LIVELY TRACT PHASE 2 Modified Contributing Zone Plan Application

April 2025



LIVELY TRACT PHASE 2 Modified Contributing Zone Plan Application

Pape-Dawson Consulting Engineers, LLC. 10801 N. MoPac Expy. Bldg. 3, Suite 200 Austin, Texas 78759 (512) 454-8711 Email: tkrause@pape-dawson.com

April 2025



April 8, 2025

Ms. Leah Whallon Texas Commission on Environmental Quality - Region 11 12100 Park 35 Circle, Bldg. A Austin, Texas 78753

Re: Lively Tract, Phase 2 Modified Contributing Zone Plan

Dear Ms. Whallon:

Please find attached one (1) original, one (1) copy and one (1) digital copy of the Lively Tract, Phase 2 Modified Contributing Zone Plan (CZP). This Modified Contributing Zone Plan has been prepared in accordance with the Texas Administrative Code (30 TAC 213), and current policies for development over the Edwards Aquifer Recharge Zone.

This Contributing Zone Plan applies to an approximate 120.60-acre site as identified by the project limits. Please review the plan information for the items it is intended to address. If acceptable, please provide a written approval of the plan in order that construction may begin at the earliest opportunity.

Appropriate review fee (\$8,000) and application fee are included. If you have any questions or require additional information, please do not hesitate to contact me at your earliest convenience.

Sincerely, Pape-Dawson Consulting Engineers, LLC.

Dustin Goss, P.E., LEED® AP Vice President

H:\PROJECTS\508\16\26\307 CONTRIBUTING ZONE PLAN\REFORT\LETTER.DOCX



Texas Commission on Environmental Quality Edwards Aquifer Application Cover Page

Our Review of Your Application

The Edwards Aquifer Program staff conducts an administrative and technical review of all applications. The turnaround time for administrative review can be up to 30 days as outlined in 30 TAC 213.4(e). Generally administrative completeness is determined during the intake meeting or within a few days of receipt. The turnaround time for technical review of an administratively complete Edwards Aquifer application is 90 days as outlined in 30 TAC 213.4(e). Please know that the review and approval time is directly impacted by the quality and completeness of the initial application that is received. In order to conduct a timely review, it is imperative that the information provided in an Edwards Aquifer application include final plans, be accurate, complete, and in compliance with <u>30 TAC 213</u>.

Administrative Review

1. <u>Edwards Aquifer applications</u> must be deemed administratively complete before a technical review can begin. To be considered administratively complete, the application must contain completed forms and attachments, provide the requested information, and meet all the site plan requirements. The submitted application and plan sheets should be final plans. Please submit one full-size set of plan sheets with the original application, and half-size sets with the additional copies.

To ensure that all applicable documents are included in the application, the program has developed tools to guide you and web pages to provide all forms, checklists, and guidance. Please visit the below website for assistance: <u>http://www.tceq.texas.gov/field/eapp</u>.

- 2. This Edwards Aquifer Application Cover Page form (certified by the applicant or agent) must be included in the application and brought to the administrative review meeting.
- 3. Administrative reviews are scheduled with program staff who will conduct the review. Applicants or their authorized agent should call the appropriate regional office, according to the county in which the project is located, to schedule a review. The average meeting time is one hour.
- 4. In the meeting, the application is examined for administrative completeness. Deficiencies will be noted by staff and emailed or faxed to the applicant and authorized agent at the end of the meeting, or shortly after. Administrative deficiencies will cause the application to be deemed incomplete and returned.

An appointment should be made to resubmit the application. The application is re-examined to ensure all deficiencies are resolved. The application will only be deemed administratively complete when all administrative deficiencies are addressed.

- 5. If an application is received by mail, courier service, or otherwise submitted without a review meeting, the administrative review will be conducted within 30 days. The applicant and agent will be contacted with the results of the administrative review. If the application is found to be administratively incomplete, it can be retrieved from the regional office or returned by regular mail. If returned by mail, the regional office may require arrangements for return shipping.
- 6. If the geologic assessment was completed before October 1, 2004 and the site contains "possibly sensitive" features, the assessment must be updated in accordance with the *Instructions to Geologists* (TCEQ-0585 Instructions).

Technical Review

- 1. When an application is deemed administratively complete, the technical review period begins. The regional office will distribute copies of the application to the identified affected city, county, and groundwater conservation district whose jurisdiction includes the subject site. These entities and the public have 30 days to provide comments on the application to the regional office. All comments received are reviewed by TCEQ.
- 2. A site assessment is usually conducted as part of the technical review, to evaluate the geologic assessment and observe existing site conditions. The site must be accessible to our staff. The site boundaries should be

clearly marked, features identified in the geologic assessment should be flagged, roadways marked and the alignment of the Sewage Collection System and manholes should be staked at the time the application is submitted. If the site is not marked the application may be returned.

- 3. We evaluate the application for technical completeness and contact the applicant and agent via Notice of Deficiency (NOD) to request additional information and identify technical deficiencies. There are two deficiency response periods available to the applicant. There are 14 days to resolve deficiencies noted in the first NOD. If a second NOD is issued, there is an additional 14 days to resolve deficiencies. If the response to the second notice is not received, is incomplete or inadequate, or provides new information that is incomplete or inadequate, the application must be withdrawn or will be denied. Please note that because the technical review is underway, whether the application is withdrawn or denied **the application fee will be forfeited**.
- 4. The program has 90 calendar days to complete the technical review of the application. If the application is technically adequate, such that it complies with the Edwards Aquifer rules, and is protective of the Edwards Aquifer during and after construction, an approval letter will be issued. Construction or other regulated activity may not begin until an approval is issued.

Mid-Review Modifications

It is important to have final site plans prior to beginning the permitting process with TCEQ to avoid delays.

Occasionally, circumstances arise where you may have significant design and/or site plan changes after your Edwards Aquifer application has been deemed administratively complete by TCEQ. This is considered a "Mid-Review Modification". Mid-Review Modifications may require redistribution of an application that includes the proposed modifications for public comment.

If you are proposing a Mid-Review Modification, two options are available:

- If the technical review has begun your application can be denied/withdrawn, your fees will be forfeited, and the plan will have to be resubmitted.
- TCEQ can continue the technical review of the application as it was submitted, and a modification application can be submitted at a later time.

If the application is denied/withdrawn, the resubmitted application will be subject to the administrative and technical review processes and will be treated as a new application. The application will be redistributed to the affected jurisdictions.

Please contact the regional office if you have questions. If your project is located in Williamson, Travis, or Hays County, contact TCEQ's Austin Regional Office at 512-339-2929. If your project is in Comal, Bexar, Medina, Uvalde, or Kinney County, contact TCEQ's San Antonio Regional Office at 210-490-3096

Please fill out all required fields below and submit with your application.

1. Regulated Entity Name: Lively Tract, Phase 2				2. Regulated Entity No.: RN110606126				
3. Customer Name: H	ures 2015 LP			4. Customer No.: 605112077				
5. Project Type: (Please circle/check one)	New	Modification H		Extension		Exception		
6. Plan Type: (Please circle/check one)	WPAI CZP	SCS	UST	AST	EXP	EXT	Technical Clarification	Optional Enhanced Measures
7. Land Use: (Please circle/check one)	Residential	Non-residential		8. Site		e (acres):	120.60	
9. Application Fee:	\$8,000	10. Permanent l			BMP(s):		2 Batch Detention, Vegetative Filter Strips	
11. SCS (Linear Ft.):	N/A	12. AST/UST (N			o. Tanks):		N/A	
13. County:	Williamson	14. Watershed:				South Fork San Gabriel River		Gabriel River

Application Distribution

Instructions: Use the table below to determine the number of applications required. One original and one copy of the application, plus additional copies (as needed) for each affected incorporated city, county, and groundwater conservation district are required. Linear projects or large projects, which cross into multiple jurisdictions, can require additional copies. Refer to the "Texas Groundwater Conservation Districts within the EAPP Boundaries" map found at:

http://www.tceq.texas.gov/assets/public/compliance/field_ops/eapp/EAPP%20GWCD%20map.pdf

For more detailed boundaries, please contact the conservation district directly.

Austin Region								
County:	Hays	Travis	Williamson					
Original (1 req.)								
Region (1 req.)								
County(ies)								
Groundwater Conservation District(s)	Edwards Aquifer Authority Barton Springs/ Edwards Aquifer Hays Trinity Plum Creek	Barton Springs/ Edwards Aquifer	NA					
City(ies) Jurisdiction	Austin Buda Dripping Springs Kyle Mountain City San Marcos Wimberley Woodcreek	Austin Bee Cave Pflugerville Rollingwood Round Rock Sunset Valley West Lake Hills	Austin Cedar Park Florence Georgetown Jerrell √_Leander Liberty Hill Pflugerville Round Rock					

San Antonio Region								
County:	Bexar	Comal	Kinney	Medina	Uvalde			
Original (1 req.)								
Region (1 req.)								
County(ies)								
Groundwater Conservation District(s) — Edwards Aquifer Authority Trinity-Glen Rose		Edwards Aquifer Authority	Kinney	_KinneyEAA Medina				
City(ies) Jurisdiction	Castle Hills Fair Oaks Ranch Helotes Hill Country Village Hollywood Park San Antonio (SAWS) Shavano Park	Bulverde Fair Oaks Ranch Garden Ridge New Braunfels Schertz	NA	San Antonio ETJ (SAWS)	NA			

I certify that to the best of my knowledge, that the application is complete and accurate. This application is hereby submitted to TCEQ for administrative review and technical review.

DUSTIN GOSS Print Name of Customer/Authorized Agent

Signature of Customer/Authorized Agent

4/8/2025 Date

FOR TCEQ INTERNAL USE ONLY						
Date(s)Reviewed: Date Administratively Complete:						
Received From:	Correct Number of Copies:					
Received By:	Distribution Date:					
EAPP File Number:	Complex:					
Admin. Review(s) (No.):	No. AR Rounds:					
Delinquent Fees (Y/N):	Review Time Spent:					
Lat./Long. Verified:	SOS Customer Verification:					
Agent Authorization Complete/Notarized (Y/N):	Payable to TCEQ (Y/N):		/N):			
Core Data Form Complete (Y/N):	Check:	Signed (Y/N):				
Core Data Form Incomplete Nos.:		Less than 90 days old (Y/				

CONTRIBUTING ZONE PLAN MODIFICATION

Modification of a Previously Approved Contributing Zone Plan

Texas Commission on Environmental Quality

for Regulated Activities on the Edwards Aquifer Recharge Zone and Transition Zone and Relating to 30 TAC 213.4(j), Effective June 1, 1999

To ensure that the application is administratively complete, confirm that all fields in the form are complete, verify that all requested information is provided, consistently reference the same site and contact person in all forms in the application, and ensure forms are signed by the appropriate party.

Note: Including all the information requested in the form and attachments contributes to more streamlined technical reviews.

Signature

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This **Modification of a Previously Approved Contributing Zone Plan** is hereby submitted for TCEQ review and executive director approval. The request was prepared by:

Print Name of Customer/Agent: Dustin Goss, P.E., LEED AP®

Date: 4/8/25

Signature of Customer/Agent:

Project Information

 Current Regulated Entity Name: <u>Lively Tract, Phase 2</u> Original Regulated Entity Name: <u>Lively Tract, Phase 2</u> Assigned Regulated Entity Number(s) (RN): <u>RN110606126</u> Edwards Aquifer Protection Program ID Number(s): <u>11002658</u>
 The applicant has not changed and the Customer Number (CN) is: 605112077

The applicant or Regulated Entity has changed. A new Core Data Form has been provided.

- 2. X Attachment A: Original Approval Letter and Approved Modification Letters. A copy of the original approval letter and copies of any modification approval letters are attached.
- 3. A modification of a previously approved plan is requested for (check all that apply):

Any physical or operational modification of any best management practices or structure(s), including but not limited to temporary or permanent ponds, dams, berms, silt fences, and diversionary structures;

Any change in the nature or character of the regulated activity from that which was originally approved;

- A change that would significantly impact the ability to prevent pollution of the Edwards Aquifer and hydrologically connected surface water; or
- Any development of land previously identified in a contributing zone plan as undeveloped.
- 4. Summary of Proposed Modifications (select plan type being modified). If the approved plan has been modified more than once, copy the appropriate table below, as necessary, and complete the information for each additional modification.

CZP Modification	Approved Project	Approved Modification #1
Summary		
Acres	<u>80.43 Ac</u>	<u>109.88 Ac</u>
Type of Development	Residential Single Family	Residential Single Family
Number of Residential	<u>58</u>	<u>136</u>
Lots		
Impervious Cover (acres)	<u>7.44 Ac</u>	<u>20.47 Ac</u>
Impervious Cover (%)	<u>9.26%</u>	<u>18.63%</u>
Permanent BMPs	1 batch detention basin;	2 batch detention basins;
Other	<u>VFS</u>	<u>VFS</u>
AST Modification	Approved Project	Proposed Modification
Summary		
Number of ASTs	<u>0</u>	<u>0</u>
Other	<u>0</u>	<u>0</u>
UST Modification	Approved Project	Proposed Modification
Summary		
Number of USTs	<u>0</u>	<u>0</u>
Other	<u>0</u>	<u>0</u>

CZP Modification	Approved Modification #2	Proposed Modification #3
Summary		
Acres	<u>116.70 Ac</u>	<u>120.60 Ac</u>
Type of Development	Residential Single Family	Residential Single Family
Number of Residential	<u>334</u>	<u>429</u>
Lots		
Impervious Cover (acres)	<u>48.77 Ac</u>	<u>63.15 Ac</u>
Impervious Cover (%)	<u>41.79%</u>	<u>52.36%</u>
Permanent BMPs	2 batch detention basins;	2 batch detention basins;
Other	<u>VFS</u>	<u>VFS</u>
AST Modification	Approved Project	Proposed Modification
Summary		
Number of ASTs	<u>0</u>	<u>0</u>
Other	<u>0</u>	<u>0</u>
UST Modification	Approved Project	Proposed Modification
Summary		
Number of USTs	<u>0</u>	<u>0</u>
Other	<u>0</u>	<u>0</u>

- 5. Attachment B: Narrative of Proposed Modification. A detailed narrative description of the nature of the proposed modification is attached. It discusses what was approved, including previous modifications, and how this proposed modification will change the approved plan.
- 6. Attachment C: Current Site Plan of the Approved Project. A current site plan showing the existing site development (i.e., current site layout) at the time this application for modification is attached. A site plan detailing the changes proposed in the submitted modification is required elsewhere.
 - The approved construction has not commenced. The original approval letter and any subsequent modification approval letters are included as Attachment A to document that the approval has not expired.
 - The approved construction has commenced and has been completed. Attachment C illustrates that the site was constructed as approved.

	The approved construction has commenced and has been completed. Attachment C
	illustrates that the site was not constructed as approved.
	The approved construction has commenced and has not been completed.
	Attachment C illustrates that, thus far, the site was constructed as approved.
	The approved construction has commenced and has not been completed.
	Attachment C illustrates that, thus far, the site was not constructed as approved.
7.	 Acreage has not been added to or removed from the approved plan. Acreage has been added to or removed from the approved plan and is discussed in Attachment B: Narrative of Proposed Modification.
8.	Submit one (1) original and one (1) copy of the application, plus additional copies as needed for each affected incorporated city, groundwater conservation district, and county in which the project will be located. The TCEQ will distribute the additional

county in which the project will be located. The TCEQ will distribute the additional copies to these jurisdictions. The copies must be submitted to the appropriate regional office.

ATTACHMENT A

2019033715 AFF Total Pages: 18

Deed Recordation Affidavit

Contributing Zone Plan

THE STATE OF TEXAS §

County of Travis §

1.4

BEFORE ME, the undersigned authority, on this day personally appeared <u>David Nairne</u> who, being duly sworn by me deposes and says:

- That my name is <u>David Nairne</u> and that I own the real property described below.
- (2) That said real property is subject to an CONTRIBUTING ZONE PLAN which was required under the 30 Texas Administrative Code (TAC) Chapter 213.
- (3) That the CONTRIBUTING ZONE PLAN for said real property was approved by the Texas Commission on Environmental Quality (TCEQ) on <u>March 13, 2019</u>.

A copy of the letter of approval from the TCEQ is attached to this affidavit as Exhibit A and is incorporated herein by reference.

(4) The said real property is located in <u>Williamson</u> County, Texas, and the legal description of the property is as follows: SEE ATTACHED EXHIBIT ''B''

NAIRNE DAVID LANDOWNER-AFFIANT SWORN AND SUBSCRIBED TO before me, on this 27 Bay of N

THE STATE OF Texas §

MARY HELEN TELLO My Notary ID # 126626500

Expires August 14, 2020

County of Travis §

BEFORE ME, the undersigned authority, on this day personally appeared <u>David Nairne</u> known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that (s)he executed same for the purpose and consideration therein expressed.

GIVEN under my hand and seal of office on this 27 day of March , 2019

PUBLIC TARY elen 10 Typed or Printed Name of Notary

MY COMMISSION EXPIRES: 08/14/2020

Jon Niermann, *Chairman* Bobby Janecka, *Commissioner* Catarina R. Gonzales, *Commissioner* Kelly Keel, *Executive Director*



TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

June 14, 2024

Mr. Tom Rielly HWY 29 Ventures 2015, LP 4910 Campus Drive Newport Beach, CA 92660

Re: Modification of an approved Contributing Zone Plan (CZPMOD) Lively Tract Phase 2; Located SW of Cross Creek Rd. and SH29; Leander, Williamson County, Texas Edwards Aquifer Protection Program ID: 11003979, Regulated Entity No. RN110606126

Dear Mr. Rielly:

The Texas Commission on Environmental Quality (TCEQ) has completed its review on the application for the above-referenced project submitted to the Edwards Aquifer Protection Program (EAPP) by Pape-Dawson Engineers, Inc. on behalf of the applicant, HWY 29 Ventures 2015 on April 23, 2024.

As presented to the TCEQ, the application was prepared in general compliance with the requirements of 30 Texas Administrative Codes (TAC) Chapter §213. The permanent best management practices (BMPs) and measures represented in the application were prepared by a Texas licensed professional engineer (PE). All construction plans and design information were sealed, signed, and dated by a Texas licensed PE. Therefore, the application for the construction of the proposed project and methods to protect the Edwards Aquifer are **approved**, subject to applicable state rules and the conditions in this letter.

This approval expires two years from the date of this letter, unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been officially requested. This approval or extension will expire, and no extension will be granted if more than 50 percent of the project has not been completed within ten years from the date of this letter.

The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this contributing zone plan or modification to a plan. A motion for reconsideration must be filed in accordance with 30 TAC §50.139.

BACKGROUND

The Lively Tract Phase 2 Contributing Zone Plan (CZP) was approved by letter dated March 13, 2019 (EAPP ID No. 11001396). The CZP consisted of 80.4 acres of a single-family residential development. A CZPMOD was approved by letter dated October 29, 2021 (EAP ID No. 11002658). The CZPMOD increased the approved acreage of the development to 109.88 acres

TCEQ Region 11 · P.O. Box 13087 · Austin, Texas 78711-3087 · 512-339-2929 · Fax 512-339-3795

Mr. Tom Rielly Page 2 June 14, 2024

PROJECT DESCRIPTION

The proposed residential project will have a total area of approximately 116.70 acres, an increase of 6.9 acres. The modification will include the construction of single-family residences, drives, utilities, streets, sidewalks, and associated appurtenances. The impervious cover will be increased to 48.77 acres (41.79 percent) for the Lively Tract Phase 2 development. Project wastewater will be disposed of by conveyance to the existing San Gabriel Wastewater Treatment Plant.

PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, two previously approved engineered vegetative filter strips (VFS D and VFS E approved under EAPP ID No. 11001396) and two previously approved batch detention basins (Pond H approved under EAPP ID No. 11001396; and, Pond J approved under EAPP ID No. 11002658), designed using the TCEQ technical guidance, *RG-348, Complying with the Edwards Aquifer Rules: Technical Guidance on Best Management Practices,* will be used to treat stormwater runoff. The required total suspended solids (TSS) treatment for this project is 42,449 pounds of TSS generated from the 48.77 acres of impervious cover. The approved permanent BMPs and measures meet the required 80 percent removal of the increased load in TSS caused by the project.

The permanent BMPS shall be operational prior to occupancy or use of the proposed project. Inspection, maintenance, repair, and retrofit of the permanent BMPs shall be in accordance with the approved application.

SPECIAL CONDITIONS

I. This modification is subject to all the special and standard conditions listed in the approval letters dated March 13, 2019 (EAPP ID No. 11001396) and October 29, 2021 (EAP ID No. 11002658).

STANDARD CONDITIONS

- 1. The plan holder (applicant) must comply with all provisions of 30 TAC Chapter §213 and all technical specifications in the approved plan. The plan holder should also acquire and comply with additional and separate approvals, permits, registrations or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, Dam Safety, Underground Injection Control) as required based on the specifics of the plan.
- 2. In addition to the rules of the Commission, the plan holder must also comply with state and local ordinances and regulations providing for the protection of water quality as applicable.

Prior to Commencement of Construction:

- 3. The plan holder of any approved contributing zone plan must notify the EAPP and obtain approval from the executive director prior to initiating any modification to the activities described in the referenced application following the date of the approval.
- 4. The plan holder must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the EAPP no later than 48 hours prior to commencement of the regulated activity. Notification must include the date on which the regulated activity will commence, the name

Mr. Tom Rielly Page 3 June 14, 2024

> of the approved plan and program ID number for the regulated activity, and the name of the prime contractor with the name and telephone number of the contact person.

5. Temporary erosion and sedimentation (E&S) controls as described in the referenced application, must be installed prior to construction, and maintained during construction. Temporary E&S controls may be removed when vegetation is established, and the construction area is stabilized. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.

During Construction:

- 6. The application must indicate the placement of permanent aboveground storage tanks facilities for static hydrocarbons and hazardous substances with cumulative storage capacity of 500 gallons or more. Subsequent permanent storage tanks on this project site require a modification to be submitted and approved prior to installation.
- 7. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50 percent. Litter, construction debris, and construction chemicals shall be prevented from becoming stormwater discharge pollutants.
- 8. Intentional discharges of sediment laden water are not allowed. If dewatering becomes necessary, the discharge must be filtered through appropriately selected BMPs.
- 9. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 10. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.

After Completion of Construction:

- 11. Owners of permanent BMPs and temporary measures must ensure that the BMPs and measures are constructed and function as designed. A Texas licensed PE **must certify** in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the EAPP within 30 days of site completion.
- 12. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property or the ownership of the property is transferred to the entity. A copy of the transfer of responsibility must be filed with the executive director through the EAPP within 30 days of the transfer. TCEQ form, Change in Responsibility for Maintenance on Permanent BMPs and Measures (TCEQ-10263), may be used.

Mr. Tom Rielly Page 4 June 14, 2024

The holder of the approved contributing zone plan is responsible for compliance with Chapter §213 subchapter B and any condition of the approved plan through all phases of plan implementation. Failure to comply with any condition within this approval letter is a violation of Chapter §213 subchapter B and is subject to administrative rule or orders and penalties as provided under §213.25 of this title (relating to Enforcement). Such violations may also be subject to civil penalties and injunction. Upon legal transfer of this property, the new owner is required to comply with all terms of the approved contributing zone plan.

This action is taken as delegated by the executive director of the Texas Commission on Environmental Quality. If you have any questions or require additional information, please contact Mr. James "Bo" Slone, P.G. of the Edwards Aquifer Protection Program at (512) 239-6994 or the regional office at 512-339-6994.

Sincerely, Lori Wilson, Director

Austin Region Texas Commission on Environmental Quality

LW/jcs

cc: Mr. Dustin Goss, P.E., Pape-Dawson Engineers, Inc.

Jon Niermann, *Chairman* Emily Lindley, *Commissioner* Bobby Janecka, *Commissioner* Toby Baker, *Executive Director*



TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

October 29, 2021

Mr. Tom Reilly Hwy 29 Ventures 2015, LP 4910 Campus Dr. New Port Beach, CA 92660

Re: Edwards Aquifer, Williamson County

NAME OF PROJECT: Lively Tract Phase 2; Located S.W. of Cross Creek Rd. and SH 29; Leander, Texas

TYPE OF PLAN: Request for Modification of an Approved Contributing Zone Plan (CZP-MOD); 30 Texas Administrative Code (TAC) Chapter 213 Subchapter B Edwards Aquifer

Edwards Aquifer Protection Program ID No. 11002658; Regulated Entity No. RN110606126

Dear Mr. Reilly:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the CZP-MOD for the above-referenced project submitted to the Austin Regional Office by Pape-Dawson Engineers, Inc. on behalf of Hwy 29 Ventures 2015, LP on September 1, 2021. Final review of the CZP-MOD was completed after additional material was received on October 15, 2021. As presented to the TCEQ, the Temporary and Permanent Best Management Practices (BMPs) were selected, and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213. These planning materials were sealed, signed, and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

BACKGROUND

The Lively Tract Phase 2 Contributing Zone Plan (CZP) was approved by letter dated March 13, 2019 (EAPP ID No. 11001396). The CZP consisted of approximately 80.4. acres, which included single-family residences, drives, utilities, and associated appurtenances.

TCEQ Region 11 • P.O. Box 13087 • Austin, Texas 78711-3087 • 512-339-2929 • Fax 512-339-3795

Mr. Tom Reilly Page 2 October 29, 2021

PROJECT DESCRIPTION

The proposed residential project will have an area of approximately 109.88 acres. It will include clearing and grading, excavation, installation of utilities and drainage improvements, streets, sidewalks and 136 single-family homes with associated driveways. The impervious cover will be 20.47 acres (18.63 percent). Project wastewater will be disposed of by conveyance to the existing San Gabriel Wastewater Treatment Plant.

PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, an existing batch detention basin (Pond H, EAPP ID 11001396), a proposed batch detention basin (Pond J), an existing engineered vegetative filter strip (VFS D, EAPP ID 11001396), and a proposed engineered vegetative filter strip (VFS E) designed using the TCEQ technical guidance document, Complying with the Edwards Aquifer Rules: Technical Guidance on Best Management Practices (2005), will be constructed to treat stormwater runoff. The required total suspended solids (TSS) treatment for this project is 17,817 pounds of TSS generated from the 20.47 acres of impervious cover. The approved measures meet the required 80 percent removal of the increased load in TSS caused by the project.

SPECIAL CONDITIONS

- I. This modification is subject to all Special and Standard Conditions listed in the CZP approval letter dated March 13, 2019.
- II. All permanent pollution abatement measures shall be operational prior to occupancy of the facility.
- III. All sediment and/or media removed from the water quality basin during maintenance activities shall be properly disposed of according to 30 TAC 330 or 30 TAC 335, as applicable.

STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

Prior to Commencement of Construction:

- 4. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved Contributing Zone Plan and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 5. Any modification to the activities described in the referenced CZP-MOD application following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.

Mr. Tom Reilly Page 3 October 29, 2021

- 6. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the Austin Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the name of the approved plan and file number for the regulated activity, the date on which the regulated activity will commence, and the name of the prime contractor with the name and telephone number of the contact person.
- 7. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved Storm Water Pollution Prevention Plan (SWPPP) must be installed prior to construction and maintained during construction. Temporary E&S controls may be removed when vegetation is established, and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.

During Construction:

- 8. During the course of regulated activities related to this project, the applicant or his agent shall comply with all applicable provisions of 30 TAC Chapter 213, Edwards Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.
- 9. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been significantly reduced. Litter, construction debris, and construction chemicals exposed to stormwater shall be prevented from becoming a pollutant source for stormwater discharges (e.g., screening outfalls, picked up daily).
- 10. Intentional discharges of sediment laden water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices. These may include vegetated filter strips, sediment traps, rock berms, silt fence rings, etc.
- 11. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 12. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.
- 13. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 5, above.

After Completion of Construction:

14. Owners of permanent BMPs and measures must insure that the BMPs and measures are constructed and function as designed. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The

Mr. Tom Reilly Page 4 October 29, 2021

certification letter must be submitted to the Austin Regional Office within 30 days of site completion.

- 15. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. Such entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred. A copy of the transfer of responsibility must be filed with the executive director through the Austin Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.
- 16. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved Contributing Zone Plan. If the new owner intends to commence any new regulated activity on the site, a new Contributing Zone Plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 17. A Contributing Zone Plan approval or extension will expire, and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new Contributing Zone Plan must be submitted to the Austin Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.
- 18. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.

This action is taken under authority delegated by the Executive Director of the Texas Commission on Environmental Quality. If you have any questions or require additional information, please contact Colin Gearing of the Edwards Aquifer Protection Program of the Austin Regional Office at (512) 339-2929.

Sincerely,

Lillian Butles

Lillian Butler, Section Manager Edwards Aquifer Protection Program Texas Commission on Environmental Quality

LIB/cmg

Enclosure: Change in Responsibility for Maintenance of Permanent BMPs, Form TCEQ-10263Cc: Mr. Dustin Goss, P.E., LEED[®] AP, Pape-Dawson Engineers, Inc.

EXHEBET " A "

TEXAS COMMISSION ON ENVIRONMENTAL OUALITY

Protecting Texas by Reducing and Preventing Pollution

March 13, 2019

Mr. David Nairne Hwy 29 Ventures 2015, LP 4910 Campus Dr. Newport Beach, CA 95660

Jon Niermann, Chairman Emily Lindley, Commissioner Toby Baker, Executive Director

Re: Edwards Aquifer, Williamson County

NAME OF PROJECT: Lively Tract Phase 2, located SW of Cross Creek Rd and SH 29, Leander (ETJ), Texas

TYPE OF PLAN: Request for Approval of a Contributing Zone Plan (CZP) Application 30 Texas Administrative Code (TAC) Chapter 213 Edwards Aquifer

Edwards Aquifer Protection Program ID No. 11001396; Regulated Entity No. RN110606126

Dear Mr. Nairne:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the CZP Application for the above-referenced project submitted to the Austin Regional Office by Pape-Dawson Engineers, Inc. on behalf of Hwy 29 Ventures 2015, LP on December 14, 2018. Final review of the CZP was completed after additional material was received on February 15, 2019, March 8, 2019, and March 12, 2019. As presented to the TCEO, the Temporary and Permanent Best Management Practices (BMPs) were selected and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213. These planning materials were sealed, signed and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

PROJECT DESCRIPTION

The proposed residential project will have an area of approximately 80.43 acres. It will include the construction of single-family residences, drives, utilities, and associated appurtenances.

TCEQ Region 11 • P.O. Box 13087 • Austin, Texas 78711-3087 • 512-339-2929 • Fax 512-339-3795

Austin Headquarters: 512-239-1000 + tceq.texas.gov + How is our customer service? tceq.texas.gov/customersurvey

Mr. David Nairne Page 2 of 4 March 13, 2019

The impervious cover will be 7.44 acres (9.26 percent). Project wastewater will be disposed of by conveyance to the existing San Gabriel Wastewater Treatment Plant.

PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, a batch detention basin ("Pond H") and engineered vegetative filter strips ("VFS D"), designed using the TCEQ technical guidance document, <u>Complying with the Edwards Aquifer Rules: Technical Guidance on Best</u> <u>Management Practices (2005)</u>, will be constructed to treat stormwater runoff. The required total suspended solids (TSS) treatment for this project is 6,476 pounds of TSS generated from the 7.44 acres of impervious cover. Pond H is designed to treat 5,866 pounds of TSS. The provided water quality volume is 161,181 ft³ at an elevation of 815.0 ft. VFS D is designed to treat 766 pounds of TSS. The approved measures meet the required 80 percent removal of the increased load in TSS caused by the project.

SPECIAL CONDITIONS

- I. All permanent pollution abatement measures shall be operational prior to occupancy of the facility.
- II. All sediment and/or media removed from the water quality basin during maintenance activities shall be properly disposed of according to 30 TAC 330 or 30 TAC 335, as applicable.

STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

Prior to Commencement of Construction:

- 4. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved CZP and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 5. Any modification to the activities described in the referenced CZP application following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.
- 6. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the Austin Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the name of the approved plan and file number

for the regulated activity, the date on which the regulated activity will commence, and the name of the prime contractor with the name and telephone number of the contact person.

7. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved Storm Water Pollution Prevention Plan (SWPPP) must be installed prior to construction and maintained during construction. Temporary E&S controls may be removed when vegetation is established and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.

During Construction:

- 8. During the course of regulated activities related to this project, the applicant or his agent shall comply with all applicable provisions of 30 TAC Chapter 213, Edwards Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.
- 9. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been significantly reduced. Litter, construction debris, and construction chemicals exposed to stormwater shall be prevented from becoming a pollutant source for stormwater discharges (e.g., screening outfalls, picked up daily).
- 10. Intentional discharges of sediment laden water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices. These may include vegetated filter strips, sediment traps, rock berms, silt fence rings, etc.
- 11. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 12. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.
- 13. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 5, above.

After Completion of Construction:

- 14. Owners of permanent BMPs and measures must insure that the BMPs and measures are constructed and function as designed. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the Austin Regional Office within 30 days of site completion.
- 15. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity

Mr. David Nairne Page 4 of 4 March 13, 2019

having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. Such entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred. A copy of the transfer of responsibility must be filed with the executive director through the Austin Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.

- 16. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved CZP. If the new owner intends to commence any new regulated activity on the site, a new CZP that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 17. A CZP approval or extension will expire and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new CZP must be submitted to the Austin Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.
- 18. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.

This action is taken under authority delegated by the Executive Director of the Texas Commission on Environmental Quality. If you have any questions or require additional information, please contact Ms. Michelle Zvonkovic of the Edwards Aquifer Protection Program of the Austin Regional Office at (512) 339-2929.

Sincerely,

Robert Sadlier, Section Manager Edwards Aquifer Protection Program Texas Commission on Environmental Quality

RCS/maz

Enclosure: Change in Responsibility for Maintenance of Permanent BMPs, Form TCEQ-10263



Morean Echbric b 3 2.52m Ul 2018 8 Dec 11. 主 Dot:



Data: Dec 13, 2018, 252pm User ID: Marson FR:: H \auney\CHR\50015-21\Exhibits\EX-5001621...CP_R2.org



Date: Dec 13, 2018, 2:52pm View Rr. biowoon File: A: (aurwy)(214),50816-21(Excepte/EX-5081621_C2P_#2.deg

EXHIBIT OF

AN 80.433 ACRE TRACT OF LAND BEING OUT OF A REMNANT PORTION OF A CALLED 437.04 ACRE TRACT CONVEYED TO HWY 29 VENTURES 2015, L.P. RECORDED IN DOCUMENT NO. 2015088162 OF THE OFFICIAL PUBLIC RECORDS OF WILLIAMSON COUNTY, TEXAS, SITUATED IN THE GREENLEAF FISK SURVEY, ABSTRACT NO. 5 IN WILLIAMSON COUNTY, TEXAS.

