAS TO GO THROUGH THE REVIEW OF THE STANDARDS COMMITTEE FOR REVIEW AND APPROVAL PRIOR TO START OF PROJECT. TESTING AND EVALUATION OF PRODUCTS ARE REQUIRED BEFORE APPROVAL WILL BE GIVEN ANY CONSIDERATION.

11. WHEN WATER SERVICES ARE DAMAGED AND THE SERVICE NATERIAL IS POLYETHYLENE (PE), THE LINE SHALL BE REPAIRED ONLY BY HEAT FUSION WELD, AT BRASS FITTINGS, OR THE FULL LENGTH SHALL BE REFLACED PER CURRENT STANDARD DETAIL(S). WHEN POLYBUTYLENE (PB) TUBING IS DAMAGED OR TAMPERED WITH IN ANY WAY, THE FULL LENGTH OF SERVICE LINE SHALL BE REFLACED. (NOTE FULL LENGTH IS FROM THE CORPORATION STOP TO THE NETER.) REPAIR COUPLINGS ARE NOT ALLOWED FOR ANY WATER OR WASTEWATER SERVICE LINE REPAIR, RECONNECT, OR REPLACEMENT.

12. WHEN AN EXISTING WATERLINE SHUT OUT IS NECESSARY AND POSSIBLE, THE CONTRACTOR SHALL NOTIFY THE CONSTRUCTION INSPECTOR WHO WILL THEN NOTIFY AUSTIN WATER DISPATCH AND THE AFFECTED CUSTOMERS A MINIMUM OF FORTY-EIGHT (48) HOURS IN ADVANCE.

13. THE CONTRACTOR SHALL NOTIFY THE CONSTRUCTION INSPECTOR SC THAT HE CAN NOTIFY THE AUSTIN WATER AT 972-0000 AT A MINIMUN OF 72 HOURS PRIOR TO RELOCATING ANY DOMESTIC OR FIRE DEMAND WATER METERS. THE CONTRACTOR SHALL CAREFULLY REMOVE ALL METERS AND METERS BOXES THAT ARE INDICATED TO BE RELOCATED OR SALVAGED. THE CONTRACTOR SHALL INSTALL THE REMOVED METER OR CITY PROVIDED METER AT THE NEW LOCATION INDICATED ON THE CONSTRUCTION PLANS.

14. THE CONTRACTOR SHALL VERIFY ALL VERTICAL AND HORIZONTAL LOCATIONS OF EXISTING UTILITIES, BELOW GROUND AND OVERHEAD, PRIOR TO STARTING ONSITE UTILITY WORK.

15. ALL WATER, WASTEWATER, AND RECLAIMED MAINS SHALL BE INSTALLED IN ACCORDANCE WITH THE SEPARATION DISTANCES INDICATED ON THE PLANS, PER UTILITY CRITERIA MANUAL AND TCEQ CHAPTERS 210, 217, AND 290.

16. PROJECT-SPECIFIC SHOP DRAWINGS SHALL BE SUBMITTED FOR AW APPRCVAL FOR PRE-CAST CIRCULAR VERTICAL MANHOLE SECTIONS LARGER THAN 48" DIAMETER. THE SHOP DRAWINGS SHALL INCLUDE THE FLOWLINE ELEVATION OF ALL CONNECTING PIPES; ELEVATIONS OF TRANSITIONS FROM LARGE DIAMETER SECTIONS TO 48" DIAMETER SECTIONS; TOP OF MANHOLE AND SURROUNDING GROUND ELEVATIONS; AND DETAILS OF SPECIAL CONSTRUCTION CONSIDERATIONS SPECIFIED IN THE CONTRACT DOCUMENTS.

17. WHEN CONCRETE MANHOLES LARGER THAN 48 INCH DIAMETER ARE USED, DRAWINGS THAT ARE SEALED BY A PROFESSIONAL ENGINEER SHALL BE SUBMITTED FOR BASE SLABS, FLAT TOP LIDS (IF USED), AND FLAT TYPE CONCRETE PIECES USED TO TRANSITION FROM LARGER TO SMALLER DIAMETER MANHOLE SECTIONS. 18. ALL FRE HYDRANTS AND VALVES THAT ARE TO BE ABANDONED SHALL BE RENOVED, SALVAGED AND RETURNED TO AUSTIN WATER. NOTICE SHOULD BE GIVEN 48

HCURS PRIOR, TO PIPELINE OPERATIONS DISTRIBUTION SYSTEM -VALVES AND HYDRANT SERVICES SUPERVISOR AT 512-972-1280. 19. ALL EXISTING WATER METERS IDENTIFIED TO BE RELOCATED OR ABANDONED AT THE DEVELOPMENT SHALL BE REMOVED FROM THE METER BOX PRIOR TO CONSTRUCTION AND GIVEN IMMEDIATELY TO THE CITY OF AUSTIN INSPECTOR.

20. THE ENGINEER SHALL CALL OUT THE SIZE, TYPE AND USE (DOMESTIC OR IRRIGATION) OF ALL EXISTING WATER METERS TO BE RELOCATED OR REPURPOSED. WATER METER NUMBERS WILL NOT BE REQUIRED TO BE PLACED ON THE PLAN SHEET. A SEPARATE AUSTIN WATER TAPS OFFICE FORM WILL BE USED TO PROVIDE RELEVANT DATA FOR THE EXISTING INFORMATION ON EXISTING METERS TO RECEIVE APPROPRIATE CREDITS. THIS FORM SHALL BE DIRECTLY SUBMITTED TO AUSTIN WATER TAPS OFFICE FOR REVIEW AND PROCESSING.

21. NO CONNECTION MAY BE MADE BETWEEN THE PRIVATE PLUMBING AND AUSTIN WATER INFRASTRUCTURE UNTIL A CITY APPROVED WATER METER HAS BEEN INSTALLED.

22. METER BOXES AND CLEAN OUTS SHALL NOT BE LCCATED WITHIN PAVED AREAS SUCH AS DRIVEWAYS AND SIDEWALKS.

Lift Station/Force Main System Application

Texas Commission on Environmental Quality

for Regulated Activities On the Edwards Aquifer Recharge Zone and Relating to 30 TAC §213.5(c)(3)(B)and(c), Effective June 1, 1999

To ensure that the application is administratively complete, confirm that all fields in the form are complete, verify that all requested information is provided, consistently reference the same site and contact person in all forms in the application, and ensure forms are signed by the appropriate party.

Note: Including all the information requested in the form and attachments contributes to more streamlined technical reviews.

Regulated Entity Name: Generational Properties

Customer Information

(If different than customer information provided on core data form)

1. The person(s) responsible for providing the engineering certification to the TCEQ pursuant to 30 TAC §213.5(f)(2)(C) during construction and 30 TAC §213.5 (c)(3)(D) upon completion of construction is:

Contact Person: Dani SattmanEntity: Apple, Inc.Mailing Address: 12545 Riata Vista Circle, MS 522-EHSCity, State: Austin, TXZip: 78727Telephone: 512-674-8221Fax: _____Email Address: dsattman598@apple.com

2. The engineer responsible for the design of this lift station and force main:

Contact Person: John Pelham, P.E. Entity: GarzaEMC, LLC Mailing Address: 7708 Rialto Blvd Suite 125 City, State: Austin, TX Zip: 78735 Telephone: 512-298-3284 Fax: _____ Email Address: jpelham@garzaemc.com Texas Licensed Professional Engineer's Serial Number: 98294

Project Information

3. This project is for the construction or replacement of:

Lift Station only.

Lift Station and Force Main system.

K Lift Station, Force Main, and Gravity system.

4. The sewage collection system will convey the wastewater to the Walnut Creek (name) Treatment Plant. The treatment facility is:

🔀 Existing Proposed

5. All components of this lift station/force main system will comply with:

 \times The City of Austin standard specifications. Other. Specifications are attached.

Site Plan Requirements

Items 6-14 must be included on the Site Plan.

6. The Site Plan must have a minimum scale of 1'' = 400'.

Site Plan Scale: 1" = 30'.

- 7. X Lift station/force main system layout meets all requirements of 30 TAC Chapter 217.
- 8. Geologic or Manmade Features:
 - No geologic or manmade features were identified in the Geologic Assessment. ig > All geologic or manmade features identified in the Geologic Assessment (caves, solution openings, sinkholes, fractures, joints, porous zones, etc.) which exist at the site of the proposed lift station and along the path(s) or within **50 feet of each side** of a proposed force main line are shown on the Site Plan and are listed in the table below. Designs used to protect the integrity of the sewer line crossing each feature are described and labeled on the attached page. A detailed design drawing for each feature is shown on Plan Sheet 22 of 235.

No Geologic Assessment is required for this project.

Line	Station to Station	Type of Feature
CEP-08	to	Cave
CEP-09	to	Cave
CEF-01	to	Karst
CEF-02	to	Karst
	to	

Table 1 - Geologic or Manmade Features
9.	Existing topographic contours are shown and labeled.	The contour interval is $\underline{1}$ feet.
	(Contour interval must not be greater than 5 feet).	

10. 🛛 Finished topograph	c contours are shown and labeled.	The contour interval is <u>1</u> feet.
(Contour interval m	ust not be greater than 5 feet).	

Finished topographic contours will not differ from the existing topographic configuration and are not shown.

11. 100-year floodplain boundaries

Some part(s) of the project site is located within the 100-year floodplain. The floodplain is shown and labeled.

No part of the project site is located within the 100-year floodplain.

The 100-year floodplain boundaries are based on the following specific (including date of material) sources(s): <u>FEMA Map - 12/20/2019</u>

12. 5-year floodplain:

After construction is complete, no part of this project will be in or cross a 5-year floodplain, either naturally occurring or manmade. (Do not include streets or concrete-lined channels constructed above sewer lines.)

After construction is complete, all sections of the force main located within the 5year floodplain will be encased in concrete or capped with concrete. These locations are listed in the table below and are shown and labeled on the Site Plan. (Do not include streets or concrete-lined channels constructed above sewer lines.)

Table 2 - 5-Year Floodplain

Line	Sheet	Station to Station
	of	to

13. All known wells (oil, water, unplugged, capped and/or abandoned, test holes, etc.):

If applicable, this must agree with Item No. 15 on the Geologic Assessment Form.

There are $\underline{1}$ (#) wells present on the project site and the locations are shown and labeled. (Check all of the following that apply)

The wells are not in use and have been properly plugged.

The wells are not in use and will be properly plugged.

The wells are in use and comply with 16 TAC Chapter 76.

There are no wells or test holes of any kind known to exist on the project site.

14. \square Legal boundaries of the site are shown.

Plan and Profile Sheets

The construction drawings and technical specifications will not be considered for review unless they are the **final plans and technical specifications** which will be used by the contractor for bidding and construction.

Items 15 – 18 must be included on the Plan and Profile sheets.

15. \square The equipment installation construction plans must have a minimum scale of 1" = 10'.

Plan sheet scale: 1'' = 30'.

- 16. 🛛 Locations, descriptions and elevations of all required equipment and piping for the lift station and force main are shown and labeled.
- 17. Air Release/Vacuum Valves will be provided at all peaks in elevation of the proposed force main. These locations are listed in the table below and labeled on the appropriate plan and profile sheets.

Line	Station	Sheet
		of

Table 3 - Air Release/Vacuum Valves

- 18. The **final plans and technical specifications** are submitted for the TCEQ's review. Each sheet of the construction plans and specifications are dated, signed, and sealed by the Texas Licensed Professional Engineer responsible for the design on each sheet.
- 19. Attachment A Engineering Design Report. An engineering design report with the following required items is attached:
 - \boxtimes The report is dated, signed, and sealed by a Texas Licensed Professional Engineer.
 - Calculations for sizing system.
 - Pump head calculations, including, but not limited to, system head and pump capacity curves, head loss calculations, and minimum and maximum static head C values for normal and peak operational conditions.
 - \boxtimes 100-year and 25-year flood considerations.
 - igtriangleq Total lift station pumping capacity with the largest pump out of service.
 - Type of pumps, including standby units.
 - Type of pump controllers, including standby air supply for bubbler controllers, as applicable.

 \boxtimes Pump cycle time.

Type of wet well ventilation; include number of air changes for mechanical ventilation.

Minimum and maximum flow velocities for the force main.

- \boxtimes Lift station security.
- ☐ Lift station emergency provisions and reliability.

Administrative Information

- 20. Upon completion of the wet well excavation, a geologist must certify that the excavation was inspected for the presence of sensitive features and submit the signed, sealed, and dated certification to the appropriate regional office.
- 21. The TCEQ Lift Stations and Force Mains General Construction Notes (TCEQ-0591) are included on the General Notes Sheet of the Final Construction Plans for this lift station and/or force main system.
- 22. Submit one (1) original and one (1) copy of the application, plus additional copies as needed for each affected incorporated city, groundwater conservation district, and county in which the project will be located. The TCEQ will distribute the additional copies to these jurisdictions. The copies must be submitted to the appropriate regional office.
- 23. Any modification of this lift station/force main system application will require TCEQ approval, prior to construction, and may require submission of a revised application, with appropriate fees.

Signature

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This **Lift Station/Force Main System Application** is hereby submitted for TCEQ review and executive director approval. The system was designed in accordance with the requirements of 30 TAC §213.5(c)(3)(C) and 30 TAC Chapter 217, and prepared by:

Print Name of Licensed Professional Engineer: John Pelham, P.E.

Place engineer's seal here:

Date: 04/02/2024

Signature of Licensed Professional Engineer:



ATTACHMENT A – ENGINEERING DESIGN REPORT

A engineering design report is included with this application

February 23, 2024

Mr. John Pelham Garza EMC 7708 Rialto Blvd #125 Austin, Texas 78735



Re: Capstone Phase 2 Building AC09 Grease Waste System Ejector Pump Design Report 6900 W. Parmer Lane Austin, TX

John,

Please reference the attachments regarding the design for the (2) sets of duplex ejector pumps serving AC09 Kitchen Grease Waste. Included are the below items regarding the design and selection of the duplex pump systems for submission to TCEQ for review and approval.

- The relevant final plan plumbing sheets Enlarged Plan, Schedule & Detail. Sheets IP3.09, IP4.01 & IP7.02.
- Calculations for sizing system. Flow and pump head.
- Cutsheets of the selected equipment. Pumps with capacity curves and system head indicated and total lift station pumping capacity, pump controllers, pit basins, wastewater valve assemblies and removal system.

Please feel free to contact me if you have any questions or concerns.

Kevin Chadwick, P.E. Mechanical Engineer



Sincerely, Bay & Associates, Inc.

Capstone Phase 2 6900 W. Parmer Lane

Calculations

SSE-1 (Serving Grease Traps, GT-1 & GT-2) Total Fixture Units = 212 + 219 = 431 DFU 1 GPM is approximately equal to 2 DFU. This approximates to **215.5 GPM**

CITY OF AUSTIN GREASE TRAP SIZING - GT-1

QTY.	FIXTURE TYPE	TRAP SIZE	FIXTURE UNITS	TOTAL FIXTURE UNITS
2	3 COMP SINK (INDIRECT WASTE)	3"	6	12
0	2 COMP SINK (INDIRECT WASTE)	3"	6	0
4	DISHWASHER (HARD PIPED)	2"	4	16
4	PRE-RINSE SINK (INDIRECT WASTE)	4"	4	16
2	MOP SINK	3"	3	6
20	3" FLOOR DRAIN (EMERGENCY)	3"	3	60
34	3" FLOOR SINK (INDIRECT WASTE)	3"	3	102
				212

* 36 FLOOR SINKS OMITTED FROM GREASE CALC FOR RECEIVING CONDENSATE WASTE FROM KITCHEN EQUIPMENT, BEVERAGE SERVICES, WARMING WELLS, ETC . . .

	60
	102
	212
3	636
12	7,632
	TRAP SIZE = 10,000

TOTAL FIXTURE UNITS X 3 GPM = GREASE TRAP FLOW RATING GREASE TRAP FLOW RATING X 12 MINUTES = GREASE TRAP LIQUID HOLDING CAPACITY (GALLONS)

QTY.	FIXTURE TYPE	TRAP SIZE	FIXTURE UNITS	TOTAL FIXTURE UNITS
2	3 COMP SINK (INDIRECT WASTE)	3"	6	12
2	2 COMP SINK (INDIRECT WASTE)	3"	6	12
2	DISHWASHER (HARD PIPED)	2"	4	8
4	PRE-RINSE SINK (INDIRECT WASTE)	4"	4	16
1	MOP SINK	3"	3	3
30	3" FLOOR DRAIN (EMERGENCY)	3"	3	90
26	3" FLOOR SINK (INDIRECT WASTE)	3"	3	78
				219

CITY OF AUSTIN GREASE TRAP SIZING - GT-2

* 18 FLOOR SINKS OMITTED FROM GREASE CALC FOR RECEIVING CONDENSATE WASTE FROM KITCHEN EQUIPMENT, BEVERAGE SERVICES, WARMING WELLS, ETC . . . 78 219 3 657 12 7,884 TRAP SIZE = 10,000

TOTAL FIXTURE UNITS X 3 GPM = GREASE TRAP FLOW RATING GREASE TRAP FLOW RATING X 12 MINUTES = GREASE TRAP LIQUID HOLDING CAPACITY (GALLONS)

SSE-1 (Serving Grease Traps, GT-3 & GT-4) Total Fixture Units = 244 + 151 = 395 DFU 1 GPM is approximately equal to 2 DFU. This approximates to **197.5 GPM**

CITY OF AUSTIN GREASE TRAP SIZING - GT-3

QTY.	FIXTURE TYPE	TRAP SIZE	FIXTURE UNITS	TOTAL FIXTURE UNITS
2	3 COMP SINK (INDIRECT WASTE)	3"	6	12
0	2 COMP SINK (INDIRECT WASTE)	3"	6	0
2	DISHWASHER (HARD PIPED)	2*	4	8
2	PRE-RINSE SINK (INDIRECT WASTE)	4"	4	8
2	MOP SINK	3"	3	6
36	3" FLOOR DRAIN (EMERGENCY)	3"	3	108
34	3" FLOOR SINK (INDIRECT WASTE)	3"	3	102
				244

* 16 FLOOR SINKS OMITTED FROM GREASE CALC FOR RECEIVING CONDENSATE WASTE FROM KITCHEN EQUIPMENT, BEVERAGE SERVICES, WARMING WELLS, ETC . . .

TOTAL FIXTURE UNITS X 3 GPM = GREASE TRAP FLOW RATING GREASE TRAP FLOW RATING X 12 MINUTES = GREASE TRAP LIQUID HOLDING CAPACITY (GALLONS)

CITY OF AUSTIN GREASE TRAP SIZING - GT-4

QTY.	FIXTURE TYPE	TRAP SIZE	FIXTURE UNITS	TOTAL FIXTURE UNITS
2	3 COMP SINK (INDIRECT WASTE)	3"	6	12
0	2 COMP SINK (INDIRECT WASTE)	3"	6	0
2	DISHWASHER (HARD PIPED)	2*	4	8
2	PRE-RINSE SINK (INDIRECT WASTE)	4"	4	8
2	MOP SINK	3"	3	6
19	3" FLOOR DRAIN (EMERGENCY)	3*	3	57
20	3" FLOOR SINK (INDIRECT WASTE)	3"	3	60
				151

* 6 FLOOR SINKS OMITTED FROM GREASE CALC FOR RECEIVING CONDENSATE WASTE FROM KITCHEN EQUIPMENT, BEVERAGE SERVICES, WARMING WELLS, ETC . . .
 151

 3
 453

 12
 5,436

 TRAP SIZE = 10,000

732

TRAP SIZE = 10,000

8,784

3

12

TOTAL FIXTURE UNITS X 3 GPM = GREASE TRAP FLOW RATING GREASE TRAP FLOW RATING X 12 MINUTES = GREASE TRAP LIQUID HOLDING CAPACITY (GALLONS)

Nominal Pipe Size: 4"

			Steel Pipes S	chedule 40 -	Pressure Loss	- 4"		
	Flow		Vel	ocity		Pressure	Drop	
(m ³ /s)	(liter/s)	(US gpm)	(m/s)	(ft/s)	(Pa/100m)	(mmH ₂ O/100m)	(psi/100ft)	(ftH ₂ O/100ft)
0.0030	3.0	48	0.37	1.2	1649	168	0.073	0.168
0.0040	4.0	63	0.49	1.61	2814	287	0.124	0.29
0.0050	5.0	79	0.61	2.0	4214	430	0.186	0.43
0.0060	6.0	95	0.73	2.4	5805	592	0.26	0.59
0.0070	7.0	111	0.86	2.8	7901	806	0.35	0.81
0.0080	8.0	127	0.98	3.2	10319	1052	0.46	1.05
0.0090	9.0	143	1.1	3.6	12467	1271	0.55	1.27
0.01	10.0	159	1.22	4.0	15391	1569	0.68	1.57
0.011	11.0	174	1.35	4.4	18623	1899	0.82	1.9
0.012	12.0	190	1.47	4.8	22163	2260	0.98	2.3
0.013	13.0	206	1.59	5.2	24772	2526	1.09	2.5
0.014	14.0	222	1.71	5.6	28730	2930	1.27	2.9
0.015	15.0	238	1.84	6.0	32981	3363	1.46	3.4
0.016	16.0	254	1.96	6.4	37525	3826	1.66	3.8
0.017	17.0	269	2.1	6.8	42362	4320	1.87	4.3
0.018	18.0	285	2.2	7.2	47493	4843	2.1	4.8
0.019	19.0	301	2.3	7.6	52916	5396	2.3	(5.4)
0.02	20	317	2.4	8.0	58633	5979	2.6	6.0
0.03	30	476	3.7	12.0	125328	12780	5.5	12.8

• Inside Diameter: 0.102 m (4.0 inches)

5.4 ft of head / 100 ft pressure drop for 4" iron pipe. 600' of run to sanitary gravity connection. Pipe losses - $5.4 \times 6 = 32.4$ ' Elevation losses - 15'Total losses = 32.4 + 15 = 47.4' Add 20% for fitting losses = $47.4 \times 20\% = 56.88$ ft of head.

100 Year and 25 Year flood considerations:

The ejector pumps referenced in this report are being proposed entirely outside the 100year and 25-year floodplain. The lowest elevation of this system is at 856.00 ft, significantly outside of the 100-year flood elevation of 834.47 and 25-year flood elevation of 833.70.

Wet Well Ventilation:

The ejector pump basin is provided with a 4" vent line which routes back to the AC09 building and ties into the building sanitary vent system. The building sanitary vent is terminated to atmosphere at the roof level.

Security:

The traffic rated (H-20 Load Rating) access cover to the duplex ejector pump basin is provided with a locking device to prevent access from unauthorized personnel, as detailed on the attached equipment cut sheets. In addition, the location of the ejector pumps and basin is within a secured yard on the campus.









3 COMPARTMENT, GALLON CAPACITY 10,000, PRECAST CONCRETE, 8-IN TRAFFIC TOP, 24-IN DIAMETER MANHOLE FOR EACH COMPARTMENT, EXTENSIONS TO GRADE, TRAFFIC MANHOLE COVERS, BUTYL SEALS AT EACH JOINT, 5500 PSI CONCRETE. PROVIDE WITH CONCRETE SAMPLING WELL. PROVIDE WITH SAMPLE WELLS DOWNSTREAM OF TRAP. PARK USA # GT-10000-TXAU

CITY OF AUSTIN GREASE TRAP SIZING - GT-1

QTY.	FIXTURE TYPE	TRAP SIZE	FIXTURE UNITS		TOTAL FIXTURE UNITS
2	3 COMP SINK (INDIRECT WASTE)	3"	6		12
0	2 COMP SINK (INDIRECT WASTE)	3"	6		0
4	DISHWASHER (HARD PIPED) 2" 4				16
4	PRE-RINSE SINK (INDIRECT WASTE) 4" 4				16
2	MOP SINK 3" 3				6
20	3" FLOOR DRAIN (EMERGENCY) 3" 3				60
34	3" FLOOR SINK (INDIRECT WASTE)	3		102	
	·			212	
* 36 FLOC	R SINKS OMITTED FROM GREASE CAL	3	636		
CONDENSATE WASTE FROM KITCHEN EQUIPMENT, BEVERAGE SERVICES, WARMING WELLS, ETC					7,632
					TRAP SIZE = 10,000

TOTAL FIXTURE UNITS X 3 GPM = GREASE TRAP FLOW RATING GREASE TRAP FLOW RATING X 12 MINUTES = GREASE TRAP LIQUID HOLDING CAPACITY (GALLONS)

CITY OF AUSTIN GREASE TRAP SIZING - GT-2						
QTY.	FIXTURE TYPE	TRAP SIZE	FIXTURE UNITS		TOTAL FIXTURE UNITS	
2	3 COMP SINK (INDIRECT WASTE)	3"	6		12	
2	2 COMP SINK (INDIRECT WASTE)	3"	6		12	
2	DISHWASHER (HARD PIPED)	2"	4		8	
4	PRE-RINSE SINK (INDIRECT WASTE)	4"	4		16	
1	MOP SINK	3"	3		3	
30	3" FLOOR DRAIN (EMERGENCY)	3"	3		90	
26 3" FLOOR SINK (INDIRECT WASTE) 3" 3					78	
				219		
* 18 FLOO	R SINKS OMITTED FROM GREASE CAL	IVING	3	657		
CONDENSATE WASTE FROM KITCHEN EQUIPMENT, BEVERAGE SERVICES, WARMING WELLS, ETC					7,884	
	, - ,				TRAP SIZE = 10,000	

TOTAL FIXTURE UNITS X 3 GPM = GREASE TRAP FLOW RATING GREASE TRAP FLOW RATING X 12 MINUTES = GREASE TRAP LIQUID HOLDING CAPACITY (GALLONS)

CITY OF AUSTIN GREASE TRAP SIZING - GT-3 QTY. FIXTURE TYPE

QTY.	FIXTURE TYPE	TRAP SIZE	FIXTURE UNITS		TOTAL FIXTURE UNITS	
2	3 COMP SINK (INDIRECT WASTE)	3"	6		12	
0	2 COMP SINK (INDIRECT WASTE)	3"	6	0		
2	DISHWASHER (HARD PIPED)	2"	4		8	
2	PRE-RINSE SINK (INDIRECT WASTE)	4"	4		8	
2	MOP SINK 3" 3				6	
36	3" FLOOR DRAIN (EMERGENCY)	3"	3		108	
34	3" FLOOR SINK (INDIRECT WASTE)	3"	3		102	
					244	
* 16 FLOO	R SINKS OMITTED FROM GREASE CAL	C FOR RECE	IVING	3	732	
SERVICES	ATE WASTE FROM KITCHEN EQUIPME , WARMING WELLS, ETC	GE	12	8,784		
				TRAP SIZE = 10,000		

TOTAL FIXTURE UNITS X 3 GPM = GREASE TRAP FLOW RATING GREASE TRAP FLOW RATING X 12 MINUTES = GREASE TRAP LIQUID HOLDING CAPACITY (GALLONS)

CITY OF A	AUSTIN GREASE TRAP SIZING - GT-4				
QTY.	FIXTURE TYPE	TRAP SIZE	FIXTURE UNITS		TOTAL FIXTURE UNITS
2	3 COMP SINK (INDIRECT WASTE)	3"	6		12
0	2 COMP SINK (INDIRECT WASTE)	3"	6		0
2	DISHWASHER (HARD PIPED)	2"	4		8
2	PRE-RINSE SINK (INDIRECT WASTE)	4"	4		8
2	MOP SINK	3"	3		6
19	3" FLOOR DRAIN (EMERGENCY)	3"	3		57
20	3" FLOOR SINK (INDIRECT WASTE)	3"	3		60
					151
* 6 FLOOR	SINKS OMITTED FROM GREASE CALC	FOR RECEIN	/ING	3	453
SERVICES	SATE WASTE FROM KITCHEN EQUIPME S. WARMING WELLS. ETC	NI, BEVERA	GE	12	5,436
TRAP SIZE = 10,000					
TOTAL FIXTURE UNITS X 3 GPM = GREASE TRAP FLOW RATING					

GREASE TRAP FLOW RATING X 12 MINUTES = GREASE TRAP LIQUID HOLDING CAPACITY (GALLONS)

- 4" PUMPED WASTE LINE. REFER TO CIVIL FOR CONTINUATION AND POINT OF CONNECTION TO SITE SANITARY SEWER SYSTEM.



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	DOMESTIC BOILER (GAS) SCHEDULE										
	RK SERVES	LOCATION G	STORAGE	RECOVERY DATA		GAS DATA		ELECTRICAL DATA			
MARK			GALLONS	GALS/HOUR	TEMP. RISE °F	MBH INPUT AT 1/2 PSI	EFF.	KW	VOLTS	MANUFACTURER AND MODEL NUMBER	
GWH-1	KITCHEN	BOILER ROOM	-	2,375	100°	1,999	98%	-	208 V, 3 PH	LOCHINVAR AWH2000NPM	
GWH-2	KITCHEN	BOILER ROOM	-	2,375	100°	1,999	98%	-	208 V, 3 PH	LOCHINVAR AWH2000NPM	
GWH-3	KITCHEN	BOILER ROOM	-	2,375	100°	1,999	98%	-	208 V, 3 PH	LOCHINVAR AWH2000NPM	
GWH-4	KITCHEN	BOILER ROOM	-	2,375	100°	1,999	98%	-	208 V, 3 PH	LOCHINVAR AWH2000NPM	

<u>NOTES:</u>

1. PROVIDE QTY. 1 - EXPANSION TANK ET-1, ST-500-CL, 132 GALLON, 1-1/4" CONNECTION, PRECHARGED THERMAL EXPANSION ABSORBER, 150 PSI WORKING PRESSURE, SEAMLESS BLADDER, 240 DEGREE F. MAX WORKING TEMPERATURE. ADD OR REDUCE AIR PRESSURE IN BLADDER UPON STARTUP AS RECOMMENDED BY MANUFACTURER. PROVIDE WITH LOCHINVAR SMP3000 LONWORKS INTEGRATED SEQUENCING CONTROLLER. PROVIDE WITH CONDENSATE NEUTRALIZATION KITS. PROVIDE WITH BOILER PUMPS (2HP, 208V, 3 PH - EACH)

2. PROVIDE A SINGLE 1,250-GALLON INSULATED ASME STORAGE TANK ST-1 (LOCHINVAR #TVG2000J). REFER TO PLUMBING PLANS AND BOILER SCHEMATIC THIS SHEET FOR DETAIL.

3. UNIT SHALL COMPLY WITH THE STATE OF TEXAS LOW-NOX REQUIREMENTS.

4. ALL PLUMBING SUPPLIES, VALVES AND ASSOCIATED APPURTENANCES SHALL BE INSTALLED.

5. SET STORAGE SETPOINT TO 160°.

6. REFER TO MECHANICAL PLANS FOR SIZING AND ROUTING OF PVC INTAKE AND EXHAUST PIPING

7. COORDINATE EXACT MOUNTING LOCATION WITH ARCHITECTURAL. 8. COORDINATE POWER DISCONNECT LOCATION WITH ELECTRICAL AND ARCHITECTURAL.

9. HEATER INSTALLATIONS SHALL MEET OR EXCEED ALL CODE REQUIREMENTS, LOCAL AMENDMENTS AND MANUFACTURERS RECOMMENDATIONS AND REQUIREMENTS.

PUMP SCHEDULE									
MARK		TYPE	FLOW GPM		ELECTRICAL DATA				MANUFACTURER AND MODEL
WARK	JERVICE			FT. WG	HP	RPM	VOLTS	PH	NUMBER
HWRP-1	HOT WATER CIRC.	CENTRIFUGAL	20	40	1	3300	120	1	GRUNDFOS MAGNA1 40-180 (SPEE
HWRP-2	HOT WATER CIRC.	CENTRIFUGAL	20	40	1	3300	120	1	GRUNDFOS MAGNA1 40-180 (SPEEI

NOTES: 1. PROVIDE HWRP WITH 24-HR, 7-DAY TIMER CONTROLLER. INSTALL AQUASTAT ON RETURN ADJACENT TO LAST FIXTURE TAP.

HEAT TRACE SPECIFICATIONS

THERMON "FLX" SELF REGULATING HEATING CABLE, 120, 8 WATTS PER FOOT (SINGLE PASS ONLY). CONTRACTOR SHALL PROVIDE ALL JUNCTION BOXES, SPLICE KITS, STRAPS AND ASSOICIATED APPURTENANCES TO PROVIDE A COMPLETE AND WORKING SYSTEM. COORDINATE WITH ELECTRICAL.

THERMOSTATIC MIXING VALVE SCHEDULE							
MARK	DESIGN FLOW RATE (GPM)	PRESSURE DROP @ DESIGN FLOW RATE (PSI)	MINIMUM FLOW RATE (GPM)	MAXIMUM FLOW RATE (GPM)	MANUFACTURER AND MODEL NUMBER		
TMV-1	45	5	0.5	50	POWERS INTELLISTATION LFIS150VL-SYS200RTN		
TMV-2	1	5	0.5	1.5	AMERICAN STANDARD 605XTMV		

NOTES: 1. MINIMUM FLOW REQUIRED TO MAINTAIN TEMPERATURE CONTROL.

2. VALVE FINISH IS TO BE ROUGH BRONZE. <u>TMV-1</u> - TEMPERATURE RANGE 50°F TO 160°F. SET POINT 140°F.
 <u>TMV-2</u> - TEMPERATURE RANGE 50°F TO 120°F. SET POINT 105°F.

SEWAGE EJECTOR PUMP SCHEDULE (GREASE)										
MARK	SERVICE	TYPE	FLOW		E	ELECTRI	CAL DATA	L.	MANUFACTURER AND	
WARK	SERVICE		GPM	FT. WG	HP	RPM	VOLTS	PH	MODEL NUMBER	
	SEWAGE PUMP 1	SUBMERSIBLE SLICER	300	60	10	1750	460	3	WEIL 1634 SERIES	
55E-1	SEWAGE PUMP 2	SUBMERSIBLE SLICER	300	60	10	1750	460	3	WEIL 1634 SERIES	
1. SUM ENCI 2. SUM SHAI	P PUMPS SHALL BE (LOSURE AND 3-PHAS P PIT SHALL BE PRO LL BE INSTALLED AS	CONTROLLED BY A WEIL SE 460V MAIN CIRCUIT BR VIDED WITH FOUR (4) FLO FOLLOWS:	8151 SERIE EAKER OP OAT SWITC	ES DUPLEX TION. MOU THES AS INI	ALTERN INT CON DICATED	ATING CO TROL PAI	ONTROL I NEL ON A P PIT SEC	PANEL. F DJACENT CTION OR	ROVIDE WITH NEMA 3R WALL. RISER DIAGRAM. THEY	
1. SUM ENCI 2. SUM SHAI 2.1. 2.2. 2.3. 2.4.	P PUMPS SHALL BE (LOSURE AND 3-PHAS P PIT SHALL BE PRO LL BE INSTALLED AS THE BOTTOM OF THE A FLOAT SHALL BE IN WITH DECREASING W A FLOAT SHALL BE IN WITH INCREASING W	CONTROLLED BY A WEIL SE 460V MAIN CIRCUIT BR VIDED WITH FOUR (4) FLG FOLLOWS: E SUMP SHALL BE CONSII NSTALLED AT AN OPERAT VATER LEVEL. NSTALLED AT AN OPERAT (ATER LEVEL AND TURN (NSTALLED AT AN OPERAT	8151 SERIE EAKER OP DAT SWITC DERED ELE FING ELEV. OFF LAG PI FING ELEV.	ES DUPLEX TION. MOU HES AS INE V. 0'-0" OF 1'-0" (Ff OF 3'-0" (Ff JMP WITH E OF 4'-0" (Ff	ALTERN INT CON DICATED ROM BO ROM BO DECREAS ROM BO	ATING CO TROL PAI ON SUM ITOM OF ITOM OF SING WAT	ONTROL I NEL ON A P PIT SEC SUMP) A SUMP) A TER LEVE SUMP) A	PANEL. F DJACENT CTION OR ND SHAL ND SHAL L. ND SHAL	ROVIDE WITH NEMA 3R WALL. RISER DIAGRAM. THEY L TURN LEAD PUMP OFF L TURN LEAD PUMP ON	

4. PROVIDE ALL NECESSARY APPURTENANCES TO PROVIDE A COMPLETE AND WORKING AUTOMATIC DUPLEX SUMP PUMP SYSTEM.

5. PUMPS SHALL BE MOUNTED WITH WEIL 2613-2 REMOVAL SYSTEM AND 2616-2 VALVE ASSEMBLY.

6. PROVIDE SSE-1 WITH 30 SECOND DELAYED START UPON LOSS OF NORMAL SOURCE POWER.

7. PROVIDE WITH BASIN DIMENSIONS 16" X 5' DIAMETER.

	WATER 1	REATME	NT EQUIPMENT SCHEDULE
TAG	DESCRIPTION	MAKE/MODEL	SPECIFICATION
\\/T_1	RO WATER	CULLIGAN	(G2 5HE RO) 9,000 GALLONS PER DAY CENTRAL REVERSE OSMOSIS SYSTEM ON STEEL FRAME, 2 HP MOTOR - 208 V, 3 PHASE
vv 1	(KITCHEN HOT WATER) (PROVIDE 3 SYSTEMS TOTAL)	WATER TECHNOLOGIES	(HE 1.5 PF CF-21) HIGH CAPACITY, AUTOMATIC BACKWASHING, HIGH EFFICIENCY CARBON FILTRATION SYSTEM, 12 GPM @ 2 F PROVIDE WITH CULLIGAN SMART CONTROLLER, FLOW METER, ELECTRONIC BY-PASS, WATER DISCHARGE QUALITY METER CONNECTION TO BUILDING AUTOMATION SYSTEM. PROVIDE WITH D101 3880 PRESSURE STORAGE KIT.
			(FWR 360) DUAL STEEL BLADDER TANKS FOR RO SYSTEMS, 120 GALLON EACH,
			(WATTS PWIOCAL15) RE-MINERALIZATION SYSTEM
	RO WATER	CULLIGAN	(G2 5HE RO) 9,000 GALLONS PER DAY CENTRAL REVERSE OSMOSIS SYSTEM ON STEEL FRAME, 2 HP MOTOR - 208 V, 3 PHASE
VV 1-2	SYSTEM (CENTRAL FILTERED WATER)	WATER TECHNOLOGIES	(HE 1.5 PF CF-21) HIGH CAPACITY, AUTOMATIC BACKWASHING, HIGH EFFICIENCY CARBON FILTRATION SYSTEM, 12 GPM @ 2 F PROVIDE WITH CULLIGAN SMART CONTROLLER, FLOW METER, ELECTRONIC BY-PASS, WATER DISCHARGE QUALITY METER CONNECTION TO BUILDING AUTOMATION SYSTEM. PROVIDE WITH D101 3880 PRESSURE STORAGE KIT.
			(FWR 360) DUAL STEEL BLADDER TANKS FOR RO SYSTEMS, 120 GALLON EACH,
			(WATTS PWIOCAL15) RE-MINERALIZATION SYSTEM
NOTES:			

1. CONTRACTOR SHALL PROVIDE ALL EQUIPMENT AND ASSOCIATED APPURTENANCES REQUIRED TO PROVIDE A FULLY FUNCTIONING SYSTEM. 2. COORDINATE EXACT MOUNTING LOCATION WITH ARCHITECT.

3. INSTALLATIONS SHALL MEET OR EXCEED ALL CODE REQUIREMENTS, LOCAL AMENDMENTS AND MANUFACTURERS RECOMMENDATIONS AND REQUIREMENTS.

4. SYSTEM COMPONENTS SHALL BE RATED BY MANUFACTURER TO ACCOMMODATE A MAXIMUM WORKING PRESSURE OF 125-PSI. 5. ASSEMBLY SHALL BE INSTALLED WITH FULL SIZE BY-PASS.

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OSMOSIS SYSTEM ON STEEL FRAME, 2 HP MOTOR - 208 V, 3 PHASE SHING, HIGH EFFICIENCY CARBON FILTRATION SYSTEM, 12 GPM @ 2 PSI ETER, ELECTRONIC BY-PASS, WATER DISCHARGE QUALITY METER /IDE WITH D101 3880 PRESSURE STORAGE KIT. MS, 120 GALLON EACH,