CURVE TABLE				UNE TABLE			LINE TABLE				
CURVE	IRVE RADIUS DELTA CHORD BEARING CHORD LENGTH		LINE	BEARING	LENGTH	UN	BEARING	LENGTH			
C1	475.00'	22'09'50"	S01'54'46"W	182.60'	183.75'	L1	\$21'36'00"E	253.35′	L38	N26'06'04"E	45,71'
C2	25,00'	82'07'35"	\$28'04'06"E	32.84'	35.83'	L2	S21'35'17"E	184.35'	L39	N18'53'56"W	37.41'
C3	340.00'	47'19'36"	S45'28'06"E	272.93'	280.84'	L3	S21'23'05"E	117.63'	L.40	N04'08'36"E	85.23'
C4	345.00'	45'28'17"	S00*55'51*W	266.67'	273.80'	L4	S80'49'51"W	143.46'	L41	N54'40'23"W	33.44'
C5	275.00'	10'04'02"	S18'37'58"W	48.26'	48.32'	L5	S12'59'41"W	41.41'	L42	N22'55'10"W	177.98'
C6	25.00'	101'27'54"	S3711'56"E	38.71'	44.27'	L6	S23'39'59"W	169.98'	L43	N64'36'42"E	15.46'
C7	325.00'	66'32'24"	S54'39'40"E	356.58	377.44'	L7	S87'55'52"E	39.11'	L44	N2210'00"W	120.00'
C8	43.76'	69"10'12"	S08'23'59"W	49.68'	52.83'	L8	N68'36'32"E	151.69'	L45	N67'50'00"E	27.60'
C9	403.98'	13'10'31*	S47'59'30"₩	92.69'	92.90'	ί.9	S21'00'53"E	200.03'	L46	N2210'00"W	73.48'
C10	419,86'	15'25'23*	S62'22'49"W	112.68'	113.02'	L10	S09'27'57"E	73.28'	L47	\$67'52'31"W	21.00'
C11	425.00'	52'07'54"	N83'39'20"W	373.49'	386.69'	L11	S70'51'14"W	144.14'	L48	\$6817'01"W	11.04'
C12	400.00'	30'53'46"	N42'08'30"W	213.09'	215.70'	L12	\$6275'36*W	112.43	L49	N22'09'21"W	205.10'
C13	375.00'	23'54'37"	\$38'44'13"E	155.36'	156.49'	L13	S59'50'40"W	138.09'	L50	N31'21'41"W	55.79'
C14	350.00'	0'54'11"	N50'14'29"W	5.52'	5.52'	L14	S58'20'23"W	105.09'	L51	N18'05'48"E	50,90'
C15	25.00'	45'00'00"	N44'21'38"E	19.13'	19.63'	L15	N48'29'56"W	303.36'	L52	N61'52'45"E	32.00'
C16	25.00'	45'00'00"	N00'38'22"W	19.13'	19.63'	L16	N57'35'23"W	129.77	L53	N17'08'05"E	122.55'
C17	525.00'	15*29'47"	N14'06'45"E	141.56'	141.99'	L17	N63'18'23"E	11.47'	L54	N01'53'16"E	80.00'
Ç18	25.00'	42'23'31*	N27'33'37"E	18.08'	18.50'	L18	S65'44'37"W	13.54'	L55	S84*27'52"E	31.81'
C19	25.00'	42'23'31"	S67'39'20"E	18.08'	18.50'	L19	N39'19'15"E	25.00'	L56	N21*37'01"E	25.54
C20	335.00'	24'28'17"	N78'54'45"E	142.00'	143.08'	L.20	N40'12'36"E	130.00'	L57	S75'26'30"E	93.16'
C21	25.00'	45'00'00"	N41'23'56"W	19.13'	19.63'	L21	N42*45'23"₩	53.88'	L58	N15'09'32"E	155.00'
C22	300.00'	23'02'32"	N07'22'40"W	119.84'	120.65'	1.22	N28*41'22"W	53.88'	L59	N74'50'28*W	20.00*
C23	25,00'	3171'01"	N19'44'07"E	13.44'	13.61'	L23	N14'37'21"₩	53.88'	L60	N08'18'41"E	50.42'
C24	768.00'	6*27*31"	N25'23'46"W	86.53'	86,57'	L24	N00'33'20"W	53.88'	L61	N19'33'44"E	69.08'
C25	25.00'	6576'35"	N6175'49"W	26.97'	28.48'	l.25	N13'26'11"E	53.31'	L62	S55*56*56*E	32,65'
C26	25.00'	62'56'59"	N01'00'33"W	26.11'	27.47'	L26	N18'02'33"E	60.13'	L63	S76"26'18"E	65.24'
C27	25.00'	45'00'01"	N54'59'03"W	19.13'	19.64'	L27	N68'08'22"W	126.07'	L64	S81'43'15"E	84.39'
C28	1002.70'	4'10'44"	N3012'45"W	73.12'	73.13'	L28	N21'51'38"E	96.80'	L65	S83'56'33"E	71.54'
·····						L29	N21'51'38"E	64.64'	L66	S8819'26"E	97.45'
						L30	N21'51'38"E	53.80'	£67	S8212'05"E	67.13'
						L31	N01'08'54"E	63.07'	L68	S72'20'21"E	45.47
						L32	588'51'06"E	27.51'	L69	N88'55'16"E	94.32
						L33	N66'40'37"E	127.77'	L70	N58'06'50*E	38.18'
						L34	N23'19'23"W	140.29'	L71	N25'20'36"E	35.94'
						L35	N71'06'04"E	10.51'	L72	N15'06'53"E	52.85'
	PAPI	Е-ДАИ	SON			L36	N18'53'66*W	120.00'	L73	N00'08'30"W	54.08'
	ENGINEERS					L37	N19'47'44"W	25.00'	L74	N11'27'13"W	0.42'

AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10001 N MOPAC EXPY, SLOG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8741 TBPE FIRM REGISTRATION #470 / TOPLE FIRM REGISTRATION #10026001

DECEMBER 12, 2018



1 🛛 🕅 🕅

FIELD NOTES

FOR

AN 80.433 ACRE TRACT OF LAND BEING OUT OF A REMNANT PORTION OF A CALLED 437.04 ACRE TRACT CONVEYED TO HWY 29 VENTURES 2015, L.P. RECORDED IN DOCUMENT NO. 2015088162 OF THE OFFICIAL PUBLIC RECORDS OF WILLIAMSON COUNTY, TEXAS, SITUATED IN THE GREENLEAF FISK SURVEY, ABSTRACT NO. 5 IN WILLIAMSON COUNTY, TEXAS. SAID 80.433 ACRE TRACT BEING MORE FULLY DESCRIBED AS FOLLOWS, WITH BEARINGS BASED ON THE NORTH AMERICAN DATUM OF 1983 (NA 2011) EPOCH 2010.00, FROM THE TEXAS COORDINATE SYSTEM ESTABLISHED FOR THE CENTRAL ZONE:

COMMENCING at a ½" iron rod with cap marked "Chaparral" found for on a point in the west boundary line of a called 491.95-acre tract of land, conveyed to Henry B. Tippie, recorded in Vol. 570, Pg. 483 of the Deed Records of Williamson County, Texas, same being the east boundary line of said 437.04-acre tract hereof;

THENCE S 21°39'09" E, with the west boundary line of said 491.95-acre tract, same being the east boundary line of said 437.04-acre tract, a distance of 24.33 feet to a calculated point, for the northeast corner and **POINT OF BEGINNING** hereof;

THENCE with the east boundary line of said 437.04-acre tract, same being the west boundary line of said 491.95-acre tract, the following four (4) courses and distances:

- 1. S 21°49'53" E, a distance of 469.33 feet to a ½" iron rod with cap marked "Chaparral" found, for an angle point hereof,
- 2. S 21°36'00" E, a distance of 253.35 feet to a ½" iron rod with cap marked "Chaparral" found, for an angle point hereof,
- 3. S 21°35'17" E, a distance of 184.35 feet to a ½" iron rod with cap marked "Chaparral" found, for an angle point hereof, and
- 4. S 21°23'05" E, a distance of 117.63 feet to a calculated point for the easternmost southeast corner hereof;

THENCE departing the west line of said 491.95-acre tract, through the interior of said 437.04acre tract, the following fifteen (15) courses and distances:

1. S 80°49'51" W, a distance of 143.46 feet to a calculated point of non-tangent curvature hereof,

TBPE Firm Registration #4701 TBPLS Firm Registration #10028801 Austin I San Antonio I Houston I Fort Worth I Dallas Transportation I Water Resources I Land Development I Surveying I Environmental 10801 N MoPac Exp., Bldg. 3, Suite 200, Austin, TX 78759 512.454.8711 www.Pape-Dawson.com 80.433 Acres Job No. 50816-21 Page 2 of 8

- along the arc of a curve to the right, having a radius of 475.00 feet, a central angle of 22°09'50", a chord bearing and distance of S 01°54'46" W, 182.60 feet, an arc length of 183.75 feet to a calculated point of non-tangency hereof,
- 3. S 12°59'41" W, a distance of 41.41 feet to a calculated point of tangent curvature hereof,
- 4. along the arc of a curve to the left, having a radius of 25.00 feet, a central angle of 82°07'35", a chord bearing and distance of S 28°04'06" E, 32.84 feet, an arc length of 35.83 feet to a calculated point of reverse curvature hereof,
- 5. along the arc of a curve to the right, having a radius of 340.00 feet, a central angle of 47°19'36", a chord bearing and distance of S 45°28'06" E, 272.93 feet, an arc length of 280.84 feet to a calculated point of tangency hereof,
- 6. S 21°48'18" E, a distance of 367.57 feet to a calculated point of tangent curvature hereof,
- 7. along the arc of a curve to the right, having a radius of 345.00 feet, a central angle of 45°28'17", a chord bearing and distance of S 00°55'51" W, 266.67 feet, an arc length of 273.80 feet to a calculated point of tangency hereof,
- 8. S 23°39'59" W, a distance of 169.98 feet to a calculated point of tangent curvature hereof,
- 9. along the arc of a curve to the left, having a radius of 275.00 feet, a central angle of 10°04'02", a chord bearing and distance of S 18°37'58" W, 48.26 feet, an arc length of 48.32 feet to a calculated point of compound curvature hereof,
- 10. along the arc of a curve to the left, having a radius of 25.00 feet, a central angle of 101°27'54", a chord bearing and distance of S 37°11'56" E, 38.71 feet, an arc length of 44.27 feet to a calculated point of tangency hereof,
- 11. S 87°55'52" E, a distance of 39.11 feet to a calculated point of tangent curvature hereof,
- 12. along the arc of a curve to the right, having a radius of 325.00 feet, a central angle of 66°32'24", a chord bearing and distance of S 54°39'40" E, 356.58 feet, an arc length of 377.44 feet to a calculated point of tangency hereof,
- 13. S 21°23'28" E, a distance of 492.53 feet to a calculated point of non-tangent curvature hereof,



80.433 Acres Job No. 50816-21 Page 3 of 8

- 14. along the arc of a curve to the right, having a radius of 43.76 feet, a central angle of 69°10'12", a chord bearing and distance of S 08°23'59" W, 49.68 feet, an arc length of 52.83 feet to a calculated point of non-tangency hereof, and
- 15. N 68°36'32" E, a distance of 151.69 feet to a calculated point in the west line of said 491.95-acre tract, same being the east line of said 437.04-acre tract for a southeast corner hereof;

THENCE S 21°00'53" E, with the east boundary line of said 437.04-acre tract, same being the west boundary line of said 491.95-acre tract, a distance of **200.03 feet** to an iron rod with cap marked "Chaparral" found for an angle point hereof;

THENCE S 09°27'57" E, with the east boundary line of said 437.04-acre tract, same being the west boundary line of said 491.95-acre tract, a distance of **73.28 feet** to a calculated point for the southeast corner hereof;

THENCE departing the west line of said 491.95-acre tract, through the interior of said 437.04acre tract, the following eighty-six (86) courses and distances:

- 1. S 70°51'14" W, a distance of 144.14 feet to a calculated angle point hereof,
- 2. S 62°15'36" W, a distance of 112.43 feet to a calculated angle point hereof,
- 3. S 59°50'40" W, a distance of 138.09 feet to a calculated angle point hereof,
- 4. S 58°20'23" W, a distance of 105.09 feet to a calculated angle point hereof,
- 5. N 48°29'56" W, a distance of 303.36 feet to a calculated point of non-tangent curvature,
- 6. along the arc of a curve to the right, having a radius of 403.98 feet, a central angle of 13°10'31", a chord bearing and distance of S 47°59'30" W, 92.69 feet, an arc length of 92.90 feet to a calculated point of compound curvature hereof,
- along the arc of a curve to the right, having a radius of 419.86 feet, a central angle of 15°25'23", a chord bearing and distance of S 62°22'49" W, 112.68 feet, an arc length of 113.02 feet to a calculated point of non-tangency hereof,
- 8. S 70°16'43" W, a distance of 459.99 feet to a calculated point of tangency hereof,
- along the arc of a curve to the right, having a radius of 425.00 feet, a central angle of 52°07'54", a chord bearing and distance of N 83°39'20" W, 373.49 feet, an arc length of 386.69 feet to a calculated point of tangency hereof,



80.433 Acres Job No. 50816-21 Page 4 of 8

- 10. N 57°35'23" W, a distance of 129.77 feet to a calculated point of tangent curvature hereof,
- 11. along the arc of a curve to the right, having a radius of 400.00 feet, a central angle of 30°53'46", a chord bearing and distance of N 42°08'30" W, 213.09 feet, an arc length of 215.70 feet to a calculated point of tangency hereof,
- 12. N 63°18'23" E, a distance of 11.47 feet to a calculated point for the westernmost southwest corner hereof,
- 13. N 65°44'37" E, a distance of 13.54 feet to a calculated point of non-tangent curvature hereof,
- 14. along the arc of a curve to the left, having a radius of 375.00 feet, a central angle of 23°54'37", a chord bearing and distance of S 38°44'13" E, 155.36 feet, an arc length of 156.49 feet to a calculated point of non-tangency hereof,
- 15. N 39°19'15" E, a distance of 25.00 feet to a calculated point of non-tangent curvature hereof,
- 16. along the arc of a curve to the right, having a radius of 350.00 feet, a central angle of 00°54'11", a chord bearing and distance of N 50°14'29" W, 5.52 feet, an arc length of 5.52 feet to a calculated point of non-tangency hereof,
- 17. N 40°12'36" E, a distance of 130.00 feet to a calculated angle point hereof,
- 18. N 42°45'23" W, a distance of 53.88 feet to a calculated angle point hereof,
- 19. N 28°41'22" W, a distance of 53.88 feet to a calculated angle point hereof,
- 20. N 14°37'21" W, a distance of 53.88 feet to a calculated angle point hereof,
- 21. N 00°33'20" W, a distance of 53.88 feet to a calculated angle point hereof,
- 22. N 13°26'11" E, a distance of 53.31 feet to a calculated angle point hereof,
- 23. N 18°02'33" E, a distance of 60.13 feet to a calculated angle point hereof,
- 24. N 68°08'22" W, a distance of 126.07 feet to a calculated angle point hereof,

PAPE-DAWSON

25. N 21°51'38" E, a distance of 96.80 feet to a calculated point of tangency,

80.433 Acres Job No. 50816-21 Page 5 of 8

- 26. along arc of a curve to the right, having a radius of 25.00 feet, a central angle of 45°00'00", a chord bearing and distance of N 44°21'38" E, 19.13 feet, an arc length of 19.63 feet to a calculated point of tangency hereof,
- 27. N 21°51'38" E, a distance of 64.64 feet to a calculated point of non-tangent curvature,
- 28. along the arc of a curve to the right, having a radius of 25.00 feet, a central angle of 45°00'00", a chord bearing and distance of N 00°38'22" W, 19.13 feet, an arc length of 19.63 feet to a calculated point of non-tangent curvature,
- 29. N 21°51'38" E, a distance of 53.80 feet to a calculated point of tangent curvature,
- 30. along the arc of a curve to the left, having a radius of 525.00 feet, a central angle of 15°29'47", a chord bearing and distance of N 14°06'45" E, 141.56 feet, an arc length of 141.99 feet to a calculated point of reverse curvature,
- 31. along the arc of a curve to the right, having a radius of 25.00 feet, a central angle of 42°23'31", a chord bearing and distance of N 27°33'37" E, 18.08 feet, an arc length of 18.50 feet to a calculated point of tangency hereof,
- 32. N 01°08'54" E, a distance of 63.07 feet to a calculated point of non-tangent curvature hereof,
- 33. along the arc of a curve to the left, having a radius of 25.00 feet, a central angle of 42°23'31", a chord bearing and distance of S 67°39'20" E, 18.08 feet, an arc length of 18.50 feet to a calculated point of non-tangency,
- 34. S 88°51'06" E, a distance of 27.51 feet to a calculated point of tangent curvature,
- 35. along the arc of a curve to the left, having a radius of 335.00 feet, a central angle of 24°28'17", a chord bearing and distance of N 78°54'45" E, 142.00 feet, an arc length of 143.08 feet to a calculated point of tangency hereof,
- 36. N 66°40'37" E, a distance of 127.77 feet to a calculated angle point hereof,
- 37. N 23°19'23" W, a distance of 140.29 feet to a calculated angle point hereof,
- 38. N 71°06'04" E, a distance of 10.51 feet to a calculated angle point hereof,
- 39. N 18°53'56" W, a distance of 120.00 feet to a calculated angle point hereof,



80.433 Acres Job No. 50816-21 Page 6 of 8

- 40. N 19°47'44" W, a distance of 25.00 feet to a calculated angle point hereof,
- 41. N 26°06'04" E, a distance of 45.71 feet to a calculated point of non-tangent curvature hereof,
- 42. along the arc of a curve to the right, having a radius of 25.00 feet, a central angle of 45°00'00", a chord bearing and distance of N 41°23'56" W, 19.13 feet, an arc length of 19.63 feet to a calculated point of non-tangency hereof,
- 43. N 18°53'56" W, a distance of 37.41 feet to a calculated point of tangent curvature hereof,
- 44. along the arc of a curve to the right, said curve having radius of 300.00 feet, a central angle of 23°02'32", a chord bearing and distance of N 07°22'40" W, 119.84 feet, an arc length of 120.65 feet to a calculated point of tangency,
- 45. N 04°08'36" E, a distance of 85.23 feet to a calculated point of tangent curvature,
- 46. along the arc of a curve to the right, having a radius of 25.00 feet, a central angle of 31°11'01", a chord bearing and distance of N 19°44'07" E, 13.44 feet, an arc length of 13.61 feet to a calculated point of tangency,
- 47. N 54°40'23" W, a distance of 33.44 feet to a calculated angle point hereof,
- 48. N 22°55'10" W, a distance of 177.98 feet to a calculated angle point hereof,
- 49. N 64°36'42" E, a distance of 15.46 feet to a calculated angle point hereof,
- 50. N 22°10'00" W, a distance of 120.00 feet to a calculated angle point hereof,
- 51. N 67°50'00" E, a distance of 27.60 feet to a calculated angle point hereof,
- 52. N 22°10'00" W, a distance of 73.48 feet to a calculated angle point hereof,
- 53. S 67°52'31" W, a distance of 21.00 feet to a calculated angle point hereof,
- 54. S 68°17'01" W, a distance of 11.04 feet to a calculated angle point hereof,
- 55. N 22°09'21" W, a distance of 205.10 feet to a calculated point of non-tangent curvature hereof,


.

- 56. along the arc of a curve to the left, having a radius of 768.00 feet, a central angle of 06°27'31", a chord bearing and distance of N 25°23'46" W, 86.53 feet, an arc length of 86.57 feet to a calculated point of compound curvature hereof,
- 57. along the arc of a curve to the left, having a radius of 25.00 feet, a central angle of 65°16'35", a chord bearing and distance of N 61°15'49" W, 26.97 feet, an arc length of 28.48 feet to a calculated point of non-tangency hereof,
- 58. N 31°21'41" W, a distance of 55.79 feet to a calculated point of non-tangent curvature hereof,
- 59. along the arc of a curve to the left, having a radius of 25.00 feet, a central angle of 62°56'59", a chord bearing and distance of N 01°00'33" W, 26.11 feet, an arc length of 27.47 feet to a calculated point of non-tangency hereof,
- 60. N 32°29'03" W, a distance of 402.82 feet to a calculated point of tangent curvature hereof,
- 61. along the arc of a curve to the left, having a radius of 25.00 feet, a central angle of 45°00'01", a chord bearing and distance of N 54°59'03" W, 19.13 feet, an arc length of 19.64 feet to a calculated point of tangency hereof,
- 62. N 18°05'48" E, a distance of 50.90 feet to a calculated point of non-tangent curvature hereof,
- 63. along the arc of a curve to the right, having a radius of 1002.70 feet, a central angle of 04°10'44", a chord bearing and distance of N 30°12'45" W, 73.12 feet, an arc length of 73.13 feet to a calculated point of non-tangency hereof,
- 64. N 61°52'45" E, a distance of 32.00 feet to a calculated angle point hereof,
- 65. N 17°08'05" E, a distance of 122.55 feet to a calculated angle point hereof,
- 66. N 01°53'16" E, a distance of 80.00 feet to a calculated angle point hereof,
- 67. S 84°27'52" E, a distance of 31.81 feet to a calculated angle point hereof,
- 68. N 21°37'01" E, a distance of 25.54 feet to a calculated angle point hereof,
- 69. S 75°26'30" E, a distance of 93.16 feet to a calculated angle point hereof,
- 70. N 15°09'32" E, a distance of 155.00 feet to a calculated angle point hereof,

INVESTIGATION CONTRACTOR AND A CONTRACTOR AND A



80.433 Acres Job No. 50816-21 Page 8 of 8

- 71. N 74°50'28" W, a distance of 20.00 feet to a calculated angle point hereof,
- 72. N 08°18'41" E, a distance of 50.42 feet to a calculated angle point hereof,
- 73. N 19°33'44" E, a distance of 69.08 feet to a calculated point for the northwest corner hereof,
- 74. S 55°56'56" E, a distance of 32.65 feet to a calculated angle point hereof,
- 75. S 76°26'18" E, a distance of 65.24 feet to a calculated angle point hereof,
- 76. S 81°43'15" E, a distance of 84.39 feet to a calculated angle point hereof,
- 77. S 83°56'33" E, a distance of 71.54 feet to a calculated angle point hereof,
- 78. S 88°19'26" E, a distance of 97.45 feet to a calculated angle point hereof,
- 79. S 82°12'05" E, a distance of 67.13 feet to a calculated angle point hereof,
- 80. S 72°20'21" E, a distance of 45.47 feet to a calculated angle point hereof,
- 81. N 88°55'16" E, a distance of 94.32 feet to a calculated angle point hereof,
- 82. N 58°06'50" E, a distance of 38.18 feet to a calculated angle point hereof,
- 83. N 25°20'36" E, a distance of 35.94 feet to a calculated angle point hereof,
- 84. N 15°06'53" E, a distance of 52.85 feet to a calculated angle point hereof,
- 85. N 00°08'30" W, a distance of 54.08 feet to a calculated angle point hereof, and
- 86. N 11°27'13" W, a distance of 0.42 feet to the POINT OF BEGINNING and containing 80.433 acres in Williamson County, Texas. Said tract being described in accordance with a survey made on the ground and exhibit prepared under Job No. 50816-21 by Pape-Dawson Engineers, Inc.

 PREPARED BY:
 Pape-Dawson Engineers, Inc.

 DATE:
 December 11, 2018

 JOB No.:
 50816-21

 DOC.ID.:
 H:\survey\CIVIL\50816-21\Exhibits\Word\FN-5081621_80.433Ac_CZP_R1.docx

 TBPLS Firm Registration #470
 TBPLS Firm Registration #100288-01

Parky. O



Jon Niermann, *Chairman* Emily Lindley, *Commissioner* Bobby Janecka, *Commissioner* Toby Baker, *Executive Director*



TEXAS COMMISSION ON ENVIRONMENTAL QUALITY

Protecting Texas by Reducing and Preventing Pollution

October 29, 2021

Mr. Tom Reilly Hwy 29 Ventures 2015, LP 4910 Campus Dr. New Port Beach, CA 92660

Re: Edwards Aquifer, Williamson County

NAME OF PROJECT: Lively Tract Phase 2; Located S.W. of Cross Creek Rd. and SH 29; Leander, Texas

TYPE OF PLAN: Request for Modification of an Approved Contributing Zone Plan (CZP-MOD); 30 Texas Administrative Code (TAC) Chapter 213 Subchapter B Edwards Aquifer

Edwards Aquifer Protection Program ID No. 11002658; Regulated Entity No. RN110606126

Dear Mr. Reilly:

The Texas Commission on Environmental Quality (TCEQ) has completed its review of the CZP-MOD for the above-referenced project submitted to the Austin Regional Office by Pape-Dawson Engineers, Inc. on behalf of Hwy 29 Ventures 2015, LP on September 1, 2021. Final review of the CZP-MOD was completed after additional material was received on October 15, 2021. As presented to the TCEQ, the Temporary and Permanent Best Management Practices (BMPs) were selected, and construction plans were prepared by a Texas Licensed Professional Engineer to be in general compliance with the requirements of 30 TAC Chapter 213. These planning materials were sealed, signed, and dated by a Texas Licensed Professional Engineer. Therefore, based on the engineer's concurrence of compliance, the planning materials for construction of the proposed project and pollution abatement measures are hereby approved subject to applicable state rules and the conditions in this letter. The applicant or a person affected may file with the chief clerk a motion for reconsideration of the executive director's final action on this Edwards Aquifer Protection Plan. A motion for reconsideration must be filed no later than 23 days after the date of this approval letter. This approval expires two (2) years from the date of this letter unless, prior to the expiration date, more than 10 percent of the construction has commenced on the project or an extension of time has been requested.

BACKGROUND

The Lively Tract Phase 2 Contributing Zone Plan (CZP) was approved by letter dated March 13, 2019 (EAPP ID No. 11001396). The CZP consisted of approximately 80.4. acres, which included single-family residences, drives, utilities, and associated appurtenances.

TCEQ Region 11 • P.O. Box 13087 • Austin, Texas 78711-3087 • 512-339-2929 • Fax 512-339-3795

Mr. Tom Reilly Page 2 October 29, 2021

PROJECT DESCRIPTION

The proposed residential project will have an area of approximately 109.88 acres. It will include clearing and grading, excavation, installation of utilities and drainage improvements, streets, sidewalks and 136 single-family homes with associated driveways. The impervious cover will be 20.47 acres (18.63 percent). Project wastewater will be disposed of by conveyance to the existing San Gabriel Wastewater Treatment Plant.

PERMANENT POLLUTION ABATEMENT MEASURES

To prevent the pollution of stormwater runoff originating on-site or upgradient of the site and potentially flowing across and off the site after construction, an existing batch detention basin (Pond H, EAPP ID 11001396), a proposed batch detention basin (Pond J), an existing engineered vegetative filter strip (VFS D, EAPP ID 11001396), and a proposed engineered vegetative filter strip (VFS E) designed using the TCEQ technical guidance document, Complying with the Edwards Aquifer Rules: Technical Guidance on Best Management Practices (2005), will be constructed to treat stormwater runoff. The required total suspended solids (TSS) treatment for this project is 17,817 pounds of TSS generated from the 20.47 acres of impervious cover. The approved measures meet the required 80 percent removal of the increased load in TSS caused by the project.

SPECIAL CONDITIONS

- I. This modification is subject to all Special and Standard Conditions listed in the CZP approval letter dated March 13, 2019.
- II. All permanent pollution abatement measures shall be operational prior to occupancy of the facility.
- III. All sediment and/or media removed from the water quality basin during maintenance activities shall be properly disposed of according to 30 TAC 330 or 30 TAC 335, as applicable.

STANDARD CONDITIONS

- 1. Pursuant to Chapter 7 Subchapter C of the Texas Water Code, any violations of the requirements in 30 TAC Chapter 213 may result in administrative penalties.
- 2. The holder of the approved Edwards Aquifer protection plan must comply with all provisions of 30 TAC Chapter 213 and all best management practices and measures contained in the approved plan. Additional and separate approvals, permits, registrations and/or authorizations from other TCEQ Programs (i.e., Stormwater, Water Rights, UIC) can be required depending on the specifics of the plan.
- 3. In addition to the rules of the Commission, the applicant may also be required to comply with state and local ordinances and regulations providing for the protection of water quality.

Prior to Commencement of Construction:

- 4. All contractors conducting regulated activities at the referenced project location shall be provided a copy of this notice of approval. At least one complete copy of the approved Contributing Zone Plan and this notice of approval shall be maintained at the project location until all regulated activities are completed.
- 5. Any modification to the activities described in the referenced CZP-MOD application following the date of approval may require the submittal of a plan to modify this approval, including the payment of appropriate fees and all information necessary for its review and approval prior to initiating construction of the modifications.

Mr. Tom Reilly Page 3 October 29, 2021

- 6. The applicant must provide written notification of intent to commence construction, replacement, or rehabilitation of the referenced project. Notification must be submitted to the Austin Regional Office no later than 48 hours prior to commencement of the regulated activity. Written notification must include the name of the approved plan and file number for the regulated activity, the date on which the regulated activity will commence, and the name of the prime contractor with the name and telephone number of the contact person.
- 7. Temporary erosion and sedimentation (E&S) controls, i.e., silt fences, rock berms, stabilized construction entrances, or other controls described in the approved Storm Water Pollution Prevention Plan (SWPPP) must be installed prior to construction and maintained during construction. Temporary E&S controls may be removed when vegetation is established, and the construction area is stabilized. If a water quality pond is proposed, it shall be used as a sedimentation basin during construction. The TCEQ may monitor stormwater discharges from the site to evaluate the adequacy of temporary E&S control measures. Additional controls may be necessary if excessive solids are being discharged from the site.

During Construction:

- 8. During the course of regulated activities related to this project, the applicant or his agent shall comply with all applicable provisions of 30 TAC Chapter 213, Edwards Aquifer. The applicant shall remain responsible for the provisions and conditions of this approval until such responsibility is legally transferred to another person or entity.
- 9. If sediment escapes the construction site, the sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain). Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been significantly reduced. Litter, construction debris, and construction chemicals exposed to stormwater shall be prevented from becoming a pollutant source for stormwater discharges (e.g., screening outfalls, picked up daily).
- 10. Intentional discharges of sediment laden water are not allowed. If dewatering becomes necessary, the discharge will be filtered through appropriately selected best management practices. These may include vegetated filter strips, sediment traps, rock berms, silt fence rings, etc.
- 11. The following records shall be maintained and made available to the executive director upon request: the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 12. Stabilization measures shall be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and construction activities will not resume within 21 days. When the initiation of stabilization measures by the 14th day is precluded by weather conditions, stabilization measures shall be initiated as soon as practicable.
- 13. This approval does not authorize the installation of temporary aboveground storage tanks on this project. If the contractor desires to install a temporary aboveground storage tank for use during construction, an application to modify this approval must be submitted and approved prior to installation. The application must include information related to tank location and spill containment. Refer to Standard Condition No. 5, above.

After Completion of Construction:

14. Owners of permanent BMPs and measures must insure that the BMPs and measures are constructed and function as designed. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The

Mr. Tom Reilly Page 4 October 29, 2021

certification letter must be submitted to the Austin Regional Office within 30 days of site completion.

- 15. The applicant shall be responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. Such entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred. A copy of the transfer of responsibility must be filed with the executive director through the Austin Regional Office within 30 days of the transfer. A copy of the transfer form (TCEQ-10263) is enclosed.
- 16. Upon legal transfer of this property, the new owner(s) is required to comply with all terms of the approved Contributing Zone Plan. If the new owner intends to commence any new regulated activity on the site, a new Contributing Zone Plan that specifically addresses the new activity must be submitted to the executive director. Approval of the plan for the new regulated activity by the executive director is required prior to commencement of the new regulated activity.
- 17. A Contributing Zone Plan approval or extension will expire, and no extension will be granted if more than 50 percent of the total construction has not been completed within ten years from the initial approval of a plan. A new Contributing Zone Plan must be submitted to the Austin Regional Office with the appropriate fees for review and approval by the executive director prior to commencing any additional regulated activities.
- 18. At project locations where construction is initiated and abandoned, or not completed, the site shall be returned to a condition such that the aquifer is protected from potential contamination.

This action is taken under authority delegated by the Executive Director of the Texas Commission on Environmental Quality. If you have any questions or require additional information, please contact Colin Gearing of the Edwards Aquifer Protection Program of the Austin Regional Office at (512) 339-2929.

Sincerely,

Lillian Butles

Lillian Butler, Section Manager Edwards Aquifer Protection Program Texas Commission on Environmental Quality

LIB/cmg

Enclosure: Change in Responsibility for Maintenance of Permanent BMPs, Form TCEQ-10263Cc: Mr. Dustin Goss, P.E., LEED[®] AP, Pape-Dawson Engineers, Inc.

ATTACHMENT B

Project Modification Narrative

The Lively Tract, Phase 2 Modified Contributing Zone Plan is located southeast of the intersection of Ronald Reagan Blvd. and SH Hwy 29, within the City of Leander ETJ in Williamson County, Texas and is being proposed for modification because of Lively Tract Phase 6 development using PBMPs constructed with the original Lively Tract Phase 2. The initial phases of the development (Lively Tract Phases 1, 2, 3, 4, & 5) have been permitted and are in various stages of construction. The entire Phase 1 boundary is located within the Recharge Zone (WPAP); thus, no Contributing Zone Plan exists for the phase. Phase 2 was divided into two sections: one located entirely over the Edwards Aguifer Recharge Zone (WPAP), and one located entirely over the Contributing Zone. The section over the Contributing Zone has an approved CZP, which was modified with Phase 4 and approved. The Phase 3 boundary is located partly over the Edwards Aquifer Recharge Zone and partly over the Contributing Zone, but was submitted as one section and treated as if over the Recharge Zone and covered by a WPAP per TCEQ policy; thus, no CZP exists for Phase 3. The Lively Tract Phase 4 boundary is located entirely within the Contributing Zone and is separated by a north-south flowing drainage way conveying treated upstream runoff to the South Fork San Gabriel River. The portion of Phase 4 to the east of the drainage way has an approved CZP, which was the modification of the aforementioned Phase 2 CZP. The portion of Phase 4 to the west of the drainage way with its own separate PBMP's was submitted as a Contributing Zone Plan and approved. The Lively Tract Phase 5 boundary is also within the Contributing Zone and has an approved modification to the aforementioned Phase 2 CZP. This is the final Phase 2 CZP modification to be done with the development's final phase, Lively Tract Phase 6.

This modification to the Lively Tract Phase 2 CZP is being pursued because of the development of Lively Tract Phase 6 and because a portion of Phase 6 development is to be treated by PMBP's built and permitted with the Phase 2 CZP. The Lively Tract Phase 6 boundary is located entirely within the Contributing Zone and is included as part of the Lively Tract Phase 2 Modified CZP. This Modified CZP will ultimately result in 120.60 acres of development over the Contributing Zone that will be served by the proposed PBMP's. No more modifications are anticipated because Phase 6 is the final phase of development.

New construction activities proposed with the Lively Tract, Phase 2 Modified CZP improvements include clearing, grading, excavation, installation of utilities and drainage improvements, streets, sidewalks, and homes with associated driveways. The increase in area/impervious area/lots from the original CZP is a result of the development of Phase 6 and its PBMP's, which was undeveloped at the time of original Phase 2 CZP approval. Of the total Phase 2 Modified CZP project limits of 120.60 acres, 28.09 acres were developed as part of the original permitted Lively Tract Phase 2 CZP, 26.94 acres were developed after Phase 4 construction with modification #1 to the Phase 2 CZP, 42.76 acres were developed after Phase 5 construction with modification #2 to the Phase 2 CZP, and 22.83 acres are proposed to be developed with Phase 6 construction and permitted through this modification to the Phase 2 CZP. After Phase 6 development, the total improvements within the Lively Tract Phase 2 Modified CZP include approximately 63.15 acres (52.36%) of impervious cover.



The project limits of the Lively Tract, Phase 2 Modified Contributing Zone Plan (CZP) are approximately 120.60 acres. 81.10 acres are treated by an existing Permanent Best Management Practices (PBMPs) batch detention basin H from the original Lively Tract Phase 2 CZP, while 15.93 acres are to be treated by another existing PBMP batch detention basin J constructed with Lively Tract Phase 4 and permitted in CZP Modification #1.

One (1) existing batch detention pond already constructed with the original Phase 2 CZP will serve as one Permanent Best Management Practice (PBMPs). One (1) existing batch detention basin and engineered vegetated filter strips (VFS) that were constructed with Phase 4's modification #1 of the Phase 2 CZP will also serve this site as a PBMP. All PBMPs have been designed in accordance with the TCEQ's Technical Guidance Manual (TGM) RG-348 (2005) to remove 80% of the increase in Total Suspended Solids (TSS) from the site. Please see the Treatment Summary Exhibit included as an attachment to this application for more information.

At full build-out, this project will generate approximately 102,960 gallons per day of average wastewater flow. Sewage flow will be disposed of by conveyance to the existing San Gabriel Wastewater Treatment Plant. Potable water will be provided by the City of Leander.