				PLUMBING FIXTURE SCHEDULE						
TAG	DESCRIPTION	MOUNTING TYPE	MANUFACTURER	SPECIFICATION	ADA	BRAI UNLE CW		INECTION ERWISE N	I SIZE OTED VENT	P-TRA SIZE
BF-1	BOTTLE FILL	WALL A	FILTRINE B103 (AUTOMATIC SENSOR OPTION)	SELF CONTAINED, BARRIER FREE, LAMINAR FLOW, 8.0 GPH CAPACITY BOTTLE FILLING STATION. STAINLESS STEEL BASINS AND WALL PLATE CARRIER: CONCEALED FLOOR MOUNTED CARRIES. REFER TO ARCHITECTS DRAWINGS FOR EXACT LOCATION AND MOUNTING HEIGHT. PROVIDE APRONS IF REQUIRED BY TAS.	ADA	1/2"	-	1-1/2"	1-1/2"	1-1/4'
BFS-1	BOTTLE FILLING STATION	COUNTER	TOPBREWER TOPWATER SCANOMAT	COUNTER MOUNTED, 8" PEDESTAL WATER STATION, LAMINAR FLOW, GOOSENECK SPOUT, SENSOR OPERATED. STAINLESS STEEL BASIN	ADA	1/2"	-	1-1/2"	1-1/2"	1-1/4
DCV-1 DEW-1	BACKFLOW PREVENTER DECK MOUNTED EYE WASH	WALL	WATTS LF709-OSY SERIES HAWS 7610	4" DOUBLE CHECK BACKFLOW PREVENTER, REPLACEABLE SEATS AND DISCS, ISOLATION BALL VALVES. BARRIER-FREE DECK MOUNTED EYE / FACE WASH. 4.2 GPM. 13 INCH DROP DOWN LENGTH, POLISHED CHROME BRASS SINGLE ACTION PULL DOWN VALVE BODY. PROVIDE WTIH THERMOSTATIC MIXING VALVE, HAWS #9201EFE.	- ADA	- 1/2"	- 1/2"	-	-	-
EW-1	EMERGENCY EYE WASH	IN WALL UNITS	BRADELY S19-294HBT	CHROME-PLATED BRASS SPRAYHEAD, IN WALL STAINLESS STEEL CABINET WITH PULL DOWN DOOR, WATER PRESSURE RANGE 30-90 PSI. PUSH/PULL PIN OPERATION. PROVIDE EMERGENCY THERMOSTATIC MIXING VALVE ON HOT WATER SUPPLY TO FAUCET, NAVIGATOR MODEL S19-2000EFX8. MOUNT MIXING VALVE IN WALL ADJACENT TO FIXTURE SUPPLY STOPS WITH ACCESS PANEL, IN COMPLIANCE WITH IECC-2015.	-	1/2"	1/2"	-	-	-
WC-1	WATER COOLER	Z WALL	2 FILTRINE 107-16-HL	SELF CONTAINED, BARRIER FREE, DUAL LEVEL, SELF CLOSING PUSH BUTTON ON FRONT, SAFETY BUBBLERS, 8.0 GPH CAPACITY, AND BOTTLE FILLING STATION. STAINLESS STEEL BASINS AND WALL PLATE CARRIER: CONCEALED FLOOR MOUNTED CARRIES. REFER TO ARCHITECTS DRAWINGS FOR EXACT LOCATION AND MOUNTING HEIGHT PROVIDE APPRONS IF REQUIRED BY TAS	ADA	1/2"	-	1-1/2"	1-1/2"	1-1/4'
FCO	FLOOR CLEANOUT	FLOOR	JAY R. SMITH 4020 SERIES	CAST-IRON BODY, ABS GASKETED CLEANOUT PLUG, SATIN NICKEL BRONZE FLANGE AND COVER. TWO-PIECE, THREADED, ADJUSTABLE HOUSING FOR FLUSH INSTALLATION. PROVIDE WITH FLANGE WITH FLASHING CLAMPS (-F-C).	-	-	-	SEE PLANS	-	-
FD-1		FLOOR	JAY R. SMITH 2005-A SERIES	CAST IRON BODY, 6 INCH ROUND ADJUSTABLE NICKEL BRONZE STRAINER, FLASHING COLLAR WITH SEEPAGE OPENINGS, TAPPED FOR STRAINER HEAD, 1/2 TRAP PRIMER CONNECTION.	-	-	-	SEE PLANS	2"	SEE PLAN
FS-1	(BACK OF HOUSE) FLOOR SINK	FLOOR	2633 SERIES ZURN	12"X12"X8" RECEPTOR, SEDIMENT BUCKET, 3/4 SLOTTED GRATE, 1/2" TRAP PRIMER.	-	-	-	4"	2"	4"
FS-2	(KITCHEN)	WALL	Z1902 3M	AND TOP, TRAP PRIMER TO DIŚCHARGE INTO TOP OF DRAIN. 0.2 MICRO FILTER, TASTE/VOC/CYSTS/SCALE/IRON FILTER, 2.5-GPM FLOW RATE,	-	-	-	3"	2"	4"
GT-1 GT-2 GT-3	GREASE TRAPS	-	DSW160-L PARK USA # GT-10000-TXAU	450-GALLON, SHUT-OFF VALVE. 3 COMPARTMENT, GALLON CAPACITY 10,000, PRECAST CONCRETE, 8-IN TRAFFIC TOP, 24-IN DIAMETER MANHOLE FOR EACH COMPARTMENT, EXTENSIONS TO GRADE, TRAFFIC MANHOLE COVERS, BUTYL 2541 2 AT EACH COMPARTMENT, EXTENSIONS TO GRADE, TRAFFIC MANHOLE COVERS, BUTYL	-	-	-	- 4" GW	4"	-
GT-4 HB-1	HOSE BIBB	WALL	WOODFORD 24 SERIES	SEALS AT EACH JOINT, 5500 PSI CONCRETE. PROVIDE WITH CONCRETE SAMPLING WELL. ROUGH CHROME-PLATED BRASS HOSE BIBB, 3/4-IN FLANGED INLET, LOOSE KEY, VANDAL-RESISTANT, SELF-DRAINING VACUUM BREAKER, 3/4-IN MALE HOSE OUTLET.	-	3/4"	-	-	-	-
HD-1	HUB DRAIN	-	-	HUB DRAIN. FIELD FABRICATED 4-IN OR 6-IN DIAMETER HUB DRAIN FITTING, REDUCER WITH P-TRAP AND TRAP ARM, INDEPENDENTLY VENTED.	-	-	-	SEE PLAN	2"	SEE PLAN
LV-1	LAVATORY	SOLID SURFACE	BY ARCHITECT	SOLID SURFACE CORIAN COUNTER AND BASIN, INTEGRAL FRONT OVERFLOW, CLAMPS. FAUCET: LACAVA # EX11.35, PLUG-IN, <u>0.35 GPM AERATOR</u> , SENSOR ACTIVATED, BRASS CONSTRUCTION AND BRUSHED STAINLESS FINISH, SINGLE HOLE CENTER-SET, <u>FACTORY SET TIME OUT SETTING AT 30 SECONDS (LEED DEFAULT)</u> , AND NAVIGATOR MIXING VALVE. SUPPLY: MCGUIRE 2167 SERIES. LOOSE KEY WITH RISER, TRAP: MCGUIRE 8902 SERIES. CAST BODY WITH CLEAN-OUT. STRAINER AND TAILPIECE: MCGUIRE 155WC OFFSET TAILPIECE, OPEN GRID STRAINER. PROTECTIVE PIPE COVERS: TRUEBRO OR	ADA	1/2"	1/2"	1-1/2"	1-1/2"	1-1/4"
LV-2	LAVATORY	WALL	AMERICAN STANDARD DECORUM 9024.011EC	EQUAL. REFER TO ARCHITECTS DRAWINGS FOR EXACT LOCATION. 20-1/2"x27", VITREOUS CHINA, INTEGRAL FRONT OVERFLOW, HALF PEDESTAL. CARRIER: CONCEALED ARM, ZURN (OR EQUAL) FAUCET: LACAVA # EX11.35, PLUG-IN, <u>0.35 GPM AERATOR</u> , SENSOR ACTIVATED, BRASS CONSTRUCTION AND BRUSHED STAINLESS FINISH, SINGLE HOLE CENTER-SET, <u>FACTORY SET TIME OUT SETTING AT 30 SECONDS (LEED DEFAULT)</u> , AND NAVIGATOR MIXING VALVE. SUPPLY: MCGUIRE 2167 SERIES. LOOSE KEY WITH RISER. TRAP: MCGUIRE 8902 SERIES. CAST BODY WITH CLEAN-OUT. STRAINER AND TAILPIECE: MCGUIRE 155WC OFFSET TAILPIECE, OPEN GRID. PROTECTIVE PIPE COVERS: TRUEBRO OR EQUAL.	ADA	1/2"	1/2"	1-1/2"	1-1/2"	1-1/4"
MS-1	MOP SINK	FLOOR	ZURN Z1996-24 SERIES	CORNER 24 X 24-IN, ONE-PIECE, MOLDED HIGH DENSITY BASIN, 3-IN PVC DRAIN BODY, STAINLESS STEEL DOME STRAINER. FAUCET: ZURN Z1996-SF SERIES. INTEGRAL VACUUM BREAKER, PAIL HOOK, STOPS, WALL BRACE AND HOSE THREADED SPOUT. ACCESSORIES: HOSE AND HOSE BRACKET, MOP HANGER AND WALL GUARDS.	-	3/4"	3/4"	3"	2"	3"
PRV-1	PRESSURE RED.	-	WATTS	PRESSURE REDUCING VALVE. BRONZE BODY CONSTRUCTION, HIGH TEMP RESISTANT DIAPHRAGM, SPRING CAGE AND SEAT ORIFICE AND SEALED SPRING CAGE, INTEGRAL STAINLESS STEEL STRAINER. TRIM: PROVIDE FULL LINE-SIZE ISOLATION	-	SEE	_	-	-	-
RPZ-1	BACKFLOW PREVENTER	WALL	WATTS LF009QT-FS SERIES	VALVES, STRAINER AND UNIONS. PROVIDE FULL SIZE BY-PASS WITH ISOLATION VALVE. REDUCED-PRESSURE ZONE, LEAD FREE FULL LINE SIZE TWO CHECK VALVES, TEST COCKS, STRAINER, PRESSURE DIFFERENTIAL RELIEF VALVE, ISOLATION VALVES, FIXED AIR GAP FITTING. STRAINER SHALL BE PART OF RATED ASSEMBLY. PROVIDE WATTS SENTRY PLUS ALERT FLOOD PROTECTION AND DETECTION SYSTEM. PROVIDE WITH SENSOR AND AUTOMATED FLOOD PROTECTION SHUTDOWN VALVE, AND INTEGRATION TO BUILDING MANAGEMENT SYSTEM (BMS) FOR NOTIFICATION.	-	3/4"	-	-	-	-
SH-1	SHOWER	-	AMERICAN STANDARD BERWICK #TU430507	TILED SHOWER STALL BY SPECIFIED BY ARCHITECT. MIXING VALVE: PRESSURE-BALANCED, FLUSH-MOUNTED VALVE, ADJUSTABLE STOP SCREW, INTEGRAL STOPS, WALL FLANGE, ANCHOR PLATE, VANDAL RESISTANT. SHOWER HEAD: AMERICAN STANDARD BERWICK #TU430507 SHOWERHEAD, WALL-MOUNTED, ANGLED ARM, <u>1.75 GPM FLOW RATE</u> . DRAIN: INFINITY DRAIN #S-TIF 6596 LINEAR DRAIN, FRAMELESS TILEABLE COVER. ARCHITECT TO GIVE FINAL APPROVAL OF GRATE	-	1/2"	1/2"	-	-	-
SH-2	SHOWER	-	AMERICAN STANDARD BERWICK #TU430507 (TRIM ONLY)	DESIGN TYPE. TILED SHOWER STALL BY SPECIFIED BY ARCHITECT. BARRIER-FREE ADA COMPLIANT MIXING VALVE: PRESSURE-BALANCED, FLUSH-MOUNTED VALVE, ADJUSTABLE STOP SCREW, INTEGRAL STOPS, WALL FLANGE, ANCHOR PLATE, VANDAL RESISTANT. SHOWER HEAD: KOHLER AWAKEN #G110 HAND SHOWERHEAD, W/ SLIDEBAR, ANGLED ARM, <u>2.0 GPM FLOW RATE.</u> DRAIN: INFINITY DRAIN #S-TIF 6596 LINEAR DRAIN. FRAMELESS TILEABLE COVER. ARCHITECT TO GIVE FINAL APPROVAL OF GRATE.	ADA	1/2"	1/2"	-	-	-
(TD-1	KITCHEN TRENCH DRAIN	FLOOR	JAY R. SMITH 9660 SERIES	DESIGN TYPE. 6" WIDE MODULAR STAINLESS STEEL TRENCH DRAIN WITH BUILT IN SLOPE, PROVIDE WITH SECURED LIGHT DUTY STAINLESS STEEL GRATE. PROVIDE FITTINGS, PLUGS, OUTLETS AND CLEANOUTS AS REQUIRED. SHALLOW INVERT = 6 IN CONTRACTOR SHALL COORDINATE REQUIRED LENGTH WITH KITCHEN CONSULTANT EQUIPMENT PLANS.	-	-	-	4"	-	-
TD-1	TRENCH DRAIN (RESTROOMS)	FLOOR	SCHLUTER KERDI-LINE	3" WIDE X 43" LONG PER DRAIN SECTION. COORDINATE FINAL PROCURED DRAIN SECTION LENGTHS WITH DIMENSIONED ARCHITECTURAL PLANS. FRAMELESS TILEABLE COVER. ARCHITECT TO GIVE FINAL APPROVAL OF GRATE DESIGN TYPE AND FINISH. PROVIDE FITTINGS, PLUGS, OUTLETS AND CLEANOUTS AS REQUIRED.	-		-	3"	2"	-
TD-2	TRENCH DRAIN (LOCKER ROOMS)	FLOOR	INFINITY DRAIN FFST #	304L STAINLESS STEEL LINEAR SLOT DRAINS. COORDINATE FINAL PROCURED DRAIN SECTION LENGTHS WITH DIMENSIONED ARCHITECTURAL PLANS. TILE INSERT CLEAN OUT. ARCHITECT TO GIVE FINAL APPROVAL OF GRATE DESIGN TYPE AND FINISH. PROVIDE FITTINGS, PLUGS, OUTLETS AND CLEANOUTS AS REQUIRED.	_	-	_	3"	2"	-
SK-1	SINK (BREAK ROOM)	SOLID SURFACE	BY ARCHITECT	SOLID SURFACE CORIAN COUNTER AND BASIN, INTEGRAL FRONT OVERFLOW, CLAMPS, ADA COMPLIANT. FAUCET: MOEN - ALIGN 7365 (NO BASEPLATE, BRUSHED SATIN FINISH). LEDGE-MOUNTED, 8-INCH CENTER-SET ESCUTCHEON, SINGLE LEVER HANDLES, 8-INCH GOOSENECK SPOUT, 1.5 GPM FLOW RATE. MCGUIRE 2167 SERIES. TRAP: MCGUIRE 8912 SERIES. STRAINER AND TAILPIECE: MCGUIRE 151 SERIES. BASKET TYPE. SOAP DISPENSER: MOEN - # S3947SRS. PROVIDE BREAK SINKS AND ADJACENT ICUP COFFEE MAKER WITH FLOOD STOP LEAK DETECTION: ONSITE PRO INC. FS38CD SINK KIT. KIT INCLUDES HOT & COLD MOTORIZED BALL VALVES, BATTERY POWERED CONTROL UNIT (UNDER COUNTER), SENSOR BOARD AND PIGTAIL FOR INTEGRATION TO BUILDING MANAGEMENT SYSTEM (BMS).	ADA	1/2"	1/2"	2"	1-1/2"	1-1/2'
SK-2	SINK (PHARMACY)	UNDERMOUN	STERLING UCL1515	18-GAUGE, SOUND PADS UNDERCOAT, STAINLESS STEEL, SINGLE-BOWL, THREE FAUCET HOLE, OFF-CENTER DRAIN, ADA COMPLIANT, 3-1/2-INCH OUTLET. FAUCET: LACAVA. #EX11.5 (0.5 GPM) DECK-MOUNTED, ESCUTCHEON, TOUCH FREE ELECTRONIC FAUCET, PLUG-IN, 6-3/4-INCH GOOSENECK SPOUT. SUPPLY: MCGUIRE 2167 SERIES. TRAP: MCGUIRE 8912 SERIES. STRAINER AND TAILPIECE: MCGUIRE 151 SERIES. BASKET TYPE.	ADA	1/2"	1/2"	2"	1-1/2"	1-1/2
SK-3	SINK (VISION)	COUNTER	ELKAY LRAD1919-3	18-GAUGE, SOUND PADS UNDERCOAT, STAINLESS STEEL, SINGLE-BOWL, THREE FAUCET HOLE, OFF-CENTER DRAIN, ADA COMPLIANT, 3-1/2-INCH OUTLET. FAUCET: LACAVA. #EX11.5 (0.5 GPM) DECK-MOUNTED, ESCUTCHEON, TOUCH FREE ELECTRONIC FAUCET, PLUG-IN, 6-3/4-INCH GOOSENECK SPOUT. SUPPLY: MCGUIRE 2167 SERIES. TRAP: MCGUIRE 8912 SERIES. STRAINER AND TAILPIECE: MCGUIRE 151 SERIES. BASKET TYPE.	ADA	1/2"	1/2"	2"	1-1/2"	1-1/2
SK-4	SINK (DENTAL - BACK OF HOUSE)	COUNTER	ELKAY LRAD1919-3	18-GAUGE, SOUND PADS UNDERCOAT, STAINLESS STEEL, SINGLE-BOWL, THREE FAUCET HOLE, OFF-CENTER DRAIN, ADA COMPLIANT, 3-1/2-INCH OUTLET. FAUCET: LACAVA. #EX11.5 (0.5 GPM) DECK-MOUNTED, ESCUTCHEON, TOUCH FREE ELECTRONIC FAUCET, PLUG-IN, 6-3/4-INCH GOOSENECK SPOUT. SUPPLY: MCGUIRE 2167 SERIES. TRAP: MCGUIRE 8912 SERIES. STRAINER AND TAILPIECE: MCGUIRE 151 SERIES. BASKET TYPE.	ADA	1/2"	1/2"	2"	1-1/2"	1-1/2
SK-5	SINK (EXAM ROOM)	SOLID SURFACE	BY ARCHITECT	SOLID SURFACE CORIAN COUNTER AND BASIN, INTEGRAL FRONT OVERFLOW, CLAMPS, ADA COMPLIANT. FAUCET: LACAVA. #EX11.5 (0.5 GPM) DECK-MOUNTED, ESCUTCHEON, TOUCH FREE ELECTRONIC FAUCET, PLUG-IN, 6-3/4-INCH GOOSENECK SPOUT. SUPPLY: MCGUIRE 2167 SERIES. TRAP: MCGUIRE 8912 SERIES. STRAINER AND TAILPIECE: MCGUIRE 151 SERIES. BASKET TYPE.	ADA	1/2"	1/2"	2"	1-1/2"	1-1/2
TP-1	TRAP		JAY R. SMITH	CHROME PLATED CAST BRASS P-TRAP, TAILPIECE TYPE TRAP PRIMER, 1/2-IN PRIMER TUBE WITH COMPRESSION FITTING,	-	1/2"	-	-	-	
TP-2	TRAP PRIMER	-	PPP PRIME-TIME	SURFACE MOUNTED ELECTRONIC TRAP PRIMER PT-# (# BASED ON NUMBER OF DRAINS SERVED), NEMA TYPE 1 ENCLOSURE, 14"X16"X" - 16 GAUGE STEEL W/ SCREW ON COVER, 120V 1PH POWER CONNECTION, 3/4" FEMALE NPT INLET, 1/2" FEMALE NPT	-	3/4"	-	-	-	-
UR-1	URINAL	WALL	SLOAN SU-7009	VITREOUS CHINA, SIPHON JET ACTION, 3/4-IN TOP SPUD, BOLT CAPS, INTEGRAL TRAP. VANDAL RESISTANT OUTLET STRAINER. FLUSH VALVE: TOTO - TEU1UAX#CP (RECLAIMED WATER), SENSOR ACTIVATED, ECOPOWER, HIGH EFFICIENCY (0.125 GPF).	ADA	3/4"	-	2"	2"	-
UR-2	URINAL	WALL	SLOAN SU-7009	CARRIER: SMITH 0637 SERIES. VITREOUS CHINA, SIPHON JET ACTION, 3/4-IN TOP SPUD, BOLT CAPS, INTEGRAL TRAP. VANDAL RESISTANT OUTLET STRAINER. FLUSH VALVE: TOTO - TEU1UAX#CP (RECLAIMED WATER), SENSOR ACTIVATED, ECOPOWER, HIGH	-	3/4"	-	2"	2"	-
WB-1	WALL BOX	WALL	IPS WATER-TITE SERIES	CARRIER: SMITH 0637 SERIES. MOUNTING HEIGHT OF URINAL AND FLUSH VALVE SHALL BE ADA COMPLIANT. ANGLE STOP WALL BOX, WITH 1/4 TURN ANGLE STOP, INTEGRAL WATER HAMMER ARRESTERS. FRONT FLANGE.	-	1/2"	-	-	-	-
WC-1	WATER CLOSET	WALL	TOTO CT728CU	VITREOUS CHINA, ELONGATED RIM, SIPHON JET ACTION, 1-1/2-IN TOP SPUD, 1.28 GAL FLUSH, BOLT CAPS, INTEGRAL TRAP. SEAT: TOTO - SC534. OPEN-FRONT SEAT WITHOUT COVER. FLUSH VALVE: TOTO - TET1LAX#CP (RECLAIMED WATER) SENSOR ACTIVATED, ECOPOWER, HIGH EFFICIENCY FLUSH VALVE (1.28 GPF).	-	1"	-	4"	2"	-
WC-2	WATER CLOSET	WALL	TOTO CT728CU	CARRIER: JR SMITH OR EQUAL. VITREOUS CHINA, ELONGATED RIM, SIPHON JET ACTION, 1-1/2-IN TOP SPUD, 1.28 GAL FLUSH, BOLT CAPS, INTEGRAL TRAP. SEAT: TOTO - SC534. OPEN-FRONT SEAT WITHOUT COVER. FLUSH VALVE: TOTO - TET1LAX#CP (RECLAIMED WATER) SENSOR ACTIVATED, ECOPOWER, HIGH EFFICIENCY FLUSH VALVE (1.28 GPF). CARRIER: JR SMITH OR EQUAL.	ADA	1"	-	4"	2"	
wco	WALL CLEANOUT	WALL	-	MOUNTING HEIGHT OF WATER CLOSET AND FLUSH VALVE SHALL BE ADA COMPLIANT. MOUNT FLUSH VALVE HANDLE TOWARD "WIDE" SIDE OF ADA COMPLIANT STALL. COORDINATE FLUSH VALVE MOUNTING HEIGHT WITH GRAB BAR. TAPPED CLEANOUT TEE, EXTRA-HEAVY, THREADED, SOLID HEXAGONAL NUT. CLEANOUTS IN HUBS OF COMBINATION WYE AND 1/8-BENDS OR WYES: TAPPED SPIGOT. CLEANOUTS AT ENDS OF HUBLESS COMBINATION WYE AND 1/8-BENDS OR WYES: BLIND PLUG. COVERS OVER CLEANOUTS IN CONCEALED VERTICAL PIPING (ALL AREAS, FINISHED AND UNFINISHED): SQUARE FRAME WITH SECURED, SMOOTH, SATIN NICKEL BRONZE ACCESS COVER. OPENING SIZES: 4-IN AND SMALLER PIPING: 6 X 6-IN. LARGER THAN 4-IN PIPING: 8 X 8-IN. CERAMIC TILE, QUARRY TILE, STONE, RESILIENT TILE, AND SHEET: FACE FLANGE TO HIDE ROUGH WALL OPENING. SMITH 4430 SERIES. TERRAZZO AND CONCRETE (FINISHED AREAS): PLASTER GROUND FLANGE AND FLUSH-WITH-WALL FRAME. SMITH 4431 SERIES	-	-	-	-	-	-
WH-1	WALL HYDRANT	WALL	WOODFORD B67 SERIES	ANTI-SIPHON FREEZE-LESS WALL HYDRANT. CHROME FINISH WITH ANTI-SIPHON VACUUM BREAKER WITH 3/4" MALE HOSE THREAD. HARDENED STAINLESS STEFL STEM WITH LOOSE TEE KEY OPERATOR. CONCEALED BOX TYPE	-	3/4"	-	-	-	-
WH-2	WALL HYDRANT	WALL	JAY R. SMITH 5518-R	NARROW BODY WALL HYDRANT. CHROME FINISH WITH ANTI-SIPHON VACUUM BREAKER WITH 3/4" MALE HOSE THREAD. HARDENED STAINLESS STEEL STEM WITH LOOSE TEE KEY OPERATOR, CONCEALED BOX TYPE.		3/4"	<u> </u>	<u> </u>	<u> </u>	-
										\sim







PROVIDE WATER

PROVIDE AIR TIGHT ACCESS COVER





DUPLEX CONTROL PANEL, DISCONNECT, ~

AND ALARM

WATER HAMMER-







-UP TO 20'-

- FLUSH VALVE

URINA

- 3/4"CW



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COLD WATER MAIN —



NOTE: SEE PLAN AND SCHEDULES FOR FIXTURE TYPES 3 CHASE WALL SECTION - LAVATORIES (BACK TO BACK) Scale: NONE



6 TYPICAL MASTER DISTRIBUTION MIXING VALVE WITH CIRCULATING PUMP Scale: NONE



10 TYPICAL HOT WATER RETURN BALANCING VALVE Scale: NONE





System: SSE-1,2

TI Build-Out

Pump

Quantity 2 of Model 2524 Submersible Quick Removal Mounted Slicer Pump, 4-inch discharge, for up to 2-inch solids, with a 15 HP 1750 RPM 3 PH 460 V 60 HZ motor.