Batch Detention Basin

The batch detention basins (Batch Detention Basin H & Batch Detention Basin J) are earthen ponds with side-slopes at 3:1 with the exception of maintenance access paths which are at 4:1 slopes. Batch Detention Basin H is designed to treat 43.35 acres of impervious cover and remove 44,271 lb. of TSS at Ultimate Buildout. Batch Detention Basin J is designed to treat 8.71 acres of impervious cover and remove 8,889 lb. of TSS at Ultimate Buildout. The following is a summary of the batch detention pond controller components:

Batch Detention Pond Controller Information				
Component	Description	Voltage		
Power System	Solar Charged 12 VDC Battery (Model MK Powered 8GU1) (Or approved equal)			
Logic Controller	IDEC FL1C-H12RCE (Or approved equal)	12		
Parts Enclosure	Southwest Photovoltaic Model BBG-1 (15.75" wide x 9.75" deep x 11.75" tall) (Or approved equal)			
Nature of Event Sensing	Anchor Scientific Float Switch (Or approved equal)			
Valve Type	Keystone 6" Butterfly Valve with over torque sensors and mechanical hand crank for physical override if necessary. Able to withstand 100 psi minimum. (Or approved equal)			
Actuator	EPI-6 12 VDC. Able to withstand 100 psi minimum. (Or approved equal)	12		
Power Consumption				
(actuator, controller,				
relay, PLC)	242.58 W, 46.5 W-hours			



The following is a circuit diagram of the controllers:



The logic controllers will provide a test sequence. The systems will be solar powered and will be equipped with a backup battery. The systems will be equipped with an on/off/reset switch. The butterfly valves will be equipped with a manual hand crank for physical override if necessary in the event of a spill or for maintenance purposes. The systems will be equipped with a clearly visible external indicator to indicate if a cycle is in progress without having to open the parts enclosure.



3

The logic controller cycle overviews are as follows:

- Case 1: A single rain event fills the batch detention basin. The basin holds the diverted storm water for the detention time (12 hours) and the releases the water. Once the batch detention basin is empty, a delay of 2 hours is started to allow the basin to completely drain, and then a close signal is sent to the actuator to close the valve.
- Case 2: A single rain event occurs, but does not completely fill the batch detention basin. The basin holds the water for the detention period (12 hours), and then releases it. Once the batch detention basin is empty, a delay of 2 hours is started to allow the basin to completely drain, and then a close signal is sent to the actuator to close the valve.
- Case 3: A single rain event fills the batch detention basin under the trip point of the level sensor. The level sensor does not trip. The captured water is held until it infiltrates / evaporates or is joined by storm water from a subsequent storm.
- Case 4: Begins the same as Case 1. During the drawdown period, one or more additional rain events occur causing additional water to enter the batch detention basin. The valve remains open and the additional water volume is drained. Once the batch detention basin is empty, a delay of 2 hours is started to allow the basin to completely drain, and then a close signal is sent to the actuator to close the valve.
- Case 5: Begins the same as Case 2. During the drawdown period, one or more additional rain events can occur causing additional water to enter the basin. The valve remains open and the additional water volume is drained. Once the batch detention basin is empty, a delay of 2 hours is started to allow the basin to completely drain, and then a close signal is sent to the actuator to close the valve.

Safety Precautions:

The system will be equipped with an alarm system that is clearly visible to indicate a system malfunction. A sign shall be posted with phone numbers of the owner and appropriate TCEQ regional office.



Vegetated Filter Strips

The remaining areas of the Modified Phase 2 CZP that are not treated in proposed Batch Detention Basin J and existing Batch Detention Basin H will be treated by 15' wide engineered vegetated filter strips (VFS). The VFS areas are identified on the Treatment Summary Exhibit. The VFS will treat 11.09 acres of impervious cover and provide 10,574 lb. of TSS removal.



ATTACHMENT C



DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANT'S ORIGINAL SIGNATURE AND SEAL

Impervious Cover & Water Quality Treatment Summary (Post Phase 2, 4, & 5 Development)					
	LIVELY TRACT, PH	ASE 2 MODIFIED CZP			
B.M.P.	Area (AC)	I.C. (AC)	TSS Removal (lb.)		
Batch Detention Pond H	80.06	33.34	34,326		
Batch Detention Pond J	16.63	7.13	7,333		
Residential VFS D	9.89	5.05	4,824		
Residential VFS E	6.59	3.25	3,108		
Open Space Area	3.53	0	0		
Total CZP	116.70	48.77	49,591	Required 49,591	

CONTRIBUTING ZONE PLAN APPLICATION

Contributing Zone Plan Application

Texas Commission on Environmental Quality

for Regulated Activities on the Contributing Zone to the Edwards Aquifer and Relating to 30 TAC §213.24(1), Effective June 1, 1999

To ensure that the application is administratively complete, confirm that all fields in the form are complete, verify that all requested information is provided, consistently reference the same site and contact person in all forms in the application, and ensure forms are signed by the appropriate party.

Note: Including all the information requested in the form and attachments contributes to more streamlined technical reviews.

Signature

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This **Contributing Zone Plan Application** is hereby submitted for TCEQ review and Executive Director approval. The application was prepared by:

Print Name of Customer/Agent: Dustin Goss, P.E., LEED* AP

Date: 4/8/25

Signature of Customer/Agent:

Regulated Entity Name: Lively Tract, Phase 2

Project Information

- 1. County: Williamson
- 2. Stream Basin: South Fork San Gabriel River
- 3. Groundwater Conservation District (if applicable): N/A
- 4. Customer (Applicant):

Contact Person: Tom Rielly Entity: Hwy 29 Ventures 2015 LP Mailing Address: 4910 Campus Drive City, State: Newport Beach, CA Zip: 92660 Telephone: 949-922-2512 Fax: _____ Email Address: tomr@shamrockcommunities.com

TCEQ-10257 (Rev. 02-11-15)

1 of 11

5. Agent/Representative (If any):

Contact Person: <u>Dustin Goss, P.E., LEED® AP</u> Entity: <u>Pape-Dawson Engineers, Inc.</u> Mailing Address: <u>10801 N Mopac Expy. Bldg. 3, Suite 200</u> City, State: <u>Austin, TX</u> Zip: <u>78759</u> Telephone: <u>512-454-8711</u> Fax: _____ Email Address: <u>dgoss@pape-dawson.com</u>

6. Project Location:

The project site is located inside the city limits of _____.

- The project site is located outside the city limits but inside the ETJ (extra-territorial jurisdiction) of <u>City of Leander</u>.
- The project site is not located within any city's limits or ETJ.
- 7. The location of the project site is described below. Sufficient detail and clarity has been provided so that the TCEQ's Regional staff can easily locate the project and site boundaries for a field investigation.
 - <u>From TCEQ's Regional Office, proceed north on IH-35 for approximately 16.6 miles. Exit</u> <u>261 toward Texas 29 / Burnet and keep right at the fork, following signs for Taylor.</u> <u>Turn left onto West University Avenue / Texas 29 W and Proceed approximately 6.5</u> <u>miles. Turn left onto Lively Ranch Road and the site will be in front in approximately</u> <u>0.5 mile.</u>
- 8. Attachment A Road Map. A road map showing directions to and the location of the project site is attached. The map clearly shows the boundary of the project site.
- 9. Attachment B USGS Quadrangle Map. A copy of the official 7 ½ minute USGS Quadrangle Map (Scale: 1" = 2000') is attached. The map(s) clearly show:

Project site boundaries.
 USGS Quadrangle Name(s).

- 10. Attachment C Project Narrative. A detailed narrative description of the proposed project is attached. The project description is consistent throughout the application and contains, at a minimum, the following details:
 - Area of the site
 Offsite areas
 Impervious cover
 Permanent BMP(s)
 Proposed site use
 Site history
 Previous development
 Area(s) to be demolished

- 11. Existing project site conditions are noted below:
 - Existing commercial site
 - ____ Existing industrial site
 - Existing residential site
 - Existing paved and/or unpaved roads
 - Undeveloped (Cleared)
 - Undeveloped (Undisturbed/Not cleared)

Other:	

12. The type of project is:

\times	Residential:	# c	of Lot	s: 429
\sim	residential			<u></u>

] Residential: # of Living Unit Equivalents: _____] Commercial] Industrial

- Other:
- 13. Total project area (size of site): <u>120.60</u> Acres

Total disturbed area: <u>120.60</u> Acres

- 14. Estimated projected population: 1716
- 15. The amount and type of impervious cover expected after construction is complete is shown below:

 Table 1 - Impervious Cover

Impervious Cover of Proposed Project	Sq. Ft.	Sq. Ft./Acre	Acres
Structures/Rooftops	2,026,533.19	÷ 43,560 =	46.52
Parking	0	÷ 43,560 =	0
Other paved surfaces	724,138.79	÷ 43,560 =	16.62
Total Impervious Cover	2,750,671.98	÷ 43,560 =	63.15

Total Impervious Cover <u>63.15</u> ÷ Total Acreage <u>120.60</u> X 100 = <u>52.38</u>% Impervious Cover

- 16. Attachment D Factors Affecting Surface Water Quality. A detailed description of all factors that could affect surface water quality is attached. If applicable, this includes the location and description of any discharge associated with industrial activity other than construction.
- 17. 🛛 Only inert materials as defined by 30 TAC 330.2 will be used as fill material.

For Road Projects Only

Complete questions 18 - 23 if this application is exclusively for a road project.

N/A

- 18. Type of project:
- TXDOT road project. County road or roads built to county specifications. City thoroughfare or roads to be dedicated to a municipality. Street or road providing access to private driveways. 19. Type of pavement or road surface to be used: Concrete Asphaltic concrete pavement Other: 20. Right of Way (R.O.W.): Length of R.O.W.: _____ feet. Width of R.O.W.: feet. $L \times W = Ft^2 \div 43,560 Ft^2/Acre = acres.$ 21. Pavement Area: Length of pavement area: _____ feet. Width of pavement area: ______ feet. $L x W = ___Ft^2 \div 43,560 Ft^2/Acre = ____acres.$ Pavement area _____ acres ÷ R.O.W. area _____ acres x 100 = ____% impervious cover. 22. A rest stop will be included in this project. A rest stop will not be included in this project. 23. Maintenance and repair of existing roadways that do not require approval from the TCEQ Executive Director. Modifications to existing roadways such as widening roads/adding shoulders totaling more than one-half (1/2) the width of one (1) existing

Stormwater to be generated by the Proposed Project

lane require prior approval from the TCEQ.

24. Attachment E - Volume and Character of Stormwater. A detailed description of the volume (quantity) and character (quality) of the stormwater runoff which is expected to occur from the proposed project is attached. The estimates of stormwater runoff quality and quantity are based on area and type of impervious cover. Include the runoff coefficient of the site for both pre-construction and post-construction conditions.

Wastewater to be generated by the Proposed Project

25. Wastewater is to be discharged in the contributing zone. Requirements under 30 TAC §213.6(c) relating to Wastewater Treatment and Disposal Systems have been satisfied.

🛛 N/A

26. Wastewater will be disposed of by:

On-Site Sewage Facility (OSSF/Septic Tank):

Attachment F - Suitability Letter from Authorized Agent. An on-site sewage facility will be used to treat and dispose of the wastewater from this site. The appropriate licensing authority's (authorized agent) written approval is attached. It states that the land is suitable for the use of private sewage facilities and will meet or exceed the requirements for on-site sewage facilities as specified under 30 TAC Chapter 285 relating to On-site Sewage Facilities.

Each lot in this project/development is at least one (1) acre (43,560 square feet) in size. The system will be designed by a licensed professional engineer or registered sanitarian and installed by a licensed installer in compliance with 30 TAC Chapter 285.

Sewage Collection System (Sewer Lines):

The sewage collection system will convey the wastewater to the <u>San Gabriel</u> (name) Treatment Plant. The treatment facility is:

Existing.

□ N/A

Permanent Aboveground Storage Tanks(ASTs) ≥ 500 Gallons

Complete questions 27 - 33 if this project includes the installation of AST(s) with volume(s) greater than or equal to 500 gallons.

N/A

27. Tanks and substance stored:

Table 2 - Tanks and Substance Storage

AST Number	Size (Gallons)	Substance to be Stored	Tank Material
1			
2			
3			

AST Number	Size (Gallons)	Substance to be Stored	Tank Material
4			
5			

Total x 1.5 = ____ Gallons

- 28. The AST will be placed within a containment structure that is sized to capture one and one-half (1 1/2) times the storage capacity of the system. For facilities with more than one tank system, the containment structure is sized to capture one and one-half (1 1/2) times the cumulative storage capacity of all systems.
 - Attachment G Alternative Secondary Containment Methods. Alternative methods for providing secondary containment are proposed. Specifications showing equivalent protection for the Edwards Aquifer are attached.

29. Inside dimensions and capacity of containment structure(s):

Table 3 - Secondary Containment

Length (L)(Ft.)	Width(W)(Ft.)	Height (H)(Ft.)	L x W x H = (Ft3)	Gallons

Total: _____ Gallons

30. Piping:

All piping, hoses, and dispensers will be located inside the containment structure. Some of the piping to dispensers or equipment will extend outside the containment

structure.

] The piping will be aboveground

The piping will be underground

- 31. The containment area must be constructed of and in a material impervious to the substance(s) being stored. The proposed containment structure will be constructed of:
- 32. Attachment H AST Containment Structure Drawings. A scaled drawing of the containment structure is attached that shows the following:

Interior dimensions (length, width, depth and wall and floor thickness).

] Internal drainage to a point convenient for the collection of any spillage.

Tanks clearly labeled

Piping clearly labeled

Dispenser clearly labeled

33. Any spills must be directed to a point convenient for collection and recovery. Spills from storage tank facilities must be removed from the controlled drainage area for disposal within 24 hours of the spill.



In the event of a spill, any spillage will be removed from the containment structure within 24 hours of the spill and disposed of properly.

In the event of a spill, any spillage will be drained from the containment structure through a drain and valve within 24 hours of the spill and disposed of properly. The drain and valve system are shown in detail on the scaled drawing.

Site Plan Requirements

Items 34 - 46 must be included on the Site Plan.

34. \boxtimes The Site Plan must have a minimum scale of 1" = 400'.

Site Plan Scale: 1" = 200'.

- 35. 100-year floodplain boundaries:
 - Some part(s) of the project site is located within the 100-year floodplain. The floodplain is shown and labeled.
 - $|\times|$ No part of the project site is located within the 100-year floodplain.

The 100-year floodplain boundaries are based on the following specific (including date of material) sources(s): FEMA FIRM Panel No. 48491C0460F for Williamson County, Effective Date December 20, 2019.

36. \times The layout of the development is shown with existing and finished contours at appropriate, but not greater than ten-foot contour intervals. Lots, recreation centers, buildings, roads, etc. are shown on the site plan.

 $\left| \! \right\rangle$ The layout of the development is shown with existing contours at appropriate, but not greater than ten-foot contour intervals. Finished topographic contours will not differ from the existing topographic configuration and are not shown. Lots, recreation centers, buildings, roads, etc. are shown on the site plan.

- 37. \times A drainage plan showing all paths of drainage from the site to surface streams.
- 38. 🖂 The drainage patterns and approximate slopes anticipated after major grading activities.
- 39. \square Areas of soil disturbance and areas which will not be disturbed.
- 40. \times Locations of major structural and nonstructural controls. These are the temporary and permanent best management practices.
- 41. 🛛 Locations where soil stabilization practices are expected to occur.
- 42. Surface waters (including wetlands).

TCEQ-10257 (Rev. 02-11-15)

N/A

43. Locations where stormwater discharges to surface water.

There will be no discharges to surface water.

44. Temporary aboveground storage tank facilities.

Temporary aboveground storage tank facilities will not be located on this site.

45. Permanent aboveground storage tank facilities.

Permanent aboveground storage tank facilities will not be located on this site.

46. \boxtimes Legal boundaries of the site are shown.

Permanent Best Management Practices (BMPs)

Practices and measures that will be used during and after construction is completed.

47. Permanent BMPs and measures must be implemented to control the discharge of pollution from regulated activities after the completion of construction.

□ N/A

- 48. These practices and measures have been designed, and will be constructed, operated, and maintained to insure that 80% of the incremental increase in the annual mass loading of total suspended solids (TSS) from the site caused by the regulated activity is removed. These quantities have been calculated in accordance with technical guidance prepared or accepted by the executive director.
 - The TCEQ Technical Guidance Manual (TGM) was used to design permanent BMPs and measures for this site.
 - A technical guidance other than the TCEQ TGM was used to design permanent BMPs and measures for this site. The complete citation for the technical guidance that was used is: _____.



49. Owners must insure that permanent BMPs and measures are constructed and function as designed. A Texas Licensed Professional Engineer must certify in writing that the permanent BMPs or measures were constructed as designed. The certification letter must be submitted to the appropriate regional office within 30 days of site completion.

🗌 N/A

50. Where a site is used for low density single-family residential development and has 20 % or less impervious cover, other permanent BMPs are not required. This exemption from permanent BMPs must be recorded in the county deed records, with a notice that if the percent impervious cover increases above 20% or land use changes, the exemption for the whole site as described in the property boundaries required by 30 TAC §213.4(g) (relating to

Application Processing and Approval), may no longer apply and the property owner must notify the appropriate regional office of these changes.

The site will be used for low density single-family residential development and has	S
20% or less impervious cover.	

The site will be used for low density single-family residential development but has more than 20% impervious cover.

The site will not be used for low density single-family residential development.

51. The executive director may waive the requirement for other permanent BMPs for multifamily residential developments, schools, or small business sites where 20% or less impervious cover is used at the site. This exemption from permanent BMPs must be recorded in the county deed records, with a notice that if the percent impervious cover increases above 20% or land use changes, the exemption for the whole site as described in the property boundaries required by 30 TAC §213.4(g) (relating to Application Processing and Approval), may no longer apply and the property owner must notify the appropriate regional office of these changes.

Attachment I - 20% or Less Impervious Cover Waiver. The site will be used for multi-family residential developments, schools, or small business sites and has 20% or less impervious cover. A request to waive the requirements for other permanent BMPs and measures is attached.

The site will be used for multi-family residential developments, schools, or small business sites but has more than 20% impervious cover.

The site will not be used for multi-family residential developments, schools, or small business sites.

52. X Attachment J - BMPs for Upgradient Stormwater.

- A description of the BMPs and measures that will be used to prevent pollution of surface water, groundwater, or stormwater that originates upgradient from the site and flows across the site is attached.
- No surface water, groundwater or stormwater originates upgradient from the site and flows across the site, and an explanation is attached.

Permanent BMPs or measures are not required to prevent pollution of surface water, groundwater, or stormwater that originates upgradient from the site and flows across the site, and an explanation is attached.

53. X Attachment K - BMPs for On-site Stormwater.

A description of the BMPs and measures that will be used to prevent pollution of surface water or groundwater that originates on-site or flows off the site, including pollution caused by contaminated stormwater runoff from the site is attached.

Permanent BMPs or measures are not required to prevent pollution of surface water or groundwater that originates on-site or flows off the site, including pollution caused by contaminated stormwater runoff, and an explanation is attached.

54. X Attachment L - BMPs for Surface Streams.	A description of the BMPs and measures
that prevent pollutants from entering surfa-	ce streams is attached.

N/A

55. Attachment M - Construction Plans. Construction plans and design calculations for the proposed permanent BMPs and measures have been prepared by or under the direct supervision of a Texas Licensed Professional Engineer, and are signed, sealed, and dated. Construction plans for the proposed permanent BMPs and measures are attached and include: Design calculations, TCEQ Construction Notes, all proposed structural plans and specifications, and appropriate details.

🗌 N/A

56. Attachment N - Inspection, Maintenance, Repair and Retrofit Plan. A site and BMP specific plan for the inspection, maintenance, repair, and, if necessary, retrofit of the permanent BMPs and measures is attached. The plan fulfills all of the following:

Prepared and certified by the engineer designing the permanent BMPs and measures

Signed by the owner or responsible party

Outlines specific procedures for documenting inspections, maintenance, repairs, and, if necessary, retrofit.

Contains a discussion of record keeping procedures

N/A

57. Attachment O - Pilot-Scale Field Testing Plan. Pilot studies for BMPs that are not recognized by the Executive Director require prior approval from the TCEQ. A plan for pilot-scale field testing is attached.

🛛 N/A

58. Attachment P - Measures for Minimizing Surface Stream Contamination. A description of the measures that will be used to avoid or minimize surface stream contamination and changes in the way in which water enters a stream as a result of the construction and development is attached. The measures address increased stream flashing, the creation of stronger flows and in-stream velocities, and other in-stream effects caused by the regulated activity, which increase erosion that result in water quality degradation.

🗌 N/A

Responsibility for Maintenance of Permanent BMPs and Measures after Construction is Complete.

59. The applicant is responsible for maintaining the permanent BMPs after construction until such time as the maintenance obligation is either assumed in writing by another entity having ownership or control of the property (such as without limitation, an

TCEQ-10257 (Rev. 02-11-15)

10 of 11

owner's association, a new property owner or lessee, a district, or municipality) or the ownership of the property is transferred to the entity. Such entity shall then be responsible for maintenance until another entity assumes such obligations in writing or ownership is transferred.

60. A copy of the transfer of responsibility must be filed with the executive director at the appropriate regional office within 30 days of the transfer if the site is for use as a multiple single-family residential development, a multi-family residential development, or a non-residential development such as commercial, industrial, institutional, schools, and other sites where regulated activities occur.

Administrative Information

- 61. Submit one (1) original and one (1) copy of the application, plus additional copies as needed for each affected incorporated city, groundwater conservation district, and county in which the project will be located. The TCEQ will distribute the additional copies to these jurisdictions.
- 62. Any modification of this Contributing Zone Plan may require TCEQ review and Executive Director approval prior to construction, and may require submission of a revised application, with appropriate fees.
- 63. The site description, controls, maintenance, and inspection requirements for the storm water pollution prevention plan (SWPPP) developed under the EPA NPDES general permits for stormwater discharges have been submitted to fulfill paragraphs 30 TAC §213.24(1-5) of the technical report. All requirements of 30 TAC §213.24(1-5) have been met by the SWPPP document.
 - The Temporary Stormwater Section (TCEQ-0602) is included with the application.

ATTACHMENT A



S DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANTS ORIGINAL SIGNATURE AND SEA

ATTACHMENT B





S DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANTS ORIGINAL SIGNATURE AND SEAL

ATTACHMENT C

Project Narrative

Lively Tract, Phase 2 is located southeast of the intersection of Ronald Reagan Blvd. and SH Hwy 29, within the City of Leander ETJ in Williamson County, Texas. The initial phases of the development (Lively Tract Phase 1 Sections 1-10, Phase 2, Phase 4, Phase 5) have been permitted and are in various stages of construction. The entire Phase 1 boundary is located within the Recharge Zone; thus no Contributing Zone Plan currently exists for the property. Phase 2 has been constructed and is located partly over the Edwards Aquifer Recharge Zone and partly over the Contributing Zone. Therefore, the total Phase 2 boundary has been divided into a Recharge Zone boundary and a Contributing Zone boundary with separate applications being submitted for the construction activities over the Recharge Zone (WPAP) and the Contributing Zone (CZP). While Phase 2 has been built as part of the originally approved CZP with 27.10 acres of development over the Contributing Zone, the PBMP's built with Phase 2 will serve portions of future phases of the development, ultimately resulting in an 120.60-acre contributing area. A modification to this Contributing Zone Plan will be submitted at the time of development of any future phase contributing to the Phase 2 PBMP's. The first modification was approved and included a portion of Lively Tract, Phase 4. The second modification was also approved and encompassed Lively Tract, Phase 5. The third and final modification is proposed with this with this CZP to include Lively Tract, Phase 6 which along with previous phases, includes development that contributes to Phase 2 constructed PBMP's. 22.83 acres of disturbed acreage will result from Phase 6 construction as part of this modified Phase 2 CZP.

Construction activities proposed with the Lively Tract improvements include clearing, grading, excavation, installation of utilities and drainage improvements, streets, sidewalks, 429 homes with associated driveways, and two (2) water quality basins. Of the 120.60-acre CZP project limits, the proposed improvements include approximately 63.15 acres (52.36%) of impervious cover in the ultimate post-development condition contributed by single-family lots and street right-of-way.

Two (2) existing batch detention basins and engineered vegetated filter strips (VFS) are proposed as the Permanent Best Management Practices (PBMPs) for this site. All PBMPs have been designed in accordance with the TCEQ's Technical Guidance Manual (TGM) RG-348 (2005) to remove 80% of the increase in Total Suspended Solids (TSS) from the site. Please see the Treatment Summary Exhibit included as an attachment to this application for more information.

At full build-out, this project will generate approximately 102,960 gallons per day of average wastewater flow. Sewage flow will be disposed of by conveyance to the existing San Gabriel Wastewater Treatment Plant. Potable water will be provided by the City of Leander.



Batch Detention Basin

The batch detention basins (Batch Detention Basins H & J) are earthen ponds with side-slopes at 3:1 with the exception of maintenance access paths which are at 4:1 slopes. Batch Detention Basin H is designed to treat 43.35 acres of impervious cover and remove 44,271 lb. of TSS at Ultimate Buildout. Batch Detention Basin J is designed to treat 8.71 acres of impervious cover and remove 8,889 lb. of TSS at Ultimate Buildout. Treatment is provided by a batch detention pond controller that will regulate the release of the captured runoff.

The following is a summary of the batch detention pond controller components:

Batch Detention Pond Controller Information			
Component	Description	Voltage	
Power System	Solar Charged 12 VDC Battery (Model MK Powered 8GU1) (Or approved equal)		
Logic Controller	IDEC FL1C-H12RCE (Or approved equal)	12	
Parts Enclosure	Southwest Photovoltaic Model BBG-1 (15.75" wide x 9.75" deep x 11.75" tall) (Or approved equal)		
Nature of Event Sensing	Anchor Scientific Float Switch (Or approved equal)		
Valve Type	Keystone 4" (Pond 1) and 6" (Pond 2) Butterfly Valve with over torque sensors and mechanical hand crank for physical override if necessary. Able to withstand 100 psi minimum. (Or approved equal)		
Actuator	EPI-6 12 VDC. Able to withstand 100 psi minimum. (Or approved equal)	12	
Power Consumption (actuator, controller, relay, PLC)	242.58 W, 46.5 W-hours		



The following is a circuit diagram of the controllers:



The logic controllers will provide a test sequence. The systems will be solar powered and will be equipped with a backup battery. The systems will be equipped with an on/off/reset switch. The butterfly valves will be equipped with a manual hand crank for physical override if necessary in the event of a spill or for maintenance purposes. The systems will be equipped with a clearly visible external indicator to indicate if a cycle is in progress without having to open the parts enclosure.

The logic controller cycle overviews are as follows:

- Case 1: A single rain event fills the batch detention basin. The basin holds the diverted storm water for the detention time (12 hours) and the releases the water. Once the batch detention basin is empty, a delay of 2 hours is started to allow the basin to completely drain, and then a close signal is sent to the actuator to close the valve.
- Case 2: A single rain event occurs, but does not completely fill the batch detention basin. The basin holds the water for the detention period (12 hours), and then releases it. Once the batch detention basin is empty, a delay of 2 hours is started to allow the basin to completely drain, and then a close signal is sent to the actuator to close the valve.
- Case 3: A single rain event fills the batch detention basin under the trip point of the level sensor. The level sensor does not trip. The captured water is held until it infiltrates / evaporates or is joined by storm water from a subsequent storm.
- Case 4: Begins the same as Case 1. During the drawdown period, one or more additional rain events occur causing additional water to enter the batch detention basin. The valve remains open and the additional water volume is drained. Once the batch detention basin is empty, a delay of 2 hours is started to allow the basin to completely drain, and then a close signal is sent to the actuator to close the valve.
- Case 5: Begins the same as Case 2. During the drawdown period, one or more additional rain events can occur causing additional water to enter the basin. The valve remains open and the additional water volume is drained. Once the batch detention basin is empty, a delay of 2 hours is started to allow the basin to completely drain, and then a close signal is sent to the actuator to close the valve.

Safety Precautions:



The system will be equipped with an alarm system that is clearly visible to indicate a system malfunction. A sign shall be posted with phone numbers of the owner and appropriate TCEQ regional office.

Vegetated Filter Strips

The remaining areas of the CZP that are not treated in proposed Batch Detention Basin J and Batch Detention Basin H will be treated by 15' wide engineered vegetated filter strips (VFS). The VFS areas are identified on the Treatment Summary Exhibit. The VFS will treat 11.09 acres of impervious cover and provide 10,574 lb. of TSS removal.


TSS Removal Calculations 04-20-2009

Ultimate Buildout

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell. Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348. Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

Project Name: Lively Tract, Phase 2 Modified CZP Date Prepared: 3/26/2025

1. The Required Load Reduction for the total project:	Calculations from RG-	348	Pages 3-27 t	o 3-30
Page 3-29 Equation 3.3: $L_{\rm M}$ = 2	27.2(A _N x P)			
		1	- the manual development - 000/ of	
where: L _{M TOTAL PROJECT} = I	Required 155 remova	i resulting from	the proposed development = 80% of the project	Increased load
P = /	Average annual precip	itation, inches	ie project	
Site Data: Determine Required Load Removal Rased on the Entire Project				
County =	Williamson			
Total project area included in plan * =	120.60	acres		
Total post-development impervious area within the limits of the plan * =	63.15	acres		
Total post-development impervious cover fraction * =	0.52			
P =	32	inches		
LM TOTAL PROJECT =	54,966	lbs.		
* The values entered in these fields should be for the total project area.				
Number of drainage basins / outfalls areas leaving the plan area =	5			
2. Drainage Basin Parameters (This information should be provided for each	<u>basin):</u>			
Drainage Basin/Outfall Area No. =	н	Ultimate C	ondition	
Total drainage basin/outfall area -	91 10	00700		
Predevelopment impervious area within drainage basin/outfall area =	0.00	acres		
Post-development impervious area within drainage basin/outfall area =	43.35	acres		
Post-development impervious fraction within drainage basin/outfall area =	0.53	lha		
LM THIS BASIN -	37,732	IDS.		
3. Indicate the proposed BMP Code for this basin.				
Proposed BMP = 1	Batch Detention Pon	d		
Removal efficiency =	91	percent	MANUALLY ADJUSTED	
4. Calculate Maximum TSS Load Removed (L_R) for this Drainage Basin by the	e selected BMP Type).		
RG-348 Page 3-33 Equation 3.7: L _R = ((BMP efficiency) x P x	(A ₁ x 34.6 + A ₁	_P x 0.54)	
	Total On Site drainage	area in the D	VD establight eres	
where: A _C =	I otal On-Site drainage	e area in the Bi	NP catchment area	
A _P = 1	Pervious area remaini	ng in the BMP	catchment area	
L _R = -	TSS Load removed fro	om this catchm	ent area by the proposed BMP	
A -	94.40			
$A_{\rm C} = $	43 35	acres		
	37.75	acres		
L _R =	44,271	lbs		
5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall an	rea			
Desired L _{M THIS BASIN} =	37,732	lbs.		
F =	0.85			
C. Coloulate Conture Volume required by the BMD Type for this drainage base	in / sutfall area		Coloulations from DC 349	Deces 2, 24 to 2, 26
6. Calculate Capture Volume required by the BMP Type for this dramage bas	an / outian area.		Calculations from RG-346	Pages 3-34 10 3-30
Rainfall Depth =	1.32	inches		
Post Development Runoff Coefficient =	0.38			
On-site Water Quality Volume =	146613	CUDIC TEET		
	Calculations from RG-	348	Pages 3-36 to 3-37	
Off-site area draining to BMP =	0.00	acres		
Off-site Impervious cover draining to BMP =	0.00	acres		
Impervious fraction of off-site area =	0			
Off-site Runott Coefficient = Off-site Water Quality Volume =	0.00 0	cubic feet		
	-			
Storage for Sediment =	29323			
Total Capture Volume (required water quality volume(s) x 1.20) =	175936	cubic feet		

TSS Removal Calculations 04-20-2009

Ultimate Buildout

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell. Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348. Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

Project Name: Lively Tract, Phase 2 Modified CZP Date Prepared: 3/26/2025

1. The Required Load Reduction for the total project:	Calculations from RG-3	48	Pages 3-27 to 3-30				
Page 3-29 Equation 3.3: L_{M} =	27.2(A _N x P)						
where: $\begin{array}{c} L_{M \ TOTAL \ PROJECT} = \\ A_{N} = \\ P = \end{array}$	Required TSS removal Net increase in impervice Average annual precipit	resulting from ous area for th ation, inches	n the proposed development = 80% of i he project	increased load			
Site Data: Determine Required Load Removal Based on the Entire Project							
County =	Williamson						
Predevelopment impervious area within the limits of the plan * =	0.00	acres					
Total post-development impervious area within the limits of the plan * =	63.15	acres					
I otal post-development impervious cover fraction * =	0.52	inches					
		Indites					
L _{M TOTAL PROJECT} = * The values entered in these fields should be for the total project area.	54,966	lbs.					
Number of drainage basins / outfalls areas leaving the plan area =	5						
2. Drainage Basin Parameters (This information should be provided for eac	:h basin):						
Drainage Basin/Outfall Area No. =	- J	Ultimate C	ondition				
Total drainage basin/outfall area =	15.93	acres					
Predevelopment impervious area within drainage basin/outfall area =	0.00	acres					
Post-development impervious area within drainage basin/outfall area =	8.71	acres					
- Post-development impervious naction within dramage basin/outlan area - L _{M THIS BASIN} =	7,581	lbs.					
3 Indicate the proposed BMP Code for this basin							
Drassed DND -	Detab Detaction Devid						
Removal efficiency =	91	percent	MANUALLY ADJUSTED				
4. Calculate Maximum TSS Load Removed (L_R) for this Drainage Basin by the	he selected BMP Type.						
RG-348 Page 3-33 Equation 3.7: La =	(BMP efficiency) x P x (A, x 34.6 + A	- x (0.54)				
where: A _C =	I otal On-Site drainage	area in the BM	MP catchment area				
A _P =	A _P = Pervious area remaining in						
L _R =	L_R = TSS Load removed from this catchment are						
Α -	15.03	acres					
A, =	8.71	acres					
A _P =	7.22	acres					
L _R =	8,889	lbs					
5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall a	area						
Desired L _{M THIS BASIN} =	7,581	lbs.					
F =	0.85						
6. Calculate Capture Volume required by the BMP Type for this drainage ba	asin / outfall area.		Calculations from RG-348	Pages 3-34 to 3-36			
Rainfall Deoth =	1.32	inches					
Post Development Runoff Coefficient =	0.38						
On-site Water Quality Volume =	29367	cubic feet					
	Calculations from RG-3	48	Pages 3-36 to 3-37				
Off-site area draining to BMP =	0.00	acres					
Off-site Impervious cover draining to BMP =	0.00	acres					
Off-site Runoff Coefficient =	0.00						
Off-site Water Quality Volume =	0	cubic feet					
Storage for Sediment =	5873						
Total Capture Volume (required water quality volume(s) x 1.20) =	35240	cubic feet					

TSS Removal Calculations 04-20-2009

Project Name: Lively Tract, Phase 2 Modified CZP Date Prepared: 3/26/2025

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell. Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348. Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations from RG	G-348	Pages 3-27 to 3-30				
Page 3-29 Equation 3.3: L _M -	= 27.2(A _N x P)						
where: L _{M TOTAL PROJECT} A _N	Required TSS removal resulting from the proposed development = 80% of increased load Net increase in impervious area for the project Average annual precipitation, inches						
Site Data: Determine Required Load Removal Based on the Entire Project	t						
County	- Williamson						
Predevelopment impervious area within the limits of the plan *	= 120.60	acres					
Total post-development impervious area within the limits of the plan *	63.15	acres					
Total post-development impervious cover fraction *	0.52	inches					
	02	moneo					
$$L_{\rm M}\ total\ {\rm project}$$ * The values entered in these fields should be for the total project area.	= 54,966	lbs.					
Number of drainage basins / outfalls areas leaving the plan area =	5						
2. Drainage Basin Parameters (This information should be provided for each	ch basin):						
Drainage Basin/Outfall Area No.	VFS D	Ultimate C	ondition				
Total drainage basin/outfall area	9.87	acres					
Predevelopment impervious area within drainage basin/outfall area =	= 0.00	acres					
Post-development impervious area within drainage basin/outrain area - Post-development impervious fraction within drainage basin/outrain area -	= 0.54	acres					
L _{M THIS BASIN}	= 4,604	lbs.					
3. Indicate the proposed BMP Code for this basin.							
Proposed BMP	Vegetated Filter Str	ips					
Removal efficiency =	- 85	percent	MANUALLY ADJUSTED				
4. Calculate Maximum TSS Load Removed (L _R) for this Drainage Basin by	the selected BMP Typ	<u>be.</u>					
RG-348 Page 3-33 Equation 3.7: L _R	= (BMP efficiency) x P	x (A ₁ x 34.6 + A _P	x 0.54)				
where: A _C -	= Total On-Site drainag	ge area in the BN	IP catchment area				
A ₁ =	 Impervious area prop 	oosed in the BMP	P catchment area				
Ap : L _R :	 Pervious area remain TSS Load removed f 	rom this catchme	catchment area ant area by the proposed BMP				
	0.07						
A _C =	- 9.87	acres					
Ap :	- 4.58	acres					
L _R .	= 5,046	lbs					
5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall	area						
	= 4 680	lbs	*includes overtreatment of 0.087 ac IC for lots t	hat			
	.,	100.	do not have fiter strips due to slopes higher the	an 20%			
	- 0.93			5			
6. Calculate Capture Volume required by the BMP Type for this drainage b	asin / outfall area.		Calculations from RG-348	Pages 3-34 to 3-36			
Rainfall Depth	= 2.20	inches					
Post Development Runon Coefficient = On-site Water Quality Volume =	29807	cubic feet					
	Calculations from RG	G-348	Pages 3-36 to 3-37				
Off-site area draining to RMP -	0.00	acres					
Off-site Impervious cover draining to BMP =	0.00	acres					
Impervious fraction of off-site area =	0						
Off-site Kunof Coefficient = Off-site Water Quality Volume =	0.00	cubic feet					
Storage for Sediment -	5961						
Total Capture Volume (required water quality volume(s) x 1.20) :	= 35768	cubic feet					

TSS Removal Calculations 04-20-2009

Project Name: Lively Tract, Phase 2 Modified CZP Date Prepared: 3/26/2025

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell. Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348. Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations from RG-3	48	Pages 3-27 to 3-30		
Page 3-29 Equation 3.3: L_{M} =	27.2(A _N x P)				
where: $\begin{tabular}{lllllllllllllllllllllllllllllllllll$	Required TSS removal Net increase in impervi Average annual precipi	resulting from ous area for tl tation, inches	n the proposed development = 80% of he project	increased load	
Site Data: Determine Required Load Removal Based on the Entire Project	t				
County =	Williamson				
Predevelopment impervious area within the limits of the plan * =	0.00	acres			
Total post-development impervious area within the limits of the plan * =	63.15	acres			
Total post-development impervious cover fraction * =	0.52	inches			
	02	mones			
L _{M TOTAL PROJECT} = * The values entered in these fields should be for the total project area.	54,966	lbs.			
Number of drainage basins / outfalls areas leaving the plan area =	5				
2. Drainage Basin Parameters (This information should be provided for each	:h basin):				
Drainage Basin/Outfall Area No. =	VFS E	Ultimate C	ondition		
Total drainage basin/outfall area =	6.68	acres			
Predevelopment impervious area within drainage basin/outfall area =	0.00	acres			
Post-development impervious area within drainage basin/outfall area =	3.68	acres			
L _{M THIS BASIN}	3,203	lbs.			
3. Indicate the proposed BMP Code for this basin.					
Proposed BMP =	Vegetative Filter Strip	s			
Removal efficiency =	85	percent	MANUALLY ADJUSTED		
4. Calculate Maximum TSS Load Removed (L_R) for this Drainage Basin by t	he selected BMP Type.				
RG-348 Page 3-33 Equation 3.7: L _R =	(BMP efficiency) x P x (A _I x 34.6 + A _I	_P x 0.54)		
where: A _c =	Total On-Site drainage	area in the BI	MP catchment area		
A ₁ =	Impervious area propos	sed in the BM	P catchment area		
A _P = L _R =	Pervious area remainin TSS Load removed from	catchment area lent area by the proposed BMP			
A _c =	6.68	acres			
A ₁ =	3.68	acres			
A _P =	3.00	acres			
L _R =	3,507	IDS			
5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall	area				
Desired $L_{M THIS BASIN}$ =	3,203	lbs.			
F =	0.91				
6. Calculate Capture Volume required by the BMP Type for this drainage ba	asin / outfall area.		Calculations from RG-348	Pages 3-34 to 3-36	
Rainfall Depth =	1.80	inches			
Post Development Runoff Coefficient =	0.39	cubic feet			
On-site Water Quality Volume -	16505	Cubic leet			
	Calculations from RG-3	48	Pages 3-36 to 3-37		
Off-site area draining to BMP =	0.00	acres			
Off-site Impervious cover draining to BMP =	0.00	acres			
Off-site Runoff Coefficient =	0.00				
Off-site Water Quality Volume =	0	cubic feet			
Storage for Sediment =	3381				
Total Capture Volume (required water quality volume(s) x 1.20) =	20285	cubic feet			

TSS Removal Calculations 04-20-2009

Project Name: Lively Tract, Phase 2 Modified CZP Date Prepared: 3/26/2025

Additional information is provided for cells with a red triangle in the upper right corner. Place the cursor over the cell. Text shown in blue indicate location of instructions in the Technical Guidance Manual - RG-348. Characters shown in red are data entry fields.

Characters shown in black (Bold) are calculated fields. Changes to these fields will remove the equations used in the spreadsheet.

1. The Required Load Reduction for the total project:	Calculations from RG-	-348	Pages 3-27 to 3-30		
Page 3-29 Equation 3.3: L_{M} =	27.2(A _N x P)				
where: $\begin{tabular}{lllllllllllllllllllllllllllllllllll$	Required TSS remova Net increase in imperv Average annual precip	Il resulting from vious area for the pitation, inches	n the proposed development = 80% of he project	f increased load	
Site Data: Determine Required Load Removal Based on the Entire Project					
County =	Williamson				
Predevelopment impervious area within the limits of the plan * =	0.00	acres			
Total post-development impervious area within the limits of the plan * =	63.15	acres			
Total post-development impervious cover fraction * =	0.52	inches			
		inones			
L _{M TOTAL PROJECT} = * The values entered in these fields should be for the total project area.	54,966	lbs.			
Number of drainage basins / outfalls areas leaving the plan area =	5				
2. Drainage Basin Parameters (This information should be provided for eac	:h basin):				
Drainage Basin/Outfall Area No. =	VFS F	Ultimate C	Condition		
Predevelopment impervious area within drainage basin/outfall area =	0.00	acres			
Post-development impervious area within drainage basin/outfall area =	2.12	acres			
Post-development impervious fraction within drainage basin/outfall area =	0.55	lba			
LM THIS BASIN -	1,040	103.			
3. Indicate the proposed BMP Code for this basin.					
Proposed BMP = Removal efficiency =	Vegetative Filter Stri 85	ps percent	MANUALLY ADJUSTED		
4. Calculate Maximum TSS Load Removed (L_{R}) for this Drainage Basin by t	he selected BMP Type).			
RG-348 Page 3-33 Equation 3.7: Las	(BMP efficiency) x P x	(A. x 34 6 + A	- x 0 54)		
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
where: A _C =	 Total On-Site drainage 	e area in the Bl	MP catchment area		
	Pervious area remaini	ng in the BMP	catchment area		
L _R =	nent area by the proposed BMP				
A -	2.96	00700			
	2.12	acres			
A _P =	1.74	acres			
L _R =	2,021	lbs			
5. Calculate Fraction of Annual Runoff to Treat the drainage basin / outfall a	area				
	1.845	lbs.			
	0.01				
r-	0.91				
6. Calculate Capture Volume required by the BMP Type for this drainage ba	<u>asin / outfall area.</u>		Calculations from RG-348	Pages 3-34 to 3-36	
Rainfall Depth =	1.80	inches			
Post Development Runoff Coefficient =	0.39				
On-site Water Quality Volume =	9742	cubic feet			
	Calculations from RG-	-348	Pages 3-36 to 3-37		
Off-site area draining to BMP =	0.00	acres			
Off-site Impervious cover draining to BMP =	0.00	acres			
Impervious fraction of off-site area = Off-site Runoff Coefficient =	0 0.00				
Off-site Water Quality Volume =	0	cubic feet			
Storage for Padiment -	1010				
Total Capture Volume (required water quality volume(s) x 1.20) =	11690	cubic feet			

PROPERTY METES & BOUNDS



FIELD NOTES FOR

A 120.620 ACRE TRACT OF LAND SITUATED IN THE GREENLEAF FISK SURVEY, ABSTRACT NO. 5, AND THE BARTHOLOMEW MANLOVE SURVEY, ABSTRACT NO. 420 IN WILLIAMSON COUNTY, TEXAS, BEING OUT OF THE REMNANT PORTION OF A CALLED 437.04 ACRE TRACT CONVEYED TO HWY 29 VENTURES 2015, L.P. RECORDED IN DOCUMENT NO. 2015088162, AND BEING OUT OF LIVELY TRACT PHASE 2, A SUBDIVISION ACCORDING TO THE PLAT RECORDED IN DOCUMENT NO 2020134123 AND BEING OUT OF LIVELY TRACT PHASE 4, A SUBDIVISION ACCORDING TO THE PLAT RECORDED IN DOCUMENT NO 2023099454, ALL OF THE OFFICIAL PUBLIC RECORDS OF WILLIAMSON COUNTY, TEXAS. SAID 120.620 ACRE TRACT BEING MORE FULLY DESCRIBED AS FOLLOWS, WITH BEARINGS BASED ON THE NORTH AMERICAN DATUM OF 1983 (NA 2011) EPOCH 2010.00, FROM THE TEXAS COORDINATE SYSTEM ESTABLISHED FOR THE CENTRAL ZONE:

BEGINNING at a ½" iron rod with yellow cap marked "Pape-Dawson" found on a point in the southwest corner of a called 491.95 acre tract, conveyed to Henry B. Tippie , recorded in Volume 570, Page 483 of the Deed Records of Williamson County, Texas, said point being the north boundary line of a called 5.00 acre tract, conveyed to SFSG, recorded in Document No. 2017001815 of the Official Public Records of Williamson County, Texas, same being the southeast corner of said Lively Tract, Phase 4 for the southeast corner and **POINT OF BEGINNING** hereof;

THENCE S 69°12'32" **W**, departing the west boundary line of said 491.95 acre tract, with the north boundary line of said 5.00 acre tract, same being the south boundary line of said Lively Tract, Phase 4, a distance of **278.63 feet** to a calculated point on the southeast corner of said Remnant Portion of said 437.04 acre tract, same being a southwest corner of said Lively Tract, Phase 4 for an angle point hereof;

THENCE N 45°57'26" W, departing the north boundary line of said 5.00 acre tract, with the west boundary line of said Lively Tract, Phase 4, same being the east boundary line of said Remnant Portion, a distance of 278.63 feet to a calculated point hereof,

THENCE, departing the west boundary line of said Lively Tract, Phase 4, though the interior of said Remnant Portion, the following fourteen (14) courses and distances:

- 1. S 50°33'25" W, a distance of 78.70 feet to a calculated angle point hereof,
- 2. S 55°16'14" W, a distance of 62.77 feet to a calculated angle point hereof,
- 3. S 61°22'08" W, a distance of 62.77 feet to a calculated angle point hereof,
- 4. S 67°26'24" W, a distance of 62.27 feet to a calculated angle point hereof,
- 5. S 70°17'29" W, a distance of 400.00 feet to a calculated angle point hereof,
- 6. S 70°16'43" W, a distance of 52.13 feet to a calculated angle point hereof,
- 7. S 74°31'06" W, a distance of 63.48 feet to a calculated angle point hereof,

- 8. S 80°57'34" W, a distance of 63.48 feet to a calculated angle point hereof,
- 9. S 87°24'02" W, a distance of 63.48 feet to a calculated angle point hereof,
- 10. N 86°09'30" W, a distance of 63.48 feet to a calculated angle point hereof,
- 11. N 79°43'02" W, a distance of 63.48 feet to a calculated angle point hereof,
- 12. N 73°16'34" W, a distance of 63.48 feet to a calculated angle point hereof,
- 13. N 66°50'06" W, a distance of 63.48 feet to a calculated angle point hereof, and
- 14. N 59°10'41" W, a distance of 112.58 feet to a calculated angle point on a southeast boundary line of said Lively Tract, Phase 4, same being a northwest boundary line of said Remnant Portion hereof,

THENCE S 32°24'37" W, with the southeast boundary line of said Lively Tract, Phase 4, same being a northwest boundary line of said Remnant Portion, a distance of **155.78 feet** to a ½" iron rod with yellow cap marked "Pape-Dawson" found on a southwest corner of said Lively Tract, Phase 4, same being an interior corner of said Remnant Portion for the southwest corner hereof,

THENCE, with the west boundary line of said Lively Tract, Phase 4, same being the east boundary line of said Remnant Portion, the following nine (9) courses and distances:

- N 57°35'23" W, a distance of 155.00 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof,
- N 32°24'37" E, a distance of 171.62 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof,
- N 51°36'14" W, a distance of 89.36 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof,
- 4. N 32°58'12" W, a distance of 111.62 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof,
- N 23°41'17" W, a distance of 76.24 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof,
- N 15°35'33" W, a distance of 76.24 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof,
- N 07°29'49" W, a distance of 76.24 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof,

- 8. N 00°35'55" E, a distance of 76.24 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof, and
- N 08°41'39" E, a distance of 76.24 feet to a ½" iron rod with yellow cap marked "Pape-Dawson" found hereof,

THENCE N 16°51'35" E, continuing with the west boundary line of said Lively Tract Phase 4, same being the east boundary line of said Remnant Portion, in part, through the interior of said Lively Tract, Phase 4, a distance of **78.29 feet** to a calculated point hereof;

THENCE, continuing through the interior of said Lively Tract, Phase 4, the following thirty seven (37) courses and distances:

- 1. N 21°51'38" E, a distance of 250.00 feet to a calculated angle point hereof,
- 2. S 68°08'22" E, a distance of 10.00 feet to a calculated angle point hereof,
- 3. N 21°51'38" E, a distance of 60.00 feet to a calculated angle point hereof,
- 4. N 17°36'40" E, a distance of 56.12 feet to a calculated angle point hereof,
- 5. N 08°18'18" E, a distance of 55.95 feet to a calculated angle point hereof,
- 6. N 01°43'06" E, a distance of 23.31 feet to a calculated angle point hereof,
- 7. N 04°52'06" W, a distance of 55.95 feet to a calculated angle point hereof,

8. N 14°10'12" W, a distance of 55.95 feet to a calculated angle point hereof,

9. N 18°53'55" W, a distance of 59.97 feet to a calculated angle point hereof,

10. N 18°53'56" W, a distance of 60.00 feet to a calculated angle point hereof,

11. N 17°42'47" W, a distance of 66.82 feet to a calculated angle point hereof,

12. N 12°02'54" W, a distance of 71.45 feet to a calculated angle point hereof,

13. N 05°59'26" W, a distance of 69.13 feet to a calculated angle point hereof,

14. N 03°56'14" W, a distance of 60.00 feet to a calculated angle point hereof,

15. S 73°13'52" W, a distance of 61.54 feet to a calculated angle point hereof,

16. S 85°51'39" W, a distance of 60.00 feet to a calculated angle point hereof,

17. N 89°44'52" W, a distance of 114.82 feet to a calculated angle point hereof, 18. S 73°29'12" W, a distance of 21.51 feet to a calculated angle point hereof, 19. N 54°00'12" W, a distance of 91.03 feet to a calculated angle point hereof, 20. N 10°26'39" W, a distance of 87.91 feet to a calculated angle point hereof, 21. N 03°16'40" E, a distance of 66.45 feet to a calculated angle point hereof, 22. N 01°08'18" W, a distance of 180.21 feet to a calculated angle point hereof, 23. N 15°24'04" W, a distance of 64.24 feet to a calculated angle point hereof, N 07°42'00" E, a distance of 75.11 feet to a calculated angle point hereof, 25. N 11°14'57" E, a distance of 77.12 feet to a calculated angle point hereof, 26. N 19°37'23" E, a distance of 77.25 feet to a calculated angle point hereof, 27. N 39°56'54" E, a distance of 16.69 feet to a calculated angle point hereof, 28. N 27°32'01" E, a distance of 64.66 feet to a calculated angle point hereof, 29. N 37°22'05" E, a distance of 79.71 feet to a calculated angle point hereof, 30. N 47°12'08" E, a distance of 79.71 feet to a calculated angle point hereof, N 55°50'07" E, a distance of 70.28 feet to a calculated angle point hereof, 32. N 57°30'57" E, a distance of 45.86 feet to a calculated angle point hereof, N 09°12'52" E, a distance of 101.37 feet to a calculated angle point hereof, 34. N 16°38'35" E, a distance of 36.19 feet to a calculated angle point hereof, 35. N 18°54'15" E, a distance of 43.66 feet to a calculated angle point hereof, 36. N 17°33'41" E, a distance of 67.52 feet to a calculated angle point hereof, and

37. N 15°38'35" E, a distance of 19.86 feet to a calculated point on the west boundary line of said Livey Tract, Phase 2, same being the east boundary line of said Lively Tract, Phase 4 for an angle point hereof,

0.154 Acre Tract Job No. 51132-03 Page 5 of 7

THENCE, with the west boundary line of said Livey Tract, Phase 2, same being the east boundary line of said Lively Tract, Phase 4, the following two (2) courses and distances:

- 1. N 33°14'57" W, a distance of 109.77 feet to a calculated point of tangent curvature hereof, and
- along a curve to the left, having a radius of 25.00 feet, a central angle of 26°33'54", a chord bearing and distance of N 46°31'54" W, 11.49 feet, an arc length of 11.59 feet to a calculated point of tangency hereof,

THENCE, departing the east boundary line of said Livey Tract, Phase 4, though the interior of said Lively Tract, Phase 2, the following twenty five (25) courses and distances:

- 1. N 08°29'38" E, a distance of 52.03 feet to a calculated point of non-tangent curvature hereof,
- along the arc of a curve to the left having a radius of 831.85 feet, a central angle of 04°39'42", a chord bearing and distance of N 28°05'47" W, 67.66 feet, an arc length of 67.68 feet to a calculated point of non-tangency hereof,
- 3. N 61°52'45" E, a distance of 32.00 feet to a calculated angle point hereof,
- 4. N 17°08'05" E, a distance of 122.55 feet to a calculated angle point hereof,
- 5. N 01°53'16" E, a distance of 80.00 feet to a calculated angle point hereof,
- 6. S 84°27'52" E, a distance of 31.81 feet to a calculated angle point hereof,
- 7. N 21°37'01" E, a distance of 25.54 feet to a calculated angle point hereof,
- 8. S 75°26'30" E, a distance of 93.16 feet to a calculated angle point hereof,
- 9. N 15°09'32" E, a distance of 155.00 feet to a calculated angle point hereof,
- 10. N 74°50'28" W, a distance of 20.00 feet to a calculated angle point hereof,
- 11. N 08°18'41" E, a distance of 50.42 feet to a calculated angle point hereof,
- 12. N 19°33'44" E, a distance of 69.08 feet to a calculated angle point hereof,
- 13. S 55°56'56" E, a distance of 32.65 feet to a calculated angle point hereof,
- 14. S 76°26'18" E, a distance of 65.24 feet to a calculated angle point hereof,
- 15. S 81°43'15" E, a distance of 84.39 feet to a calculated angle point hereof,
- 16. S 83°56'33" E, a distance of 71.54 feet to a calculated angle point hereof,

- 17. S 88°19'26" E, a distance of 97.45 feet to a calculated angle point hereof,
- 18. S 82°12'05" E, a distance of 67.13 feet to a calculated angle point hereof,
- 19. S 72°20'21" E, a distance of 45.47 feet to a calculated angle point hereof,
- 20. N 88°55'16" E, a distance of 94.32 feet to a calculated angle point hereof,
- 21. N 58°06'50" E, a distance of 38.18 feet to a calculated angle point hereof,
- 22. N 25°20'36" E, a distance of 35.94 feet to a calculated angle point hereof,
- 23. N 15°06'53" E, a distance of 52.85 feet to a calculated angle point hereof,
- 24. N 00°08'30" W, a distance of 54.08 feet to a calculated angle point hereof, and
- 25. N 11°27'13" W, a distance of 0.42 feet to a calculated point on the west boundary line of said 491.95 acre tract, same being the east boundary line of said Lively Tract, Phase 2 for the northeast corner hereof,

THENCE, with the west boundary line of said 491.95 acre tract, same being the east boundary line of said Lively Tract, Phase 2, the following

- 1. S 21°49'53" E, a distance of 469.33 feet to a calculated angle point hereof,
- 2. S 21°36'00" E, a distance of 253.35 feet to a calculated angle point hereof,
- 3. S 21°35'17" E, a distance of 184.35 feet to a calculated angle point hereof,
- 4. S 21°23'05" E, a distance of 117.63 feet to a calculated angle point hereof,
- 5. S 21°23'05" E, a distance of 545.06 feet to a calculated angle point hereof,
- 6. S 21°27'49" E, a distance of 804.43 feet to a calculated angle point hereof,
- 7. S 21°22'30" E, a distance of 229.85 feet to a calculated angle point hereof,
- 8. S 21°21'35" E, a distance of 259.16 feet to a calculated angle point hereof,
- 9. S 20°46'39" E, a distance of 134.61 feet to a calculated angle point hereof,
- 10. S 21°02'38" E, a distance of 137.67 feet to a calculated angle point hereof,
- 11. S 20°59'40" E, a distance of 200.44 feet to a calculated angle point hereof,

0.154 Acre Tract Job No. 51132-03 Page 7 of 7

- 12. S 09°27'57" E, a distance of 103.90 feet to a calculated angle point hereof, and
- 13. S 21°00'01" E, a distance of 141.14 feet to the POINT OF BEGINNING and containing 120.620 acres in Williamson County, Texas. Said tract being described in accordance with a survey made on the ground and a map prepared under Job No. 50816-25 by Pape Dawson Consulting Engineers, LLC.

PREPARED BY:Pape-Dawson Consulting Engineers, LLC.DATE:April 9, 2025JOB No.:50816-26DOC.ID.:H:\Survey\CIVIL\50816-26\Exhibits\Word\FN-50816-26_CZP_120.620Ac.docxTBPE Firm Registration #470TBPLS Firm Registration #100288-01

Porking. S. 08/2025



Date: Apr 09, 2025, 12:17pm User ID: DRodriguez File: \\pape-dawson.com\ous-pd\Survey\CIVIL\50516-25\Exhibits\EX50516-28...120.6Ac.dwg



Date: Apr 09, 2025, 12:17pm User ID: DRodriguez File: \\paps-dawson.com\aus-pd\Survey\ClVIL\50816-26\Exhibits\EX50816-26...120.6Ac.dwg



Date: Apr 09, 2025, 12:17pm User (D: DRodriguez File: \\pape-dawson.com\aus-pd\Survey\ClVL\50518-28\Exhibits\Ex50818-28_120.8Ac.dwg

-															
		LINE TABLE LINE TAB			LINE TABLE		LINE TABLE					LINE TABLE			CZP EXHIBIT OF
	LINE	BEARING	LENGTH	LIN	E BEARING	LENGTH		LINE	BEARING	LENGTH		LINE	BEARING	LENGTH	A 120,620 ACRE TRACT OF LAND SITUATED IN
	L1	S69'12'32"W	471.11'	L2	N16"51'35"E	78.29'		L53	N19"37'23"E	77.25'		L79	S81*43'15"E	84.39'	THE GREENLEAF FISK SURVEY, ABSTRACT NO. 5,
	L2	N45*57'26"W	278.63'	L2	8 N21*51'38"E	250.00'		L54	N39*56'54"E	16.69'		L80	S83'56'33"E	71.54'	ABSTRACT NO. 420 IN WILLIAMSON COUNTY,
	L3	S50*33'25"W	78.70'	L2	9 S68'08'22"E	10.00'		L55	N27'32'01"E	64.66'		L81	S88"19'26"E	97.45'	A CALLED 437.04 ACRE TRACT CONVEYED TO
	L4	S5516'14"W	62.77'	L3	N21"51'38"E	60.00'		L56	N37°22'05"E	79.71'		L82	S82"12'05"E	67.13'	DOCUMENT NO. 2015088162, AND BEING OUT OF
	L5	S61*22'08"W	62.77'	L3	N17°36'40"E	56.12'		L57	N47"12'08"E	79.71'		L83	S72*20'21"E	45.47'	LIVELY TRACT PHASE 2, A SUBDIVISION ACCORDING TO THE PLAT RECORDED IN
	L6	S67*26'24"W	62.27'	L3	2 N08"18'18"E	55.95'		L58	N55*50'07"E	70.28'		L84	N88*55'16"E	94.32'	DOCUMENT NO 2020134123 AND BEING OUT OF LIVELY TRACT PHASE 4, A SUBDIVISION
	L7	S70'17'29"W	400.00'	L3	3 N01*43'06"E	23.31'		L59	N57'30'57"E	45.86'		L85	N58*06'50"E	38.18'	ACCORDING TO THE PLAT RECORDED IN DOCUMENT NO 2023099454, ALL OF THE OFFICIAL
ļ.	L8	S70"16'43"W	52.13'	L3	N04'52'06"W	55.95'		L60	N09"12'52"E	101.37'		L86	N25"20"36"E	35.94'	PUBLIC RECORDS OF WILLIAMSON COUNTY, TEXAS.
	L9	S74'31'06"W	63.48'	L3	5 N14"10'12"W	55.95'		L61	N16'38'35"E	36.19'		L87	N15"06'53"E	52.85'	NOTES:
	L10	S80*57'34"W	63.48'	L3	6 N18*53'55"W	59.97'		L62	N18*54'15"E	43.66'	1	L88	N00"08'30"W	54.08'	1. THE PROFESSIONAL SERVICES PROVIDED HEREWITH INCLUDE THE PREPARATION OF A
	L11	S87*24'02"W	63.48'	L3	7 N18*53'56"W	60.00'		L63	N17'33'41"E	67.52'		L89	N11*27'13"W	0.42'	FIELD NOTE DESCRIPTION. 2. THE BEARINGS ARE BASED ON THE NORTH
	L12	N86°09'30"W	63.48'	L3	3 N17*42'47"W	66.82'		L64	N15'38'35"E	19.86'		L90	S21*49'53"E	469.33'	AMERICAN DATUM OF 1983 (NA 2011) EPOCH
	L13	N79*43'02"W	63.48'	L3	9 N12'02'54"W	71.45'		L65	N3314'57"W	109.77'		L91	S21"36'00"E	253.35'	SYSTEM ESTABLISHED FOR THE CENTRAL
	L14	N73"16'34"W	63.48'	L4	N05*59'26"W	69.13'		L66	N08'29'38"E	52.03'	1	L92	S21°35'17"E	184.35'	3. ADJOINERS ARE FOR INFORMATIONAL USE
	L15	N66*50'06"W	63.48'	L4	1 N03"56'14"W	60.00'	1	L67	N61"52'45"E	32.00'	1	L93	S21"23'05"E	117.63'	UNET.
	L16	N59"10'41"W	112.58'	L4	2 S73°13'52"W	61.54'	1	L68	N17'08'05"E	122.55'	1	L94	S21*23'05"E	545.06'	
	L17	S32*24'37"W	155.78'	L4	3 S85'51'39"W	60.00'		L69	N01*53'16"E	80.00'	1	L95	S21*27'49"E	804.43'	
ł	L18	N57"35'23"W	155.00'	L4	4 N89*44'52"W	114.82'	1	L70	S84*27'52"E	31.81'	1	L96	S21"22'30"E	229.85'	AN
	L19	N32"24'37"E	171.62'	L4	5 S73*29'12"W	21.51'		L71	N21°37'01"E	25.54'		L97	S21°21'35"E	259.16'	KE OF TEL
	L20	N51*36'14"W	89.36'	L4	6 N54'00'12"W	91.03'	1	L72	S75*26'30"E	93.16'	1	L98	S20'46'39"E	134.61'	
	L21	N32*58'12"W	111.62'	L4	7 N10°26'39"W	87.91'	1	L73	N15'09'32"E	155.00'	1	L99	S21"02'38"E	137.67'	PARKER GRAHAM
	L22	N23°41'17"W	76.24'	L4	B N03"16'40"E	66.45'	1	L74	N74*50'28"W	20.00'		L100	S20'59'40"E	200.44'	5556 556
	L23	N15'35'33"W	76.24'	L4	9 N01'08'18"W	180.21'		L75	N08"18'41"E	50.42'		L101	S09*27'57"E	103.90'	TTO FESSION
	L24	N07*29'49"W	76.24'	L5	N15*24'04"W	64.24'		L76	N19"33'44"E	69.08'		L102	S21'00'01"E	141.14'	SURVICE
	L25	N00"35'55"E	76.24'	L5	1 N07*42'00"E	75.11'		L77	S55*56'56"E	32.65'					05/08/2025
	L26	N08*41'39"E	76.24'	L5	2 N11"14'57"E	77.12'		L78	S76'26'18"E	65.24'	1				farken deal in

AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10801 N MOPAC EXPY, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711 TBPE FIRM REGISTRATION #470 1 TBPLS FIRM REGISTRATION #10028801

CURVE RADIUS DELTA CHORD BEARING CHORD 26'33'54" C1 25.00' N46"31'54"W C2 831.85' 4'39'42" N28'05'47"W

CURVE TABLE

APRIL 09, 2025

11.49'

67.66'

LENGTH

11.59'

67.68'

SHEET 4 OF 4 JOB No.:50816-25

Date: Apr 09, 2025, 12:18pm User ID: DRodriguez File: \\pape-dawson.com\aus-pd\Survey\ClVIL\50818-28\Exhibits\EX50816-26_120.6Ac.dwg

ATTACHMENT D

ATTACHMENT D – FACTORS AFFECTING SURFACE WATER QUALITY

Potential sources of pollution that may reasonably be expected to affect the quality of stormwater discharges from the construction site include:

- Soil erosion due to the clearing of the site for roads, residential homes, and drainage structures.
- Oil, grease, fuel, and hydraulic fluid contamination from construction equipment and vehicle drippings.
- Hydrocarbons from asphalt paving operations.
- Miscellaneous trash and litter from construction workers and material wrappings.
- Construction debris.
- Concrete truck washout.
- Potential overflow/spills from portable toilets

Potential sources of pollution that may reasonably be expected to affect the quality of stormwater discharges from the site after development include:

- Oil, grease, fuel and hydraulic fluid contamination from vehicle drippings;
- Dirt and dust which may fall off vehicles; and
- Miscellaneous trash and litter.



ATTACHMENT E

ATTACHMENT E- VOLUME AND CHARACTER OF STORMWATER

Stormwater runoff will increase as a result of this development. All stormwater runoff generated on-site will be routed through one of the on-site water quality ponds. Peak flows going into Basin H after the development of Phases 2, 4, 5, and 6 in the ultimate condition will be 482.40 cfs for the 100 yr scenario and 337.79 cfs for the 25 year scenario. The curve number for the Pond H basin changes from approximately 80.00 pre-development to 81.43 after ultimate development. Peak flows going into Basin J after development of Phases 2, 4, 5, and 6 in the ultimate condition will be 193.01 cfs and 136.06 for the 100 yr and 25 yr scenarios. The curve number for the Pond J basin changes from approximately 61.00 pre-development to 82.97 after ultimate development. Values are based on the Rational Method using runoff coefficients per the City of Austin Drainage Criteria Manual. Stormwater runoff from the development can be characterized as overland, shallow-concentrated, and channelized flow from the proposed single-family subdivision.



ATTACHMENT J

ATTACHMENT J – BMP'S FOR UPGRADIENT STORMWATER

There is minimal amount of upgradient stormwater passing through the site, as the site is bordered to the north by Lively Tract Phase 1 which diverts upstream flows by means of curb inlets running along either side of the roadway. Upgradient stormwater that does pass through the site will be collected by the proposed curb inlets and conveyed via the proposed storm drain system into the proposed permanent BMP's. The permanent BMP's have been designed to accommodate these upgradient flows. For more information on upgradient stormwater, see the Proposed Drainage Area Map located within the plan set provided with this application.

Construction of two (2) batch detention ponds and installation of three (3) fifteen-foot (15') wide Engineered Vegetative Filter Strips (VFS) are proposed as the Permanent Best Management Practices (PBMP's) for this development. All PBMP's have been designed in accordance with the Texas Commistion on Environmental Quality's (TCEQ) Technical Guidance Manual (TGM) RG-348 (2005) to remove 80% of the increase in Total Suspended Solids (TSS) from the site.



ATTACHMENT K

ATTACHMENT K – BMP'S FOR ON-SITE STORMWATER

Construction of two (2) batch detention ponds and installation of three (3) fifteen-foot (15') wide Engineered Vegetative Filter Strips (VFS) are proposed as the Permanent Best Management Practices (PBMPs) for this development. All PBMPs have been designed in accordance with the Texas Commission on Environmental Quality's (TCEQ) Technical Guidance Manual (TGM) RG-348 (2005) to remove 80% of the increase in Total Suspended Solids (TSS) from the site. Detailed design and construction drawings for the PBMP's can be found in the plan set provided with the application.



ATTACHMENT L

ATTACHMENT L – BMP'S FOR SURFACE STREAMS

Construction of two (2) batch detention ponds and installation of three (3) fifteen-foot (15') wide Engineered Vegetative Filter Strips (VFS) are proposed as the Permanent Best Management Practices (PBMPs) for this development. All PBMPs have been designed in accordance with the Texas Commission on Environmental Quality's (TCEQ) Technical Guidance Manual (TGM) RG-348 (2005) to remove 80% of the increase in Total Suspended Solids (TSS) from the site. Runoff from impervious cover areas will be treated by the proposed water quality basins and VFS prior to discharge downstream and eventually into the South Fork San Gabriel River.

ATTACHMENT M

ATTACHMENT M – CONSTRUCTION PLANS

See attached drawing set for relevant construction plans and design drawings for Lively Phase 2, 4, 5, & 6.

ATTACHMENT N

ATTACHMENT N - MAINTENANCE PROCEDURES FOR PERMANENT BMPs

Note: Additional guidance can be obtained from TCEQ's Technical Guidance Manual (TGM) RG-348 (2005) Section 3.5.

A written record will be kept of inspection results and maintenance performed.

3.5.8 Vegetative Filter Strips

Once a vegetated area is well established, little additional maintenance is generally necessary. The key to establishing a viable vegetated feature is the care and maintenance it received in the first few months after it is planted. Once established, all vegetated BMPs require some basic maintenance to insure the health of the plants including:

- <u>Pest Management.</u> An Integrated Pest Management (IPM) Plan should be developed for vegetated areas. This plan should specify how problem insects and weeds will be controlled with minimal or no use of insecticides and herbicides.
- <u>Seasonal Mowing and Lawn Care.</u> If the filter strip is made up of turf grass, it should be mowed as needed to limit vegetation height to 18 inches, using a mulching mower (or removal of clippings). If native grasses are used, the filter may require less frequent mowing, but a minimum of twice annually. Grass clippings and brush debris should not be deposited on vegetated filter strip areas. Regular mowing should also include weed control practices, however herbicide use should be kept to a minimum (Urbonas et al., 1992). Healthy grass can be maintained without using fertilizers because runoff usually contains sufficient nutrients. Irrigation of the site can help assure a dense and healthy vegetative cover.
- <u>Inspection</u>. Inspect filter strips at least twice annually for erosion or damage to vegetation; however, additional inspection after periods of heavy runoff is most desirable. The strip should be checked for uniformity of grass cover, debris and litter, and areas of sediment accumulation. More frequent inspections of the grass cover during the first few years after establishment will help to determine if any problems are developing, and to plan for long-term restorative maintenance needs. Bare spots and areas of erosion identified during semi-annual inspections must be replanted and restored to meet specifications. Construction of a level spreader device may be necessary to reestablish shallow overland flow.
- <u>Debris and Litter Removal.</u> Trash tends to accumulate in vegetated areas, particularly along highways. Any filter strip structures (i.e. level spreaders) should be kept free of obstructions to reduce floatables being flushed downstream, and for aesthetic reasons. The need for this practice is determined through periodic inspection, but should be performed no less than 4 times per year.



- <u>Sediment Removal.</u> Sediment removal is not normally required in filter strips, since the
 vegetation normally grows through it and binds it to the soil. However, sediment may
 accumulate along the upstream boundary of the strip preventing uniform overland flow. Excess
 sediment should be removed by hand or with flat-bottomed shovels.
- <u>Grass Reseeding and Mulching.</u> A healthy dense grass should be maintained on the filter strip. If areas are eroded, they should be filled, compacted, and reseeded so that the final grad is level. Grass damaged during the sediment removal process should be promptly replaced using the same seed mix used during filter strip establishment. If possible, flow should be diverted from the damaged areas until the grass is firmly established. Bare spots and areas of erosion identified during semi-annual inspections must be replanted and restored to need specifications. Corrective maintenance, such as weeding or replanting should be done more frequently in the first two to three years after installation to ensure stabilization. Dense vegetation may require irrigation immediately after planting, and during particularly dry periods, particularly as the vegetation is initially established.