Details

- *Design Flow (GPM per Pump): 300
- *Flow (GPM per Pump): 300
- *Head (TDH in Feet): 60
- Impeller Trim: 894
- Lifting Cable Length: 20 FT
- Power Cable Length: 40 FT
- Quantity: 2

Options

- Option (3): Extra Power Cable
- Option (3): Extra Sensor Cable
- Option (1): Sensors Moisture and Temp Limiter
- Option (1): Stainless Steel Lift Cable (20ft)

Pump Accessory

Quantity 1 of Model 2613 Sub Base. Order Number 2613K501. Galvanized steel sub base for a duplex set of 2 inch 2613 removal systems.

Details

• Quantity: 1

Pump Accessory

Quantity 1 of Model 2613-4. Order Number 2613K7023. Two removal systems for a duplex set of 4 inch pumps, with cast iron sliding brackets and a duplex BCB upper guide pipe bracket (for discharge pipe mounting).

Details

• Quantity: 1

Options

- Option (1): 205.666.001 Intermediate Guide Pipe Brackets
- Option (1): 2613K204 Discharge Flange Kits
- Option (1): 2613K801 Level Control Lifting Assembly

Pump Accessory

Quantity 1 of Model 2616-4. Order Number 2616K1023B. Duplex wastewater valve assembly, 4 inch.

Details

• Quantity: 1

Level Control

Quantity 4 of Model 8233. Order Number 8233K1014. Single pole tethered float switch with cord grip and 40ft cord length.

Details

• Quantity: 4

Level Control Accessory

Quantity 1 of Model 8200 Mounting Pipe. Order Number 303.935.103. 1 inch schedule 40 mounting pipe, 10 feet long, threaded on one end.

Details

Control Panel

Quantity 1 of Model 8151 Duplex Control Panel in a Type 4X GRP enclosure for use with 3 phase 208-230/460 volts motor(s) drawing between 20 and 25 amps each. Order Number 8151-T-250.

Details

- Quantity: 1
- Voltage: 460

Options

- Option (1): 8100K7102 HWA Dome Light (Type 4X)
- Option (1): 8100K7111 Larger Enclosure (Type 4X)
- Option (1): 8100K7224D Moisture Sensor / Temp Limiter Feature

/ H. II.

Duplex Submersible Pump

S-9016

2613 Removal System - Discharge Below Cover 2616 Valve Assembly Below Cover

Date: _____January 22, 2024



Weill Pump Company Inc.

ETT,

6-Inch Submersible Wastewater Pump

UL/CUL Explosion Proof Motor

Additional Power Cable Lengths

Flow - To prevent

solids from settling out

Minimum

Flow GPM

90

200

Stainless Steel Lifting Cable

Discharge

Pipe Size

Dia Inches

4

6

575 Volt 3 Phase 60hz Motor



Heavy duty pump for commercial and industrial applications. Pump clear water, gray water, effluent and wastewater with solids up to 3 inch diameter.

Options

Bronze Impeller

Moisture Sensor and

Temperature Limiter

2524

Dis	ch. S	ize	6 Inch
Dis	ch. T	уре	ANSI
Soli	ds M	lax.	3 Inch

Mounting Style 2613 Removal

Capaci	ties - Wet Wells						
Dia or Side	Gallons per Foot of Depth						
Inches	Round	nd Square					
48	94	120					
60	147	187					
72	212	269					



Maximum 10 starts per hour. Minimum run time - 1 1/2 minutes.





Pump Case - Cast Iron Impeller - Cast Iron Stainless Steel Hardware

Motor

Double Seal - Tandem

- Upper Carbon against Ceramic
- Lower Silicon Carbide against
- Silicon Carbide **Air-Filled Hermetically Sealed** Shaft - Stainless Steel Series 300 Motor Shell - Cast Iron Insulation - Class F Ball Bearings - 2 - Double Sealed Power Cable Length - 25 ft Three-phase motor
- 1150 and 1750 RPM
- 60 Hz, 230 or 460 volts



Replaces SN-2524, JULY 1, 2015

SN-2524-A-4

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Duplex Alternating Pump Control Panel

Single-Phase or Three-Phase - U/L Type 1 or 4XFRP

• The 8151 Duplex Panel controls two pumps. It is a customer full featured panel that includes a high water alarm system, alternator, and a lockable through-the-door disconnect. · Panel can be operated on 50 or 60 Hertz power.

- · Select level controls
 - 8213 Mechanical Lever (not shown)
 - 8220 Pressure Diaphragm (not shown)
 - 8230 Tethered



8230 Tethered



	Motor		Order Number		Approx.
	Protector Amp Range	Single-Phase 115 Volts	Single-Phase 208 or 230 Volts	Three-Phase 208, 230, 460 Volts	Weight Lbs.
1	1.0 - 1.6	8151-L-016	8151-D-016	8151-T-016	55
	1.6 - 2.5	8151-L-025	8151-D-025	8151-T-025	55
	2.5 - 4.0	8151-L-040	8151-D-040	8151-T-040	55
	4.0 - 6.3	8151-L-063	8151-D-063	8151-T-063	55
	6.3 - 10.0	8151-L-100	8151-D-100	8151-T-100	56
	10.0 - 16.0	8151-L-160	8151-D-160	8151-T-160	56
	16.0 - 20.0	8151-L-200	8151-D-200	8151-T-200	57
	20.0 - 25.0	-8151-L-250	8151-D-250	8151-T-250	57
-	*25.0 - 32.0	8151-L-320	8151-D-320	8151-T-320	72
	*32.0 - 40.0	8151-L-400	8151-D-400	8151-T-400	72
	*40.0 - 50.0	8151-L-500	8151-D-500	8151-T-500	74

^{*} Includes two disconnects and larger enclosure

How to Order: Specify Order Number, System Phase, Voltage, Pump HP, Motor Amps and any options.

F.O.B. Cedarburg (Milwaukee), Wisconsin

Replaces June 12, 2020

SN-8151

May 20, 2022

Panel Includes:

- U/L Listed Label.
- · LED Lights, hour meter, switches and test buttons are mounted on door.
- One lockable panel disconnect through-the-door with door interlock. The mechanical interlock prevents the door from being opened when the disconnect is in the ON position. Lock is not provided.
- · Padlocking hasp on door, padlock not included.
- · Two lockable pump disconnects, on motor overload protectors. Lock is not provided.
- Electric Alternator has a 3 position selector switch; that locks the pumps in Auto, Pump 1-2 or Pump 2-1 sequencing.
- Two
- Contactors industrial duty.
 - Two Overloads Ambient compensated bi-metallic (class 10) motor overloads circuit protector. Instantaneous magnetic trip for short circuit protection. Single-phase protection for three phase motors. Field adjustable within the amp range.
 - · Control transformer, with fused primary and fused secondary on all three phase and single phase 208 and 230 volt. Single phase 115 volt has a fused control circuit.
 - Pump Run Switches Three position TOA (Test-Off-Automatic) with spring return to off from test. One per pump.
- · Green light on the door indicates power to pump motors.
- · White light on the door indicates control power on.
- High Water Alarm System, Type 4X. Hold finger over hole of horn for 1-2 seconds and remove to silence horn (95 dB).
 - Red HWA light and test button on the door.
 - Two isolated contacts for remote monitoring and or to use as a connection to a phone dialer.
- · Control terminal board, numbered and wired.
- · Layout and schematic CAD diagrams are provided. Installer connections at terminal board are clearly marked.

Control Panel Selection Guide - Determine Phase and Voltage

- Determine maximum run current in
- amps required by the pump motor.
- -Determine Enclosure Type,
- 1 or 4XGRP

WEIL

Duplex Alternating Pump Control Panel

Single-Phase or Three-Phase - U/L Type 1 or 4XFRP

Options:

		Options.
	8100K7037:	Motor Overload - per pump. Red light on door indicates motor overload condition and pump is off. Light remains
	00001/2022	on and pump remains off until manually reset.
	8000K/0/5:	Additional final disconnect (manual disconnect.
V	8000K/0/0:	Additional fused disconnect (second disconnect).
6	0100K/055;	HWA Dome Light - Type 1 - Lexan, red flashing, on top of panel. Light remains on until condition is corrected.
	8100K/102: 9100K7105	Hour meter, per nump. Non resetting meter indicates total nump run time, mounted on floor
	8100K7105.	Oty 1 soft starter for gentle ramp up/ramp down of an electric motor. A diustable from 0-20 second ramp time
	0100183000.	Provides for enhanced motor life and systems operation (One required per motor)
	OPTIONS, I	Provides for enhanced motor me and systems operation. (One required per motor)
-	OPTIONS: F	cequiring a Larger Enclosure when more than one (1) of the following is ordered:
	8100K7024:	Isolated contact. Can be used for Building Management Service monitor. Closure indicates monitor condition (dry
	8100K7031+	Lighting Arrestor Surge Protection for panel components
	8100K7031;	Digning Arrestor - Surge Protection for panel components.
	8100K7107-3.	Circuit Breaker - 3 nole inside enclosure May 30 amp breaker per nump
	8100K7109-3.	Euse Block - 3 pole for type "LP-CC" Fuses Max 30 amp fuses per pump.
	ODTIONS, F	Tuse block - 5 poie for type - Er -Co - Fuses, Max 50 amp fuses per pump, Fuses not metaded.
	OPTIONS: F	cequiring a Larger Enclosure:
	8100K7074:	Disconnect Switch. One additional through-the-door with interlock.
	8100K7222D:	Moisture Sensor circuit - for duplex set of pumps with 9712, 9725 motors only. Moisture sensor relay and tetst
		buttons. Two amber lights indicate moisture in pump motor.
1	8100K7224D:	Moisture Sensor and Temperature limit Circuits - for duplex set of pumps with standard Non Explosion Proof
		Motors (9706, 9709, 9727).
		- Moisture sensor relay and test buttons. Two amber lights indicate moisture in the pump motor.
		- Temperature limiter circuit shuts down pump motor when motor over temperature is sensed. Automatic reset
		when the motor temperature falls to motors normal operating range. Two blue lights indicate motor over
	After dollars	for Larger Enclosure:
1	8100K7110:	Larger 24H x 20W x 6D type 1 enclosure adder.
-	8100K7111:	Larger 24H x 20W x 8D type 4X GRP enclosure.
	8100K2001:	BACnet Option (through gateway).
	8100KXXXX:	Anti-Condensation Heater with adjustable thermostat control.
	8000KXXXX:	ISR Circuits - Provides a low output voltage for level control switches and maintains UL compliant spacing of
	9000KXXXX.	Components.
	QUUNKAAAA.	Clear cover gasketed and lockable for mounting over door face components
	8100KXXXXX	Digital basin level display (requires 826X level sensor)
	STOOKXXXX.	Motor soft starter/soft stop
	8100KXXXX	Panel Floor Mount Kit (Riser)
	8100KXXXX	Convenience recentacle - 120V duplex - interior (120V + other)
	8100KXXXX	Hand-off-auto in lieu of test-off-auto for pump switches.
	8100KXXXX	4" NEMA 4X Bell in lieu of horn.
	8100KXXXX:	Time delay circuit - non-simultaneous start
	8100KXXXX:	Exercise timer circuit
	8100KXXXX:	Low level alarm light and 150 contact.
	8100KXXXX:	Alternate light colors to standard.
	na ana ana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana dia mampiasa amin'ny	

How to Order: Specify Order Number, System Phase, Voltage, Pump HP, Motor Amps and any options. F.O.B. Cedarburg (Milwaukee), Wisconsin



WEIL PUMP A WILO COMPANY

GND 1/16/2017

WEIL WI 4/27/2021 5:35 AM H8151-T1-11 Schematic 3-Phase .dwg





6-Inch ANSI - 6 Inch Solids

The 2616-6 Valve Assmbly has the check valve and isolation valve requirements for a duplex pumping system combined into one unit.

The 2616-6 cast iron assembly consists of two check valves and one four-way isolation valve.

The check valve ball is ground to close spherical tolerances which assures positive sealing at low back pressures.

The low friction, easy to operate four-way valve is marked to locate each of the four positions. The valve is lockable in any of the four positions. The assembly has standard ANSI B61 iron 125 PSI flanges and standard 32-inch spacing.

Use with submersible pumps and 2613 Removal System.

2616-6 Includes

- 2 90 degree Ball Check Valves
- 1 4-way Isolation Valve
- 1 Lockable Handle



The 2616-6 Isolation Valve has four positions:



Discharge Normal Operation Pump A And Pump B Open To Discharge Line



Discharge Pump A Isolated Pump B Open To Discharge Line



Discharge Pump B Isolated Pump A Open To Discharge Line

Position 4



Discharge Discharge Line Blocked To Both Pump A And Pump B

Model	Disch.	Disch. Mount	Wt. Lbs.
2616K1063	6-Inch	90 degrees	450

SN-2616-6

November 23, 2022

WEIL Duplex Wastewater Valve Assembly 2616-6

6-Inch ANSI - 6 Inch Solids

charge is below cover.

Install check valves upright.

A valve box compartment could be eliminated when the dis-

Field installation cost is greatly reduced. Space

requirements are the same as two elbows and one tee.

In a typical duplex wastewater discharge piping arrangement the 2616 assembly replaces the following components:

- * 4 Elbows
- * 1 Tee
- * 2 Check Valves
- * 2 or 3 Isolation Valves





Intermediate Guide Pipe Bracket:

205.666.001 Intermediate Guide Pipe Bracket

Replaces June 12, 2020

System Includes:

- Discharge Floor Elbow one
- Sliding Bracket one
- Iron or
- Bronze for use with Explosion Proof Motors
- 316 Stainless Steel
- Guide Pipe Bracket one
- A Flat (cover mount) bolts to wet well cover or
- B Angle 90° (side mount) bolts to vertical side wall or
- C BCB Bracket Duplex or Simplex mounts to discharge pipe(s) see pg 2 diagrams
- Not Included:
- Discharge Pipe. Guide Pipe 2 inch schedule 40 & Flange Kit
- **Options:**
 - Discharge Flange Kit for Floor Elbow
 - Intermediate Guide Pipe Bracket
 - · Sub Base for Floor Elbow
 - · Level Control Lifting Assembly for BCB Duplex Bracket
- Removal System:

Simplex							
Order Number	Sliding Bracket	Guide Pipe Bracket	Mount Type	Wt Lbs			
2613K1024	Iron	Flat	Cover	196			
2613K5014	Iron	Angle	Side	196			
2613K2024	Bronze	Flat	Cover	196			
2613K6035	Bronze	Angle	Side	196			
2613K3024	Iron	BCB	Pipe	196			
2613K4024	Bronze	BCB	Pipe	196			



July 12, 2023

2613-6



BCB - Simplex

HALLIDAY PRODUCTS, INC.

ORLANDO, FL

LOCKING DEVICE

THIS SIDE

http://www.hallidayproducts.com

3/4

DRAIN LOCATION

LIFTING HANDLE

(CLEAR OPENING = DOOR OPENING)

DOOR OPENING (MAX. 36")

24"



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36"

CONCRETE

4

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OPENING DPENING

CONCRETE I

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6 3/4"

MODEL NO. H1W024036C-B-----QUANTITY: 1 DOCUMENT NO. Q47041 DATE: 1/18/24 LOCATION/TAG:

STANDARD FEATURES:

H-20 LOAD RATING 1/4 ALUMINUM TREAD PLATE COVER 1/4 THICK ALUM. CHANNEL FRAME EXTRUSION SINGLE LEAF CONSTRUCTION 1 1/2" DRAIN COUPLING S.STL & ALUM, HOLD OPEN ARM S.STL SLAM LOCK W/ KEY RECESSED LIFT HANDLE(S) T-316 S.STL. HINGES AND ATTACHING HARDWARE S,STL. COMPRESSION SPRING ASSIST LIFETIME GUARANTEE



OPTIONS/FEATURES:

PADLOCK BAR RECESSED LOCK BOX KEYED CYLINDER LOCK EPDM GASKET/CUSHION **BITUMINOUS COATING PVC PROTECTIVE FILM** SLAB SKIRT HEIGHT (INCLUDING FRAME) CLEAR ANODIZED FINISH SAFETY CHAIN WITH POSTS SAFETY CABLE WITH POSTS 3" INSULATION W/ CAPTIVE PAN NUTRAIL - SPECIFY LENGTH & LOCATION RETRO-GRATE (SEE ATTACHED DETAIL) BOLT DOWN COVER INSPECTION DOOR MODULAR DESIGN SIDE DRAIN MISCELLANEOUS

NOTES:

1) SUITABLE FOR USE IN OFF STREET LOCATION WHERE NOT SUBJECTED TO TRAFFIC.

2) PROVIDE A FULL BED OF CLASS "A" CONCRETE UNDER FRAME AND SUPPORT ANGLES.

NOTE: STANDARD PRODUCT WARRANTY DOES NOT COVER CORROSION FROM CHLORINE CONTACT.

H1R with C5 REINF 10/25/05

	Agent Authorization Form For Required Signature Edwards Aquifer Protection Program Relating to 30 TAC Chapter 213 Effective June 1, 1999	
l ·	Edwin Bayloris	
Seniur	Print Name Manager, 645	
	Title - Owner/President/Other	
of	Apple Inc.	
·	Corporation/Partnership/Entity Name	
have authorized	John Pelham, P.E. Print Name of Agent/Engineer	
of	GarzaEMC,LLC.	
	Print Name of Firm	

to represent and act on the behalf of the above named Corporation, Partnership, or Entity for the purpose of preparing and submitting this plan application to the Texas Commission on Environmental Quality (TCEQ) for the review and approval consideration of regulated activities.

I also understand that:

- 1. The applicant is responsible for compliance with 30 Texas Administrative Code Chapter 213 and any condition of the TCEQ's approval letter. The TCEQ is authorized to assess administrative penalties of up to \$10,000 per day per violation.
- 2. For those submitting an application who are not the property owner, but who have the right to control and possess the property, additional authorization is required from the owner.
- 3. Application fees are due and payable at the time the application is submitted. The application fee must be sent to the TCEQ cashier or to the appropriate regional office. The application will not be considered until the correct fee is received by the commission.
- 4. A notarized copy of the Agent Authorization Form must be provided for the person preparing the application, and this form must accompany the completed application.
- 5. No person shall commence any regulated activity on the Edwards Aquifer Recharge Zone, Contributing Zone or Transition Zone until the appropriate application for the activity has been filed with and approved by the Executive Director.

SIGNATURE PAGE:

Applicant's Signature

3 29/24

Date

THE STATE OF <u>CALIFORNIA</u> §

County of Santa Clara §

BEFORE ME, the undersigned authority, on this day personally appeared $\underline{E_{M,J,M}}$ \underline{H} $\underline{E_{M,J,M}}$ known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that (s)he executed same for the purpose and consideration therein expressed.

GIVEN under my hand and seal of office on this <u>2</u>⁴ day of <u>March</u>, <u>2024</u>.