3.5.20 Batch Detention Basin

Batch detention basins may have somewhat higher maintenance requirements than an extended detention basin since they are active stormwater controls. The maintenance activities are identical to those of extended detention basins with the addition of maintenance and inspections of the automatic controller and the valve at the outlet.

- Inspections. Inspections should take place a minimum of twice a year. One inspection should take place during wet weather to determine if the basin is meeting the target detention time of 12 hours and a drawdown time of no more than 48 hours. The remaining inspections should occur between storm events so that manual operation of the valve and controller can be verified. The level sensor in the basin should be inspected and any debris or sediment in the area should be removed. The outlet structure and the trash screen should be inspected for signs of clogging. Debris and sediment should be removed from the orifice and outlet(s) as described in previous sections. Debris obstructing the valve should be removed. During each inspection, erosion areas inside and downstream of this BMP should be identified and repaired/revegetated immediately.
- Mowing. The basin, basin side-slopes, and embankment of the basin must be mowed to
 prevent woody growth and control weeds. A mulching mower should be used, or the
 grass clippings should be caught and removed. Mowing should take place at least twice
 a year, or more frequently if vegetation exceeds 18 inches in height. More frequent
 mowing to maintain aesthetic appeal may be necessary in landscaped areas.



- Litter and Debris Removal. Litter and debris removal should take place at least twice a year, as part of the periodic mowing operations and inspections. Debris and litter should be removed from the surface of the basin. Particular attention should be paid to floatable debris around the outlet structure. The outlet should be checked for possible clogging or obstructions and any debris removed.
- *Erosion control.* The basin side slopes and embankment all may periodically suffer from slumping and erosion. To correct these problems, corrective action, such as regrading and revegetation, may be necessary. Correction of erosion control should take place whenever required based on the periodic inspections.
- Nuisance Control. Standing water or soggy conditions may occur in the basin. Some standing water may occur after a storm event since the valve may close with 2 to 3 inches of water in the basin. Some flow into the basin may also occur between storms due to spring flow and residential water use that enters the storm sewer system. Twice a year, the facility should be evaluated in terms of nuisance control (insects, weeds, odors, algae, etc.).
- Structural Repairs and Replacement. With each inspection, any damage to structural elements of the basin (pipes, concrete drainage structures, retaining walls, etc.) should be identified and repaired immediately. An example of this type of repair can include patching of cracked concrete, sealing of voids, removal of vegetation from cracks and joints. The various inlet/outlet structures in a basin will eventually deteriorate and must be replaced.
- Sediment Removal. A properly designed batch detention basin will accumulate quantities of
 sediment over time. The accumulated sediment can detract from the appearance of the facility
 and reduce the pollutant removal performance of the facility. The sediment also tends to
 accumulate near the outlet structure and can interfere with the level sensor operation.
 Sediment shall be removed from the basin at least every 5 years, when sediment depth exceeds
 6 inches, when the sediment interferes with the level sensor or when the basin does not drain
 within 48 hours. Care should be taken not to compromise the basin lining during maintenance.
- Logic Controller. The Logic Controller should be inspected as part of the twice yearly
 investigations. Verify that the external indicators (active, cycle in progress) are operating
 properly by turning the controller off and on, and by initiating a cycle by triggering the level
 sensor in the basin. The valve should be manually opened and closed using the open/close
 switch to verify valve operation and to assist in inspecting the valve for debris. The solar panel
 should be inspected and any dust or debris on the panel should be carefully removed. The
 controller and all other circuitry and wiring should be inspected for signs of corrosion, damage



from insects, water leaks, or other damage. At the end of the inspection, the controller should be reset.

Signature

3/27/24 Date

Tom Rielly, President Hwy 29 Ventures 2015 LP



ATTACHMENT P

ATTACHMENT P – MEASURES FOR MINIMIZING SURFACE STREAM CONTAMINATION

Where erosive velocities exist at drain discharge points, energy dissipators will be constructed to reduce the potential for erosion. These include mortared rock riprap and concrete headwalls with velocity dissipating devices.


TEMPORARY STORMWATER

Temporary Stormwater Section

Texas Commission on Environmental Quality

for Regulated Activities on the Edwards Aquifer Recharge Zone and Relating to 30 TAC §213.5(b)(4)(A), (B), (D)(I) and (G); Effective June 1, 1999

To ensure that the application is administratively complete, confirm that all fields in the form are complete, verify that all requested information is provided, consistently reference the same site and contact person in all forms in the application, and ensure forms are signed by the appropriate party.

Note: Including all the information requested in the form and attachments contributes to more streamlined technical reviews.

Signature

To the best of my knowledge, the responses to this form accurately reflect all information requested concerning the proposed regulated activities and methods to protect the Edwards Aquifer. This **Temporary Stormwater Section** is hereby submitted for TCEQ review and executive director approval. The application was prepared by:

Print Name of Customer/Agent: Dustin Goss, P.E., LEED * AP

Date: 4/2/25

Signature of Customer/Agent:

Regulated Entity Name: Lively Tract, Phase 2

Project Information

Potential Sources of Contamination

Examples: Fuel storage and use, chemical storage and use, use of asphaltic products, construction vehicles tracking onto public roads, and existing solid waste.

 Fuels for construction equipment and hazardous substances which will be used during construction:

The following fuels and/or hazardous substances will be stored on the site: <u>Diesel Fuel</u>, <u>Gasoline</u>, <u>Etc.</u>

These fuels and/or hazardous substances will be stored in:

Aboveground storage tanks with a cumulative storage capacity of less than 250 gallons will be stored on the site for less than one (1) year.

TCEQ-0602 (Rev. 02-11-15)

Aboveground storage tanks with a cumulative storage capacity between 250 gallons and 499 gallons will be stored on the site for less than one (1) year.
 Aboveground storage tanks with a cumulative storage capacity of 500 gallons or more will be stored on the site. An Aboveground Storage Tank Facility Plan application must be submitted to the appropriate regional office of the TCEQ prior to moving the tanks onto the project.

- Fuels and hazardous substances will not be stored on the site.
- 2. Attachment A Spill Response Actions. A site specific description of the measures to be taken to contain any spill of hydrocarbons or hazardous substances is attached.
- 3. Temporary aboveground storage tank systems of 250 gallons or more cumulative storage capacity must be located a minimum horizontal distance of 150 feet from any domestic, industrial, irrigation, or public water supply well, or other sensitive feature.
- 4. Attachment B Potential Sources of Contamination. A description of any activities or processes which may be a potential source of contamination affecting surface water quality is attached.

Sequence of Construction

5. Attachment C - Sequence of Major Activities. A description of the sequence of major activities which will disturb soils for major portions of the site (grubbing, excavation, grading, utilities, and infrastructure installation) is attached.

For each activity described, an estimate (in acres) of the total area of the site to be disturbed by each activity is given.

For each activity described, include a description of appropriate temporary control measures and the general timing (or sequence) during the construction process that the measures will be implemented.

6. Name the receiving water(s) at or near the site which will be disturbed or which will receive discharges from disturbed areas of the project: <u>South Fork San Gabriel River</u>

Temporary Best Management Practices (TBMPs)

Erosion control examples: tree protection, interceptor swales, level spreaders, outlet stabilization, blankets or matting, mulch, and sod. Sediment control examples: stabilized construction exit, silt fence, filter dikes, rock berms, buffer strips, sediment traps, and sediment basins. Please refer to the Technical Guidance Manual for guidelines and specifications. All structural BMPs must be shown on the site plan.

7. X Attachment D – Temporary Best Management Practices and Measures. TBMPs and measures will prevent pollution of surface water, groundwater, and stormwater. The construction-phase BMPs for erosion and sediment controls have been designed to retain sediment on site to the extent practicable. The following information is attached:

		A description of how BMPs and measures will prevent pollution of surface water, groundwater or stormwater that originates upgradient from the site and flows across the site.
		A description of how BMPs and measures will prevent pollution of surface water or groundwater that originates on-site or flows off site, including pollution caused by contaminated stormwater runoff from the site.
		A description of how BMPs and measures will prevent pollutants from entering surface streams, sensitive features, or the aquifer.
		A description of how, to the maximum extent practicable, BMPs and measures will maintain flow to naturally-occurring sensitive features identified in either the geologic assessment, TCEQ inspections, or during excavation, blasting, or construction.
8.		The temporary sealing of a naturally-occurring sensitive feature which accepts recharge to the Edwards Aquifer as a temporary pollution abatement measure during active construction should be avoided.
		 Attachment E - Request to Temporarily Seal a Feature. A request to temporarily seal a feature is attached. The request includes justification as to why no reasonable and practicable alternative exists for each feature. There will be no temporary sealing of naturally-occurring sensitive features on the
	<u> </u>	site.
9.		Attachment F - Structural Practices. A description of the structural practices that will be used to divert flows away from exposed soils, to store flows, or to otherwise limit runoff discharge of pollutants from exposed areas of the site is attached. Placement of structural practices in floodplains has been avoided.
10.		Attachment G - Drainage Area Map. A drainage area map supporting the following requirements is attached:
		For areas that will have more than 10 acres within a common drainage area disturbed at one time, a sediment basin will be provided.
		For areas that will have more than 10 acres within a common drainage area disturbed at one time, a smaller sediment basin and/or sediment trap(s) will be used.
		For areas that will have more than 10 acres within a common drainage area disturbed at one time, a sediment basin or other equivalent controls are not attainable, but other TBMPs and measures will be used in combination to protect down slope and side slope boundaries of the construction area.
		There are no areas greater than 10 acres within a common drainage area that will be disturbed at one time. A smaller sediment basin and/or sediment trap(s) will be used in combination with other erosion and sediment controls within each disturbed drainage area.

There are no areas greater than 10 acres within a common drainage area that will be disturbed at one time. Erosion and sediment controls other than sediment basins or sediment traps within each disturbed drainage area will be used.

- 11. Attachment H Temporary Sediment Pond(s) Plans and Calculations. Temporary sediment pond or basin construction plans and design calculations for a proposed temporary BMP or measure have been prepared by or under the direct supervision of a Texas Licensed Professional Engineer. All construction plans and design information must be signed, sealed, and dated by the Texas Licensed Professional Engineer. Construction plans for the proposed temporary BMPs and measures are attached.
 - 🗌 N/A
- 12. Attachment I Inspection and Maintenance for BMPs. A plan for the inspection of each temporary BMP(s) and measure(s) and for their timely maintenance, repairs, and, if necessary, retrofit is attached. A description of the documentation procedures, recordkeeping practices, and inspection frequency are included in the plan and are specific to the site and/or BMP.
- 13. All control measures must be properly selected, installed, and maintained in accordance with the manufacturer's specifications and good engineering practices. If periodic inspections by the applicant or the executive director, or other information indicate a control has been used inappropriately, or incorrectly, the applicant must replace or modify the control for site situations.
- 14. If sediment escapes the construction site, off-site accumulations of sediment must be removed at a frequency sufficient to minimize offsite impacts to water quality (e.g., fugitive sediment in street being washed into surface streams or sensitive features by the next rain).
- 15. Sediment must be removed from sediment traps or sedimentation ponds not later than when design capacity has been reduced by 50%. A permanent stake will be provided that can indicate when the sediment occupies 50% of the basin volume.
- 16. 🖂 Litter, construction debris, and construction chemicals exposed to stormwater shall be prevented from becoming a pollutant source for stormwater discharges (e.g., screening outfalls, picked up daily).

Soil Stabilization Practices

Examples: establishment of temporary vegetation, establishment of permanent vegetation, mulching, geotextiles, sod stabilization, vegetative buffer strips, protection of trees, or preservation of mature vegetation.

17. Attachment J - Schedule of Interim and Permanent Soil Stabilization Practices. A schedule of the interim and permanent soil stabilization practices for the site is attached.

- 18. Records must be kept at the site of the dates when major grading activities occur, the dates when construction activities temporarily or permanently cease on a portion of the site, and the dates when stabilization measures are initiated.
- 19. Stabilization practices must be initiated as soon as practicable where construction activities have temporarily or permanently ceased.

Administrative Information

- 20. \square All structural controls will be inspected and maintained according to the submitted and approved operation and maintenance plan for the project.
- 21. If any geologic or manmade features, such as caves, faults, sinkholes, etc., are discovered, all regulated activities near the feature will be immediately suspended. The appropriate TCEQ Regional Office shall be immediately notified. Regulated activities must cease and not continue until the TCEQ has reviewed and approved the methods proposed to protect the aquifer from any adverse impacts.
- 22. Silt fences, diversion berms, and other temporary erosion and sediment controls will be constructed and maintained as appropriate to prevent pollutants from entering sensitive features discovered during construction.

ATTACHMENT A

ATTACHMENT A – SPILL RESPONSE ACTIONS

In the event of an accidental leak or spill:

- Spill must be contained and cleaned up immediately.
- Spills will not be merely buried or washed with water.
- Contractor shall take action to contain spill. Contractor may use sand or other absorbent material stockpiled on site to absorb spill. Absorbent material should be spread over the spill area to absorb the spilled product.
- In the event of an uncontained discharge the contractor shall utilize onsite equipment to construct berms downgradient of the spill with sand or other absorbent material to contain and absorb the spilled product.
- Spill containment/absorbent materials along with impacted media must be collected and stored in such a way so as not to continue to affect additional media (soil/water). Once the spill has been contained, collected material should be placed on poly or plastic sheeting until removed from the site. The impacted media and cleanup materials should be covered with plastic sheeting and the edges weighed down with paving bricks or other similarly dense objects as the material is being accumulated. This will prevent the impacted media and cleanup materials from becoming airborne in windy conditions or impacting runoff during a rain event. The stockpiled materials should not be located within an area of concentrated runoff such as along a curb line or within a swale.
- Contaminated soils and cleanup materials will be sampled for waste characterization. When the
 analysis results are known the contaminated soils and cleanup materials will be removed from the
 site and disposed in a permitted landfill in accordance with applicable regulations.

1

• The contractor will be required to notify the owner, who will in turn contact TCEQ to notify them in the event of a significant hazardous/reportable quantity spill. Additional notifications as required by the type and amount of spill will be conducted by owner or owner's representative.

In the event of an accidental significant or hazardous spill:

- The contractor will be required to report significant or hazardous spills in reportable quantities to:
 - the National Response Center at (800) 424-8802
 - the TCEQ Regional Office (512) 339-2929 (if during business hours: 8 AM to 5 PM) or
 - the State Emergency Response Center (800) 832-8224 (if after hours)
- Contaminated soils will be sampled for waste characterization. When the analysis results are known the contaminated soils will be removed from the site and disposed in a permitted landfill in accordance with applicable regulations.

Additional guidance can be obtained from TCEQ's Technical Guidance Manual (TGM) RG-348 (2005) Section 1.4.16. Contractor shall review this section.

ATTACHMENT B

ATTACHMENT B – POTENTIAL SOURCES OF CONTAMINATION

Other potential sources of contamination during construction include:

Potential Source

• Asphalt products used on this project.

Preventative Measure

 After placement of asphalt, emulsion or coatings, the contractor will be responsible for immediate cleanup should an unexpected rain occur. For the duration of the asphalt product curing time, the contractor will maintain standby personnel and equipment to contain any asphalt wash-off should an unexpected rain occur. The contractor will be instructed not to place asphalt products on the ground within 48 hours of a forecasted rain.

Potential Source

• Oil, grease, fuel and hydraulic fluid contamination from construction equipment and vehicle dripping.

Preventative Measure

- Vehicle maintenance when possible will be performed within the construction staging area.
- Construction vehicles and equipment shall be checked regularly for leaks and repaired immediately.

Potential Source



• Accidental leaks or spills of oil, petroleum products and substances listed under 40 CFR parts 110, 117, and 302 used or stored temporarily on site.

Preventative Measure

- Contractor to incorporate into regular safety meetings, a discussion of spill prevention and appropriate disposal procedures.
- Contractor's superintendent or representative overseer shall enforce proper spill prevention and control measures.
- Hazardous materials and wastes shall be stored in covered containers and protected from vandalism.
- A stockpile of spill cleanup materials shall be stored on site where it will be readily accessible.

Potential Source

• Miscellaneous trash and litter from construction workers and material wrappings.

Preventive Measure

• Trash containers will be placed throughout the site to encourage proper trash disposal.

Potential Source

• Construction debris.

Preventive Measure

 Construction debris will be monitored daily by contractor. Debris will be collected weekly and placed in disposal bins. Situations requiring immediate attention will be addressed on a case by case basis.

Potential Source

• Spills/Overflow of waste from portable toilets

Preventative Measure



- Portable toilets will be placed away from high traffic vehicular areas and storm drain inlets.
- Portable toilets will be placed on a level ground surface.
- Portable toilets will be inspected regularly for leaks and will be serviced and sanitized at time intervals that will maintain sanitary conditions.

ATTACHMENT C

Attachment C – Sequence of Major Activities

The sequence of major activities which disturb soil during construction on this site will be divided into two stages. The first is the common infrastructure improvements including public right-of-way, streets, and utilities. This will disturb approximately 23.02 acres. The second is construction that will include home building and landscaping improvements. This will disturb approximately 97.58 acres.

SEQUENCE OF MAJOR ACTIVITIES

COMMON INFRASTRUCTURE IMPROVEMENTS

- 1. Install temporary erosion and sedimentation control per construction plans.
- 2. Hold pre-construction meeting.
- 3. Clear & Grub the extents of the proposed right-of-way and water quality pond locations.
- 4. Excavate water quality ponds and begin utility trenching.
- 5. Install water/wastewater lines per the Construction Plans (including offsite wastewater construction).
- 6. Install proposed storm drain system (including connections to water quality ponds).
- 7. Install remaining water quality pond elements.
- 8. Rough grade streets and right-of-ways.
- 9. Finish pavement, curbs, and sidewalks.
- 10. Restore staging area to natural grade.
- 11. Obtain Engineer's Concurrence Letter.
- 12. Complete permanent erosion and sedimentation control measures and restoration of site vegetation.
- 13. Temporary erosion and sedimentation controls to remain in place as needed for the construction of next phase.

RESIDENTIAL SUBDIVISION IMPROVEMENTS

- 1. Install erosion controls per construction plans.
- 2. Begin mass grading of single family lots within limits of construction.
- 3. Install building foundations and connect underground utilities.
- 4. Begin home construction.
- 5. Final paving and sidewalk construction.
- 6. Complete final grading and restore construction spoils and staging area to natural grade.
- 7. Obtain Engineer's concurrence letter.
- 8. Complete permanent erosion control and restoration of site vegetation.
- 9. Remove temporary erosion and sedimentation controls and complete any necessary final revegetation. Temporary erosion and sedimentation controls to remain in place as needed for the construction of next phase.



ATTACHMENT D

ATTACHMENT D - TEMPORARY BMP AND MEASURES

Please see the Erosion Control sheets included in the Construction Plans Section for TBMP layout and the responses below for more details.

Upgradient stormwater will cross the site from along the northern edges of the project limits. However, this upgradient land has been developed and has completed infrastructure with its own TBMPs subject to their own SWPPP requirements, no additional TBMPs are necessary. All TMBPs utilized are adequate for the drainage areas served.

Site preparation, which is the initiation of all activity on the project, will disturb the largest amount of soil. Therefore, before any of this work can begin, the clearing and grading contractor will be responsible for the installation of all on-site control measures. The methodology for pollution prevention of on-site stormwater will include: (1) erection of silt fences along the downgradient boundary of construction activities for temporary erosion and sedimentation controls, (2) installation of rock berms downgradient from areas of concentrated stormwater flow for temporary erosion control, (3) installation of stabilized construction entrance/exit(s) to reduce the dispersion of sediment from the site, (4) installation of construction staging area(s), and (5) construction of temporary sediment basins.

Prior to the initiation of construction, all previously installed control measures will be repaired or reestablished for their designed or intended purpose. This work, which is the remainder of all activity on the project, may also disturb additional soil. The construction contractor will be responsible for the installation of all remaining on-site control measures that includes installation of the concrete truck washout pit(s), as construction phasing warrants.

Temporary measures are intended to provide a method of slowing the flow of runoff from the construction site in order to allow sediment and suspended solids to settle out of the runoff. By containing the sediment and solids within the site, they will not enter the aquifer, surface streams and/or sensitive features that may exist downstream of the site.



As the site is located entirely over the Edwards Aquifer Contributing Zone, a Geologic Assessment was not conducted and is not required by 30 TAC 213 regulations. Therefore, no naturally-occurring sensitive features are known to exist on the site. 30 TAC 213.5(f)(2) only applies to projects located on the Edwards Aquifer Recharge Zone. A combination of TBMPs including silt fence and rock berm are proposed to capture sediment from onsite stormwater runoff and preserve the quality of Block House Creek.

Temporary measures are intended to provide a method of slowing the flow of runoff from the construction site in order to allow sediment and suspended solids to settle out of the runoff. By containing the sediment and solids within the site, they will not enter the aquifer, surface streams and/or sensitive features that may exist downstream of the site.



ATTACHMENT F

ATTACHMENT F – STRUCTURAL PRACTICES

The following structural measures will be installed prior to the initiation of site preparation activities:

- Erection of silt fences along the downgradient boundary of construction activities and rock berms for secondary protection, as located on the Erosion and Sedimentation Control Plan Sheet.
- Installation of stabilized construction entrance/exit(s) and construction staging area(s), as located on the Erosion and Sedimentation Control Plan Sheet.

The following structural measures will be installed at the initiation of construction activities or as appropriate based on the construction sequencing:

- Installation of concrete truck washout pit(s), as required and located on the Erosion Control Plan Sheet.
- Installation of inlet protection, as located on the Erosion Control Plan Sheet.

ATTACHMENT G

ATTACHMENT G – DRAINAGE AREA MAP

A copy of an exhibit delineating the existing common 57.89 and 8.94 acre drainage areas draining to the temporary sedimentation ponds have been added to this section. A Proposed Drainage Area map broken out by PBMP with acreage and impervious cover is included in the Construction Plans. All TBMPs utilized are adequate for the drainage areas served.





			COMPO	DSITE C				SHEET F	LOW		SHALL	OW CONCE	NTRATED	FLOW		CHANNE	LIZED FL	ow		Cumulative	INTEN	ISITY	DISCH	ARGE
DRAINAGE	INLET	AREA	C	C	A.C25	A.C100	Length	Manning's	Slope	Tc	Length	Paved/	Slope	Tc	Length	Manning's	Slope	Velocity	Tc	Тс	I 25yr	I 100yr	Q 25	Q 100
AREA	NUMBER	(acres)	025	C100			(ft)	(n)	ft/ft	(min)	(ft)	Unpaved	ft/ft	(min)	(ft)	(n)	ft/ft	ft/s	(min)	(min)	(in/hr)	(in/hr)	(cfs)	(cfs)
EXISTING CONDITION DRAINAGE AREAS																								
EX-1	EX-1	57.89	0.54	0.61	31.054	35.459	100	0.24	0.118	6.34	49.16	U	0.125	0.14	3635.74	0.015	0.023	5.8	10.387	16.87	7.29	9.67	226.3	343.0
EX-2	EX-2	8.94	0.58	0.65	5.147	5.843	100	0.24	0.005	22.45	224.9	U	0.047	1.07	1522.73	0.128	0.018	0.6	41.797	65.32	3.34	4.51	17.2	26.3

ATTACHMENT H

ATTACHMENT H - TEMPORARY SEDIMENT POND(S) PLANS AND CALCULATIONS

The proposed batch detention basin may be used as a temporary sediment basin during site construction. Qualified personnel shall inspect the temporary sediment basin every fourteen (14) calendar days and within twenty-four (24) hours after a rainfall event greater than 0.5 inches. Depth of silt deposit and erosion in basin shall also be checked within twenty-four (24) hours after every rainfall event greater than 0.5 inches and every seven (7) days until lot construction is complete in the basin's drainage area.

The equipment for batch detention will be installed concurrently with the first construction phase of each watershed. If a basin has been converted to a Permanent BMP, but a portion of the watershed is not stabilized, then the basin shall continue to be inspected in accordance with the inspection requirements of a temporary sediment trap until final stabilization of the entire watershed. Prior to final acceptance by the owner, the contractor will remove trash, debris and accumulated silt from the basin and re-establish it to proper operating condition. All permanent pollution abatement measures shall be operational prior to occupancy of any facility within the drainage area of the respective permanent pollution abatement measure. After inspection of the finished batch detention basin, a licensed professional engineer will certify the basin in accordance with the TCEQ requirements.

Capture Volume Calculation:

Volume required = 3,600 cubic feet (CF) storage per 1 acre drained. Temporary Sediment Basin "H" 3,600 CF x 57.89 ac (Construction Area) = 208,404 CF Volume provided = 221,562 cf (At 816.00)

Temporary Sediment Basin "J" 3,600 CF x 8.94 ac (Construction Area) = 32,184 CF Volume provided = 58,222 CF (At 827.00)



Riser Pipe Perforation Calculation:

$$A_o = \frac{A_s \times \sqrt{2h}}{C_d \times 980,000}$$

Temporary Sediment Basin "H" $A_s = 35,818 \text{ ft}^2; C_d = 0.6; h = 4.5 \text{ ft}$ $A_o = 0.193 \text{ ft}^2 = 27.75 \text{ in}^2$

Temporary Sediment Basin "J" $A_s = 12,750.39 \text{ ft}^2; C_d = 0.6; h = 6.9 \text{ ft}$ $A_o = 0.081 \text{ ft}^2 = 11.60 \text{ in}^2$

Please note, these temporary sediment basins are being utilized in combination with other TBMP measures for the site and all are adequate for the drainage areas served.



ATTACHMENT I

ATTACHMENT I - INSPECTION AND MAINTENANCE OF TEMPORARY BMP'S

INSPECTIONS & MAINTENANCE

Designated and qualified person(s) shall inspect Pollution Control Measures weekly and within 24 hours after a storm event. An inspection report that summarizes the scope of the inspection, names and qualifications of personnel conducting the inspection, date of the inspection, major observations, and actions taken as a result of the inspection will be recorded and maintained as part of Storm Water TPDES data for a period of three years after the Notice of Termination (NOT) has been filed. A copy of the Inspection Report Form is provided in this Storm Water Pollution Prevention Plan.

As a minimum, the inspector shall observe: (1) significant disturbed areas for evidence of erosion, (2) storage areas for evidence of leakage from the exposed stored materials, (3) structural controls (rock berm outlets, silt fences, drainage swales, etc.) for evidence of failure or excess siltation (over 6 inches deep), (4) vehicle exit point for evidence of off-site sediment tracking, (5) vehicle storage areas for signs of leaking equipment or spills, (6) concrete truck rinse-out pit for signs of potential failure, (7) embankment, spillways, and outlet of sediment basin (where applicable) for erosion damage, and (8) sediment basins (where applicable) for evidence that basin has accumulated 50% of its volume in silt. Deficiencies noted during the inspection will be corrected and documented within seven calendar days following the inspection or before the next anticipated storm event if practicable. Temporary sediment basins and permanent basins will be inspected until final stabilization of 70% within the basin watershed is achieved.

Contractor shall review Sections 1.3 and 1.4 of TCEQ's Technical Guidance Manual for additional BMP inspection and maintenance requirements.



LIVELY TRACT PHASE 2

Temporary Stormwater Section

Dellection	in e	Corrective Action Required						
Pollution Prevention Measure	lnspected i Compliance	Description (use additional sheet if necessary)	Date Completed					
Best Management Practices								
Natural vegetation buffer strips								
Temporary vegetation								
Permanent vegetation								
Sediment control basin								
Silt fences								
Rock berms								
Gravel filter bags								
Drain inlet protection								
Other structural controls								
Vehicle exits (off-site tracking)								
Material storage areas (leakage)								
Equipment areas (leaks, spills)								
Concrete washout pit (leaks, failure)								
General site cleanliness								
Trash receptacles								
Evidence of Erosion								
Site preparation								
Roadway or parking lot construction								
Utility construction								
Drainage construction								
Building construction								
Major Observations								
Sediment discharges from site								
BMPs requiring maintenance								
BMPs requiring modification								
Additional BMPs required								

____ A brief statement describing the qualifications of the inspector is included in this SWP3.

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am



aware there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations."

"I further certify I am an authorized signatory in accordance with the provisions of 30 TAC §305.128."

Inspector's Name

Inspector's Signature

Date



LIVELY TRACT PHASE 2

Temporary Stormwater Section

PROJECT MILESTONE DATES

Date when major site grading activities begin:

Construction Activity		Date	
Installation of BMPs	_		
	_		
Dates when construction activities temporarily or pe	rmanently	y cease on all or a portion of the proje	ect:
Construction Activity		Date	
Dates when stabilization measures are initiated:			
Stabilization Activity		Date	
	_		
Removal of BMPs			



ATTACHMENT J

ATTACHMENT J – SCHEDULE OF INTERIM AND PERMANENT SOIL STABILIZATION PRACTICES

Interim on-site stabilization measures, which are continuous, will include minimizing soil disturbances by exposing the smallest practical area of land required for the shortest period of time and maximizing use of natural vegetation. As soon as practical, all disturbed soil will be stabilized as per project specifications in accordance with pages 1-35 to 1-60 of TCEQ's Technical Guidance Manual (TGM) RG-348 (2005). Mulching, netting, erosion blankets and seeding are acceptable.

Stabilization measures will be initiated as soon as practicable in portions of the site where construction activities have temporarily or permanently ceased, and except as provided below, will be initiated no more than fourteen (14) days after the construction activity in that portion of the site has temporarily or permanently ceased. Where construction activity on a portion of the site is temporarily ceased, and earth disturbing activities will be resumed within twenty-one (21) days, temporary stabilization measures do not have to be initiated on that portion of site. In areas experiencing droughts where the initiation of stabilization measures by the 14th day after construction activity has temporarily or permanently ceased is precluded by seasonably arid conditions, stabilization measures must be initiated as soon as practicable.



NOTICE OF INTENT

TCEQ Office Use Only Permit No: CN: RN:



Notice of Intent (NOI) for an Authorization for Stormwater Discharges Associated with Construction Activity under TPDES General Permit TXR150000

IMPORTANT INFORMATION

Please read and use the General Information and Instructions prior to filling out each question in the NOI form.

Use the NOI Checklist to ensure all required information is completed correctly. **Incomplete applications delay approval or result in automatic denial.**

Once processed your permit authorization can be viewed by entering the following link into your internet browser: http://www2.tceq.texas.gov/wq_dpa/index.cfm or you can contact TCEQ Stormwater Processing Center at 512-239-3700.

ePERMITS

Effective September 1, 2018, this paper form must be submitted to TCEQ with a completed electronic reporting waiver form (TCEQ-20754).

To submit an NOI electronically, enter the following web address into your internet browser and follow the instructions: https://www3.tceq.texas.gov/steers/index.cfm

APPLICATION FEE AND PAYMENT

The application fee for submitting a paper NOI is \$325. The application fee for electronic submittal of a NOI through the TCEQ ePermits system (STEERS) is \$225.

Payment of the application fee can be submitted by mail or through the TCEQ ePay system. The payment and the NOI must be mailed to separate addresses. To access the TCEQ ePay system enter the following web address into your internet browser: http://www.tceq.texas.gov/epay.

Provide your payment information for verification of payment:

- If payment was mailed to TCEQ, provide the following:
 - Check/Money Order Number:
 - Name printed on Check:
- If payment was made via ePay, provide the following:
 - Voucher Number:
 - A copy of the payment voucher is attached to this paper NOI form.

RE	RENEWAL (This portion of the NOI is not applicable after June 3, 2018)						
Is	Is this NOI for a renewal of an existing authorization? \Box Yes \boxtimes No						
If Y	If Yes, provide the authorization number here: TXR15						
NC	NOTE: If an authorization number is not provided, a new number will be assigned.						
SECTION 1 OPERATOR (APPLICANT)							
0.6							
a)	If the applicant is currently a customer with TCEQ, what is the Customer Number (CN) issued to this entity? CN <u>605112077</u>						
	(Refer to Section 1.a) of the Instructions)						
b)	What is the Legal Name of the entity (applicant) applying for this permit? (The legal name must be spelled exactly as filed with the Texas Secretary of State, County, or in the legal document forming the entity.)						
	Hwy 29 Ventures 2015 LP						
c)	What is the contact information for the Operator (Responsible Authority)?						
	Prefix (Mr. Ms. Miss): <u>Mr.</u>						
	First and Last Name: <u>Tom Rielly</u> Suffix: <u>N/A</u>						
	Title: <u>President</u> Credentials: <u>N/A</u>						
	Phone Number: <u>949-922-2512</u> Fax Number:						
	E-mail: tomr@shamrockcommunities.com						
	Mailing Address: <u>4910 Campus Drive</u>						

City, State, and Zip Code: Newport Beach, CA, 92660

Mailing Information if outside USA:

Territory:

Country Code:

Postal Code:

- d) Indicate the type of customer:
 - Individual
 Federal Government
 Limited Partnership
 County Government
 General Partnership
 State Government
 Trust
 City Government
 Sole Proprietorship (D.B.A.)
 Other Government
 Corporation
 Other:

e)	Is the applicant an independent operator?	🖾 Yes	🗆 No

TCEO-20022	(3/6/2018)
(If a governmental entity, a subsidiary, or part of a larger corporation, check No.)

- f) Number of Employees. Select the range applicable to your company.
 - ⊠ 0-20
 - □ 21-100

□ 251-500

21-100

 \Box 501 or higher

- □ 101-250
- g) Customer Business Tax and Filing Numbers: (**Required** for Corporations and Limited Partnerships. **Not Required** for Individuals, Government, or Sole Proprietors.)

State Franchise Tax ID Number:

Federal Tax ID: <u>475180278</u>

Texas Secretary of State Charter (filing) Number:

DUNS Number (if known):

SECTION 2. APPLICATION CONTACT

Is the application contact the same as the applicant identified above?

- □ Yes, go to Section 3
- \boxtimes No, complete this section

Prefix (Mr. Ms. Miss): <u>Mr.</u>

First and Last Name: <u>Dustin Goss, P.E., LEED® AP</u> Suffix: <u>N/A</u>

Title: <u>Vice President</u> Credential:

Organization Name: Pape-Dawson Engineers, Inc.

Phone Number: <u>512-454-8711</u> Fax Number:

E-mail: <u>dgoss@pape-dawson.com</u>

Mailing Address: <u>10801 N Mopac Expy. Bldg. 3, Suite 200</u>

Internal Routing (Mail Code, Etc.):

City, State, and Zip Code: <u>Austin, TX, 78759</u>

Mailing information if outside USA:

Territory:

Country Code:

Postal Code:

SECTION 3. REGULATED ENTITY (RE) INFORMATION ON PROJECT OR SITE

a) If this is an existing permitted site, what is the Regulated Entity Number (RN) issued to this site? RN <u>110606126</u>

(Refer to Section 3.a) of the Instructions)

- b) Name of project or site (the name known by the community where it's located): <u>Lively Tract Phase 2</u>
- c) In your own words, briefly describe the type of construction occurring at the regulated site (residential, industrial, commercial, or other): <u>Residential Single Family</u>
- d) County or Counties (if located in more than one): <u>Williamson</u>
- e) Latitude: <u>30.636983</u> Longitude: <u>97.800311</u>
- f) Site Address/Location

If the site has a physical address such as 12100 Park 35 Circle, Austin, TX 78753, complete *Section A*.

If the site does not have a physical address, provide a location description in *Section B*. Example: located on the north side of FM 123, 2 miles west of the intersection of FM 123 and Highway 1.

Section A:

Street Number and Name:

City, State, and Zip Code:

Section B:

Location Description: West of intersection of TX Hwy 29 and Cross Creek Road.

City (or city nearest to) where the site is located: Leander

Zip Code where the site is located: <u>78628</u>

SECTION 4. GENERAL CHARACTERISTICS

- a) Is the project or site located on Indian Country Lands?
 - Yes, do not submit this form. You must obtain authorization through EPA Region 6.

🛛 No

- **b**) Is your construction activity associated with a facility that, when completed, would be associated with the exploration, development, or production of oil or gas or geothermal resources?
 - Yes. Note: The construction stormwater runoff may be under jurisdiction of the Railroad Commission of Texas and may need to obtain authorization through EPA Region 6.

🛛 No

- c) What is the Primary Standard Industrial Classification (SIC) Code that best describes the construction activity being conducted at the site? <u>1521</u>
- d) What is the Secondary SIC Code(s), if applicable? <u>1794</u>
- e) What is the total number of acres to be disturbed? <u>120.60</u>
- f) Is the project part of a larger common plan of development or sale?

TCEQ-20022 (3/6/2018)

🛛 Yes

- □ No. The total number of acres disturbed, provided in e) above, must be 5 or more. If the total number of acres disturbed is less than 5, do not submit this form. See the requirements in the general permit for small construction sites.
- g) What is the estimated start date of the project? December 2021
- h) What is the estimated end date of the project? December 2026
- i) Will concrete truck washout be performed at the site? \square Yes \square No
- j) What is the name of the first water body(ies) to receive the stormwater runoff or potential runoff from the site? <u>South Fork San Gabriel River</u>
- k) What is the segment number(s) of the classified water body(ies) that the discharge will eventually reach? <u>1250</u>
- l) Is the discharge into a Municipal Separate Storm Sewer System (MS4)?

□ Yes 🛛 🖾 No

If Yes, provide the name of the MS4 operator:

Note: The general permit requires you to send a copy of this NOI form to the MS4 operator.

m) Is the discharge or potential discharge from the site within the Recharge Zone, Contributing Zone, or Contributing Zone within the Transition Zone of the Edwards Aquifer, as defined in 30 TAC Chapter 213?

 \boxtimes Yes, complete the certification below.

 \square No, go to Section 5

I certify that the copy of the TCEQ-approved Plan required by the Edwards Aquifer Rule (30 TAC Chapter 213) that is included or referenced in the Stormwater Pollution Prevention Plan will be implemented.

SECTION 5. NOI CERTIFICATION

- a) I certify that I have obtained a copy and understand the terms and conditions of the Construction General Permit (TXR150000).
- c) I understand that a Notice of Termination (NOT) must be submitted when this authorization is no longer needed.
- d) I certify that a Stormwater Pollution Prevention Plan has been developed, will be implemented prior to construction and to the best of my knowledge and belief is compliant with any applicable local sediment and erosion control plans, as required in the Construction General Permit (TXR150000).

Note: For multiple operators who prepare a shared SWP3, the confirmation of an operator may be limited to its obligations under the SWP3, provided all obligations are confirmed by at least one operator.

🖾 Yes

SECTION 6. APPLICANT CERTIFICATION SIGNATURE

Operator Signatory Name: Tom Rielly

Operator Signatory Title: President

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

I further certify that I am authorized under 30 Texas Administrative Code §305.44 to sign and submit this document, and can provide documentation in proof of such authorization upon request.

JCD Date: 3/27/24

Signature (use blue ink): _____

TEXAS COMMISSION ON ENVIRONMENTAL QUALITY



REQUEST FOR ELECTRONIC REPORTING WAIVER

If you have questions about completing this form please contact the Applications Review and Processing Team at 512-239-4671.

Section 1. Applicant Information

What is the contact information for the applicant? Prefix (Mr. Ms. or Miss): Mr.

First and Last Name: Tom Rielly

Suffix: N/A

Title: Owner

Credentials: N/A

Phone Number: 949-922-2512

Fax Number:

Email: tomr@shamrockcommunities.com

Mailing Address: 4910 Campus Drive

City, State, and Zip Code: Newport Beach, CA, 92660

- b) Does the applicant have a water quality individual permit or general authorization issued by TCEO?
 - Yes. Complete Sections 3, 4, and 5
 - \square No. Complete Sections 2, 4, and 5

Section 2. New Customers

- a) What is the Legal Name of the applicant applying for this waiver? (The legal name must be spelled exactly as filed with the Texas Secretary of State, County, or in the legal document forming the entity.) Hwy 29 Ventures 2015 LP
- b) What type of permit or authorization are you applying for? <u>Edwards Aquifer</u>

Contributing Zone Plan [Notice of Intent].

- c) Is the permit application identified in question c) submitted together with this form?
 - \bowtie Yes. Skip to Section 4
 - No. Answer question e) below
- d) What date did you submit the permit application to TCEQ?

Section 3. Existing Customers

- a) What is the TCEQ Water Quality Permit or Authorization Number related to this request for an electronic waiver? A separate request for electronic reporting waiver form is required for each permit or authorization. Edwards Aquifer Protection Program ID Number 11001396
- b) What is the current permittee name on the permit or authorization: Hwy 29 Ventures 2015 LP
- c) What is the Customer Number (CN) for the current permittee? CN 605112077

d) What is the Regulated Entity Number (RN): RN 110606126

Section 4. Reason for the Waiver

Select the reason for requesting a waiver from electronic reporting:

- I need additional training on electronic I don't have a computer. reporting.
- I don't have internet access.
- I have limited internet
- I have a religious objection to electronic reporting.

speed.

Section 5. Certification and Signature

Applicant's Name: Mr. Tom Rielly Applicant's Title: President

I understand that this waiver will expire on the same date as my permit or authorization, unless the reason for the waiver is additional training is needed or religious objection.	Yes
I understand that this waiver is not transferrable. If the permit is transferred, this waiver will be terminated and the new permittee must request and obtain a new waiver.	Yes
I understand that an approved electronic reporting waiver allows me to submit required information on paper rather than electronically. It does not change the type of information that is required to be submitted to TCEQ.	Yes
I understand that having an approved waiver does not prevent me from using electronic reporting if the reason for requesting the	Yes

waiver changes.

I certify under penalty of law, that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that gualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is to the best of my knowledge and belief, true, accurate, and complete. I am aware there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

I further certify that I am authorized under 30 Texas Administrative Code §305.44 to sign and submit this document, and can provide documentation in proof of such authorization upon request.

Signature (use blue ink):

TCEQ -20754 (09/01/2016) REOUEST FOR ELECTRONIC REPORTING WAIVER

Date: 3/27/21

OWNER AUTHORIZATION



Owner Authorization Form

Edwards Aquifer Protection Program

Instructions

Complete the following form by adding the requested information in the fields below. The form must be notarized for it to be considered complete. Attach it to other programmatic submittals required by 30 Texas Administrative Code (30 TAC), Chapter 213, and provide it to TCEQ's Edwards Aquifer Protection Program (EAPP) as part of your application.

If you have questions on how to fill out this form or about EAPP, please contact us by phone at 512-339-2929 or by e-mail at <u>eapp@tceq.texas.gov</u>.

Landowner Authorization

I, Tom Reilly of Hwy 29 Ventures 2015 LP

am the owner of the property located at:

A 120.620 ACRE TRACT OF LAND SITUATED IN THE GREENLEAF FISK SURVEY, ABSTRACT NO. 5, AND THE BARTHOLOMEW MANLOVE SURVEY, ABSTRACT NO. 420 IN WILLIAMSON COUNTY, TEXAS, BEING OUT OF THE REMNANT PORTION OF A CALLED 437.04 ACRE TRACT CONVEYED TO HWY 29 VENTURES 2015, L.P. RECORDED IN DOCUMENT NO. 2015088162, AND BEING OUT OF LIVELY TRACT PHASE 2, A SUBDIVISION ACCORDING TO THE PLAT RECORDED IN DOCUMENT NO 2020134123 AND BEING OUT OF LIVELY TRACT PHASE 4, A SUBDIVISION ACCORDING TO THE PLAT RECORDED IN DOCUMENT NO 2023099454, ALL OF THE OFFICIAL PUBLIC RECORDS OF WILLIAMSON COUNTY, TEXAS.

and am duly authorized in accordance with 30 TAC 213.4(c)(2) and 213.4(d)(1), or 30 TAC 213.23(c)(2) and 213.23(d), relating to the right to submit an application, signatory authority, and proof of authorized signatory.

I do hereby authorize Dustin Goss, P.E., LEED® AP To conduct Preparing and submitting the plan to TCEQ for review and approval of the development.

At 1602 Magnolia Farm Way, Georgetown, TX 78628

Landowner Acknowledgement

I understand that Hwy 29 Ventures 2015 LP

Is ultimately responsible for the compliance with the approved or conditionally approved Edwards Aquifer protection plan and any special conditions of the approved plan through all phases of plan implementation even if the responsibility for compliance and the right to possess and control the property referenced in the application has been contractually assumed by another legal entity. I further understand that any failure to comply with any condition of the executive director's approval is a violation and subject to administrative rule or orders and penalties as provided under 30 TAC 213.10, relating to enforcement. Such violations may also be subject to civil penalties. Landowner Signature

Landowner Signature

Date

THE STATE § OF TEXAS County § of Travis

BEFORE ME, the undersigned authority, on this day personally appeared

Tom Riell

known to me to be the person whose name is subscribed to the foregoing instrument and acknowledged to me that (s)he executed same for the purpose and consideration therein expressed.

GIVEN under my hand and seal of office on this 3^{H} day of May 2025

NOTARY PUBLIC Marytele 24

MY COMMISSION EXPIRES: 08/14/2028



Optional Attachments

Select All that apply:

- □ Lease Agreement
- □ Signed Contract
- □ Deed Restricted Easement
- □ Other legally binding documents

AGENT AUTHORIZATION

Agent Authorization Form For Required Signature

Edwards Aquifer Protection Program Relating to 30 TAC Chapter 213 Effective June 1, 1999

l	Tom Rielly
	Print Name
	President
	Title - Owner/President/Other
of	Hwy 29 Ventures 2015 LP
	Corporation/Partnership/Entity Name
have authorized	Dustin Goss, P.E., LEED® AP
	Print Name of Agent/Engineer
of	Pape-Dawson Consulting Engineers, LLC
	Print Name of Firm

to represent and act on the behalf of the above named Corporation, Partnership, or Entity for the purpose of preparing and submitting this plan application to the Texas Commission on Environmental Quality (TCEQ) for the review and approval consideration of regulated activities.

I also understand that:

- 1. The applicant is responsible for compliance with 30 Texas Administrative Code Chapter 213 and any condition of the TCEQ's approval letter. The TCEQ is authorized to assess administrative penalties of up to \$10,000 per day per violation.
- 2. For those submitting an application who are not the property owner, but who have the right to control and possess the property, additional authorization is required from the owner.
- 3. Application fees are due and payable at the time the application is submitted. The application fee must be sent to the TCEQ cashier or to the appropriate regional office. The application will not be considered until the correct fee is received by the commission.
- 4. A notarized copy of the Agent Authorization Form must be provided for the person preparing the application, and this form must accompany the completed application.
- 5. No person shall commence any regulated activity on the Edwards Aquifer Recharge Zone, Contributing Zone or Transition Zone until the appropriate application for the activity has been filed with and approved by the Executive Director.

SIGNATURE PAGE:

Applicant's Signature

Date 8/a/se

THE STATE OF TEXAS 8

County of TRAVIS §

BEFORE ME, the undersigned authority, on this day personally appeared <u>Nevner</u> <u>Rielly</u> known to me to be the person whose name is subscribed to the foregoing instrument, and acknowledged to me that (s)he executed same for the purpose and consideration therein expressed.

GIVEN under my hand and seal of office on this 11th day of August , 2021.

MARY HELEN TELLO My Notary ID # 126626500 Expires August 14, 2024

Typed of Printed Name of Notary

MY COMMISSION EXPIRES: 08/14/2024

APPLICATION FEE FORM

Application Fee Form

Name of Proposed Regulated Entity: Lively Tract, Phase 2 Regulated Entity: Location: TX Hwy 29 and Cross Creek Road within the City of Leander ETJ. Name of Customer: Hwy 29 Ventures 2015 LP Contact Person: Tom Rielly Phone: [949] 922-2512 Customer Reference Number (if issued):RN 110606126 Austin Regional Office (3373)	Texas Commission on Environm	ental Quality		
Regulated Entity Location: TX Hwy 29 and Cross Creek Road within the City of Leander ETJ. Name of Customer: Hwy 29 Ventures 2015 LP Contact Person: Tom Rielly Phone: (949) 922-2512 Customer Reference Number (if issued):RN 110606126 Austin Regional Office (3373) Hays Travis Bexar Medina Uvalde Comal Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Mailed to: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Maile do: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Plan: One Single Family Residential Dwelling Acres Water Pollution Abatement Plan, Contributing Zone Transition Zone Plan: One Single Family Residential and Parks 120.6 Acres \$ 8,000 </td <td>Name of Proposed Regulated En</td> <td>tity: Lively Tract, Phase 2</td> <td></td> <td></td>	Name of Proposed Regulated En	tity: Lively Tract, Phase 2		
Name of Customer: Hwy 29 Ventures 2015 LP Contact Person: Tom Rielly Phone: [949] 922-2512 Customer Reference Number (if issued):CN 605112077 Regulated Entity Reference Number (if issued):RN 110606126 Austin Regional Office (3373) Hays Travis Bexar Medina Comal Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Maile dto: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Mater Pollution Abatement Plan, Contributing Zone Transition Zone Water Pollution Abatement Plan, Contributing Zone Pian: One Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Pian: Non-residen	Regulated Entity Location: TX Hv	vy 29 and Cross Creek Road	d within the City of Le	ander ETJ.
Contact Person: Tom Rielly Phone: (949) 922-2512 Customer Reference Number (if issued):CN 605112077 Regulated Entity Reference Number (if issued):RN 110606126 Austin Regional Office (3373) Hays Travis Bexar Medina Comal Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Maile dto: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone 120.6 Acres \$ 8,000 Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone 120.6 Acres \$ 8,000 Plan: Non-residential	Name of Customer: Hwy 29 Vent	tures 2015 LP		
Customer Reference Number (if issued):CN 605112077 Regulated Entity Reference Number (if issued):RN 110606126 Austin Regional Office (3373) Hays Travis Williamson San Antonio Regional Office (3362) Bexar Medina Uvalde Comal Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Austin TX 78711-3088 Austin, TX 78753 Austin, Austin, TX	Contact Person: Tom Rielly	Phone:	: <u>(949) 922-2512</u>	
Regulated Entity Reference Number (if issued):RN 110606126 Austin Regional Office (3373)	Customer Reference Number (if	issued):CN <u>605112077</u>		
Austin Regional Office (3373) Hays Travis Williamson San Antonio Regional Office (3362) Williamson Bexar Medina Uvalde Comal Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Mailed to: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Maile do: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Recharge Zone Contributing Zone Transition Zone Vater Pollution Abatement Plan, Contributing Zone \$ \$ Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone \$ \$ Plan: Multiple Single Family Residential Davelling Acres \$ Sewage Collection Sy	Regulated Entity Reference Num	ber (if issued):RN <u>1106061</u>	126	
□ Hays □ Travis Williamson San Antonio Regional Office (3362) □ Uvalde □ Comal □ Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: □ Austin Regional Office □ San Antonio Regional Office □ Mailed to: TCEQ - Cashier □ Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): □ □ Recharge Zone □ Contributing Zone □ Transition Zone □ Water Pollution Abatement Plan, Contributing Zone □ Plan: One Single Family Residential Dwelling Acres Water Pollution Abatement Plan, Contributing Zone □ Plan: Nultiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone □ □ <td>Austin Regional Office (3373)</td> <td></td> <td></td> <td></td>	Austin Regional Office (3373)			
San Antonio Regional Office (3362) Bexar Medina Comal Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Mailed to: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Recharge Zone Contributing Zone Transition Zone Vater Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone Plan: Nultiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Nultiple Single Family Residential and Parks 120.6 Acres \$ Sewage Collection System L.F. \$ Lift Stations without sewer lines Acres \$ Underground or Aboveground Stora	Hays	Travis	🖂 will	iamson
Bexar Medina Uvalde Comal Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Mailed to: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Recharge Zone Contributing Zone Transition Zone Water Pollution Abatement Plan, Contributing Zone Plan: One Single Family Residential Dwelling Acres Plan: One Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone L.F. \$ S Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000<	San Antonio Regional Office (33	62)		
□ Comal □ Kinney Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: □ Austin Regional Office □ San Antonio Regional Office □ Mailed to: TCEQ - Cashier □ Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): □ □ Recharge Zone □ Contributing Zone □ Transition Zone Vater Pollution Abatement Plan, Contributing Zone □ Transition Zone Plan: One Single Family Residential Dwelling Acress \$ Water Pollution Abatement Plan, Contributing Zone 120.6 Acress \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acress \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acress \$ Sewage Collection System L.F. \$	Bexar	Medina	Uva	lde
Application fees must be paid by check, certified check, or money order, payable to the Texas Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Mailed to: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Recharge Zone Contributing Zone Transition Zone Water Pollution Abatement Plan, Contributing Zone \$ Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone \$ \$ Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone P \$ Plan: Non-residential Acrees \$ \$ Sewage Collection System L.F. \$ \$ \$ Lift Stations without sewer lines Acres	Comal	Kinney		
Commission on Environmental Quality. Your canceled check will serve as your receipt. This form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Mailed to: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Recharge Zone Contributing Zone Transition Zone Water Pollution Abatement Plan, Contributing Zone Acres \$ Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Plan: Non-residential Acres \$ Support L.F. \$ Lift Stations without sewer lines Acres \$ Support Support Support Support Support Support Support Support Support <	Application fees must be paid by	check, certified check, or	money order, payable	e to the Texas
form must be submitted with your fee payment. This payment is being submitted to: Austin Regional Office San Antonio Regional Office Mailed to: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Recharge Zone Contributing Zone Transition Zone Water Pollution Abatement Plan, Contributing Zone Plan: One Single Family Residential Dwelling Acres Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Plan: Non-residential Acres \$ 8,000 Sewage Collection System L.F. \$ Lift Stations without sewer lines Acres \$ S Sewage Specific Science \$ Piping System(s)(only) Each \$ \$ S \$ \$ Exception Each \$ \$ \$ \$ <	Commission on Environmental	Quality. Your canceled che	eck will serve as your	receipt. This
Austin Regional Office □ San Antonio Regional Office □ Mailed to: TCEQ - Cashier □ Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): □ Transition Zone □ Recharge Zone □ Contributing Zone □ Transition Zone Water Pollution Abatement Plan, Contributing Zone Plan: One Single Family Residential Dwelling Acres Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Plan: Non-residential Acres \$ S Sewage Collection System L.F. \$ Lift Stations without sewer lines Acres \$ S S S S Piping System(s)(only) Each \$ S S S S S <td>form must be submitted with y</td> <td>our fee payment. This pay</td> <td>ment is being submit</td> <td>ted to:</td>	form must be submitted with y	our fee payment. This pay	ment is being submit	ted to:
Mailed to: TCEQ - Cashier Overnight Delivery to: TCEQ - Cashier Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): □ Recharge Zone ☑ Contributing Zone □ Transition Zone Water Pollution Abatement Plan, Contributing Zone □ Transition Zone Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone 120.6 Acres \$ 8,000 Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Plan: Non-residential Acres \$ 8,000 \$ \$ Underground or Aboveground Storage Tank Facility Tanks \$ \$ Underground or Aboveground Storage Tank Facility Tanks \$ \$ Piping System(s)(only) Each \$ \$ \$ Exception Each \$ \$ \$ \$	Austin Regional Office	Sar	n Antonio Regional Off	fice
Revenues Section 12100 Park 35 Circle Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Transition Zone Recharge Zone Contributing Zone Transition Zone Water Pollution Abatement Plan, Contributing Zone Acres \$ Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone 120.6 Acres \$ 8,000 Plan: Nultiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Plan: Nultiple Single Family Residential and Parks 120.6 Acres \$ 8,000 \$ Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Lift Stations without sewer lines Acres \$ \$ Underground or Aboveground Storage Tank Facility Tanks \$ Piping System(s)(only) Each \$ \$ Exception Each \$ \$ \$	Mailed to: TCEQ - Cashier	Ov	ernight Delivery to: TO	EQ - Cashier
Mail Code 214 Building A, 3rd Floor P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Recharge Zone Contributing Zone Transition Zone Image: Recharge Zone Contributing Zone Transition Zone Water Pollution Abatement Plan, Contributing Zone Acres \$ Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Sewage Collection System L.F. \$ \$ \$ Lift Stations without sewer lines Acres \$ \$ \$ Underground or Aboveground Storage Tank Facility Tanks \$ \$ \$ Piping System(s)(only) Each \$ \$ \$ \$ \$ Exception Each \$ \$<	Revenues Section	12:	100 Park 35 Circle	
P.O. Box 13088 Austin, TX 78753 Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Recharge Zone Contributing Zone Transition Zone Type of Plan Size Fee Due Water Pollution Abatement Plan, Contributing Zone Acres \$ Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Plan: Non-residential Acres \$ \$ Sewage Collection System L.F. \$ \$ Lift Stations without sewer lines Acres \$ \$ Underground or Aboveground Storage Tank Facility Tanks \$ \$ Piping System(s)(only) Each \$ \$ \$ Exception Each \$ \$ \$	Mail Code 214	Bui	ilding A, 3rd Floor	
Austin, TX 78711-3088 (512)239-0357 Site Location (Check All That Apply): Recharge Zone Contributing Zone Transition Zone Mater Pollution Abatement Plan, Contributing Zone Fee Due Water Pollution Abatement Plan, Contributing Zone Acres \$ Water Pollution Abatement Plan, Contributing Zone 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Plan: Non-residential Acres \$ Sewage Collection System L.F. \$ Lift Stations without sewer lines Acres \$ Underground or Aboveground Storage Tank Facility Tanks \$ Piping System(s)(only) Each \$ Exception Each \$ Extension of Time Each \$	P.O. Box 13088	Au	stin, TX 78753	
Site Location (Check All That Apply): Recharge Zone Contributing Zone Transition Zone Type of Plan Size Fee Due Water Pollution Abatement Plan, Contributing Zone Acres \$ Plan: One Single Family Residential Dwelling Acres \$ Water Pollution Abatement Plan, Contributing Zone 120.6 Acres \$ 8,000 Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Acres \$ Plan: Multiple Single Family Residential and Parks 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Plan: Non-residential Acres \$ 120.6 Acres \$ 8,000 Water Pollution Abatement Plan, Contributing Zone Plan: Non-residential Acres \$ Sewage Collection System L.F. \$ S Sewage Collection System L.F. \$ Lift Stations without sewer lines Acres \$ S S S S S Piping System(s)(only) Each \$ S Exception Each	Austin, TX 78711-3088	(51	2)239-0357	
Recharge ZoneContributing ZoneTransition ZoneType of PlanSizeFee DueWater Pollution Abatement Plan, Contributing Zone Plan: One Single Family Residential DwellingAcres\$Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks120.6 Acres\$ 8,000Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks120.6 Acres\$ 8,000Water Pollution Abatement Plan, Contributing Zone Plan: Non-residentialAcres\$\$Sewage Collection SystemL.F.\$\$\$Lift Stations without sewer linesAcres\$\$\$Underground or Aboveground Storage Tank FacilityTanks\$\$\$Piping System(s)(only)Each\$\$\$\$ExceptionEach\$\$\$\$Extension of TimeEach\$\$\$\$	Site Location (Check All That Ap	oply):		
Type of PlanSizeFee DueWater Pollution Abatement Plan, Contributing Zone Plan: One Single Family Residential DwellingAcres\$Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks120.6 Acres\$ 8,000Water Pollution Abatement Plan, Contributing Zone Plan: Non-residentialAcres\$Sewage Collection SystemL.F.\$Lift Stations without sewer linesAcres\$Underground or Aboveground Storage Tank FacilityTanks\$Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Recharge Zone	🔀 Contributing Zone	Transiti	on Zone
Water Pollution Abatement Plan, Contributing Zone Plan: One Single Family Residential DwellingAcresWater Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks120.6 AcresWater Pollution Abatement Plan, Contributing Zone Plan: Non-residentialAcresPlan: Non-residentialAcresSewage Collection SystemL.F.Lift Stations without sewer linesAcresUnderground or Aboveground Storage Tank FacilityTanksPiping System(s)(only)EachExceptionEachExtension of TimeEach	Type of F	lan	Size	Fee Due
Plan: One Single Family Residential DwellingAcres\$Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks120.6 Acres\$ 8,000Water Pollution Abatement Plan, Contributing Zone Plan: Non-residentialAcres\$Sewage Collection SystemL.F.\$Lift Stations without sewer linesAcres\$Underground or Aboveground Storage Tank FacilityTanks\$Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Water Pollution Abatement Pla	an, Contributing Zone		
Water Pollution Abatement Plan, Contributing Zone Plan: Multiple Single Family Residential and Parks120.6 Acres\$ 8,000Water Pollution Abatement Plan, Contributing Zone Plan: Non-residentialAcres\$Sewage Collection SystemL.F.\$Lift Stations without sewer linesAcres\$Underground or Aboveground Storage Tank FacilityTanks\$Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Plan: One Single Family Reside	ntial Dwelling	Acres	\$
Plan: Multiple Single Family Residential and Parks120.6 Acres\$ 8,000Water Pollution Abatement Plan, Contributing Zone Plan: Non-residentialAcres\$Sewage Collection SystemL.F.\$Lift Stations without sewer linesAcres\$Underground or Aboveground Storage Tank FacilityTanks\$Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Water Pollution Abatement Pla	an, Contributing Zone		
Water Pollution Abatement Plan, Contributing Zone Plan: Non-residentialAcresSewage Collection SystemL.F.Lift Stations without sewer linesAcresUnderground or Aboveground Storage Tank FacilityTanksPiping System(s)(only)EachExceptionEachExtension of TimeEach	Plan: Multiple Single Family Re	sidential and Parks	120.6 Acres	\$ 8,000
Plan: Non-residentialAcres\$Sewage Collection SystemL.F.\$Lift Stations without sewer linesAcres\$Underground or Aboveground Storage Tank FacilityTanks\$Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Water Pollution Abatement Pla	an, Contributing Zone		
Sewage Collection SystemL.F.\$Lift Stations without sewer linesAcres\$Underground or Aboveground Storage Tank FacilityTanks\$Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Plan: Non-residential		Acres	\$
Lift Stations without sewer linesAcres\$Underground or Aboveground Storage Tank FacilityTanks\$Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Sewage Collection System		L.F.	\$
Underground or Aboveground Storage Tank FacilityTanks\$Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Lift Stations without sewer line	es .	Acres	\$
Piping System(s)(only)Each\$ExceptionEach\$Extension of TimeEach\$	Underground or Aboveground	Storage Tank Facility	Tanks	\$
ExceptionEach\$Extension of TimeEach\$	Piping System(s)(only)		Each	\$
Extension of Time Each \$	Exception		Each	\$
	Extension of Time		Each	\$

Signature: _ 1 of 2

TCEQ-0574 (Rev. 02-24-15)

Application Fee Schedule

Texas Commission on Environmental Quality

Edwards Aquifer Protection Program 30 TAC Chapter 213 (effective 05/01/2008)

Water Pollution Abatement Plans and Modifications

Contributing Zone Plans and Modifications

	Project Area in	
Project	Acres	Fee
One Single Family Residential Dwelling	< 5	\$650
Multiple Single Family Residential and Parks	< 5	\$1,500
	5 < 10	\$3,000
	10 < 40	\$4,000
	40 < 100	\$6 <i>,</i> 500
	100 < 500	\$8,000
	≥ 500	\$10,000
Non-residential (Commercial, industrial,	< 1	\$3,000
institutional, multi-family residential, schools, and	1 < 5	\$4,000
other sites where regulated activities will occur)	5 < 10	\$5,000
	10 < 40	\$6 <i>,</i> 500
	40 < 100	\$8,000
	≥ 100	\$10,000

Organized Sewage Collection Systems and Modifications

Project	Cost per Linear Foot	Minimum Fee- Maximum Fee
Sewage Collection Systems	\$0.50	\$650 - \$6,500

Underground and Aboveground Storage Tank System Facility Plans and Modifications

Project	Cost per Tank or Piping System	Minimum Fee- Maximum Fee
Underground and Aboveground Storage Tank Facility	\$650	\$650 - \$6,500

Exception Requests

Project	Fee
Exception Request	\$500

CORE DATA FORM



TCEQ Core Data Form

For detailed instructions on completing this form, please read the Core Data Form Instructions or call 512-239-5175.

SECTION I: General Information

1. Reason for Submission (If other is checked please describe in space provided.)							
New Permit, Registration or Authorization (Core Data Form should be submitted with the program application.)							
Renewal (Core Data Form should be submitted with the	Renewal (Core Data Form should be submitted with the renewal form) Other						
2. Customer Reference Number (<i>if issued</i>) Follow this link to search for CN or PN numbers in 3. Regulated Entity Reference Number (<i>if issued</i>)							
CN 605112077 Central Registry** RN 110606126							

SECTION II: Customer Information

4. General Customer Information 5. Effective Date for Customer Information Updates (mm/dd/yyyy)											
New Custor	New Customer Update to Customer Information Change in Regulated Entity Ownership Change in Legal Name (Verifiable with the Texas Secretary of State or Texas Comptroller of Public Accounts)										
The Custome	The Customer Name submitted here may be updated automatically based on what is current and active with the Texas Secretary of State										
(SOS) or Texa	s Comptro	oller of Public Accou	nts (CPA).								
6. Customer	Legal Nam	ie (If an individual, prii	nt last name first	: eg: Doe, Jo	ohn)			<u>If new Customer, e</u>	enter pre	vious Custom	<u>er below:</u>
Hwy 29 Ventur	es 2015 LP										
7. TX SOS/CP	A Filing N	umber	8. TX State Ta	x ID (11 di	gits)			9. Federal Tax II	D	10. DUNS	Number (if
								(9 digits)		applicable)	
475180278											
11. Type of C	ustomer:	Corporat	ion				🗌 Individ	lual	Partne	rship: 🗌 Ger	neral 🔀 Limited
Government:	City 🗌 🤇	County 🗌 Federal 🗌	Local 🗌 State [Other			Sole Pr	roprietorship	🗌 Oth	ner:	
12. Number o	of Employ	ees						13. Independen	ntly Own	ned and Ope	erated?
⊠ 0-20 □ 2	21-100	101-250 251-	500 🗌 501 ar	nd higher				🛛 Yes 🛛 [No		
14. Customer	Role (Pro	posed or Actual) – <i>as i</i>	t relates to the R	egulated En	ntity list	ed on t	this form. I	Please check one of	the follo	wing	
Owner	lliconsoo	Operator	Own	er & Opera	tor			Other:			
				п дол дрр	licant						
15. Mailing	4910 Can	npus Drive									
Address:											
	City	Newport Beach		State	CA		ZIP	92660		ZIP + 4	
16. Country Mailing Information (if outside USA) 17. E-Mail Address (if applicable)						e)					
						tom	r@shamro	ckcommunities.com	ı		

18. Telephone Number	19. Extension or Code	20. Fax Number (if applicable)
(949) 922-2512		() -

SECTION III: Regulated Entity Information

21. General Regulated Entity Information (If 'New Regulated Entity" is selected, a new permit application is also required.)								
New Regulated Entity	🔀 New Regulated Entity 🗌 Update to Regulated Entity Name 🔲 Update to Regulated Entity Information							
The Regulated Entity Nar	ne submitted	may be updated, i	n order to mee	t TCEQ Core	e Data Stan	dards (removal of o	rganization	al endings such
as Inc, LP, or LLC).								
22. Regulated Entity Nam	ie (Enter name	of the site where the	regulated action	is taking pla	ce.)			
Lively Tract, Phase 2 CZP								
23. Street Address of								
the Regulated Entity:								
<u>(No PO Boxes)</u>	City		State		ZIP		ZIP + 4	
24. County								

If no Street Address is provided, fields 25-28 are required.

25. Description to	West of Inte	rsection of TX Hwy	29 and Cross Creek	Road.				
Physical Location:								
26. Nearest City						State	Nea	rest ZIP Code
Leander						ТХ	7862	28
Latitude/Longitude are r	equired and	may be added/u	pdated to meet T	CEQ Core D	ata Standar	ds. (Geocoding of t	he Physical	Address may be
used to supply coordinate	es where no	ne have been pro	vided or to gain o	accuracy).				
27. Latitude (N) In Decim	al:	30.636983		28. Lo	ongitude (W) In Decimal:	97.80031	1
Degrees	Minutes	S	econds	Degree	25	Minutes		Seconds
30		38	13.14		97	48	5	1.12
29. Primary SIC Code	30.	Secondary SIC Co	de	31. Primar	y NAICS Coo	le 32. Sec	ondary NAI	CS Code
(4 digits)	(4 d	igits)		(5 or 6 digit	s)	(5 or 6 d	igits)	
1521	179	4		236115		238990		
33. What is the Primary E	Business of t	his entity? (Do r	not repeat the SIC or	NAICS descri	ption.)			
Single Family Residential Sub	division							
34. Mailing								
Address:		1	•	1				
	City		State		ZIP		ZIP + 4	
35. E-Mail Address:			1					
36. Telephone Number			37. Extension or (Code	38. Fa	x Number (if applica	ible)	
() -					()	-		

39. TCEQ Programs and ID Numbers Check all Programs and write in the permits/registration numbers that will be affected by the updates submitted on this form. See the Core Data Form instructions for additional guidance.

Dam Safety	Districts	Edwards Aquifer	Emissions Inventory Air	Industrial Hazardous Waste
Municipal Solid Waste	New Source Review Air	OSSF	Petroleum Storage Tank	D PWS
Sludge	Storm Water	Title V Air	Tires	Used Oil
Voluntary Cleanup	Wastewater	Wastewater Agriculture	Water Rights	Cther:

SECTION IV: Preparer Information

40. Name:	Pape-Dawson Consulting Engineers, LLC			41. Title:	
42. Telephone	e Number	43. Ext./Code	44. Fax Number	45. E-Mail Address	
(512)44-8711			() -	tkrause@pape-dawson.com	

SECTION V: Authorized Signature

46. By my signature below, I certify, to the best of my knowledge, that the information provided in this form is true and complete, and that I have signature authority to submit this form on behalf of the entity specified in Section II, Field 6 and/or as required for the updates to the ID numbers identified in field 39.