Brei

ANNA MARJE BREWSTER Typed or Printed Name of Notary

MY COMMISSION EXPIRES: August 14,2027

Application Fee Form

Texas Commission on Environmental Quality									
Name of Proposed Regulated Entity: Generational Properties									
Regulated Entity Location: 6900 W Parmer Lane Austin, TX 78729									
Name of Customer: <u>Apple Inc.</u>									
Contact Person: <u>Dani Sattman</u>	e: <u>512-674-8221</u>								
Customer Reference Number (if issued):CN <u>603691783</u>									
Regulated Entity Reference Number (if issued):RN <u>110792173</u>									
Austin Regional Office (3373)									
🗌 Hays	🔀 Travis	\boxtimes w	illiamson						
San Antonio Regional Office (3362))								
Bexar	Medina		valde						
 Comal	 Kinney								
Application fees must be paid by ch	eck. certified check. c	or money order, payab	le to the Texas						
Commission on Environmental Qua	ality. Your canceled c	heck will serve as you	r receipt. This						
form must be submitted with your	fee payment. This pa	avment is being submi	itted to:						
Austin Pagional Offica		, an Antonio Pogional O	ffico						
Mailed to: TCEO - Cashier		San Antonio Regional Office							
	12100 Dark 2E Circlo								
Mail Code 214	L	12100 Park 55 Circle							
	D	unuing A, Siù Floui							
P.U. BUX 15066	A /(103111, 1A 70700							
Austin, TX 78/11-5088).).	512/259-0557							
	J.	_							
Recharge Zone	Contributing Zone	Transi	tion Zone						
Type of Plan		Size	Fee Due						
Water Pollution Abatement Plan, Co	ontributing Zone								
Plan: One Single Family Residential	Dwelling	Acres	\$						
Water Pollution Abatement Plan, Co	ontributing Zone								
Plan: Multiple Single Family Resider	ntial and Parks	Acres	\$						
Water Pollution Abatement Plan, Co	ontributing Zone								
Plan: Non-residential		Acres	\$						
Sewage Collection System	1085 L.F.	\$ 650.00							
Lift Stations without sewer lines	Acres	\$							
Underground or Aboveground Stora	Tanks	\$							
Piping System(s)(only)		Each	\$						
Exception		Each	\$						
Extension of Time		Each	\$						
Signature:	Date	<u>: 04/</u> 02/2024							

V

Application Fee Schedule

Texas Commission on Environmental Quality

Edwards Aquifer Protection Program 30 TAC Chapter 213 (effective 05/01/2008)

Water Pollution Abatement Plans and Modifications

Contributing Zone Plans and Modifications

	Project Area in	
Project	Acres	Fee
One Single Family Residential Dwelling	< 5	\$650
Multiple Single Family Residential and Parks	< 5	\$1,500
	5 < 10	\$3,000
	10 < 40	\$4,000
	40 < 100	\$6,500
	100 < 500	\$8,000
	≥ 500	\$10,000
Non-residential (Commercial, industrial, institutional,	< 1	\$3,000
multi-family residential, schools, and other sites	1 < 5	\$4,000
where regulated activities will occur)	5 < 10	\$5,000
	10 < 40	\$6,500
	40 < 100	\$8,000
	≥ 100	\$10,000

Organized Sewage Collection Systems and Modifications

Project	Cost per Linear Foot	Minimum Fee- Maximum Fee		
Sewage Collection Systems	\$0.50	\$650 - \$6,500		

Underground and Aboveground Storage Tank System Facility Plans and Modifications

Project	Cost per Tank or Piping System	Minimum Fee- Maximum Fee
Underground and Aboveground Storage Tank Facility	\$650	\$650 - \$6,500

Exception Requests

Project	Fee
Exception Request	\$500

Extension of Time Requests

Project	Fee
Extension of Time Request	\$150



TCEQ Core Data Form

TCEQ Use Only

For detailed instructions regarding completion of this form, please read the Core Data Form Instructions or call 512-239-5175.

DECTION	I: Gen	eral morn	ation								
1. Reason for	Submis	sion (If other is	checked please	describe in	n space	provid	led.)				
New Pern	nit, Regis	tration or Authoriz	zation (Core Da	ta Form she	ould be	subm	itted wi	ith the p	rogram applicatio	n.)	
Renewal	(Core D	ata Form should	be submitted wi	th the rene	wal forr	n)	0	ther	Modification Approved Pl	of a Pre	eviously
2. Customer Reference Number (if issued) Follow this link to search					arch	3. Re	egulate	d Entity Referen	ce Number	(if issued)	
CN 603691783						ers în	RI	V 110	792173	2 16	
SECTION 1	II: Cu	stomer Info	rmation								
4. General Cu	istomer l	nformation	5. Effective D	ate for Cu	stomer	Inform	nation	Update	es (mm/dd/yyyy)	-1	ile e s
New Custo	omer Legal Na	me (Verifiable wit	Up h the Texas Sec	odate to Cu cretary of S	stomer tate or	Inform Texas	nation Compt	troller of	Change in Public Accounts)	Regulated	Entity Ownership
The Custon Texas Secr	ner Nar retary o	ne submitted f State (SOS)	here may be or Texas Co	updated mptrolle	d auto r of Pi	matio Iblic	cally l Acco	based unts (on what is cu CPA).	rrent and	active with the
6. Customer I	Legal Na	me (If an individual	l, print last name f	īrst: eg: Doe	, John)		<u>lf</u>	new Cu	stomer, enter previ	ious Custom	er below:
Apple Inc.				e						2	-
7. TX SOS/CP	PA Filing	Number	8. TX State Ta	ax ID (11 digi	its)		9. Federal Tax ID (9 digits) 10. DUNS Number (if applicable)				
000478980)6		194240411	101			94-2404110 060704780				
11. Type of C	ustomer	: 🛛 Corporati	on		Individ	ual		Par	tnership: 🗌 Gener	ral 🔲 Limited	
Government:	🗆 City 🔲	County 🔲 Federal	State 🗌 Other		Sole P	ropriet	orship		Other:		
12. Number o	f Employ 21-100	/ees	251-500	⊠ 501 a	nd high	ier	13	3. Indep Yes	endently Owned	l and Opera	ited?
14. Customer	Role (Pr	oposed or Actual) -	- as it relates to th	e Regulated	Entity I	isted or	this fo	rm. Plea	se check one of the	following:	
Owner		Operat	tor	Ø)wner 8	Opera	ator	G		-	
	al Licens	see 🗌 Respo	nsible Party	Πv	/oluntar	y Clea	nup Ap	oplicant	Other:		
	One A	pple Park Wa	ay	2							
15. Mailing	319-3I	EHS									
	City	Cupertino		State	CA		ZIP	950	14	ZIP+4	
16. Country N	lailing In	formation (if outsi	de USA)			17. E	-Mail /	Addres	s (if applicable)		
						ebay	ylosis	s@app	ole.com		
18. Telephone	e Numbe	r	1	9. Extensi	on or (Code			20. Fax Numbe	r (if applicat	ble)
(408) 783	3-7928								()-	3	1

SECTION III: Regulated Entity Information

 21. General Regulated Entity Information (If 'New Regulated Entity" is selected below this form should be accompanied by a permit application)

 New Regulated Entity

 Update to Regulated Entity Information

The Regulated Entity Name submitted may be updated in order to meet TCEQ Agency Data Standards (removal of organizational endings such as Inc, LP, or LLC.)

22. Regulated Entity Name (Enter name of the site where the regulated action is taking place.)

Generational Proper	ties											
22 Street Address of	One Apple	e Park Way										
the Regulated Entity:	319-3EHS							•				
(No PO Boxes)	City	Cupertino	State	CA	ZIP	9501	.4	ZIP + 4				
24. County	Santa Cla	Santa Clara										
	Enter	Physical Locati	on Descriptio	n if no stre	et address	is provid	ed.					
25. Description to Physical Location:												
26. Nearest City				5 1 <u>1</u> 1		State		Nea	arest ZIP Code			
27. Latitude (N) In Decimal: 30.451912					Longitude	(W) In	Decimal:	-97.7455	63			
Degrees	Minutes	Sec	onds	Deg	rees		Minutes		Seconds			
30	27	,	6.8832		-97		44		44.0268			
29. Primary SIC Code (4 c	tigits) 30. Se	econdary SIC Co	de (4 digits)	31. Primary NAICS Code 32. Secondary NAICS Code (5 or 6 digits) (5 or 6 digits)								
3663	357			334111 334220								
33. What is the Primary I	Business of thi	s entity? (Do no	ot repeat the SIC c	or NAICS des	ription.)							
General Office Space	ce and Rese	ach and Deve	elopment S	pace								
				One A	ople Park W	ay						
34. Mailing				3	19-3EHS							
Address:	City	Cupertino	State	CA	ZIP		95014	ZIP+4				
35. E-Mail Address			- Charles and the second se	ebay	losis@appl	e.com	<u>,,, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u>	•				
36. Teleph	one Number		37. Extens	ion or Coc	e	38	. Fax Num	ber <i>(if appli</i> e	cable)			
(408)	783-7928						() -				

Dam Safety	Districts	Edwards Aquifer	Emissions Inventory Air	Industrial Hazardous Waste
		11001603 and		
		11001604		
Municipal Solid Waste	New Source Review Air		Petroleum Storage Lank	
Sludge	Storm Water	Title V Air	Tires	Used Oil
Voluntary Cleanup	Waste Water	Wastewater Agriculture	U Water Rights	Other:

SECTION IV: Preparer Information

40. Name: John Pelham, P.E.		41. Title: Sr. Vice President
42. Telephone Number 43. Ext./Code	44. Fax Number	45. E-Mail Address
(512) 298-3284	() -	jpelham@garzaemc.com

SECTION V: Authorized Signature

46. By my signature below, I certify, to the best of my knowledge, that the information provided in this form is true and complete, and that I have signature authority to submit this form on behalf of the entity specified in Section II, Field 6 and/or as required for the updates to the ID numbers identified in field 39.

Company:	Apple Inc.	Job Title:	Sr Manag	jer, EHS	·
Name(In Print) :	Edwin Baylosis			Phone:	(925) 413-7150

Signature: CUMG	Date:	3/29/	24





SP-2023-0292C



NOTES:

- RELEASE OF THIS APPLICATION DOES NOT CONSTITUTE A VERIFICATION OF ALL DATA, INFORMATION, AND CALCULATIONS SUPPLIED BY THE APPLICANT. THE ENGINEER OF RECORD IS SOLELY RESPONSIBLE FOR THE COMPLETENESS, ACCURACY, AND ADEQUACY OF HIS/HER SUBMITTAL, WHETHER OR NOT THE APPLICATION IS REVIEWED FOR CODE COMPLIANCE BY CITY ENGINEERS.
- ALL RESPONSIBILITY FOR THE ADEQUACY OF THESE PLANS REMAINS WITH THE ENGINEER WHO PREPARED THEM. IN REVIEWING THESE PLANS, THE CITY OF AUSTIN MUST RELY UPON THE ADEQUACY OF THE WORK OF THE DESIGN ENGINEER.
- 3. THIS PROJECT IS WITHIN THE EDWARDS AQUIFER RECHARGE ZONE AS DEFINED BY THE CITY OF AUSTIN.
- 4. THE ENVIRONMENTAL INSPECTOR HAS THE AUTHORITY TO CHANGE OR MODIFY EROSION/SEDIMENTATION CONTROLS, PER SECTION 25-8-183 OF THE CITY OF AUSTIN'S LAND DEVELOPMENT CODE.
- 5. THE PLAN IS COMPLETE, ACCURATE AND IN COMPLIANCE WITH CHAPTER 25-8 SUBCHAPTER A OF THE LAND DEVELOPMENT CODE. [LDC 25-8-152] 6. NO NATURALLY OCCURRING SLOPES IN EXCESS OF 15% EXIST WITHIN
- THE LIMITS OF CONSTRUCTION FOR THIS PROJECT. 7. APPROVAL OF THESE PLANS BY THE CITY OF AUSTIN INDICATES COMPLIANCE WITH APPLICABLE CITY REGULATIONS ONLY. APPROVAL BY OTHER GOVERNMENTAL ENTITIES MAY BE REQUIRED PRIOR TO THE START OF CONSTRUCTION. THE APPLICANT IS RESPONSIBLE FOR
- DETERMINING WHAT ADDITIONAL APPROVALS MAY BE NECESSARY. 8. THIS PROJECT HAS PRIVATE HYDRANTS LOCATED WITHIN THE PROPERTY. THE PROPERTY OWNER IS REQUIRED TO COMPLY WITH AUSTIN FIRE CODE. FAILURE TO COMPLY MAY RESULT IN CIVIL AND/OR CRIMINAL REMEDIES AVAILABLE TO THE CITY. THE PERFORMANCE OF THIS OBLIGATION SHALL ALWAYS REST WITH THE OWNER OF RECORD. FIRE HYDRANTS ON PRIVATE PROPERTY ARE REQUIRED TO BE SERVICED, MAINTAINED AND FLOWED ANNUALLY, USING A CONTRACTOR REGISTERED WITH THE CITY TO PROVIDE THE
- SERVICE, THIS PROJECT INCLUDES TWO (2) PRIVATE HYDRANTS. 9. THIS PROJECT IS SUBJECT TO THE VOID AND WATER FLOW MITIGATION RULE (COA ECM 1.12.0 AND COA ITEM NO. 658S OF THE SSM) PROVISION THAT ALL TRENCHING GREATER THAN 5 FEET DEEP MUST BE INSPECTED BY A GEOLOGIST (TEXAS P.G.) OR A GEOLOGIST'S REPRESENTATIVE.
- 10. COMPLIANCE WITH THE COMMERCIAL AND MULTI-FAMILY RECYCLING ORDINANCE IS MANDATORY FOR MULTI-FAMILY COMPLEXES, BUSINESSES AND OFFICE BUILDINGS.
- 11. APPROVAL OF THESE PLANS BY THE CITY OF AUSTIN INDICATES COMPLIANCE WITH APPLICABLE CITY REGULATIONS ONLY. APPROVAL BY OTHER GOVERNMENTAL ENTITIES MAY BE REQUIRED PRIOR TO THE START OF CONSTRUCTION. THE APPLICANT IS RESPONSIBLE FOR DETERMINING WHAT ADDITIONAL APPROVALS MAY BE NECESSARY.
- 12. AN ADMINISTRATIVE ENVIRONMENTAL VARIANCE HAS BEEN GRANTED IN ACCORDANCE WITH LDC 25-8-42 AND THE ROBINSON RANCH PUD REGULATIONS IN EFFECT ON THE DATE OF THE ORDINANCE TO ALLOW CUT OR FILL TO EXCEED THE ALLOWABLE FOUR FEET FOR A WATER QUALITY OR DETENTION FACILITY.
- 13. AN ADMINISTRATIVE ENVIRONMENTAL VARIANCE HAS BEEN GRANTED IN ACCORDANCE WITH LDC 25-8-42 AND THE ROBINSON RANCH PUD REGULATIONS IN EFFECT ON THE DATE OF THE ORDINANCE TO ALLOW CUT OR FILL BETWEEN FOUR TO EIGHT FEET FOR THE SITE.
- 14. IF, DURING CONSTRUCTION OF THE WATERLINE, A VOID IS ENCOUNTERED THAT IS LOCATED WITHIN TRAVIS COUNTY AND MEETS THE NOTIFICATION CRITERIA OUTLINED BY THE CITY OF AUSTIN AND TCEQ(SHT 4, TCEQ WPAP GENERAL NOTES- NOTE 3 AND SHT 87, P-1 EROSION CONTROL NOTES- NOTE 8), NICO HAUWERT (512-972-1661) AND DAVID GIMNICH (512-972-1663) WITH AUSTIN WATER - WILDLAND CONSERVATION SHALL BE NOTIFIED IN ADDITION TO THE TCEQ AND THE CITY OF AUSTIN ENVIRONMENTAL INSPECTOR 15. PHASES TO BE CONSTRUCTED IN NUMBER SEQUENCED ORDER PER
- LDC 25-5-21(A) TO ENSURE SUFFICIENT PARKING 16. IF AT ANY TIME DURING CONSTRUCTION OF THIS PROJECT AN UNDERGROUND STORAGE TANK (UST) IS FOUND, CONSTRUCTION IN THAT AREA MUST STOP UNTIL A CITY OF AUSTIN UST CONSTRUCTION PERMIT IS APPLIED FOR AND APPROVED. ANY UST REMOVAL WORK MUST BE CONDUCTED BY A UST CONTRACTOR THAT IS REGISTERED WITH THE TEXAS COMMISSION OF ENVIRONMENTAL QUALITY (TCEQ). CONTACT ELIZABETH SIMMONS AT ELIZABETH.SIMMONS@AUSTINTEXAS.GOV IF YOU HAVE ANY
- QUESTIONS. [COA TITLE 6] 17. RETAINING WALLS OVER FOUR FEET IN HEIGHT, MEASURED FROM THE BOTTOM OF THE FOOTING TO THE TOP OF THE WALL, SHALL BE
- ENGINEERED AND WILL REQUIRE A SEPARATE PERMIT (UNIFORM BUILDING CODE 106.2.5). 18. CRITICAL ENVIRONMENTAL FEATURES (CEF) ARE PRESENT ON THIS
- SITE. ALL ACTIVITIES WITH THE CEF SETBACK MUST COMPLY WITH THE CITY OF AUSTIN CODE AND CRITERIA. 19. ALL PERMANENT FENCING MUST BE INSTALLED AT THE PERIMETER OF THE CRITICAL ENVIRONMENTAL FEATURE (CEF) SETBACK PRIOR
- TO THE INITIATION OF ANY CONSTRUCTION OR CLEARING ACTIVITY. THE FENCE MATERIAL SHALL BE IN ACCORDANCE WITH COA ITEM NO. 701S.3(E) OF THE SSM, UNLESS OTHER MATERIALS ARE APPROVED BY THE CITY OF AUSTIN. A LOCKABLE ACCESS GATE SHALL BE INSTALLED FOR EACH CRITICAL ENVIRONMENTAL FEATURE (CEF) SETBACK. 20. CITY OF AUSTIN MAY REQUIRE THE DEDICATION OF OPEN SPACE UPON MEETING THE TRIGGER DESCRIBED IN SECTION 3.06.b.1 OF ZONING ORDINANCE 040617-39.

SITE DEVELOPMENT PERMIT PLANS

FOR CAPSTONE

PERMIT NO. :	SP-2023-0292C
SUBDIVISION NO. :	C8J-2018-0223. C8-2023-0182.0
ADDRESS :	6900 W. PARME
SUBMITTAL DATE :	JULY 28, 2023

223.0A, C8-2021-0160.0APA,

82.0A RMER LANE

SUBMITTED BY :

Nexandra Boond

ALEXANDRA A. BOONE, P.E. GARZA EMC, LLC. 7708 RIALTO BLVD, SUITE 125 AUSTIN, TEXAS 78735 (512) 298-3284



DATE

03-29-2024

CITY OF AUSTIN WATER AND WASTEWATER UTILITY SPECIAL SERVICES DIVISION (512) 972-1060

AUSTIN WATER UTILITIES NOTES: THIS PROJECT HAS PRIVATE HYDRANTS LOCATED WITHIN THE PROPERTY. THE PROPERTY OWNER IS REQUIRED TO COMPLY WITH AUSTIN FIRE CODE. FAILURE TO COMPLY MAY RESULT IN CIVIL AND/OR CRIMINAL REMEDIES AVAILABLE TO THE CITY. THE PERFORMANCE OF THIS OBLIGATION SHALL ALWAYS REST WITH THE OWNER OF RECORD. FIRE HYDRANTS ON PRIVATE PROPERTY ARE REQUIRED TO BE SERVICED, MAINTAINED AND FLOWED ANNUALLY, USING CONTRACTOR REGISTERED WITH THE CITY TO PROVIDE THE SERVICE. THIS PROJECT INCLUDES 28 PRIVATE HYDRANTS. TRACKING#: UCC-190328-11-01 ROW ID#12144360

TRAFFIC CONTROL NOTES: TEMPORARY TRAFFIC CONTROL STRATEGY WITH THE FULL WAY MANAGEMENT DIVISION FOR REVIEW.

PLAN SUBMITTALS:

NO.	DATE	COMMENTS

ALEXANDRA A. BOONE, P.E., CERTIFY THAT THESE ENGINEERING DOCUMENTS ARE COMPLETE, ACCURATE AND ADEQUATE FOR THE INTENDED PURPOSES, INCLUDING CONSTRUCTION, BUT ARE NOT AUTHORIZED FOR CONSTRUCTION PRIOR TO FORMAL CITY APPROVAL

WILLIAMSON COUNTY DATE FOR CITY USE ONLY: SITE PLAN APPROVAL Sheet <u>001</u> of <u>238</u> FILE NUMBER: **SP-2023-0292C** APPLICATION DATE: ____ APPROVED BY COMMISSION ON: _____ UNDER SECTION 112 OF CHAPTER ______ OF THE CITY OF AUSTIN CODE. EXPIRATION DATE (25-5-81,LDC) CASE MANAGER ROSEMARY AVILA PROJECT EXPIRATION DATE (ORD.#970905-A)_____DWPZ ____DDZ ____ Director, Development Services Departmen **RELEASED FOR GENERAL COMPLIANCE:** ZONING: **PUD** Correction 1 Correction 2 _ SHEET Correction 3 -FINAL PLAT MUST BE RECORDED BY THE PROJECT EXPIRATION DATE, IF APPLICABLE. SUBSEQUENT SITE PLANS WHICH DO NOT COMPLY WITH THE CODE CURRENT AT THE TIME OF FILING, AND ALL REQUIRED BUILDING PERMITS AND/OR A NOTICE OF CONSTRUCTION (IF A BUILDING PERMIT IS NOT REQUIRÉD), MUST ALSO BE APPROVED PRIÒR TO THE PROJECT EXPIRATION DATE. 238 OF

AUSTIN WATER UTILITY DEPARTMENT

CITY OF AUSTIN FIRE DEPARTMENT

INDUSTRIAL WASTE DEPARTMENT

DEVELOPMENT SERVICES DEPARTMENT

DATE

DATE

DATE

DATE

APPROVED FOR ACCEPTANCE

AUSTIN FIRE DEPARTMENT - PROJECT INFORMATION TABLE						
FIRE DESIGN CODES	IFC 2015					
FIRE FLOW DEMAND @ 20 PSI (GPM)	6000 GPM					
INTENDED USE	OFFICE					
CONSTRUCTION CLASSIFICATION	IB/ IIB					
BUILDING FIRE AREA (SF)	1,076,454 SF					
AUTOMATIC FIRE SPRINKLER SYSTEM TYPE (IF APPLICABLE)	FULLY SPRINKLERED					
REDUCED FIRE FLOW DEMAND @ 20 PSI FOR HAVING A SPRINKLER SYSTEM (GMP) (IF APPLICABLE)	1500 GPM					
AFD FIRE HYDRANT FLOW TEST DATE	09-14-2018					
AFD FIRE HYDRANT FLOW TEST LOCATION	7000 BLK W PARMER LN & 6000 BLK MCNEIL DR.					
HIGH-RISE	YES					
WILDLAND URBAN INTERFACE CODE	2015 INTERNATIONAL WILDLAND-URBAN INTERFACE CODE (IWUIC) WITH CITY OF AUSTIN LOCAL AMENDMENTS					
ALTERNATIVE METHOD OF COMPLIANCE (AMOC), IF APPLICABLE TO YOUR PROJECT	YES					

DEMOLITION NOTE: A PRECONSTRUCTION MEETING WITH THE ENVIRONMENTAL INSPECTOR IS REQUIRED PRIOR TO ANY SITE DISTURBANCE.