Company:	Pape-Dawson Consulting Engineers, LLC Job Title: Vice President			
Name (In Print):	Dustin Goss, P.E., LEED® AP		Phone:	(512)454-8711
Signature:	Mas		Date:	4/8/25

CONSTRUCTION PLANS

STATE OF TEXAS COUNTY OF WILLIAMSON



SUBMITTED BY:

PAPE-DAWSON ENGINEERS

REVIEWED BY THE CITY ENGINEER(S)

DUSTIN J. GOSS, P.E. #91805

VICE PRESIDENT



VICINITY MAP NOT TO SCALE

NOTE:

STREET IMPROVEMENTS TO BE DEDICATED TO WILLIAMSON COUNTY WATER & WASTEWATER IMPROVEMENTS TO BE DEDICATED TO CITY OF LEANDER. DRAINAGE IMPROVEMENTS TO BE DEDICATED TO WEST WILLIAMSON COUNTY MUNICIPAL UTILITY DISTRICT NO. 2. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE TH EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES. TOTAL ACREAGE: 120.6 ACRES DISTURBED ACREAGE: 120.6 ACRES REVISION # DESCRIPTION APPROVAL DATE

S DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED FLECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANT'S ORIGINAL SIGNATURE AND SEA

WEST WILLIAMSON COUNTY MUNICIPAL UTILITY DISTRICT No. 2 LIVELY TRACT, PHASE 2 CITY OF LEANDER, TX

PUBLIC IMPROVEMENTS MODIFIED CZP **CONSTRUCTION PLANS**



LOCATION MAP NOT-TO-SCALE

HWY 29 VENTURES 2015 L.P. 4910 CAMPUS DRIVE NEWPORT BEACH, CA 92660

APRIL 2025



AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10801 N MOPAC EXPY, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711 TBPE FIRM REGISTRATION #470 | TBPLS FIRM REGISTRATION #10028801

ENGINEER: PAPE-DAWSON ENGINEERS

10801 N. MoPac Expy., Bldg 3, Suite 200 AUSTIN, TEXAS 78759 (512) 454-8711 F (512) 459-8867

OWNER: HWY 29 VENTURES 2015 L.P. 4910 CAMPUS DRIVE NEWPORT BEACH, CA

SURVEYOR:

(949) 955-3700

PAPE-DAWSON ENGINEERS 10801 N. MoPac Expy., Bldg 3, Suite 200 AUSTIN, TEXAS 78759 (512) 454-8711 F (512) 459-8867

	Sheet List Table
Sheet Number	
1	COVER SHELL
2	
3	CONSTRUCTION NOTES (2 of 3)
4	CONSTRUCTION NOTES (3 of 3)
5	CONDITIONS
EROSION & SEDIME	ENTATION CONTROL
6	PHASE 6 ESC
7	PH 5 EXISTING ESC
8	PH 4 EXISTING ESC
9	PH 2 EXISTING ESC (1 OF 2)
10	PH 2 EXISTING ESC (2 OF 2)
PHASE 2 EXISTING	STORM DRAIN
11	PH 2 SD OVERALL (1)
12	PH 2 SD OVERALL (2)
13	PH 2 DRAINAGE CALCULATIONS
14	PH 2 SD-B11.1 (1)
15	PH 2 SD-B11.1 (2)
16	PH 2 SD-B LATERALS
17	PH 2 SD-B12.1
PHASE 4 EXISTING	STORM DRAIN
18	PH 4 SD OVERALL
19	PH 4 DRAINAGE CALCULATIONS
20	LINE B-CH (1 OF 2)
21	LINE B-CH (2 OF 2)
22	LINE SD-B1.01 (2 OF 2)
23	LINE SD-B1.01 (1 OF 2)
24	LATERALS B1.02–B1.07
25	LINE B11.01 & B11.06-B11.08
26	LINE J-CH
27	LINE J1.01
28	LINE J2.01 (1 OF 2)
29	LINE J2.01 (2 OF 2)
30	LATERALS J2.02–J2.08
31	LINE J3.01
PHASE 5 EXISTING	STORM DRAIN
32	PH 5 SD OVERALL
33	PH 5 SD OVERALL (2 of 3)
34	PH 5 SD OVERALL (3 of 3)
35	PH 5 DRAINAGE CALCULATIONS (1 of 2)
36	PH 5 DRAINAGE CALCULATIONS (2 of 2)
37	LINE SD-B1.01 (1 of 3)
38	LINE SD-B1.01 (2 of 3)
39	LINE SD-B1.01 (3 of 3) & LATERALS B1.08-B1.09
40	LINE SD-B1.01 LATERALS B1.10-B1.17
41	UNE SD-B2.01
42	LINE SD-B2.01 LATERALS B2.02-B2.07
43	LINE SD-B3.01
44	LINE SD-B3.01 LATERALS B3.02-B3.08
45	LINE SD-B4.01
46	LINE SD-B4.01 LATERALS B4.02-B4.11
47	LINE SD-B5.01 & LATERAL B5.02
48	LINE SD-B6.01
49	LINE SD-B6.01 LATERALS B6.07-B6.13
50	LINE SD-B7.01 (1 of 2)
51	LINE SD-B7.01 (2 of 2) & LATERALS B7.02-B7.04
52	LINE SD-B7.01 LATERALS B7.05-B7.12
53	LINE SD-B8.01 & LATERAL B8.02
54	LINE SD-B12.01 (1 of 2)
55	LINE SD-B12.01 (2 of 2) & LATERALS B12.02-B12.04
56	LINE SD-B12.01 LATERALS B12.05-B12.09
57	LINE J1.01 (1 of 2)
58	LINE J1.01 (2 of 2)
59	
60	LINE .13.01 & LATERALS .13.02-3.03

Sh	eet List Table		
Sheet Number Sheet Title			
PHASE 6 STORM D	RAIN		
61	PH 6 SD OVERALL		
62	PH 6 DRAINAGE CALCULATIONS (1 of 2)		
63	PH 6 DRAINAGE CALCULATIONS (2 of 2)		
64	SD-B6.01		
65	SD-B6.01 LATERALS B6.02-B6.09		
66	SD-B6.01 LATERALS B6.10-B6.13 & B1.16-B1.17		
67	SD-B7.01 LATERALS B7.05-B7.12		
68	SD-B9.01 & LATERALS B9.02-B9.05		
69	69 SD 10.01 & LATERALS B10.03-B10.04		
POND PLAN			
70	PH 4 EXISTING POND J		
71	1 PH 4 EXISTING POND J DETAILS		
72	PH 2 EXISTING POND H		
73	PH 2 EXISTING POND H DETAILS (1 OF 2)		
74	PH 2 EXISTING POND H DETAILS (2 OF 2)		
75	ELECTRICAL NOTES SYMBOLS & ABBREVIATIONS		
76	ELECTRICAL SPECIFICATIONS		
77	ELECTRICAL OVERALL SITE PLAN		
78	ELECTRICAL SITE PLAN POND J		
79	PH 2 EXISTING ELECTRICAL SITE PLAN POND H		
80	ELECTRICAL LADDER DIAGRAM		
81	ELECTRICAL DETAILS		
CONSTRUCTION DET	TAILS		
82	EROSION & SEDIMENTATION CONTROL		
83	83 DRAINAGE		



sheet <u>1 of</u> 83

CITY OF LEANDER GENERAL NOTES (03/27/2023)	CITY OF LEAN
CITY CONTACTS:	1. CALL CIT WORK. C
ENGINEERING MAIN LINE: 512–528–2721 PLANNING DEPARTMENT: 512–528–2750 PUBLIC WORKS MAIN LINE: 512–259–2640 STORMWATER INSPECTIONS: 512–285–0055	ANY WOR 2. THE CON MEASURE
UTILITIES MAIN LINE: 512-259-1142 UTILITIES ON-CALL: 512-690-4760	3. THE OWN
PEC CONTACTS: PUBLIC SAFETY LINE: 1–888–343–7702	4. WITH THE
CUSTOMER OUTAGE LINE: 1-800-396-9037 1. CONTRACTORS SHALL HAVE AN APPROVED SET OF PLANS WITH APPROVED REVISIONS ONSITE AT ALL TIMES. FAILURE TO HAVE APPROVED PLANS ON SITE MAY RESULT IN ISSUANCE OF WORK STOPPAGE.	TEMPORA EXCAVATI LOW-LEV
2. CONTACT 811 SYSTEM FOR EXISTING WATER AND WASTEWATER LOCATIONS 48 HOURS PRIOR TO	REQUIRED
a. REFRESH ALL LOCATES <u>BEFORE</u> 14 DAYS – LOCATE REFRESH REQUESTS <u>MUST INCLUDE A COPY OF</u> <u>YOUR 811 TICKET</u> . TEXAS PIPELINE DAMAGE PREVENTION LAWS REQUIRE THAT A LOCATE REFRESH	6. DELIVER
REQUEST BE SUBMITTED BEFORE 14 DAYS, OR IF LOCATION MARKERS ARE NO LONGER VISIBLE. b. REPORT PIPELINE DAMAGE IMMEDIATELY — IF YOU WITNESS OR EXPERIENCE PIPELINE EXCAVATION DAMAGE, PLEASE CONTACT THE CITY OF LEANDER BY PHONE AT 512—259—2640.	7. ROUGH G AS REQU BASE THI
3. THE CONTRACTOR SHALL CONTACT THE CITY INSPECTOR 48 HOURS BEFORE: a. BEGINNING EACH PHASE OF CONSTRUCTION. CONTACT ASSIGNED CITY INSPECTOR. b. ANY TESTING CONTRACTOR SHALL PROVIDE QUALITY TESTING FOR ALL INFRASTRUCTURES TO BE	8. DELIVER
ACCEPTED AND MAINTAINED BY THE CITY OF LEANDER AFTER COMPLETION. c. PROPERDING SUB-GRADE AND EVERY LIFT OF ROADWAY EMBANKMENT, IN-PLACE DENSITY TESTING	9. INSTALL /
OF EVERY BASE COURSE, AND ASPHALT CORES. ALL OF THIS TESTING MUST BE WITNESSED BY A CITY OF LEANDER REPRESENTATIVE. d. CONNECTING TO THE EXISTING WATER LINES.	11. BEGIN IN
e. THE INSTALLATION OF ANY DRAINAGE FACILITY WITHIN A DRAINAGE EASEMENT OR STREET ROW. THE METHOD OF PLACEMENT AND COMPACTION OF BACKFILL IN THE CITY'S ROW MUST BE APPROVED PRIOR	AS POSS PLANS.
4. ALL RESPONSIBILITILY FOR THE ACCURACY OF THESE PLANS REMAINS WITH THE ENGINEER OF RECORD WHO	12. DELIVER
PREPARED THEM. IN REVIEWING THESE PLANS, THE CITY MUST RELY ON THE ADEQUACY OF THE WORK OF THE ENGINEER OF RECORD.	14. INSURE
5. EXCESS SOIL SHALL BE REMOVED AT THE CONTRACTOR'S EXPENSE. NOTIFY THE CITY OF LEANDER IF THE DISPOSAL SITE IS INSIDE THE CITY'S JURISDICTIONAL BOUNDARIES.	MATERIAL
6. BURNING IS PROHIBITED.	16. LAY FINA
7. NO WORK IS TO BE PERFORMED BETWEEN THE HOURS OF 9:00 P.M. AND 7:00 A.M. OR WEEKENDS. THE CITY INSPECTOR RESERVES THE RIGHT TO REQUIRE THE CONTRACTOR TO UNCOVER ALL WORK PERFORMED	17. LAY ASPI
WITHOUT INSPECTION. 8. CONTACT THE CITY INSPECTOR 4 DAYS PRIOR TO WORK FOR APPROVAL TO SCHEDULE ANY INSPECTIONS	18. COMPLET
ON WEEKENDS OR CITY HOLIDAYS.	CONSTRU
9. NO BLASTING IS ALLOWED. 10. ANY CHANGES OR REVISIONS TO THESE PLANS MUST FIRST BE SUBMITTED TO THE CITY BY THE DESIGN	20. COMPLET
ENGINEER FOR REVIEW AND WRITTEN APPROVAL PRIOR TO CONSTRUCTION OF THE REVISION. ALL CHANGES AND REVISIONS SHALL USE REVISION CLOUDS TO HIGHLIGHT ALL REVISIONS AND CHANGES WITH EACH SUBMITTAL REVISION TRIANCLE MARKERS AND NUMBERS SHALL REVISIONS AND CHANGES WITH EACH	21. REMOVE
CLOUDS AND TRIANGLE MARKERS AND NUMBERS SHALL BE USED TO MARK REVISIONS. ALL CLOUDS AND TRIANGLE MARKERS FROM PREVIOUS REVISIONS MUST BE REMOVED. REVISION INFORMATION SHALL BE UPDATED ON COVER SHEET AND AFFECTED PLAN SHEET TITLE BLOCK.	23. IF DISTUR BE STABI
11. THE CONTRACTOR AND ENGINEER SHALL KEEP ACCURATE RECORDS OF ALL CONSTRUCTION THAT DEVIATES FROM THE PLANS. THE ENGINEER SHALL FURNISH THE CITY OF LEANDER ACCURATE "RECORD DRAWINGS" FOLLOWING THE COMPLETION OF ALL CONSTRUCTION.THESE "RECORD DRAWINGS' SHALL MEET THE SATISFACTION OF THE ENGINEERING DEPARTMENTS PRIOR TO FINAL ACCEPTANCE.	CITY OF LE
12. THE CONTRACTOR WILL REIMBURSE THE CITY FOR ALL REPAIR AND/OR COST INCURRED AS A RESULT OF ANY DAMAGE TO ANY PUBLIC INFRASTRUCTURE WITHIN CITY EASEMENT OR PUBLIC RIGHT-OF-WAY, REGARDLESS OF THESE PLANS.	CONTRAC MAKE AN REMOVED
13. WHEN CONSTRUCTION IS BEING CARRIED OUT WITHIN EASEMENTS, THE CONTRACTOR SHALL CONFINE HIS WORK TO WITHIN THE PERMANENT AND TEMPORARY EASEMENTS. PRIOR TO ACCEPTANCE, THE CONTRACTOR SHALL BE RESPONSIBLE FOR REMOVING ALL TRASH AND DEBRIS WITHIN THE PERMANENT EASEMENTS. CLEANUP SHALL BE TO THE SATISFACTION OF THE ENGINEER OF RECORD AND CITY.	2. THE TEMP 3. ANY ON- SHOWN OI
14. CONTRACTOR TO LOCATE, PROTECT, AND MAINTAIN BENCHMARKS, MONUMENTS, CONTROL POINTS AND PROJECT ENGINEERING REFERENCE POINTS. RE-ESTABLISH DISTURBED OR DESTROYED ITEMS BY REGISTERED PROFESSIONAL LAND SURVEYOR IN THE STATE OF TEXAS, AT NO ADDITIONAL COST TO THE PROPERTY OWNER.	4. ALL AREA INCHES O HOME CO COMPOST.
15. ALL CONSTRUCTION OPERATIONS SHALL BE ACCOMPLISHED IN ACCORDANCE WITH APPLICABLE REGULATIONS OF THE U.S. OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA). OSHA STANDARDS MAY BE PURCHASED FROM THE GOVERNMENT PRINTING OFFICE; INFORMATION AND RELATED REFERENCE MATERIALS MAY BE PURCHASED FROM OSHA 1033 LA POSADA DR SUITE 375 AUSTIN	5. SEEDING WILLIAMSC EROSION
TEXAS 78752-3832.	6. STABILIZE EXITING
16. ALL MANHOLE FRAMES/COVERS AND WATER VALVE/METER BOXES MUST BE ADJUSTED TO FINISHED GRADE AT THE OWNER'S EXPENSE BY THE CONTRACTOR FOR CITY CONSTRUCTION INSPECTOR INSPECTION. ALL UTILITY ADJUSTMENTS SHALL BE COMPLETED PRIOR TO FINAL PAVING. CONTRACTOR SHALL BACKFILL AROUND MANHOLES AND VALVE BOXES WITH CLASS A CONCRETE.	7. TEMPORAF CONDITION
17. ALL MATERIALS AND CONSTRUCTION PROCEDURES WITHIN THE SCOPE OF THIS CONTRACT WHERE NOT SPECIFICALLY COVERED IN THE PROJECT SPECIFICATIONS SHALL CONFORM TO ALL CITY OF LEANDER DETAILS AND CITY OF AUSTIN STANDARD SPECIFICATIONS.	8. IN THE E ^V SHALL RE
18. PROJECT SPECIFICATIONS TAKE PRECEDENCE OVER PLANS AND SPECIAL CONDITIONS GOVERN OVER TECHNICAL SPECIFICATIONS.	CITY OF
19. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ACQUIRING ALL PERMITS, TESTS, APPROVALS AND ACCEPTANCES REQUIRED TO COMPLETE CONSTRUCTION OF THIS PROJECT.	WATER A
20. THE CONTRACTOR MUST OBTAIN A CONSTRUCTION WATER METER FOR ALL WATER USED DURING CONSTRUCTION. A COPY OF THIS PERMIT MUST BE CARRIED AT ALL TIMES BY ALL WHO USE WATER.	1. ALL NE STANDAR
21. THE CONTRACTOR SHALL BE RESPONSIBLE FOR KEEPING ROADS AND DRIVES ADJACENT TO AND NEAR THE SITE FREE FROM SOIL, SEDIMENT AND DEBRIS. CONTRACTOR WILL NOT REMOVE SOIL, SEDIMENT OR DEBRIS FROM ANY AREA OR VEHICLE BY MEANS OF WATER. ONLY SHOVELING AND SWEEPING WILL BE ALLOWED. THE CONTRACTOR WILL BE RESPONSIBLE FOR DUST CONTROL FROM THE SITE. THE CONTRACTOR SHALL KEEP THE SITE AREA CLEAN AND MAINTAINED AT ALL TIMES, TO THE SATISFACTION OF THE CITY. THE SUBDIVISION (OR SITE) WILL NOT BE ACCEPTED (OR CERTIFICATE OF OCCUPANCY ISSUED) UNTIL THE SITE HAS BEEN CLEANED TO THE SATISIFACTION OF THE CITY.	2. ALL WA AS FOLL
22. TREES IN EXISTING ROW SHOULD BE PROTECTED OR NOTED IN THE PLANS TO BE REMOVED.	3. OPEN U WASTEW FNCASE
	4. INTERIOR
	CEMENT-

IDER CONSTRUCTION SEQUENCE NOTES

Y OF LEANDER PUBLIC WORKS DEPARTMENT AT 259-2640 48 HOURS PRIOR TO BEGINNING ANY ALL THE ONE CALL CENTER AT 472-2822 FOR UTILITY LOCATIONS AND OBTAIN PERMIT FOR K WITHIN CITY OF LEANDER R.O.W.

TRACTOR SHALL INSTALL TEMPORARY EROSION/SEDIMENTATION CONTROL AND TREE PROTECTION S AS SHOWN WITHIN THESE PLANS.

ER OR HIS AUTHORIZED REPRESENTATIVE SHALL CONVENE A PRE-CONSTRUCTION CONFERENCE.

APPROVAL OF ALL AFFECTED PARTIES, THE CONTRACTOR MAY BEGIN CLEARING AND GRUBBING.

UT ALL REQUIRED OR NECESSARY PONDS. EITHER THE PERMANENT OUTLET STRUCTURE OR A RY OUTLET MUST BE CONSTRUCTED PRIOR TO DEVELOPMENT OF ANY EMBANKMENT OR ON THAT LEADS TO PONDING CONDITIONS. THE OUTLET SYSTEM MUST CONSIST OF A EL OUTLET AND AN EMERGENCY OVERFLOW MEETING THE REQUIREMENTS OF THE DRAINAGE MANUAL (SECTION 8.3) AND/OR THE ENVIRONMENTAL CRITERIA MANUAL (SECTION 1.4.2.K) AS THE OUTLET SYSTEM SHALL BE PROTECTED FROM EROSION AND SHALL BE MAINTAINED OUT THE COURSE OF CONSTRUCTION UNTIL FINAL RESTORATION IS ACHIEVED.

APPROVED ROUGH CUT SHEETS TO THE CITY OF LEANDER PRIOR TO CLEARING AND GRUBBING.

RADE STREETS. NO DEVELOPMENT OF EMBANKMENT WILL BE PERMITTED AT THIS TIME, EXCEPT RED FOR UTILITY CONSTRUCTION. GEOTECHNICAL ENGINEER TO VERIFY SUBGRADE AND REQUIRED CKNESS.

WATER & WASTEWATER CUT SHEETS TO CITY OF LEANDER.

ALL UTILITIES TO BE LOCATED UNDER THE PROPOSED PAVEMENT.

STORM SEWER CUT SHEETS TO CITY OF LEANDER.

STALLATION OF STORM SEWER LINES. UPON COMPLETION, RESTORE AS MUCH DISTURBED AREA BLE, PARTICULARLY CHANNELS AND LARGE OPEN AREAS. INSTALL INLET PROTECTION AS PER

FINAL GRADE CUT SHEETS TO CITY OF LEANDER.

STREETS TO SUBGRADE.

THAT ALL UNDERGROUND UTILITY CROSSINGS ARE COMPLETED. LAY FIRST COURSE BASE ON ALL STREETS.

CURB AND GUTTER.

BASE COURSE ON ALL STREETS.

HALT.

ALL ROUGH GRADING AND UNDERGROUND INSTALLATIONS WITHIN THE R.O.W.

FINAL GRADING AND INSTALL SIDEWALK IN R.O.W. ALONG AREAS DESIGNATED. RESTORE CTION SPOILS & STAGING AREA TO NATURAL GRADE.

PERMANENT EROSION CONTROL AND RESTORATION OF SITE VEGETATION.

AND DISPOSE OF TEMPORARY EROSION CONTROL, INCLUDING CONSTRUCTION SPOILS AREA.

ANY NECESSARY FINAL DRESS UP OF AREAS DISTURBED.

BED AREA IS NOT TO BE WORKED ON FOR MORE THAN 14 DAYS, DISTURBED AREA NEEDS TO LIZED BY REVEGETATION, MULCH, TARP OR REVEGETATION MATTING.

ANDER EROSION CONTROL NOTES

FRACTOR IS REQUIRED TO INSPECT THE CONTROLS AND FENCES AT WEEKLY INTERVALS AND GNIFICANT RAINFALL EVENTS TO ENSURE THAT THEY ARE FUNCTIONING PROPERLY. THE FOR IS RESPONSIBLE FOR MAINTENANCE OF CONTROLS AND FENCES AND SHALL IMMEDIATELY Y NECESSARY REPAIRS TO DAMAGED AREAS. SILT ACCUMULATION AT CONTROLS MUST BE WHEN THE DEPTH REACHES SIX (6) INCHES.

ORARY SPOILS DISPOSAL SITE IS TO BE SHOWN IN THE EROSION CONTROL MAP.

SITE SPOILS DISPOSAL SHALL BE REMOVED PRIOR TO ACCEPTANCE UNLESS SPECIFICALLY IN THE PLANS. THE DEPTH OF SPOIL SHALL NOT EXCEED 10 FEET IN ANY AREA.

AS DISTURBED OR EXPOSED DURING CONSTRUCTION SHALL BE RESTORED WITH A MINIMUM OF 6 TOPSOIL AND COMPOST BLEND. TOPSOIL ON SINGLE FAMILY LOTS MAY BE INSTALLED WITH NSTRUCTION. THE TOPSOIL AND COMPOST BLEND SHALL CONSIST OF 75% TOPSOIL AND 25%

FOR REESTABLISHING VEGETATION SHALL COMPLY WITH THE AUSTIN GROW GREEN GUIDE OR IN COUNTY'S PROTOCOL FOR SUSTAINABLE ROADSIDES (SPEC 164--WCOO1 SEEDING FOR CONTROL). RESEEDING VARIETIES OF BERMUDA SHALL NOT BE USED.

D CONSTRUCTION ENTRANCE IS REQUIRED AT ALL POINTS WHERE CONSTRUCTION TRAFFIC IS THE PROJECT ONTO EXISTING PAVEMENT. LINEAR CONSTRUCTION PROJECTS MAY REQUIRE CONSIDERATION. ROADWAYS SHALL REMAIN CLEAR OF SILT AND MUD.

RY STOP SIGNS SHOULD BE INSTALLED AT ALL CONSTRUCTION ENTRANCES WHERE A STOP DOES NOT ALREADY EXIST.

/ENT OF INCLEMENT WEATHER THAT MAY RESULT IN A FLOODING SITUATION. THE CONTRACTOR MOVE INLET PROTECTION MEASURES UNTIL SUCH TIME AS THE WEATHER EVENT HAS PASSED.

LEANDER WATER AND WASTEWATER NOTES (7/22/24)

ND WASTEWATER GENERAL NOTES

WLY INSTALLED PIPES AND RELATED PRODUCTS MUST CONFORM TO AMERICAN NATIONAL RDS INSTITUTE/NATIONAL SANITATION FOUNDATION (ANSI/NSF) STANDARD 61 AND MUST BE ED BY AN ORGANIZATION ACCREDITED BY ANSI.

FER SERVICE, WASTEWATER SERVICE AND VALVE LOCATIONS SHALL BE APPROPRIATELY STAMPED OWS:

WATER SERVICE	"W" ON	TOP	OF	CURE
WASTEWATER SERVICE	"S" ON	TOP	OF	CURE
VALVE	"V" ON	TOP	OF	CURE

TILITIES SHALL NOT BE PERMITTED ACROSS THE EXISTING PAVED SURFACES. WATER AND ATER LINES ACROSS THE EXISTING PAVED SURFACES SHALL BE BORED AND INSTALLED IN STEEL MENT PIPES. BELL RESTRAINTS SHALL BE PROVIDED AT JOINTS.

SURFACES OF ALL DUCTILE IRON POTABLE OR RECLAIMED WATER PIPE SHALL BE -MORTAR LINED AND SEAL COATED AS REQUIRED BY AWWA C104.

5. SAND, AS DESCRIBED IN AUSTIN SPECIFICAT AS BEDDING FOR WATER AND WASTEWATER ARE PIPE BEDDING STONE, PEA GRAVEL OCCURRING OR MANUFACTURED STONE MAT STONE QUALITY AND MEETING THE FOLLOWING

SIEVE	SIZE	PERCENT	RETAI
	1/2"		0
	3/8"		0-2
	#4		40-8
	<i>"</i> #10		95-1

6. DENSITY TESTING FOR TRENCH BACKFILL SHA

WATER

- 1. SAMPLING TAPS SHALL BE BROUGHT UP TO EASILY ACCESSIBLE FOR CITY PERSONNEL. HIS PRESENCE, SAMPLES FOR BACTERIOLOGIC CITY OF LEANDER NOT LESS THAN 24 HOUI FLUSHED OF THE CONCENTRATED CHLORINE APPROVED BY THE CITY.
- 2. CITY PERSONNEL WILL OPERATE OR AUTHOR WATER VALVES THAT WILL PASS THROUG CONTRACTOR MAY BE FINED \$500 OR M WATER FINES, IF A WATER VALVE IS OPE REGARDLESS OF WHO OPERATED THE VALVE.
- 3. THE CONTRACTOR IS HEREBY NOTIFIED THA TERMINATING EXISTING UTILITY LINES MAY SUCH HOURS ARE USUALLY OUTSIDE NO BETWEEN 12 AM AND 6 AM AFTER CO INSPECTORS AND INFORMING AFFECTED PROF
- 4. PRESSURE TAPS OR HOT TAPS SHALL BE STANDARD SPECIFICATIONS. THE CONTRACTO SHALL FURNISH, INSTALL AND AIR TEST LEANDER INSPECTOR MUST BE PRESENT W AND/OR ASSOCIATED TESTS. A MINIMUM REQUIRED. "SIZE ON SIZE" TAPS SHALL NOT USE OF AN APPROVED FULL-CIRCLE GASKET BLOCKS SHALL BE PLACED BEHIND AND UND HOURS PRIOR TO THE BRANCH BEING PLACE BE INSPECTED PRIOR TO BACKFILL.
- 5. FIRE HYDRANTS ON MAINS UNDER CONSTR WITH A BLACK POLY WRAP BAG AND TAPED REMOVED WHEN THE MAINS ARE ACCEPTED
- 6. THRUST BLOCKS OR RESTRAINTS SHALL E LEANDER STANDARD SPECIFICATIONS AND RE MANUFACTURER'S RECOMMENDATION. ALL BLOCKS AND RESTRAINTS.
- 7. ALL DEAD END WATER MAINS SHALL HAVE 'FIRE HYDRANT ASSEMBLY' OR 'BLOW-OFF VALVE AND THRUST BLOCK" OR "BLOW-OFF VALVE AND THRUST RESTRAINTS". THRUST RESTRAINTS SHALL BE INSTALLED ON THE MINIMUM LAST THREE PIPE LENGTHS (STANDARD 20' LAYING LENGTH). ADDITIONAL THRUST RESTRAINTS MAY BE REQUIRED BASED UPON THE MANUFACTURERS RECOMMENDATION AND/OR ENGINEER'S DESIGN.
- 8. PIPE MATERIAL FOR PUBLIC WATER MAINS SHALL BE PVC (AWWA C900-DR14 MIN. 305 PSI PRESSURE RATING). WATER SERVICES (2"OR LESS) SHALL BE POLYETHYLENE TUBING (BLACK, 200PSI, AND SDR-(9)). COPPER PIPES AND FITTINGS ARE NOT ALLOWED IN THE PUBLIC RIGHT OF WAY. ALL PLASTIC PIPES FOR USE IN PUBLIC WATER SYSTEMS MUST BEAR THE NATIONAL SANITATION FOUNDATION SEAL OF APPROVAL (NSF-PW).
- 9. ALL FIRE HYDRANT LEADS SHALL BE DUCTILE IRON PIPE (AWWA C115/C151 PRESSURE CLASS 350).
- 10. ALL IRON PIPE AND FITTINGS SHALL BE WRAPPED WITH MINIMUM 8-MIL POLYETHYLENE.
- 11. LINE FLUSHING OR ANY ACTIVITY USING A LARGE QUANTITY OF WATER MUST BE COORDINATED WITH THE PUBLIC WORKS DEPARTMENT.
- 12. ALL WATER METER BOXES SHALL BE:
 - a. SINGLE, 1"METER AND BELOW DFW37F-12-1CA, OR EQUAL b. DUAL. 1"METERS AND BELOW DFW39F-12-1CA. OR EQUAL
 - c. 1.5" SINGLE METER DFW65C-14-1CA, OR EQUAL
 - d. 2" SINGLE METER DFW1730F-12-1CA, OR EQUAL

13. ALL WATER VALVE COVERS ARE TO BE PAINTED BLUE. WASTEWATER NOTES:

- 1. CURVILINEAR WASTEWATER DESIGN LAYOUT IS NOT PERMITTED.
- 2. MANDREL TESTING SHALL BE CONDUCTED AFTER THE FINAL BACKFILL HAS BEEN IN

PLACE AT LEAST 30 DAYS.

- 3. MANHOLES SHALL BE COATED PER CITY OF AUSTIN SPL WW-511 (RAVEN 405 OR SPRAYWALL). PENETRATIONS TO EXISTING WASTEWATER MANHOLES REQUIRE THE CONTRACTOR TO RECOAT THE ENTIRE MANHOLE IN ACCORDANCE WITH CITY OF AUSTIN STANDARD SPECIFICATIONS SECTION NO. 506.5.
- 4. RECLAIMED AND RECYCLED WATER LINE SHALL BE CONSTRUCTED OF "PURPLE PIPE." ALL RECLAIMED AND RECYCLED WATER VALVE COVERS SHALL BE SQUARE AND PAINTED PURPLE.
- 5. FORCE MAIN PIPES NEED TO HAVE SWEEPING WYES FOR JOINTS.

ION ITEM 510 PIPE, SHALL NOT BE USED LINES. ACCEPTABLE BEDDING MATERIALS AND IN LIEU OF SAND, A NATURALLY TERIAL CONFORMING TO ASTM C33 FOR G GRADATION SPECIFICATION:
TAINED BY WEIGHT
-2)-85)-100
ALL BE DONE IN MAXIMUM 12" LIFTS.
D 3 FEET ABOVE GRADE AND SHALL BE AT THE CONTRACTORS' REQUEST, AND IN CAL TESTING WILL BE COLLECTED BY THE IRS AFTER THE TREATED LINE HAS BEEN E SOLUTION AND CHARGED WITH WATER
RIZE THE CONTRACTOR TO OPERATE ALL GH THE CITY'S POTABLE WATER. THE IORE, INCLUDING ADDITIONAL THEFT OF ERATED IN AN UNAUTHORIZED MANNER,
AT CONNECTING TO, SHUTTING DOWN, OR HAVE TO OCCUR AT OFF-PEAK HOURS. ORMAL WORKING HOURS AND POSSIBLY DORDINATING WITH CITY CONSTRUCTION PERTIES.
IN ACCORDANCE WITH CITY OF LEANDER OR SHALL PERFORM ALL EXCAVATION AND THE SLEEVE AND VALVE. A CITY OF WHEN THE CONTRACTOR MAKES A TAP, OF TWO (2) WORKING DAYS NOTICE IS T BE PERMITTED UNLESS MADE BY THE TED TAPPING SLEEVE. CONCRETE THRUST DER ALL TAP SLEEVES A MINIMUM OF 24 ED INTO SERVICE. THRUST BLOCKS SHALL
RUCTION SHALL BE SECURELY WRAPPED INTO PLACE. THE POLY WRAP SHALL BE AND PLACED INTO SERVICE.
BE IN ACCORDANCE WITH THE CITY OF EQUIRED AT ALL FITTINGS PER DETAIL OR FITTINGS SHALL HAVE BOTH THRUST

	DATE
	NO. REVISION
	DUSTIN J. GOSS 91805 91805 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	THE FIRM REGISTRATION #701 TEPLS FIRM REGISTRATION #10028801
	LIVELY TRACT, PHASE 6 CITY OF LEANDER, TEXAS CONSTRUCTION NOTES (1 OF 3)
CITY OF LEANDER APPROVAL	CITY NO JOB NO DATE DATE JANUARY 2025 DESIGNER BB CHECKED TCK DRAWN DY/SL SHEET

<u>CI</u>	TY OF LEANDER STREET AND DRAINAGE NOTES	27. CONTRA OVERB
1.	THE CITY OF LEANDER HAS NOT REVIEWED THESE PLANS FOR COMPLIANCE WITH THE AMERICANS WITH DISABILITIES ACT (ADA). IT IS THE RESPONSIBILITY OF THE OWNER TO PROVIDE COMPLIANCE WITH ALL LEGISLATION RELATED TO ACCESSIBLITY WITHIN THE LIMITS OF CONSTRUCTION SHOWN IN THESE PLANS. ALL SIDEWALKS SHALL COMPLY WITH THE AMERICANS WITH DISABILITIES ACT AND TEXAS ACCESSIBILITY STANDARDS (TAS).	TRENCH S 1. TRENCH SAFETY SAFETY S
2.	BACKFILL BEHIND THE CURB SHALL BE COMPACTED TO OBTAIN A MINIMUM OF 95% MAXIMUM DENSITY TO WITHIN 6" OF TOP OF CURB. MATERIAL USED SHALL BE PRIMARILY GRANULAR WITH NO ROCKS LARGER THAN 6"IN THE GREATEST DIMENSION. THE REMAINING 6" SHALL BE CLEAN TOPSOIL FREE FROM ALL CLODS AND SUITABLE FOR SUSTAINING PLANT LIFE.	ADMINIST
3.	A MINIMUM OF 6" OF TOPSOIL SHALL BE PLACED BETWEEN THE CURB AND RIGHT-OF-WAY AND IN ALL DRAINAGE CHANNELS EXCEPT CHANNELS CUT IN STABLE ROCK.	PROJECT.
4.	DEPTH OF COVER FOR ALL CROSSINGS UNDER PAVEMENT, INCLUDING GAS, ELECTRIC TELEPHONE, CABLE TV, ETC., SHALL BE A MINIMUM OF 36" BELOW SUBGRADE.	AND CON STANDAR
5.	STREET RIGHT-OF-WAY SHALL BE GRADED AT A SLOPE OF 1/4" PER FOOT TOWARD THE CURB UNLESS OTHERWISE INDICATED.	3. AREAS C AREAS W
6.	ALL DRAINAGE PIPE IN PUBLIC RIGHT OF WAY OR EASEMENTS SHALL BE REINFORCED CONCRETE PIPE MINIMUM CLASS III OF TONGUE AND GROOVE OR O-RING JOINT DESIGN. CORRUGATED METAL PIPE IS NOT ALLOWED IN PUBLIC RIGHT OR WAY OR EASEMENTS.	BENCHMA
7.	THE CONTRACTOR MUST PROVIDE A PNEUMATIC TRUCK PER TXDOT SPEC FOR PROOF ROLLING.	Pt.
8.	ALL STRIPING, WITH THE EXCEPTION OF STOP BARS, CROSS WALKS, WORDS AND ARROWS, IS TO BE TYPE II (WATER BASED). STOP BARS, CROSS WALKS, WORDS AND ARROWS REQUIRE TYPE I THERMOPLASTIC.	5
9.	MANHOLE FRAMES, COVERS, VALVES, CLEAN-OUTS, ETC. SHALL BE RAISED TO GRADE PRIOR TO FINAL PAVEMENT CONSTRUCTION.	BENCHMAR
10.	. A STOP BAR SHALL BE PLACED AT ALL STOP SIGN LOCATIONS.	
11.	THE GEOTECHNICAL ENGINEER SHALL INSPECT THE SUBGRADE FOR COMPLIANCE WITH THE DESIGN ASSUMPTIONS MADE DURING PREPARATION OF THE SOILS REPORT. ANY ADJUSTMENTS THAT ARE REQUIRED SHALL BE MADE THROUGH REVISIONS OF THE APPROVED CONSTRUCTION PLANS	<u>CITY OF L</u>
12.	. GEOTECHNICAL INVESTIGATION INFORMATION AND PAVEMENT RECOMMENDATIONS WERE PROVIDED BY	1. CONTAC
	MLA GEOTECHNICAL. PAVEMENT RECOMMENDATIONS ARE AS FOLLOWS:	2. FOR PL WORKS
	Street Classification Subgrade Material Subgrade	3. THE CO FOR EX CONTRA CROSSE
	Iocal Streets PI 20 to 35 2:0 14 8 PI 20 to 35 2:0 12 8	OPERAT 4. CONTAC STREET
F(IN	OR FURTHER INFORMATION REFER TO LIVELY PHASE 5 & 6, LEANDER, TEXAS GEOTECHNICAL IVESTIGATION, PAVEMENT THICKNESS RECOMMENDATIONS PREPARED BY MLA GEOTECHNICAL DATED	a. LOCA
DI 13.	ECEMBER 2023. A TRAFFIC CONTROL PLAN, IN ACCORDANCE WITH THE TEXAS MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES, CITY OF AUSTIN TRANSPORATION CRITERIA MANUAL, CITY OF LEANDER STANDARD DETAILS AND TEXAS DEPARTMENT OF TRANSPORTATION CRITERIA, SHALL BE SUBMITTED TO THE CITY OF LEANDER FOR REVIEW AND APPROVAL PRIOR TO ANY PARTIAL OR COMPLETE ROADWAY CLOSURES. TRAFFIC CONTROL PLANS MUST BE SITE SPECIFIC AND SIGNED AND SEALED BY A REGISTERED PROFESSIONAL ENGINEER.	b. REFR <u>OF YOU</u> REFRESI VISIBLE. c. REPC EXCAVA
14.	ALL LANE CLOSURES SHALL OCCUR ONLY BETWEEN THE HOURS OF 9 AM AND 4 PM UNLESS OTHERWISE NOTED ON THE PLANS. ANY NIGHT TIME LANE CLOSURES REQUIRE APPROVAL OF THE CITY ENGINEER AND SHALL OCCUR BETWEEN THE HOURS OF 8 PM AND 6 AM. LANE CLOSURES OBSERVED BY THE CITY DURING PEAK HOURS OF 6 AM TO 9 AM OR 4 PM TO 8 PM WILL BE SUBJECT TO A FINE AND OR SUBSEQUENT ISSUANCE OF WORK STOPPAGE	5. A PREC APPLICA
15.	. TEMPORARY ROCK CRUSHING IS NOT ALLOWED. ALL SOURCES OF FLEXIBLE BASE MATERIAL ARE REQUIRED TO BE APPROVED BY THE CITY. PRIOR TO BASE PLACEMENT ALL CURRENT TRIAXIAL TEST REPORTS FOR PROPOSED STOCK PILES ARE TO BE SUBMITTED TO THE CITY CONSTRUCTION INSPECTOR FOR REVIEW AND APPROVAL	EROSION BEGINNI AT 512- 6. 6. CITY
16.	AT ROAD INTERSECTIONS THAT HAVE A VALLEY GUTTER, THE CROWN TO THE INTERSECTING ROAD WILL BE CULMINATED AT A DISTANCE OF 40 FEET FROM THE INTERSECTING CURB LINE UNLESS OTHERWISE NOTED.	9 PM A COUNCIL 7. CONTRA OPEN C
17.	NO PONDING OF WATER SHALL BE ALLOWED TO COLLECT ON OR NEAR THE INTERSECTION OF PRIVATE DRIVEWAYS AND PUBLIC STREETS. RECONSTRUCTION OF THE DRIVEWAY APPROACH SHALL BE AT THE CONTRACTOR'S EXPENSE.	8. CONTRA AND AL SPECIFIC
18.	ALL DRIVEWAY APPROACHES SHALL HAVE A UNIFORM TWO PERCENT SLOPE WITHIN THE PUBLIC RIGHT OF WAY UNLESS APPROVED IN WRITING BY THE ENGINEERING DEPARTMENT.	9. THE CU
19.	. IMPROVEMENTS THAT INCLUDE RECONSTRUCTION OF AN EXISTING TYPE II DRIVEWAY SHALL BE DONE IN A MANNER WHICH RETAINS OPERATIONS OF NOT LESS THAN HALF OF THE DRIVEWAY TO REMAIN	ULAWSU WASTE LIBERTY
	OPEN AT ALL TIMES. FULL CLOSURE OF SUCH DRIVEWAY CAN BE CONSIDERED WITH WRITTEN AUTHORIZATION OBTAINED BY THE CONTRACTOR FROM ALL PROPERTY OWNERS AND ACCESS EASEMENT RIGHT HOLDERS ALLOWING THE FULL CLOSURE OF THE DRIVEWAY.	10. ALL UNI
20.	. CONTRACTOR MUST CLEAR FIVE (5) FEET BEYOND ALL PUBLIC RIGHT OF WAY TO PREVENT FUTURE VEGETATIVE GROWTH INTO THE SIDEWALK AREAS.	SHALL I
01	SLOPE OF NATURAL CROUND AD ACENT TO THE RURLIC RICHT OF WAY SHALL NOT EVOLED 3.1	EROSION CO