RSMP PARTICIPATION NOTE:

PARTICIPATION IN THE REGIONAL STORMWATER MANAGEMENT PROGRAM THROUGH PAYMENT TO, AND AGREEMENT WITH, THE UPPER BRUSHY CREEK WATER CONTROL AND IMPROVEMENT DISTRICT WAS APPROVED FOR THIS SITE ON ______APRIL 24, 2020 BY THE CITY OF AUSTIN WATERSHED PROTECTION DEPARTMENT, OFFICE OF THE DIRECTOR. THE RSMP NUMBER FOR THIS CASE IS: RAT-RS-2020-00240."

AUSTIN TRANSPORTATION DEPARTMENT NOTE: A MINIMUM 15 FT WIDE SIDEWALK TRAIL AND RECREATION EASEMENT ENCOMPASSING THE TRAIL SHOWN EXTENDING FROM THE NORTHERN DRIVEWAY TO THE NORTHERN MOST PROPERTY LINE ALONG WEST PARMER LANE AND FROM WEST PARMER LANE TO THE EASTERN PROPERTY LINE WITHIN THE OPEN SPACE, MUST BE DEDICATED AND RECORDATION NUMBER ADDED TO THE SITE PLAN PRIOR TO APPROVAL OF ANY CERTIFICATE OF OCCUPANCY WITHIN THE SITE.

NO CERTIFICATE OF OCCUPANCY SHALL BE RELEASED FOR THIS PROJECT UNTIL THE PROPOSED SPM RESTRICTIVE COVENANT HAS BEEN APPROVED BY COA LEGAL AND COA WATERSHED, RECORDED BY THE COUNTY AND RECORDATION NUMBERS INCLUDED IN THE PLANS. RECORDED WM. DOC#2019064152 INTEGRATED PEST MANAGEMENT PLAN NOTE NO CERTIFICATE OF OCCUPANCY SHALL BE RELEASED FOR THIS PROJECT UNTIL THE PROPOSED IPM RESTRICTIVE COVENANT HAS BEEN APPROVED BY COA LEGAL AND COA WATERSHED, RECORDED BY THE COUNTY AND RECORDATION NUMBERS INCLUDED IN THE PLANS. RECORDED WM. DOC#2019064153

PLEASE NOTE THAT OUR SITE DEVELOPMENT PERMIT APPLICATION IS PROTECTED UNDER THE "GARZA EMC" COPYRIGHT AND OUR DOCUMENTS SHOULD NOT BE COPIED NOR PROVIDED TO ANY REQUESTOR

SUBSURFACE POND MAINTENANCE NOTE

	Sheet List Table		Sheet List Table	Sheet List Table							
SHEET	SHEET TITLE	SHEET	SHEET TITLE	SHEET	SHEET TITLE						
001 002	COVER SHEET SHEET LIST	110 111	GRADING PLAN V GRADING PLAN W	216 217	SEWER METERTING VAULT DETAILS (FOR REFERENCE ONLY)						
003	GENERAL NOTES	112	GRADING PLAN X	217	CIVIL DETAILS (FOR REFERENCE ONLY)						
005	AWU – GENERAL NOTES	114	GRADING AND DRAINAGE DETAILS 1 OF 2	219 220	INTERCEPT LIFT STATION PLAN AND DETAILS (FOR REFERENCE ONLY) INTERCEPT LIFT STATION SECTIONS (FOR REFERENCE ONLY)						
006 007	SURVEY SHEET 1 SURVEY SHEET 2	115 116	GRADING AND DRAINAGE DETAILS 2 OF 2 EXISTING DRAINAGE AREA MAP	221	MECHANICAL DETAILS (FOR REFERENCE ONLY)						
008 009	SURVEY SHEET 3 SURVEY SHEET 4	117 118	PROPOSED DRAINAGE AREA MAP INLET DRAINAGE AREA MAP 1 OF 2	222 223	ELECTRICAL NOTES AND LEGENDS (FOR REFERENCE ONLY)						
010	SURVEY SHEET 5	119	INLET DRAINAGE AREA MAP 2 OF 2	224	ELECTRICAL SITE PLAN (FOR REFERENCE ONLY)						
012	SURVEY SHEET 6 SURVEY SHEET 7	120	INLET CALCULATIONS 1 OF 2 INLET CALCULATIONS 2 OF 2	225	ELECTRICAL DIAGRAMS (FOR REFERENCE ONLY)						
013 014	SURVEY SHEET 8 PLAT SHEET 1	122 123	REGIONAL DETENTION PLAN AND CALCULATIONS 1 (FOR REFERENCE ONLY) REGIONAL DETENTION PLAN AND CALCULATIONS 2 (FOR REFERENCE ONLY)	227 228	ELECTRICAL DETAILS (FOR REFERENCE ONLY) ARCH PG - PG2 LEVEL 0 PARKING (FOR REFERENCE ONLY)						
015 016	PLAT SHEET 2 PLAT SHEET 3	124	WATER QUALITY POND PLAN (FOR REFERENCE ONLY)	229	ARCH PG - PG2 LEVEL 01 PARKING (FOR REFERENCE ONLY)						
017	PLAT SHEET 4	125 126	WATER QUALITY POND SECTION PROFILES (FOR REFERENCE ONLY) WATER QUALITY POND DETAILS SHEET 1 (FOR REFERENCE ONLY)	230 231	ARCH PG — PG2 LEVEL 02 PARKING (FOR REFERENCE ONLY) ARCH PG — PG2 LEVEL 3—7 PARKING (FOR REFERENCE ONLY)						
018	PLAT SHEET 6	127 128	WATER QUALITY POND DETAILS SHEET 2 (FOR REFERENCE ONLY)	232	ARCH PG - PG2 LEVEL 08 PARKING (FOR REFERENCE ONLY)						
020 021	PLAT SHEET 7 PLAT SHEET 8	129	WATER QUALITY POND DETAILS SHEET	233	ARCH PG – PGZ ENLARGED PLANS (FOR REFERENCE ONLY) ARCH PG – PG3 LEVEL 01 PARKING (FOR REFERENCE ONLY)						
022 023	PLAT SHEET 9 MASTER EXISTING CONDITIONS AND SLOPE MAP	130 131	MASTER UTILITY PLAN STORMSEWER PLAN A	235 236	ARCH PG – PG3 LEVEL 02 PARKING (FOR REFERENCE ONLY) ARCH PG – PG3 LEVELS 03 & 05 PARKING (FOR REFERENCE ONLY)						
024	EXISTING CONDITIONS AND DEMOLITION PLAN A	132 133	STORMSEWER PLAN B STORMSEWER PLAN C	237	ARCH PG - PG3 LEVELS 04 & 06 PARKING (FOR REFERENCE ONLY)						
025	EXISTING CONDITIONS AND DEMOLITION PLAN B EXISTING CONDITIONS AND DEMOLITION PLAN C	134 135	STORMSEWER PLAN D	238	ARCH PG - PG3 LEVEL 07 PARKING (FOR REFERENCE ONLY)						
027 028	EXISTING CONDITIONS AND DEMOLITION PLAN D EXISTING CONDITIONS AND DEMOLITION PLAN E	136	STORMSEWER PLAN F								
029 030	EXISTING CONDITIONS AND DEMOLITION PLAN F EXISTING CONDITIONS AND DEMOLITION PLAN G	137 138	STORMSEWER PLAN I STORMSEWER PLAN J								
031	EXISTING CONDITIONS AND DEMOLITION PLAN H	139 140	STORMSEWER PLAN K STORMSEWER PLAN V								
032	EXISTING CONDITIONS AND DEMOLITION PLAN I EXISTING CONDITIONS AND DEMOLITION PLAN J	141	STORMSEWER PLAN X								
034 035	EXISTING CONDITIONS AND DEMOLITION PLAN K EXISTING CONDITIONS AND DEMOLITION PLAN L	143	STORMSEWER PLAN Z								
036 037	EXISTING CONDITIONS AND DEMOLITION PLAN M	144 145	PRIVATE WATER-WASTEWATER PLAN A PRIVATE WATER-WASTEWATER PLAN B								
038	EXISTING CONDITIONS AND DEMOLITION PLAN N EXISTING CONDITIONS AND DEMOLITION PLAN O	146 147	PRIVATE WATER-WASTEWATER PLAN C PRIVATE WATER-WASTEWATER PLAN D								
039	EXISTING CONDITIONS AND DEMOLITION PLAN P EXISTING CONDITIONS AND DEMOLITION PLAN Q	148	PRIVATE WATER WASTEWATER PLAN E		r - r						
041 042	EXISTING CONDITIONS AND DEMOLITION PLAN R EXISTING CONDITIONS AND DEMOLITION PLAN T	149 150	PRIVATE WATER-WASTEWATER PLAN F PRIVATE WATER-WASTEWATER PLAN I								
043	EXISTING CONDITIONS AND DEMOLITION PLAN U	151 152	PRIVATE WATER-WASTEWATER PLAN J PRIVATE WATER-WASTEWATER PLAN K		NO.						
045	EXISTING CONDITIONS AND DEMOLITION PLAN V EXISTING CONDITIONS AND DEMOLITION PLAN W	153 154	PRIVATE WATER-WASTEWATER PLAN V PRIVATE WATER-WASTEWATER PLAN X								
046 047	EXISTING CONDITIONS AND DEMOLITION PLAN X EXISTING CONDITIONS AND DEMOLITION PLAN Y	155	PRIVATE WATER-WASTEWATER PLAN Z								
048 049	EXISTING CONDITIONS AND DEMOLITION PLAN Z EXISTING CONDITIONS AND DEMOLITION PLAN AA	156	PRIVATE FORCEMAIN PLAN J								
050 051	EXISTING CONDITIONS AND DEMOLITION PLAN AB	158 159	PRIVATE FORCEMAIN PLAN K PRIVATE FORCEMAIN PLAN M								
052	PHASING PLAN	160 161	PRIVATE FORCEMAIN PLAN N WATER-WASTEWATER NOTES AND DETAILS 1 OF 4								
053	FIRE ACCESS SITE PLAN	162	WATER-WASTEWATER NOTES AND DETAILS 2 OF 4								
055 056	WILDLAND URBAN INTERFACE VICINITY MAP SUBCHAPTER E PARITAL COMPLIANCE PLAN	164	WATER-WASTEWATER NOTES AND DETAILS 5 OF 4								
057 058	MASTER SITE PLAN SITE PLAN A	165 166	RECLAIMED WATER PLAN D RECLAIMED WATER PLAN E								
059	SITE PLAN B	167 168	RECLAIMED WATER PLAN J RECLAIMED WATER PLAN K								
060	SITE PLAN D	169	LANDSCAPE REFERENCE PLAN								
062 063	SITE PLAN E SITE PLAN F	170	LANDSCAPE PLAN & (FOR REFERENCE ONLY) LANDSCAPE PLAN B (FOR REFERENCE ONLY)								
064 065	SITE PLAN I SITE PLAN J	172 173	LANDSCAPE PLAN C (FOR REFERENCE ONLY) LANDSCAPE PLAN D (FOR REFERENCE ONLY)								
066	SITE PLAN K	174	LANDSCAPE PLAN E (FOR REFERENCE ONLY)								
067	SITE PLAN N SITE PLAN O	175 176	LANDSCAPE PLAN F (FOR REFERENCE ONLY) LANDSCAPE PLAN G (FOR REFERENCE ONLY)								
069 070	SITE PLAN V SITE PLAN W	177	LANDSCAPE PLAN H (FOR REFERENCE ONLY)								
071 072	SITE PLAN X SITE PLAN Y	178 179	LANDSCAPE PLAN I (FOR REFERENCE ONLY) LANDSCAPE PLAN J (FOR REFERENCE ONLY)								
072	SITE PLAN Z	180 181	LANDSCAPE PLAN K (FOR REFERENCE ONLY) LANDSCAPE PLAN L (FOR REFERENCE ONLY)								
074	SITE PLAN NOTES AND DETAILS 1 OF 4 SITE PLAN NOTES AND DETAILS 2 OF 4	182	LANDSCAPE PLAN M (FOR REFERENCE ONLY)								
076 077	SITE PLAN NOTES AND DETAILS 3 OF 4 SITE PLAN NOTES AND DETAILS 4 OF 4	183 184	LANDSCAPE PLAN N (FOR REFERENCE ONLY) LANDSCAPE PLAN O (FOR REFERENCE ONLY)								
078 079	MASTER EROSION AND SEDIMENTATION CONTROL PLAN PHASES 8-15 MASTER EROSION AND SEDIMENTATION CONTROL PLAN PHASES 16-20	185 186	LANDSCAPE PLAN P LANDSCAPE PLAN O								
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083 084	EROSION AND SEDIMENTATION CONTROL PLAN C EROSION AND SEDIMENTATION CONTROL PLAN D	190 191	LANDSCAPE PLAN V LANDSCAPE PLAN W								
085 086	EROSION AND SEDIMENTATION CONTROL PLAN E EROSION AND SEDIMENTATION CONTROL PLAN F	192 193	LANDSCAPE PLAN X LANDSCAPE PLAN Y								
087	EROSION AND SEDIMENTATION CONTROL PLAN I FROSION AND SEDIMENTATION CONTROL PLAN J	194	LANDSCAPE PLAN Z								
089	EROSION AND SEDIMENTATION CONTROL PLAN K	195	LANDSCAPE PLAN AA LANDSCAPE PLAN AB								
090 091	EROSION AND SEDIMENTATION CONTROL PLAN N EROSION AND SEDIMENTATION CONTROL PLAN O	197 198	LANDSCAPE PLAN AC TREE LIST 1 (FOR REFERENCE ONLY)								
092 093	EROSION AND SEDIMENTATION CONTROL PLAN V EROSION AND SEDIMENTATION CONTROL PLAN W	199	TREE LIST 2 (FOR REFERENCE ONLY)								
094	EROSION AND SEDIMENTATION CONTROL PLAN X	200	TREE LIST 4								
096	EROSION AND SEDIMENTATION CONTROL PLAN Z	202 203	TREE LIST 5 OAK WILT EXHIBIT (FOR REFERENCE ONLY)								
097 098	ERUSION AND SEDIMENTATION CONTROL NOTES AND DETAILS 1 OF 2 EROSION AND SEDIMENTATION CONTROL NOTES AND DETAILS 2 OF 2	204	BARLETT TREE ASSESSMENTS (FOR REFERENCE ONLY)								
099 100	MASTER GRADING PLAN GRADING PLAN A	205 206	LANDSCAPE NUTES & DETAILS (FOR REFERENCE UNLY) EXPANSION PARCEL CALCULATIONS								
101 102	GRADING PLAN B	207 208	BARTLETT TREE REPORT BIOFILTRATION POND PLANTING (FOR REFERENCE ONLY)								
103	GRADING PLAN D	209	KEY SHEET (FOR REFERENCE ONLY)								
104 105	GRADING PLAN E GRADING PLAN F	210 211	LIFT STATION SHE PLAN (FOR REFERENCE UNLY) DIMENSION CONTROL PLAN (FOR REFERENCE ONLY)		THE LOCATION OF EXISTING UNDE SHOWN IN AN APPROXIMATE WAY SHALL DETERMINE THE EXACT LO						
106 107	GRADING PLAN I GRADING PLAN J	212 21 3	LIFT STATION GRADING PLAN (FOR REFERENCE ONLY) SEWER EXTRACTION PLAN AND PROFILE (FOR REFERENCE ONLY)		UTILITIES BEFORE COMMENCING W FULLY RESPONSIBLE FOR ANY AN						
108 109	GRADING PLAN K GRADING PLAN N	214	FORCE MAIN PLAN AND PROFILE (FOR REFERENCE ONLY)		AND PRESERVE ANY AND ALL UN						
		215	FURGE MAIN PLAN AND PROFILE Z (FOR REFERENCE ONLY)								

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Ί) ONLY)							0. REVISION		ZTOR Rialto Rivel Suite 125	Austin, Texas 78735 Tel. (512) 298-3284 Fax (512) 298-2592	TBPE # F-14629
ONLY) ONLY)							DATE NC	ALEX Der	ANDRA 1389 SSIONAT	A. BOO 51 51 03/29/20	** NE Duy 224
DESCRIPTION		REVISE (R) ADD (A) VOID (V) SHEET NO.'S	TOTAL # SHEETS IN PLAN SET	NET CHANGE IMP. COVER (sq. ft.)	TOTAL SITE IMP. COVER (sq. ft.) [%]	CITY OF AUSTIN APPROVAL/DATE	DATE IMAGED				
								CAPSTONE	6900 W. PARMER LANE	APPI F INC.	
NG UNDERGROUND UTILITIES ARE ATE WAY ONLY. THE CONTRACTOR XACT LOCATION OF ALL EXISTING INCING WORK. HE AGREES TO BE X ANY AND ALL DAMAGES WHICH BY HIS FAILURE TO EXACTLY LOCATE O ALL UNDERGROUND UTILITIES.	Know what's below. Call before you	FOR CITY US	E ONLY:					OF OF OF	DESIGNED BY: ANG, IHR, HCH	dar:	80 PROJECT NO.: 101649.00031








1649-00031/Civil\00-CAD\Replacement SDP\101649-00031-SITE-MAS.dwg modified







BUILDING	DESCRIPTION
BUILDING CBC	GI #1 SERVING CAFETERIA BUILDING KITCHEN LEVELS
(AC09)	1 AND 2
BUILDING CBC	GI #2 SERVING CAFETERIA BUILDING KITCHEN LEVELS
(AC09)	1 AND 2
BUILDING CBC	GI #3 SERVING CAFETERIA BUILDING KITCHEN LEVELS
(AC09)	1 AND 2
BUILDING CBC	GI #4 SERVING CAFETERIA BUILDING KITCHEN LEVELS
(AC09)	1 AND 2
BUILDING CDB	GI #5 SERVING DAYCARE CENTER KITCHEN LEVEL 1
(AC12)	
	GI #6 SERVING CATERING KITCHEN ON LEVEL 4 AND 5
	OF BUILDING (AC01)
	GI #7 SERVING BUILDING B2 (AC02) CAFFE ON LEVELS
BUILDING 2	1 AND BASEMENT
	GI #8 SERVING BUILDING B2 (AC02) CAFFE ON LEVELS
	1 AND BASEMENT
	GI #9 SERVING HOTEL KITCHEN ON LEVEL 1
CARACES	SOL #1 SERVING THE ENTIDE DADVING CARAGE 2
GARAGE Z	SOI #1 SERVING THE ENTIRE PARKING GARAGE Z
	BUILDING CBC (AC09) BUILDING CBC (AC09) BUILDING CBC (AC09) BUILDING CBC (AC09) BUILDING CBC (AC09) BUILDING CDB (AC12) BUILDING CONF BUILDING 2 BUILDING 2 HOTEL

Р P

<u>NOTES:</u> PHASES WILL BE COMPLETED SUCH THAT REQUIRED PARKING IS ALWAYS LESS THAN PARKING PROVIDED.

							TOTAL PAR	KING			TOTAL	SHOWERS		TOTAL AD	A PARKING	VAN ADA	PARKING	STD ADA	PARKING	REGULAR	PARKING	COMPACT	PAR
						REQUIRED																	
			GROSS FL	APPENDIX A PARKING		W/ 10%		CUMULATIVE				CUMULATIVE	CUMULATIVE									ALLOWABLE	<i>:</i>
BLDG	PHASE	PROP USE	AREA (SF)	REQUIREMENT	REQUIRED	REDUCTION	I PROVIDED	REQUIRED	PROVIDED	REQUIRED**	PROVIDED**	REQUIRED	PROVIDED	REQUIRED	PROVIDED	REQUIRED	PROVIDED	REQUIRED	PROVIDED	REQUIRED	PROVIDED	(30% max)	PRO
					PHASE GRO	OUP A (CONST	RUCTED)																
NWUB	EX. 1	UTILITY ENCLOSURE	2,880	N/A				0	0					0	0	0	0	0	0	0	0	0	
PG4	EX. 2	GARAGE	353,347	N/A			1082	0	1082					21	33	6	4	15	29	0	899	325	
CENTRAL PLANT	EX. 3	UTILITY ENCLOSURE	2,985	OFFICE 1/275SF*	11	10		10	1082					0	0	0	0	0	0	11	0	0	
PG1	EX. 4	GARAGE	495,681	NA			1537	10	2619					25	42	7	5	18	37	0	1267	461	
B2/KITCHEN*	EX. 5	OFFICE (PROFESSIONAL)	318,111	OFFICE 1/275SF*	1157	1041		1051	2619	2	11	2	11	0	0	0	0	0	0	1157	0	0	
B1/CONF*	EX. 6	OFFICE (PROFESSIONAL)	270,608	OFFICE 1/275SF*	984	886		1936	2619	2	0	4	11	0	0	0	0	0	0	984	0	0	
RD1*	EX. 7	RESEARCH &	208,602	RESEARCH 1/275SF*	759	683		2619	2619	2	0	6	11	0	0	0	0	0	0	759	0	0	
				PHASE GROUP	B (UNDER C	ONSTRUCTION	N PER. SP-2018	8-0602C(R2))															
G2	***8	GARAGE	1,109,180	N/A			3421	2619	6040			6	11	44	54	9	8	35	46	0	2883	865	
AC03*	***9	OFFICE (PROFESSIONAL)	368,651	OFFICE 1/275SF*	1341	1206		3826	6040	2		8	11	0	0	0	0	0	0	1341	0	0	
AC09 Office*	***10	OFFICE (PROFESSIONAL)	70,945	OFFICE 1/275SF*	258	232		4058	6040	2	22	10	33	0	0	0	0	0	0	258	0	0	
AC09 Kitchen*	***10	FOOD PREP	29,734	F PREP- SCH A 1/500SF*	59	54		4111	6040			10	33	0	0	0	0	0	0	59	0	0	
AC09 Fitness	***10	FITNESS	31,489	N/A	0		0	4111	6040			10	33										
AC09 Wellness	***10	WELLNESS	25,464	N/A	0		0	4111	6040			10	33										
AC09 TOTAL	***10	AMENITY	203,884	ACCESSORY																			
AC08	***11	RESEARCH &	292,898	RESEARCH 1/275SF	1065	959		5070	6040	2		12	33	0	0	0	0	0	0	1065	0	0	
AC07	***12	RESEARCH &	212,566	RESEARCH 1/275SF	773	696		5766	6040	2		14	33	0	0	0	0	0	0	773	0	0	
AC12	***13	CHILDCARE	32,353	1 PER STAFF	60	60	42	5826	6082			14	33	2	2	0	0	2	2	58	40	12	
M4 Office	***14	OFFICE (PROFESSIONAL)	1,132	OFFICE 1/275SF	4	4		5830	6082			14	33							4			
M4 TOTAL	***14	Central Waste Collection	16,378	ACCESSORY										0	0	0	0	0	0	0	0	0	
M5 Office	***15	OFFICE (PROFESSIONAL)	1,200	OFFICE 1/275SF	4	4		5834	6082			14	33							4			
M5 TOTAL	***15	WWTP	6,529	ACCESSORY										0	0	0	0	0	0	0	0	0	
			•					-		_		-		-				-					
					PHASE G	ROUP C (PRO	POSED)																
G3	16	GARAGE	855,495	NA			2638	5834	8720			14	33	36	44	7	8	29	36	0	2299	690	
B4	17	OFFICE (PROFESSIONAL)	221,207	OFFICE 1/275SF	804	724		6558	8720	2		16	33	0	0	0	0	0	0	804	0	0	
B5	18	OFFICE (PROFESSIONAL)	213,762	OFFICE 1/275SF	777	700		7258	8720	2		18	33	0	0	0	0	0	0	777	0	0	
B6/BMR	19	OFFICE (PROFESSIONAL)	316,143	OFFICE 1/275SF	1150	1035		8292	8720	2		20	33	0	0	0	0	0	0	1150	0	0	-
HOTEL	20	HOTEL	199,175	1.1 FOR EACH RM(192 RM)	211	211		8503	8720			20	33	0	0	0	0	0	0	211	0	0	
B7	21	AMENITY	1,936	ACCESSORY																			-
B8	21	AMENITY	1,936	ACCESSORY																			-
В9	21	AMENITY	1,936	ACCESSORY				1		1				0	0	0	0	0	0	0	0	0	1
TOTAL			5,706,243		9417	8503	8720			20	33			129	175	29	25	100	150	9415	7388	2352	1
*REQUIRED AFTER 109	6 REDUC	TION FOR PROVIDING SHOW	ERS AND CH	ANGING FACILITY PER 25-6-4	78 (D)	-	•	-	-	-		-		-	•	-	•	-	-	-	•		

** SHOWERS PER GENDER *** PHASES UNDER CONSTRUCTION PER SP-2018-0602C(R2)

							BUILDING TABLE						
BLDG	BLDG Number Address	PHASE	BLDG HT (FT)	# STORIES	PROP USE	BLDG FFE	FOUNDATION TYPE	BLDF FOOTPRINT (SF)	GROSS FLOOR AREA (SF)	BUILDING TYPE	SPRINKLED	FIRE FLOW (GPM)	REDUCED FIRE FLOW (GPM)
B1	1	6 - EXISTING	75	5	OFFICE (PROFESSIONAL)	882	SLAB	47,493	270,608	IB	YES	6000	1500
B2	2	5 - EXISTING	75	5	OFFICE (PROFESSIONAL)	880	SLAB	63,114	318,111	IB	YES	6000	1500
AC03	3	9	72	5	OFFICE (PROFESSIONAL)	876	SLAB	65,000	368,651	IB	YES	6000	1500
B4	4	17	75	5	OFFICE (PROFESSIONAL)	864	SLAB	51,278	221,207	IB	YES	4750	1500
B5	5	18	75	5	OFFICE (PROFESSIONAL)	857	SLAB	52,276	213, 762	IB	YES	5000	1500
B6	6	19	75	5	OFFICE (PROFESSIONAL)	862.5	SLAB	<i>89,243</i>	316,143	IB	YES	6000	1500
RD1	10	7 - EXISTING	81	5	RESEARCH & DEVELOPMENT	882	SLAB	40,085	208,602	IB	YES	4750	1500
AC08	8	11	78	5	RESEARCH & DEVELOPMENT	868	SLAB	61,744	292,898	IB	YES	6000	1500
AC07	7	12	78	5	RESEARCH & DEVELOPMENT	868	SLAB	45,300	212,566	IB	YES	5500	1500
AC09	9	10	73' 6"	4	ACCESSORY	875.5	SLAB	64,128	203,884	IB	YES	5,750	1500
NWUB	M1	1 - EXISTING	19	1	UTILITY ENCLOSURE	868	SLAB	4,600	2,880	IIB	NO	1500	1500
CENTRAL PLANT	M2	2 - EXISTING	66	1	COOLING PLANT	862	SLAB	26,200	30,000	IIB	YES	3000	1500
HOTEL	11	20	113	9	HOTEL	888	SLAB	83,509	199,175	IB	YES	5500	1500
M4- Central Waste	M4	14	24	1	ACCESSORY	889	SLAB	16,378	16,378	5B	YES	1500	1500
AC12 - Child Care	12	13	15	1	ACCESSORY	883	SLAB	32,353	32,353	5B	YES	3750	1500
PG1	GAR1	4 - EXISTING	75'6"	8	GARAGE	887	SLAB	64,242	495,681	IB	YES	6000	1500
G2	GAR2	8	98'8"	9	GARAGE	883	SLAB	128,285	1,109,180	IB	YES	6000	1500
PG3	GAR3	16	75'6"	8	GARAGE	861	SLAB	119,430	855,495	IB	YES	6000	1500
PG4	GAR4	3 - EXISTING	43'6"	5	GARAGE	874	SLAB	78,069	353,347	IB	YES	6000	1500
M5	M5	15	24	1	ACCESSORY	881.4	SLAB	3,000	6,529	IB	YES	N/A	N/A
B7	13	21	15	1	ACCESSORY	872.3	SLAB	1,936	1,936	IB	NO	1500	1500
B8	14	21	15	1	ACCESSORY	872.3	SLAB	1,936	1,936	IB	NO	1500	1500
B9	15	21	15	1	ACCESSORY	873	SLAB	1,936	1,936	IB	NO	1500	1500
TOTAL								1,141,535	5,733,258				

APPENDIX Q-2:

IMPERVIOUS COVER

SUBURBAN WATERSHEDS

NOTE: Q-1 TABLES ARE NOT REQUIRED FOR SUBURBAN WATERSHEDS

1	IMPERVIOUS COVER	ALLOWED AT	90	_% X_	174.3 ACRES	. =	156.9	_ACRES
	PROPOSED IMPERVI	OUS COVER						
2	EXIS	SITING IMPER'	VIOUS COV	VER PR	OPOSED TO REMAIN	=	14.7	ACRES
3			PROPOSE) NEW	IMPERVIOUS COVER	=	40.9	ACRES
4		тс	OTAL PROP	OSED	IMPERVIOUS COVER	=	55.6	ACRES
	ALLOWABLE IMPER	/IOUS COVER	BREAKDO	WN B	SLOPE CATEGORY			
5	TOTAL ACREA	GE WITH SLOP	PES 15-25%	5 = _	0.2ACRES X 10%	=	0.02	ACRES
								-
	PROPOSED IMPERVI	OUS COVER C	ON SLOPES					
				I	MPERVIOUS COVER			
			BUILD	ING &	OTHER IMPERVIOUS		DRIV	/ES /
	SLOPES	5			COVER		ROAD	WAYS
	SLOPE CATEGORIES	ACRES	ACRES	9	% OF SLOPE CATEGOR	١Y	ACRES	
6	0-15%	174.0	31.7		18%		23.9	
7	15-25%	0.2	0		0%		0	-
8	25-35%	0.1	0		0%		0	_
9	OVER 35%	0	0		0%		0	-
10	GROSS SITE AREA	174.3				-		-

THE LOCATION OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK. HE AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE OCCASIONED BY HIS FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.

OFFSTRI ROVIDED 1 0 3	EET LOADING CUMULATIVE REQUIRED	CUMULATI PROVIDEI	DATE NO. REVISION		UDTES AND 138 138 138 138 138	24 OF 4 14 OF 4 15 C F F F F F F F F F F F F F F F F F F	FOR DE FORMER DE FORMER DE FORMER EN 14629 Garza EMC, LLC © Copyright 2024
5 2 1 0 3 1 7 0 0 2 6 0	1 4 7 10 10 13 15 16 22 31 32 35	9 11 12 12 12 15 16 23 23 23 23 23 23 23 23 23 23 23 23 23			SITE PLAN N	DETAILS	
0 0 1 2 1 0 0 0 0 0 0 0	31 16 19 25 28 35 35 35 35 35 35	31 31 32 34 35 35 35 35 35 35		CAPSTONE	6900 W. PARMER LANE		
				DRAWN BY:SPM	DESIGNED BY: ANG, IHR, HCH	ad ac ad ac	B PROJECT NO.: 101649.00031



FOR CITY USE ONLY:

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Know what's **below. Call** before you dig.



GENERAL PROPERTIES Proposed Conditions <u>Peak Discharge Calculations:</u>	Area:	Area: BYPASS Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.92 0.92 0.92 0.92 0.92 0.92 4.50-yr 5.00 5.	Area: J-1 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.52 0.52 0.52 0.52 0.52 0.52 0.52 10.454 46.15 C 0.52 0.59 0.63 0.71 0.77 Grass, Fair, 2-7% 0.28 12,197 53.85 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0.52 22,651 100 Q 1.6 2.6 3.3 4.6 6.4 Total 0.52 22,651 100	Area: PG2-NE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.98 0.98 0.98 0.98 0.98 0.98 0.98 10.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 Total 0.98 42,689 100 Q 4.2 7.0 8.7 11.9 15.6 Total 0.98 42,689 100
STM A NETWORK Area: B4-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.49 0.49 0.49 0.49 0.49 0.00 0 0.00 0 0.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.1 3.5 4.4 6.0 7.8 Total 0.49 21,344 100	Area: A Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.67 0.67 0.67 0.67 0.67 Acres SF % C 0.65 0.72 0.77 0.86 0.91 Concrete 0.09 3,920 13.43 0 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.14 6,098 20.90 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.5 4.1 5.2 7.2 9.7 Total 0.67 29,185 100	Area: HB-N Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.29 0.29 0.29 0.29 0.29 0.29 0.29 100.00 0.00	Area: J-3 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.81 0.81 0.81 0.81 0.81 0.81 0.81 2.97 10-yr 500-yr Surface Acres SF % Acres 0.81 0.81 0.81 0.81 0.81 Concrete 0.36 15,682 44.44 C 0.52 0.58 0.62 0.70 0.77 Grass, Fair, 2-7% 0.45 19,602 55.56 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.4 4.0 5.1 7.1 9.9 Total 0.81 35,284 100	Area: PG3-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.27 1.27 1.27 1.27 1.27 Asphalt 0.40 17,424 31.50 C 0.49 0.55 0.59 0.67 0.75 Concrete 0.10 4,356 7.87 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.77 33,541 60.63 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 3.6 6.0 7.6 10.7 15.1 Total 1.27 55,321 100
Area:	Are a: A-10 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.22 0.22 0.22 0.22 0.22 Acres SF % Acres 0.22 0.22 0.22 0.22 Asphalt 0.07 3,049 31.82 C 0.72 0.80 0.85 0.94 0.98 Concrete 0.14 6,098 63.64 J9 7c 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.01 436 4.55 03 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 0.9 1.5 1.9 2.6 3.4 Total 0.22 9,583 100	Area: The v Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acress 0.29 0.29 0.29 0.29 0.29 0.29 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 1.3 2.1 2.6 3.5 4.6 Total 0.29 12,632 100	Area: CB-C-E2 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.25 0.25 0.25 0.25 0.25 Acres SF % C 0.48 0.54 0.58 0.66 0.73 Concrete 0.06 2,614 24.00 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.16 6,970 64.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 0.7 1.2 1.5 2.1 2.9 Total 0.25 10,890 100	Are a: PG2-S Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.67 0.67 0.67 0.67 0.67 Acres 12,197 41.79 C 0.58 0.65 0.69 0.78 0.84 Concrete 0.13 5,663 19.40 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.26 11,326 38.81 i 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.2 3.7 4.7 6.5 8.9 Total 0.67 29,185 100
Area: A-3 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.85 1.85 1.85 1.85 1.85 Asphalt 0.76 33,106 41.0 C 0.58 0.65 0.69 0.77 0.84 Concrete 0.37 16,117 20.0 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.72 31,363 38.9 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 6.2 10.2 13.0 18.0 24.6 Total 1.85 80,586 100	Area: B2-NE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.52 0.52 0.52 0.52 0.52 Acres 5.02 23.08 08 C 0.58 0.64 0.69 0.77 0.83 Concrete 0.19 8,276 36.54 00 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.21 9,148 40.38 92 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 00 Q 1.7 2.9 3.6 5.0 6.9 Total 0.52 22,651 100	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.24 1.24 1.24 1.24 1.24 1.24 1.24 1.00 0 0.	Area: A-1 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.47 0.47 0.47 0.47 0.47 Asphalt 0.31 13,504 65.96 C 0.67 0.74 0.79 0.88 0.93 Concrete 0.08 3,485 17.02 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.08 3,485 17.02 i 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.8 3.0 3.7 5.2 6.9 Total 0.47 20,473 100	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.47 1.47 1.47 1.47 1.47 0.06 2,614 4.08 C 0.40 0.46 0.50 0.57 0.65 Concrete 0.19 8,276 12.93 Tc 5.00 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 1.22 53,143 82.99 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 3.4 5.7 7.4 10.5 15.2 Total 1.47 64,033 100
Area: B3-NE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.51 0.51 0.51 0.51 0.51 0.51 22,216 100.0 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.2 3.6 4.5 6.2 8.1 Total 0.51 22,216 100	Area: X-4 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.76 0.76 0.76 0.76 0.76 0.76 0.76 5.00 19,602 59.21 00 C 0.58 0.65 0.69 0.77 0.83 Grass, Fair, 2-7% 0.31 13,504 40.79 00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 01 4.576 8.57 10.11 12.54 15.93 0.00 0 0.00 02 2.5 4.2 5.3 7.4 10.0 Total 0.76 33,106 100	Area: Norm Surface Acres SF % Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.92 0.00 0 0 0 0 0 0 0	Area: B4-NE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.49 0.49 0.49 0.49 0.49 0.49 21,344 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.04 0concrete 0.27 11,761 79.60 0.00 0 0 <t< td=""></t<>
Area: B3-N Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.51 0.51 0.51 0.51 0.51 0.51 22,216 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.2 3.6 4.5 6.2 8.1 Total 0.51 22,216 100	Area: I-3 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.67 0.00 <t< td=""><td>Area: D-1 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.86 0.86 0.86 0.86 0.86 Asphalt 0.39 16,988 45.35 C 0.52 0.58 0.62 0.70 0.78 Concrete 0.01 436 1.16 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.46 20,038 53.49 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.6 4.3 5.4 7.6 10.6 Total 0.86 37,462 100</td><td>Area: FG3-S Event 2-yr 10-yr 500-yr Surface Acres SF % Acres 0.69 0.28 0.21 <td< td=""><td>Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.27 0.27 0.27 0.27 0.27 10.0 v 0.07 11,761 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 0 0.00</td></td<></td></t<>	Area: D-1 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.86 0.86 0.86 0.86 0.86 Asphalt 0.39 16,988 45.35 C 0.52 0.58 0.62 0.70 0.78 Concrete 0.01 436 1.16 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.46 20,038 53.49 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.6 4.3 5.4 7.6 10.6 Total 0.86 37,462 100	Area: FG3-S Event 2-yr 10-yr 500-yr Surface Acres SF % Acres 0.69 0.28 0.21 <td< td=""><td>Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.27 0.27 0.27 0.27 0.27 10.0 v 0.07 11,761 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 0 0.00</td></td<>	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.27 0.27 0.27 0.27 0.27 10.0 v 0.07 11,761 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 0 0.00
Area: B3-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.51 0.51 0.51 0.51 0.51 0.51 22,216 100.0 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00	Area: Big Startage Acres S.F % Acres 0.50 0.50 0.50 0.50 0.50 2.1780 100.00 00 C 0.75 0.83 0.88 0.97 1.00 0.00	Area: D-2 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.88 0.88 0.88 0.88 0.88 Asphalt 0.27 11,761 30,68 C 0.46 0.52 0.57 0.64 0.72 Concrete 0.02 871 2.27 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.59 25,700 67.05 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.3 3.9 5.0 7.1 10.1 Total 0.88 38,333 100	Area: i-4 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.27 0.27 0.27 0.27 0.27 0.27 2.9.63 C 0.45 0.51 0.56 0.63 0.70 Grass, Fair, 2-7% 0.19 8,276 70.37 7c 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 <i>i</i> 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 0.7 1.2 1.5 2.1 3.0 Total 0.27 11,761 100	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.95 0.95 0.95 0.95 0.95 Asphalt 0.52 22,651 54,74 C 0.62 0.69 0.74 0.82 0.88 Concrete 0.16 6,970 16.84 Tc 5.00 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.27 11,761 28.42 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 3.4 5.6 7.1 9.8 13.3 Total 0.95 41,382 100
Area: PG4-SE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.61 0.61 0.61 0.61 0.61 26,572 100.0 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.6 4.3 5.4 7.4 9.7 Total 0.61 26,572 100	Area: B1-N Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.38 0.38 0.38 0.38 0.38 0.38 16,553 100.00 0 C 0.75 0.83 0.88 0.97 1.00 0.00 0	D-3 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.29 0.29 0.29 0.29 0.29 Acres 0.29 12,632 100.00 C 0.73 0.81 0.86 0.95 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.2 2.0 2.5 3.5 4.6 Total 0.29 12,632 100	Area: B-7 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.30 0.30 0.30 0.30 0.30 0.30 5.00 Surface 0.16 6,970 53.33 C 0.55 0.62 0.67 0.75 0.80 Grass, Fair, 2-7% 0.14 6,098 46.67 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.0 1.6 2.0 2.8 3.8 Total 0.30 13,068 100	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.88 0.88 0.88 0.88 0.88 0.88 0.77 34,412 89,77 C 0.72 0.80 0.85 0.93 0.99 Concrete 0.06 2,614 6.82 Tc 5.00 5.00 5.00 5.00 Grass, Good, 2-7% 0.03 1,307 3.41 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 3.6 6.0 7.5 10.3 13.8 Total 0.88 38,333 100
Area: PG4-S Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.61 0.61 0.61 0.61 0.61 26,572 100.0 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.6 4.3 5.4 7.4 9.7 Total 0.61 26,572 100	Area: B1-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.38 0.38 0.38 0.38 0.38 0.38 10.00 00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0	Area: CB-C-S Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.35 0.35 0.35 0.35 0.35 Asphalt 0.32 13,939 91.43 C 0.73 0.81 0.86 0.95 1.00 Concrete 0.03 1,307 8.57 7c 5.00 5.00 5.00 5.00 0.00 0 0.00 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.5 2.4 3.0 4.2 5.6 Total 0.35 15,246 100	Area: BMR-S Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.59 0.59 0.59 0.59 0.59 0.59 0.59 100-00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 <td>Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.50 1.50 1.50 1.50 1.50 1.60 1.50 1.50 24.00 C 0.43 0.48 0.53 0.60 0.68 Grass, Fair, 2-7% 1.14 49,658 76.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0 0 0</td>	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.50 1.50 1.50 1.50 1.50 1.60 1.50 1.50 24.00 C 0.43 0.48 0.53 0.60 0.68 Grass, Fair, 2-7% 1.14 49,658 76.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0 0 0
Area: PG4-SW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.61 0.61 0.61 0.61 0.61 26,572 100.0 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.01 0.61 26,572 100.0 Q 2.6 4.3 5.4 7.4 9.7 Total 0.61 26,572 100.0	Area: CONF-5 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.53 0.53 0.53 0.53 0.53 23,087 100.00 0 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0 0.00	Area: CB-C-W Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.76 0.76 0.76 0.76 0.76 0.76 0.00 0.00 0.00 0.00 0.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 <t< td=""><td>Area: RD3-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.45 0.45 0.45 0.45 0.45 0.45 0.45 10.90 55.56 C 0.56 0.63 0.68 0.76 0.81 Grass, Fair, 2-7% 0.20 8,712 44.44 7c 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.5 2.4 3.1 4.3 5.8 Total 0.45 19,602 100</td><td>Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.77 0.77 0.77 0.77 0.77 0.77 500-yr Concrete 0.45 19,602 58,44 C 0.62 0.69 0.74 0.82 0.88 Asphalt 0.12 5,227 15.58 Tc 5.00 5.00 5.00 5.00 5.00 Grass, Fair, 0-2% 0.20 8,712 25.97 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.7 4.5 5.7 7.9 10.8 Total 0.77 33,541 100</td></t<>	Area: RD3-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.45 0.45 0.45 0.45 0.45 0.45 0.45 10.90 55.56 C 0.56 0.63 0.68 0.76 0.81 Grass, Fair, 2-7% 0.20 8,712 44.44 7c 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.5 2.4 3.1 4.3 5.8 Total 0.45 19,602 100	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.77 0.77 0.77 0.77 0.77 0.77 500-yr Concrete 0.45 19,602 58,44 C 0.62 0.69 0.74 0.82 0.88 Asphalt 0.12 5,227 15.58 Tc 5.00 5.00 5.00 5.00 5.00 Grass, Fair, 0-2% 0.20 8,712 25.97 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.7 4.5 5.7 7.9 10.8 Total 0.77 33,541 100
Area: CP-S Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.07 0.07 0.07 0.07 0.07 0.07 3,049 100.0 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 0.3 0.5 0.6 0.9 1.1 Total 0.07 3,049 100	Area: B-4 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.12 0.12 0.12 0.12 0.12 0.00 0.00 0.00 0 0.00 <td< td=""><td>Area: PG1-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.76 0.76 0.76 0.76 0.76 0.76 0.00 0 0.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 3.3 5.4 6.8 9.2 12.1 Total 0.76 33,106 100</td><td>Area: RD2-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.74 0.74 0.74 0.74 0.74 0.74 3.74 3.514 C 0.51 0.57 0.62 0.70 0.77 Concrete 0.07 3.049 9.46 7c 5.00 5.00 5.00 5.00 6.50 Grass, Fair, 2-7% 0.41 17,860 55,41 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.2 3.6 4.6 6.5 9.0 Total 0.74 32,234 100</td><td>Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.50 0.50 0.50 0.50 0.50 0.50 21,780 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.2 3.6 4.4 6.1 8.0 Total 0.50 21,780 100</td></td<>	Area: PG1-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.76 0.76 0.76 0.76 0.76 0.76 0.00 0 0.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 3.3 5.4 6.8 9.2 12.1 Total 0.76 33,106 100	Area: RD2-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.74 0.74 0.74 0.74 0.74 0.74 3.74 3.514 C 0.51 0.57 0.62 0.70 0.77 Concrete 0.07 3.049 9.46 7c 5.00 5.00 5.00 5.00 6.50 Grass, Fair, 2-7% 0.41 17,860 55,41 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.2 3.6 4.6 6.5 9.0 Total 0.74 32,234 100	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.50 0.50 0.50 0.50 0.50 0.50 21,780 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.2 3.6 4.4 6.1 8.0 Total 0.50 21,780 100
Area: A-5 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.02 1.02 1.02 1.02 1.02 1.02 44,431 100.0 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 4.4 7.3 9.1 12.4 16.2 Total 1.02 44,431 100	Area: REP CTR Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.32 0.32 0.32 0.32 0.32 0.32 1.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0	Area: PG1-NE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.76 0.76 0.76 0.76 0.76 0.76 0.76 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 0.00 0 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 3.3 5.4 6.8 9.2 12.1 Total 0.76 33,106 100	Area: RD2-NE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.69 0.69 0.69 0.69 0.69 0.69 0.00 100.00 100.00 0 0.00 0	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.50 0.50 0.50 0.50 0.50 0.50 21,780 100.00 C 0.75 0.83 0.88 0.97 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 2.2 3.6 4.4 6.1 8.0 Total 0.50 21,780 100
Area: A-9 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.01 1.01 1.01 1.01 4.01 4.01 4.01 5.04 0.60 26,136 59.4 C 0.57 0.64 0.68 0.76 0.83 Grass, Fair, 2-7% 0.41 17,860 40.5 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 3.3 5.5 7.0 9.7 13.3 Total 1.01 43,996 100	Area: CB-C-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % 41 Acres 0.76	Area: C-3 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.55 0.55 0.55 0.55 0.55 Asphalt 0.29 12,632 52,73 C 0.59 0.66 0.70 0.78 0.85 Concrete 0.06 2,614 10.91 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.20 8,712 36.36 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.9 3.1 3.9 5.4 7.4 Total 0.55 23,958 100	Area: E-1 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.96 0.96 0.96 0.96 0.96 Asphalt 0.31 13,504 32.29 C 0.54 0.60 0.65 0.73 0.79 Concrete 0.18 7,841 18.75 7c 5.00 5.00 5.00 5.00 5.00 6.30 48.96 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 3.0 5.0 6.3 8.8 12.1 Total 0.96 41,818 100	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.13 1.13 1.13 1.13 1.13 4.002 22,651 46.02 C 0.52 0.58 0.63 0.71 0.78 Concrete 0.01 436 0.88 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.60 26,136 53.10 / 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 3.4 5.6 7.2 10.0 14.0 Total 1.13 49,223 100
Area: B2-N Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.00 0 0.00	Area: B-6 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.37 0.37 0.37 0.37 0.37 Acres 0.17 7,405 45.95 00 C 0.67 0.75 0.80 0.88 0.93 Concrete 0.14 6,098 37.84 00 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.06 2,614 16.22 10 Tc 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 0 I.4 2.4 3.0 4.1 5.5 Total 0.37 16,117 100	Area: John String S	Area: E-3B Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.46 0.46 0.46 0.46 0.46 0.46 20,038 100.00 C 0.73 0.81 0.86 0.95 1.00 0.00 0 0.00 7c 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 1 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.9 3.2 4.0 5.5 7.3 Total 0.46 20,038 100	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.55 0.55 0.55 0.55 0.55 Concrete 0.02 871 3.64 C 0.35 0.40 0.44 0.51 0.60 Grass, Fair, 2-7% 0.53 23,087 96.36 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.1 1.9 2.4 3.5 5.2 Total 0.55 23,958 100
Area: B2-NW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.00 0 0.00 <td>Area: B1-SE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % 0.00 Acres 0.09 0.09 0.09 0.09 0.09 0.09 44.44 00 C 0.52 0.58 0.62 0.70 0.77 Grass, Fair, 2-7% 0.05 2,178 55.56 00 Tc 5.00 5.00 5.00 5.00 0.00</td> <td>Area: CB-C-NE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.00 0</td> <td>Area: E-3C Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.72 0.72 0.72 0.72 0.72 0.72 31,363 100.00 C 0.73 0.81 0.86 0.95 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00</td> <td>Event 2-yr 10-yr 25-yr 100-yr Sourace Acres Strace Acres Strace % Acres 0.74 0.74 0.74 0.74 0.74 0.74 Concrete 0.33 14,375 44.59 C 0.52 0.58 0.63 0.70 0.77 Grass, Fair, 2-7% 0.41 17,860 55.41 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 2.2 3.7 4.7 6.5 9.0 Total 0.74 32,234 100</td>	Area: B1-SE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % 0.00 Acres 0.09 0.09 0.09 0.09 0.09 0.09 44.44 00 C 0.52 0.58 0.62 0.70 0.77 Grass, Fair, 2-7% 0.05 2,178 55.56 00 Tc 5.00 5.00 5.00 5.00 0.00	Area: CB-C-NE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.00 0	Area: E-3C Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.72 0.72 0.72 0.72 0.72 0.72 31,363 100.00 C 0.73 0.81 0.86 0.95 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00	Event 2-yr 10-yr 25-yr 100-yr Sourace Acres Strace Acres Strace % Acres 0.74 0.74 0.74 0.74 0.74 0.74 Concrete 0.33 14,375 44.59 C 0.52 0.58 0.63 0.70 0.77 Grass, Fair, 2-7% 0.41 17,860 55.41 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 2.2 3.7 4.7 6.5 9.0 Total 0.74 32,234 100
Area: A-6 Event 2-yr 10-yr 25-yr 100-yr Son-yr Surface Acres SF % Acres 0.58 0.58 0.58 0.58 0.58 Asphalt 0.38 16,553 65.53 C 0.61 0.69 0.73 0.82 0.88 Concrete 0.03 1,307 5.17 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.17 7,405 29.3 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 2.0 3.4 4.3 5.9 8.1 Total 0.58 25,265 100	Area: B1-SW Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % 52 Acres 0.12 0.12 0.12 0.12 Concrete 0.06 2,614 50.00 7 C 0.54 0.61 0.65 0.73 0.79 Grass, Fair, 2-7% 0.06 2,614 50.00 31 Tc 5.00 5.00 5.00 5.00 0.00 0.00 0 0.00 1/ 5.76 8.57 10.11 12.54 15.93 0.00 0.00 0 0.00 0 0.4 0.6 0.8 1.1 1.5 Total 0.12 5,227 100	Area: RD2-N Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.69 0.69 0.69 0.69 0.69 0.69 0.00	Area: CB-CE Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.76	event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.10 1.10 1.10 1.10 1.10 1.00 1.00 0.00 0.000
Area: B2-W Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.24 0.24 0.24 0.24 0.24 Acres 0.24 10,454 100.0 C 0.73 0.81 0.86 0.95 1.00 0.00 0 0.00 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 1.0 1.7 2.1 2.9 3.8 Total 0.24 10,454 100	Area: B-8 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % 0.00 Acres 1.17 1.17 1.17 1.17 Concrete 0.12 5,227 10.26 0.01 C 0.37 0.43 0.47 0.54 0.62 Grass, Fair, 2-7% 1.05 45,738 89.74 0.01 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 0.01 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 0.01 Q 2.5 4.3 5.5 7.9 11.6 Total 1.17 50,965 100	Area: B-3 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.57 1.57 1.57 1.57 1.57 0.57 0.51 0.51 0.52 27,007 39.49 C 0.58 0.65 0.70 0.78 0.83 Grass, Fair, 2-7% 0.62 27,007 39.49 Tc 5.00 5.00 5.00 5.00 0.00 0 0.000 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 5.3 8.8 11.1 15.4 20.9 Total 1.57 68,389 100	Area: Formation of the stress of	Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.15 0.15 0.15 0.15 0.15 Grass, Fair, 2-7% 0.09 3,920 60.00 C 0.50 0.56 0.60 0.68 0.75 Concrete 0.06 2,614 40.00 Tc 5.00 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 Q 0.4 0.7 0.9 1.3 1.8 Total 0.15 6,534 100
Area: A-7 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 1.83 1.83 1.83 1.83 1.83 1.83 0.18 7,841 9.84 C 0.37 0.42 0.47 0.54 0.62 Grass, Fair, 2-7% 1.65 71,874 90.1 Tc 5.00 5.00 5.00 5.00 0.00 0 0.00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 Q 3.9 6.7 8.6 12.3 18.1 Total 1.83 79,715 100	Area: B-5 Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % 44 Acres 1.05 1.05 1.05 1.05 Acres 0.60 26,136 57.14 16 C 0.60 0.67 0.72 0.80 0.86 Concrete 0.11 4,792 10.48 00 Tc 5.00 5.00 5.00 5.00 Grass, Fair, 2-7% 0.34 14,810 32.38 00 I 5.76 8.57 10.11 12.54 15.93 0.00 0 0.00 0 0.00 0 Q 3.6 6.1 7.6 10.6 14.4 Total 1.05 45,738 100	Area: J0-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.20 0.20 0.20 0.20 0.20 0.20 3,049 3,049 3,049 3,040	Area: FG2-N Event 2-yr 10-yr 25-yr 100-yr 500-yr Surface Acres SF % Acres 0.98 0.98 0.98 0.98 0.98 0.98 0.98 0.00	Event2-yr10-yr25-yr100-yr500-yrSurfaceAcresSF%Acres1.031.031.031.031.03Asphalt0.2711,76126.21C0.510.570.620.690.76Concrete0.187,84117.48Tc5.005.005.005.005.00Grass, Fair, 2-7%0.5825,26556.31/5.768.5710.1112.5415.930.0000.00Q3.05.06.49.012.5Total1.0344,867100

01649-00031/Civil\00-CAD\Replacement SDP\101649-00031-DAM-CALC.dwg modified by irussell on Mar 28, 24 5:19 PN

				S	TM F NET	WORK			
rea:						F-7			
/ent	2-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
cres	0.12	0.12	0.12	0.12	0.12	Concrete	0.12	5,140	100.00
C Tc	U.75	U.83	0.88	0.97 5.00	1.00 1.00		0.00	U	
1	5.76	3.00 8.57	3.00 10 11	5.00 12 54	5.00 15 93		0.00	n	0.00
Q	0.5	0.8	1.0	1.4	1.9	Total	0.12	5.140	100
								_,	
						F-8			
vent	2-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
cres	0.07	0.07	0.07	0.07	0.07	Asphalt	0.05	2,178	71.43
C T	0.62	0.69	0.73	0.82	0.88	Grass, Fair, 2-7%	0.02	871	28.57
	5.00	5.00 8.57	5.00 10.11	5.00 12.54	5.00 15.93		0.00	0	0.00
Q	0.2	0.4	0.5	0.7	1.0	Total	0.07	3,049	100
ea:						F-9			
vent	2-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
cres	0.07	0.07	0.07	0.07	0.07	Asphalt	0.05	2,178	71.43
C Tc	0.62 5.00	0.69 5.00	U.73 5 00	U.82 5 NN	U.88 5 00	Gruss, Fair, 2-7%	0.02	۲/۶ ۱	∠8.57 0.00
1	5.76	8.57	10.11	12.54	15.93		0.00	0	0.00
Q	0.2	0.4	0.5	0.7	1.0	Total	0.07	3,049	100
a:						F-10			
vent	2-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
Acres	0.07 0.67	0.07 0.75	0.07	0.07	0.07	Asphalt Grass Eair 2,7%	0.06	2,614 126	85.71
Tc	5.00	5.00	0.80 5.00	0.88 5.00	0.94 5.00	Gruss, Fuir, 2-7%	0.01	430 0	0.00
1	5.76	8.57	10.11	12.54	15.93		0.00	0	0.00
Q	0.3	0.4	0.6	0.8	1.0	Total	0.07	3,04 9	100
ea:						F-11			
vent	2-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
C	0.10 0.65	0.10 0.72	0.10 0 77	0.10 0.86	0.10 N 92	Asphalt Grass Eair 2-7%	0.08	3,485 871	80.00 20.00
Tc	5.00	5.00	5.00	5.00	5.00	01033, 1 Uli, 2-770	0.02	0	0.00
I	5.76	8.57	10.11	12.54	15.93		0.00	0	0.00
Q	0.4	0.6	0.8	1.1	1.5	Total	0.10	4,356	100
ea:	3	10	35	100	E00 ····	F-12	Λ στο σ	с г	0/
Acres	∠-y r 0.20	0,20	0,20	<u> </u>	<u> </u>	Asphalt	0.16	6.970	20.00
С	0.65	0.72	0.77	0.86	0.92	Grass, Fair, 2-7%	0.04	1,742	20.00
Тс	5.00	5.00	5.00	5.00	5.00		0.00	0	0.00
1	5.76	8.57	10.11	12.54	15.93		0.00	0	0.00
Q	0.7	1.2	1.6	2.2	2.9	Total	0.20	8,712	100
a: vent	2-1/r	10-vr	25_vr	10 ட .vr	500-1/2	G-1W Surface	Acros	٩F	%
cres	0.45	0.45	ريم 0.45	0.45	0.45	Grass, Fair, 2-7%	0.45	19,602	100.00
С	0.33	0.38	0.42	0.49	0.58	, , , , , , , , , , , , , , , , , , , ,	0.00	0	0.00
Тс	5.00	5.00	5.00	5.00	5.00		0.00	0	0.00
1	5.76	8.57	10.11	12.54	15.93	Tetel	0.00	0	0.00
ų	0.9	1.5	1.9	2.8	4.2	ιοται	0.45	19,602	100
						C 15]
a: /ent	2-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
Acres	0.30	0.30	0.30	0.30	0.30	Grass, Fair, 2-7%	0.30	13,068	100.00
С	0.33	0.38	0.42	0.49	0.58		0.00	0	0.00
Tc	5.00	5.00	5.00	5.00	5.00		0.00	0	0.00
Q	0.6	ö.57	10.11 1.3	12.54 1.8	15.93 2.8	Total	0.00	13,068	100
a:						G3-N			
vent	2-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
Acres	1.35	1.35	1.35	1.35	1.35	Concrete	1.35	58,588	100.00
C Tc	0.75 5.00	0.83	0.88	0.97	1.00		0.00	0	0.00
IC I	5.00 5.76	5.00 8.57	5.00 10.11	5.00 12.54	5.00 15.93		0.00	0	0.00
Q	5.8	9.6	12.0	16.4	21.4	Total	1.35	58,588	100
									_
ea:						G3-S			
Event	2-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
Acres	1.54	1.54	1.54	1.54	1.54	Concrete	1.54	67,170	100.00
C Tc	0.75 5 00	0.83	0.88 5 00	0.97 5.00	1.00		0.00	0	0.00
l I	5.00 5.76	5.00 8.57	5.00 10.11	5.00 12.54	5.00 15.93		0.00	0	0.00
Q	6.7	11.0	13.7	18.8	24.6	Total	1.54	67,170	100
-						•			

					H-1			
-vr	10-vr	25-vr	100-vr	500-vr	Surface	Acres	SE	%
11	2 11	2.11	2 11	2 11	Grass Good 2-7%	2 11	91 912	100.00
29	0.35	0.39	0.46	0.56		0.00	0	0.00
.25	5.00	5.00	5.40	5.00		0.00	0	0.00
.00 76	9.00 8.57	10 11	12 54	15 93		0.00	0	0.00
35	63	83	12.34	18.8	Total	2 11	91 912	100
,,,,,	0.5	0.5	16.6	10.0	lotai	2.11	51,512	100
					J-1			
-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
.87	2.87	2.87	2.87	2.87	Grass, Fair, 2-7%	2.87	124,974	100.00
.33	0.38	0.42	0.49	0.58		0.00	0	0.00
.00	5.00	5.00	5.00	5.00		0.00	0	0.00
.76	8.57	10.11	12.54	15.93		0.00	0	0.00
5.4	9.3	12.2	17.6	26.5	Total	2.87	124,974	100
					J-2			
-vr	10-vr	25-vr	100-vr	500-vr	Surface	Acres	SF	%
.11	0.11	0.11	0.11	0.11	Concrete	0.11	4,792	100.00
.75	0.83	0.88	0.97	1.00		0.00	0	0.00
.00	5.00	5.00	5.00	5.00		0.00	0	0.00
76	8 57	10 11	12 54	15 93		0.00	Õ	0.00
	0.8	1.0	1.3	1.8	Total	0.11	4,792	100
					J-3			
-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
.10	0.10	0.10	0.10	0.10	Concrete	0.10	4,312	100.00
.75	0.83	0.88	0.97	1.00		0.00	0	0.00
.00	5.00	5.00	5.00	5.00		0.00	0	0.00
.76	8.57	10.11	12.54	15.93		0.00	0	0.00
).4	0.7	0.9	1.2	1.6	Total	0.10	4,312	100
					J-4			
-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
.14	0.14	0.14	0.14	0.14	Concrete	0.14	5,881	100.00
.75	0.83	0.88	0.97	1.00		0.00	0	0.00
.00	5.00	5.00	5.00	5.00		0.00	0	0.00
.76	8.57	10.11	12.54	15.93		0.00	0	0.00
).6	1.0	1.2	1.6	2.1	Total	0.14	5,881	100
	47		455		J-5	-		
-yr	10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
.13	0.13	0.13	0.13	0.13	Concrete	0.13	5,619	100.00
.75	0.83	0.88	0.97	1.00		0.00	0	0.00
.00	5.00	5.00	5.00	5.00		0.00	0	0.00
.76	8.57	10.11	12.54	15.93		0.00	0	0.00
).6	0.9	1.1	1.6	2.1	Total	0.13	5,619	100

				J-6			
10-yr	25-yr	100-yr	500-yr	Surface	Acres	SF	%
0.25	0.25	0.25	0.25	Asphalt	0.25	10,846	100.00
0.81	0.86	0.95	1.00		0.00	0	0.00
5.00	5.00	5.00	5.00		0.00	0	0.00
8.57	10.11	12.54	15.93		0.00	0	0.00
1.7	2.2	3.0	4.0	Total	0.25	10,846	100

CAPSTONE Control 6900 W. PARMER LANE INLET CALCULATIONS 2 OF 2 APPLE INC. INLET CALCULATIONS 2 OF 2	DRAWN BY:SPM	DESIGNED BY: ANG, IHR, HCH QA / QC: JDP	PROJECT NO.: 101649.00031
INLET CALCULATIONS 2 OF 2	CAPSTONE	6900 W. PAKMEK LANE	APPLE INC.
DATE NO. DATE NO. DATE NO. DATE NO. DATE NO. REVISION REV			
REVISION REVISION REVISION REVISION TOB Rialto Blvd., Suite 125 Austin, Texas 78735 Tel. (512) 298-3284 Fax (512) 298-255 TBPE # F-14629 Garza EMC, LLC © Copyright 2024	DATE NO.	ANDRA A. BO 138951 SONAL EN SONAL EN	10 DONE 3 000 e 9/2024
<u>6</u>		7708 Rialto Blvd., Suite 125 Austin, Texas 78735	lei. (512) 298-3284 Fax (512) 298-2592 TBPE # F-14629 Garza EMC, LLC © Copyright 2024

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