- 21. SLOPE OF NATURAL GROUND ADJACENT TO THE PUBLIC RIGHT OF WAY SHALL NOT EXCEED 3:1 SLOPE. IF A 3:1 SLOPE IS NOT POSSIBLE, SLOPE PROTECTION OR RETAINING WALL MUST BE SUBMITTED TO THE CITY FOR REVIEW AND APPROVAL PRIOR TO FINAL ACCEPTANCE.
- 22. THERE SHALL BE NO WATER, WASTEWATER OR DRAINAGE APPURTENANCES, INCLUDING BUT NOT LIMITED TO VALVES, FITTINGS, METERS, CLEAN-OUTS, MANHOLES, OR VAULTS IN ANY DRIVEWAY, SIDEWALK, TRAFFIC OR PEDESTRIAN AREA.
- 23. PUBLIC SIDEWALKS SHALL NOT USE CURB INLETS AS PARTIAL WALKING SURFACE. SIDEWALKS SHALL NOT USE TRAFFIC CONTROL BOXES, METERS, CHECK VALVE VAULTS, COMMUNICATION VAULTS, OR OTHER BURIED OR PARTIALLY BURIED INFRASTRUCTURE AS A VEHICULAR OR PEDESTRIAN SURFACE.
- 24. ALL WET UTILITIES SHALL BE INSTALLED AND ALL DENSITIES MUST HAVE PASSED INSPECTION(S) PRIOR TO THE INSTALLATION OF DRY UTILITIES.
- 25. DRY UTILITIES SHALL BE INSTALLED AFTER SUBGRADE IS CUT AND BEFORE THE FIRST COURSE OF BASE. NO TRENCHING COMPACTED BASE. IF NECESSARY DRY UTILITIES INSTALLED AFTER FIRST COURSE BASE SHALL BE BORED ACROSS THE FULL WIDTH OF THE PUBLIC RIGHT-OF-WAY.

DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANT'S ORIGINAL SIGNATURE AND SEAL.

ACTOR TO AVOID INSTALLATION OF IRRIGATION, PLANTINGS, SILT FENCE, ETC. IN THE BASE UILD BEYOND BACK OF CURB.

SAFETY NOTES

SAFETY SYSTEMS TO BE UTILIZED FOR THIS PROJECT ARE DESCRIBED IN ITEM 509S "TRENCH SYSTEMS" OF THE CITY OF AUSTIN STANDARD SPECIFICATIONS AND SHALL BE IN ACCORDANCE IE LAWS OF THE STATE OF TEXAS AND THE U.S. OCCUPATION SAFETY AND HEALTH RATION REGULATIONS.

NOTES

DRAINAGE SHALL BE MAINTAINED ON ALL SURFACE AREAS WITHIN THE SCOPE OF THIS CONTRACTOR SHOULD TAKE PRECAUTIONS NOT TO ALLOW ANY PONDING OF WATER.

ITRACTOR SHALL CONSTRUCT EARTHEN EMBANKMENTS WITH SLOPES NO STEEPER THAN 3:1 MPACT SOIL TO 95% OF MAXIMUM DENSITY IN ACCORDANCE WITH THE CITY OF AUSTIN RD SPECIFICATIONS.

OF SOIL DISTURBANCE ARE LIMITED TO GRADING AND IMPROVEMENTS SHOWN. ALL OTHER VILL NOT BE DISTURBED.

RK NOTES

	Grid Northing	Grid Easting	Elevation	Full Description
	10203233.6'	3094593.4'	975.8'	SET ½" IRON ROD WITH RED CAP "PAPE-DAWSON"
ARK 110			879.48'	SET CHISELED SQUARE ON GAS VALVE ON THE

<u>EANDER DRY UTILITIES NOTES (2024)</u>

NOTES:

TOR SHALL MAINTAIN MINIMUM 24" CLEARANCE FROM ALL EXISTING UTILITIES.

JBLIC WATER & WASTEWATER LINE EMERGENCIES, CONTACT THE CITY OF LEANDER PUBLIC EMERGENCY 24-HOUR ON-CALL LINE AT 512-690-4760.

SOUTH SIDE OF DUKE ROAD

INTRACTOR SHALL CONTACT THE TEXAS EXCAVATION SAFETY SYSTEM AT 1-800-344-8377 XISTING UTILITY LOCATIONS 48 HOURS PRIOR TO THE START OF CONSTRUCTION. THE CTOR SHALL VERIFY THE LOCATIONS OF ALL UTILITIES THAT ARE TO BE EXTENDED, TIED TO, ED, OR ALTERED; OR SUBJECT TO DAMAGE/INCONVENIENCE BY THE CONSTRUCTION IONS.

T THE CITY OF LEANDER PUBLIC WORKS DEPARTMENT FOR EXISTING WATER, WASTEWATER, LIGHT ELECTRICAL WIRING, AND TRAFFIC SIGNAL WIRING LOCATIONS A MINIMUM OF 48 HOURS TO START OF CONSTRUCTION.

ATE REQUESTS MUST INCLUDE A COPY OF YOUR 811 TICKET.

RESH ALL LOCATES <u>BEFORE</u> 14 DAYS –LOCATE REFRESH REQUESTS <u>MUST INCLUDE A COPY</u> R 811 TICKET. TEXAS PIPELINE DAMAGE PREVENTION LAWS REQUIRE THAT A LOCATE H REQUEST BE SUBMITTED BEFORE 14 DAYS, OR IF LOCATION MARKERS ARE NO LONGER

ORT ALL DAMAGE TO CITY INFRASTRUCTURE IMMEDIATELY -IF YOU WITNESS OR EXPERIENCE TION DAMAGE, PLEASE CONTACT THE CITY OF LEANDER PUBLIC WORKS DEPARTMENT BY IF DAMAGE IS WITNESSED OR EXPERIENCED AFTER HOURS, CALL THE CITY OF LEANDER S ON-CALL LINE AT THE NUMBER LISTED ABOVE.

CONSTRUCTION CONFERENCE SHALL BE HELD WITH THE CONTRACTOR, DESIGN ENGINEER/PERMIT ANT & CITY OF LEANDER REPRESENTATIVES PRIOR TO INSTALLATION OF N/SEDIMENTATION CONTROLS & TREE PROTECTION MEASURES AS WELL AS PRIOR TO NG CONSTRUCTION. CONTRACTOR SHALL NOTIFY THE CITY OF LEANDER PLANNING DEPARTMENT -528-2750 AT LEAST THREE (3) DAYS PRIOR TO MEETING DATE.

OF LEANDER NOISE ORDINANCE PROHIBITS CONSTRUCTION ACTIVITY BETWEEN THE HOURS OF AND 7 AM. REQUESTS FOR EXCEPTIONS TO THE ORDINANCE MUST BE MADE TO LEANDER CITY

CTOR SHALL BORE UNDER ALL DRIVEWAYS, STREET CROSSINGS AND OTHER PAVED AREAS. UT CROSSING SHALL NOT BE ALLOWED.

CTOR SHALL REPLACE ALL DAMAGED PAVEMENT, CURB & GUTTER, SIDEWALK, CURB INLETS L OTHER INFRASTRUCTURE DAMAGED BY CONSTRUCTION PER CITY OF LEANDER STANDARDS & CATIONS.

RRENT COMPANIES THAT HOLD CONTRACTS WITH THE CITY FOR WASTE HAULING ARE AL IN DISPOSAL, INC., ARROW ROLL OFF'S AND RECYCLING, BIN DUMPED, HOOK N HAUL, CENTRAL & RECYCLING, CENTRAL TEXAS REFUSE, LOSSEN BROTHERS CONSTRUCTION, RECON SERVICES, DUMPSTER REMOVAL, TEXAS DISPOSAL SYSTEM.

DERGROUND UTILITY LINES SHALL CROSS UNDERNEATH WATERLINES.

NIMUM DEPTH OF COVER FOR UTILITY LINES INSTALLED UNDER CITY OF LEANDER ROADWAYS BE 36" BENEATH FINISHED GRADE.

ONTROL & RESTORATION:

1. THE CITY OF LEANDER ENVIRONMENT INSPECTOR HAS THE AUTHORITY TO ADD OR MODIFY EROSION/SEDIMENTATION CONTROLS ON SITE THROUGHOUT THE DURATION OF THE PROJECT.

2. ALL AREAS DISTURBED OR EXPOSED DURING CONSTRUCTION SHALL BE RESTORED WITH A MINIMUM OF 6" TOPSOIL. THE 6" MINIMUM SOIL DEPTH SHALL CONSISTS OF 75% SOIL BLENDED WITH 25% COMPOST.

3. ALL DISTURBED AREAS SHALL BE RE-VEGETATED USING ONLY APPROVED GRASSES FROM THE GROW GREEN GUIDE.

MUD DISTRICT NOTES:

1. THE DISTRICT ENGINEER, JONES-HEROY & ASSOCIATES, INC. (KEN HEROY, Ph: 512/989-2200) SHALL BE CONTACTED 48 HOURS PRIOR TO:

PRE-CONSTRUCTION MEETINGS; ii) BEGINNING EACH PHASE OF CONSTRUCTION; iii) TESTING OF WATER AND/OR WASTEWATER LINES; AND, iv) FINAL WALK-THROUGH OF FACILITIES.

Edwards Aquifer Protection Program Construction Notes – Legal Disclaimer

The following/listed "construction notes" are intended to be advisory in nature only and do not constitute an approval or conditional approval by the Executive Director (ED), nor do they constitute a comprehensive listing of rules or conditions to be followed during construction. Further actions may be required to achieve compliance with TCEQ regulations found in Title 30. Texas Administrative Code (TAC), Chapters 213 and 217, as well as local ordinances and regulations providing for the protection of water quality. Additionally, nothing contained in the following/listed "construction notes" restricts the powers of the ED, the commission or any other governmental entity to prevent, correct, or curtail activities that result or may result in pollution of the Edwards Aquifer or hydrologically connected surface waters. The holder of any Edwards Aquifer Protection Plan containing "construction notes" is still responsible for compliance with Title 30, TAC, Chapters 213 or any other applicable TCEQ regulation, as well as all conditions of an Edwards Aguifer Protection Plan through all phases of plan implementation Failure to comply with any condition of the ED's approval, whether or not in contradiction of any "construction notes," is a violation of TCEQ regulations and any violation is subject to administrative rules, orders, and penalties as provided under Title 30, TAC § 213.10 (relating to Enforcement). Such violations may also be subject to civil penalties and injunction. The following/listed "construction notes" in no way represent an approved exception by the ED to any part of Title 30 TAC, Chapters 213 and 217, or any other TCEQ applicable regulation

include: - the name of the approved project;

- the activity start date; and - the contact information of the prime contractor.

- source, distribution system, well, or sensitive feature.
- Any sediment that escapes the construction site must be collected and properly disposed of etc.
- 6. 50% of the basin's design capacity.
- prevented from being discharged offsite.
- All excavated material that will be stored on-site must have proper E&S controls.

TCEQ-0592A (Rev. July 15, 2015)

stabilization in those areas shall be initiated as soon as possible prior to the 14th day of inactivity. If activity will resume prior to the 21st day, stabilization measures are not required. If drought conditions or inclement weather prevent action by the 14th day, stabilization measures shall be initiated as soon as possible.

- the dates when major grading activities occur;
 the dates when construction activities temporarily or permanently cease on a portion of the site; and - the dates when stabilization measures are initiated.
- silt fences, and diversionary structures;
- originally approved;
- Edwards Aquifer; or
- contributing zone plan.

Austin Regional Office 12100 Park 35 Circle, Building A Austin, Texas 78753-1808 Phone (512) 339-2929 Fax (512) 339-3795

PLANS PROVIDED TO THE CONTRACTOR AND ALL SUBCONTRACTORS.

TCEQ-0592A (Rev. July 15, 2015)

Texas Commission on Environmental Quality Contributing Zone Plan **General Construction Notes**

1. A written notice of construction must be submitted to the TCEQ regional office at least 48 hours prior to the start of any ground disturbance or construction activities. This notice must

2. All contractors conducting regulated activities associated with this project should be provided with complete copies of the approved Contributing Zone Plan (CZP) and the TCEQ letter indicating the specific conditions of its approval. During the course of these regulated activities, the contractor(s) should keep copies of the approved plan and approval letter on-

No hazardous substance storage tank shall be installed within 150 feet of a water supply

Prior to beginning any construction activity, all temporary erosion and sedimentation (E&S) control measures must be properly installed and maintained in accordance with the manufacturers specifications. If inspections indicate a control has been used inappropriately, or incorrectly, the applicant must replace or modify the control for site situations. These controls must remain in place until the disturbed areas have been permanently stabilized.

before the next rain event to ensure it is not washed into surface streams, sensitive features,

Sediment must be removed from the sediment traps or sedimentation basins when it occupies

Litter, construction debris, and construction chemicals exposed to stormwater shall be

9. If portions of the site will have a cease in construction activity lasting longer than 14 days, soil Page 1 of 2

10. The following records should be maintained and made available to the TCEQ upon request:

11. The holder of any approved CZP must notify the appropriate regional office in writing and obtain approval from the executive director prior to initiating any of the following:

A. any physical or operational modification of any best management practices (BMPs) or structure(s), including but not limited to temporary or permanent ponds, dams, berms,

B. any change in the nature or character of the regulated activity from that which was

C. any change that would significantly impact the ability to prevent pollution of the

D. any development of land previously identified as undeveloped in the approved

San Antonio Regional Office 14250 Judson Road
San Antonio, Texas 78233-4480
Findle (210) 490-3096 Fax (210) 545-4329

THESE GENERAL CONSTRUCTION NOTES MUST BE INCLUDED ON THE CONSTRUCTION

	NO.	REVISION	DATE
X P S			
TE			
F			
TE			
A.C.			
•••			





T, PHASE 6 DER, TEXAS	
NOTES (2 OF 3)	

TION

()

RU

Ś

NO

CITY NO. _____

JOB NO. 50816-26

DATE JANUARY 2025

CHECKED TCK DRAWN DY/S

 $_{\mbox{\tiny SHEET}}$ 3 of 83

RBB

DESIGNER

S \triangleleft T V TRAC Ш

 \geq

CITY OF LEANDER APPROVAI

Page 2 of 2



DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANT'S ORIGINAL SIGNATURE AND SEAL.

below non-fractured rock_or 3 ft below fractured rock. The pavement design must meet at least the minimum of one of the approved County designs and provided in the geotechnical report for review and approval prior to the review and approval of the construction plans. In addition to the basis of the pavement design, the soils report shall contain the results of sampled and tested subgrade for

rban/F	Rural) Flexib	le Pavement design			
-35	PI 35-55 (4)				
Clay	Fat Clay	Material Requirements			
	07	TxDOT Item 340 D- GR HMA			
	2	PG 70-22 SAC B			
	YES	AEP or TxDOT Item 316 TxDOT Item 247 FLBS TY A GR 5			
	14"				
	8"	TxDOT Item 260			
See Ap lowed I	pendix B7 – B1 37.11	0 for HMA material requirements.			
lix B6 1	for additional F	lexible Base specifications.			
me is n s are n	ot allowed. Us	e hydrated lime or lime slurry. oil.			

reviewed and approved by the County Engineer. (5) Should solid rock be encountered prior to the depth necessary for 12" of base material underneath 2" HMA, a substitute pavement design may

be allowed. Substitute pavement design shall have a base thickness no less than 8" and existing material shall be excavated to the exposed solid rock layer. No significant amount of existing material shall be left remaining between the base layer and the rock layer.

(Urba	an/Rural) Flex	kible Pavement design		
0-35	PI 35-55 (4)			
n /	Fat Clay	Material Requirements		
	01	TxDOT Item 340 D- GR HMA		
	2	PG 70-22 SAC B		
3	YES	AEP or TxDOT Item 316		
	16"	TxDOT Item 247 FLBS TY A GR 5		
	8"	TxDOT Item 260		
ban S Rura	ee Appendix B I is also allowed	7 – B10 for HMA material I B7.11		

Page 38

for Construction, "Flexible Base". The base material shall be Type A Grade 4, or as approved by the County Engineer. Grade 4 material shall conform to the requirements of Table B6.1 below:

*	
lative % Retained	
-	
0	
10% - 35%	
30% - 65%	

45% - 75% 70% - 90% 87% - 95%

thickness. The number and location of all base test samples shall be determined by the County

(Proctor) dry density or as approved by the County Engineer upon recommendation by the testing laboratory. The maximum lift shall not exceed six inches. The base must be inspected and approved by an Independent Testing Laboratory and a certified copy of the test results furnished to the County Engineer for approval. Prior to the placement of the first lift of base, the stockpile

TxDOT certified plant and the mix design shall be submitted to the County Engineer for approval

that does not contain Recycled Engine Oil Bottoms (REOBs) or Poly Phosphoric Acid (PPA). Recycled Asphalt Pavement (RAP) is not permitted for use as a component of the HMACP. The Contractor is also not permitted the use Recycled Asphalt Shingles (RAS) as a component of the

or PPA. For subsurface course Type B, the use of twenty percent (20%) RAP is permitted in the

Page 43

(2) See Appendix B6 for additional Flexible Base specifications. (3) Pelletized lime is not allowed. Use hydrated lime or lime slurry. Confirm sulfates are not present in soil.

(4) For PI >55 additional pavement structure is necessary and shall be reviewed and approved by the County Engineer.

(5) Should solid rock be encountered prior to the depth necessary for 14" of base material underneath 2" HMA, a substitute pavement design may be allowed. Substitute pavement design shall have a base thickness no less than 10" and existing material shall be excavated to the exposed solid rock laver. No significant amount of existing material shall be left remaining between the base layer and the rock layer

Minimum Arterial Roadway (Urban/Rural) Flexible Pavement design						
Plasticity Index	PI <20	PI <20 PI 20-35 PI 35-5				
Soil Classification	Clayey Sand	Lean Clay	Fat Clay	Material Requirements		
HMA Surface (1)	2"	2"	2"	TxDOT Item 340 D- GR HMA PG 70-22 SAC B		
Prime Coat or One Course Underseal	YES	YES	YES	AEP or TxDOT Item 316		
Flexible Base (2)	20"	20"	22"	TxDOT Item 247 FLBS TY A GR 5		
Lime treated Subgrade (3)	NO	8"	10"	TxDOT Item 260		
	(1) See Appendix B7 for material requirements for HMA.					
	(2) See Appendix B6 for additional Flexible Base specifications.					
Notes:	(3) Pelletized lime is not allowed. Use hydrated lime or lime slurry. Confirm sulfates are not present in soil.					
	(4) For PI >55 additional pavement structure is necessary and shall be reviewed and approved by the County Engineer.					

B4.6 Rigid Pavement Designs based on Roadway Classification

Loca	I Roadway (U	rban/ Rura	I) Rigid Par	vement design	
Plasticity Index	PI <20	PI 20-35 Lean Clay	PI 35-55 (4)	. Material Requirements	
Soil Classification	Clayey Sand		Fat Clay		
	67	6"	8"	TxDOT Item 421 – Class P Concrete	
				CRCP – 13, Continuously Reinforced Concrete Pavement, One-layer steel bar placement	
HMA Bond Breaker	1"	1"	1"	TxDOT Item D- GR HMA TY D of TY F PG 64-22	
Flexible Base (2)	6"	8"	8 ⁿ	TxDOT Item 247 FLBS TY A GR	

Williamson County, Texas - Subdivision Regulations

Page 39

B7.4 Target laboratory molded density is 96.5% for all mixtures without RAP and when using a Texas Gyratory Compactor (TGC) for designing the mixture. When using Superpave Gyratory Compactor (SGC) to design mixtures, submit the SGC mix design to the Engineer for approval.

B7.5 All mixtures must meet the Hamburg requirement as stated in the table below.

High-Temperature	Test Method	Hamburg Wheel Test Requirements*				
Binder Grade		Minimum # of Passes @ 0.5" Rut Depth, Tested @122°F				
PG 64 or lower	Tex-242-F	7,000				
PG 70	Tex-242-F	15,000				
PG 76 or higher	Tex-242-F	20,000				

* The County Engineer may accept Hamburg Wheel test results for production and placement if no more than 1of the 5 most recent tests is below the specified number of passes and the failing test is no more than 2,000 passes below the specified number of passes.

B7.6 Submit any proposed adjustments or changes to a job mix formula to the County Engineer before production of the new job mix formula.

B7.7 Unless otherwise approved, provide Type B mixtures that have no less than 4.5% asphalt binder, and TY C and D mixtures with no less than 4.7% binder.

- B7.8 For Mixture Design Verification, provide the Engineer with two 5-gallon buckets of each aggregate stockpile to be used on the project and three gallons of each PG binder to be used on the project. Also provide sufficient quantities of any other additives that will be used in the HMA mixture. This must be done prior to approval of the mix design, unless already performed within a one-year time period.
- B7.9 Prior to allowing production of the trial batch, the Engineer will use the materials provided by the Contractor to perform the following tests to verify the HMA mixture design.
 - 1. Indirect Tensile Test in accordance with Tex-226-F
 - 2. Hamburg Wheel Test in accordance with Tex-242-F 3. Overlay Test in accordance with Tex-248-F
 - 4. Cantabro Test in accordance with Tex-245-F

For mixtures designed with a Texas Gyratory Compactor (TGC), the Engineer may require that the target laboratory molded density be raised to no more than 97.5% or may lower the design number of gyrations to no less than 35 for mixtures designed with an SGC if any of the following conditions exist.

- 1. The Indirect Tensile Test results in a value greater than 200 PSI
- 2. The Hamburg Wheel Test results in a value less than 3.0 mm
- 3. The Overlay Test results in a value less than 100 cycles 4. The Cantabro Test results in a value of more than 20% loss

In lieu of, or in addition to evaluating the mixture design prior to allowing a trial batch to be produced, the Engineer may also evaluate the mixture produced during the trial batch for

compliance with the 4 tests listed above. Williamson County, Texas - Subdivision Regulations

Page 44

Lime treated Subgrae

Plasticity Index

Soil Classification

CRCP (1)

HMA Bond Breake Flexible Base (2)

Lime treated Subg

Plasticity Index
Soil Classification

CRCP (1)

HMA Bond Breake Flexible Base (2) Lime treated Subg

Williamson County, Texas - Subdivision Regulations

B7.10 Contractor's Quality Control (CQC) test reports shall be submitted to the County Engineer on a daily basis. As a minimum, daily CQC testing on the produced mix shall include: Sieve Analysis TEX-200-F, Asphalt Content TEX-236-F, Hveem Stability TEX-208-F, Laboratory Compacted Density TEX-207-F, and Maximum Specific Gravity TEX-227-F. The number and location of all HMAC tests shall be determined by the County Engineer with a minimum of three, 6-inch diameter field cores secured and tested by the contractor from each day's paving. Each HMAC course shall be tested for in-place density, bituminous content and aggregate gradation, and shall be measured for compacted thickness. The number and location of all HMAC test samples shall be determined by the County Engineer.

B7.11 Rural roads may use either the specifications found in Section B7.1 or a two-course surface in accordance with Item 316, treatment wearing surface, of the current edition of the TxDOT Standard Specifications for Construction. The type and rate of asphalt and aggregate shall be indicated on the plans as a basis of estimate and shall be determined at the preconstruction conference. Aggregate used in the mix shall be on the TxDOT Quality Monitoring Schedule. Aggregate shall be Type B Grade 4. Gradation tests shall be required for each 300 cubic yards of material placed with a minimum of two tests per each grade per each project. Test results shall be reviewed by the County Engineer prior to application of the material.

B8.1 In lieu of bituminous pavement, Portland cement concrete pavement may be used. In such cases, the pavement thickness shall be a minimum of 9 inches of concrete, and shall be jointed and reinforced in accordance with the detail included in Appendix I. The mix shall be from a TxDOT certified plant. The mix design shall be submitted to the County Engineer for approval prior to placement of the material.

applicable item.

of te	st c	ylind	ders.	On
and	the	rem	aining	g tw

Williamson County, Texas - Subdivision Regulations

de (3)			8"	TxDOT Item 260
	(1) See A	ppendix B7 f	or material re	equirements for CRCP
	(2) See A	ppendix B6 f	or additional	Cement Treated Base specifications
	(3) Pelleti: Confirm s	zed lime is n ulfates are n	ot allowed. U ot present in	lse hydrated lime or lime slurry. soil.
	(4) For Pl reviewed	>55 addition and approve	al pavement d by the Cou	structure is necessary and shall be inty Engineer
lector F	Roadway (Urban/ Run	al) Rigid P	avement design

	PI <20	PI 20-35 (4)		Material Requirements
	Clayey Sand	Lean Clay	Fat Clay	motorial responsibility
				TxDOT Item 421 – Class P Concrete
	6"	6"	8"	CRCP – 13, Continuously Reinforced Concrete Pavement, One-layer steel bar placement
r	1"	1"	1"	TxDOT Item D- GR HMA TY D or TY F PG 64-22
	8"	10"	10"	TxDOT Item 247 FLBS TY A GR 4 (2)
rade (3)			8"	TxDOT Item 260 ⁽³⁾
	(1) See A	ppendix B7 f	or material re	quirements for CRCP
	(2) See A	ppendix B6 f	or additional (Cement Treated Base specifications
	(3) Pelleti Confirm s	zed lime is n ulfates are n	ot allowed. Us ot present in s	se hydrated lime or lime slurry. soil.
	(4) For PI reviewed	>55 addition and approve	al pavement d by the Cour	structure is necessary and shall be nty Engineer

Arterial Roadway (Urban/ Rural) Rigid Pavement design

	PI <20	PI 20-35	PI 35- 55 (4)	Material Requirements
	Clayey Sand	Lean Clay	Fat Clay	Material requirements
				TxDOT Item 421 – Class P Concrete
	11"	11"	11"	CRCP – 13, Continuously Reinforced Concrete Pavement, One-layer steel bar placement
r	1"	1"	1"	TxDOT Item D- GR HMA TY D or TY F PG 64-22
:	12"	12"	12"	TxDOT Item 247 FLBS TY A GR 4
rade (3)		6"	10"	TxDOT Item 260

Page 40

B8 - Concrete Pavement

B9 - Concrete - General

B9.1 Unless otherwise specified, concrete shall be in accordance with Item 421 of the current edition of the TxDOT Standard Specifications for Construction and be placed in accordance with the

B9.2 All concrete shall be tested for compressive strength. One set of three concrete test cylinders shall be molded for every 50 cubic yards of concrete placed for each class of concrete per day, or at any other interval as determined by the County Engineer. A slump test shall be required with each set ne cylinder shall be tested for compressive strength at an age of seven days vo cylinders shall be tested at 28 days of age.

Page 45



CITY OF LEANDER APPROVAI

S

NO

 \mathbf{O}

CITY NO. -----

JOB NO. 50816-26

DATE JANUARY 2025

CHECKED_TCK_DRAWN_DY/SI

SHEET 4 of 83

DESIGNER

RBB_



Impervious Cover &	Water Quality Treatment S	ummary (Ultimate Develo	pment, including Phase {	5)
	LIVELY TRACT, PH	ASE 2 MODIFIED CZP		
B.M.P.	Area (AC)	I.C. (AC)	TSS Removal (lb.)	
Batch Detention Pond H	81.10	43.35	44,271	
Batch Detention Pond J	15.93	8.71	8,889	
Residential VFS D	9.87	5.29	5,046	
Residential VFS E	6.68	3.68	3,507	
Residential VFS F	3.86	2.12	2,021	
Open Space Area	3.16	0	0	
				Required
Total CZP	120.60	63.15	63,734	63,734









THE LOCATIONS OF LEXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS EXACT-LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY UNDERGROUND UTILITIES. GROUND AND VEGETATION ESTABLISHED PRIOR TO FINAL SUBDIVISION ACCEPTANCE.

REFER TO MLA LABS, INC. GEOTECHNICAL INVESTIGATION PAVEMENT THICKNESS RECOMMENDATIONS FOR LIVELY TRACT, WILLIAMSON COUNTY, TEXAS, LOT FILL SPECIFICATIONS:

REFER TO GEOTECHNICAL INVESTIGATION REPORT.

STREET FILL SPECIFICATIONS:

(I) PERMISSION TO STORE FILL MATERIAL IN THE SUBDIVISION WILL EXPIRE AND TERMINATE IN THE EVENT THAT A PRELIMINARY PLAT, CONSTRUCTION PLANS, OR A FINAL PLAT FOR ANY PORTION OF THE LAND EXPIRES, OR AT SUCH TIME THAT THE IMPROVEMENTS FOR THE LAST PHASE OF THE SUBDIVISION ARE ACCEPTED.

BY THE SETBACK REQUIREMENTS MAY BE REDUCED BY TWENTY-FIVE (25%) PERCENT IF SCREENING OF THE FILL MATERIAL IS PROVIDED SCREENING INCLUDES A SIX (6.) FOOT PRIVACY FENCE CONSTRUCTED OF CEDAR WITH STEEL POSTS SUNK IN CONCRETE. THE SMOOTH SIDE OF THE FENCE SHALL FACE AWAY FROM THE FILL MATERIAL.

(3) 100 SETBACK FROM RESIDENTIAL STRUCTURES. (4) THE SETBACK REQUIREMENTS MAY BE REDUCED

(1) 400 SEIBACK FROM MAJOR ROADWAYS AS IDENTIFIED ON THE ROADWAY PLAN;
 (2) 100 SETBACK FROM ALL OTHER ROADWAYS PLATTED AT THE TIME OF THE FILL MATERIAL PLE APPROVAL;

ENGINEER. (G) THE HEIGHT OF THE FILL MATERIAL SHALL NOT EXCEED TEN (10) FEET # H) THE LOCATION OF THE FILL MATERIAL MUST COMPLY WITH THE FOLLOWING SETBACK REQUIREMENTS:

FROM NEIGHBORING PROPERTIES. (F) FISCAL SURETY THAT COMPLIES WITH SECTION 28 OF THIS ORDINANCE IN AN AMOUNT EQUAL TO 110% OF THE COST OF REMOVAL OF THE FILL MATERIAL WILL BE FILED WITH THE CITY PRIOR TO THE ACCEPTANCE OF THE SUBDIVISION THAT GENERATES THE FILL MATERIAL THE FISCAL SURETY WILL BE BASED ON AN ESTIMATE PREPARED BY THE ENGINEER FOR THE SUBDIVISION AND APPROVED BY THE CITY ENGINEER

EXIST IN THE SUBDIMISION, AND WILL BE PLACED IN ADVERSELY AFFECT THE NATURAL COURSE OF DRAINAGE ACROSS THE LAND OR IMPEDE DRAINAGE.

FROM NEIGHBORING PROPERTIES.

(0) THE FILL MATERIAL WILL BE PLACED AND STORED IN SUCH MANNER SO THAT IT IS STABLE. WITH THE SIDE SLOPES NO STEEPER THAN A 3:1 (h:v) SLOPE. (E) THE FILL MATERIAL WILL BE LOCATED SO AS NOT, TO DISTURB ANY WETLAND AREAS. THAT MAY A MANNER AND LOCATION SO AS NOT TO

WITH THE STORM WATER POLLUTION DISTURBED AREAS AND OTHER SEDIMENTATION AND EROSION CONTROLS ADOPTED BY THE TEXAS. COMMISSION ON ENVIRONMENTAL QUALITY.

SUBDIVISION. PREVENTION PLAN INCLUDING REVEGETATION OF

INCLUDE ANY MATERIAL FROM OUTSIDE OF THE (C) STORAGE OF THE FILL MATERIAL SHALL COMPLY

SUBDIVISION. THE FILL MATERIAL MAY NOT

DEBRIS, AND SHALL BE SUITABLE FOR USE AS FILL MATERIAL ON THE FUTURE PHASES OF THE

CONSTRUCTION PLANS. SUBDIVISION ONLY, SHALL REMAIN FREE FROM

(A) THE FILL MATERIAL SHALL BE STORED AT THE LOCATION SHOWN ON THE APPROVED (B) THE FILL MATERIAL SHALL CONSIST OF EARTHEN MATERIAL ORIGINATING FROM THE

THE SUBJECT OF A SUBDIVISION APPLICATION MAY BE TEMPORARILY STORED ON SAID LAND PROVIDED THAT FOLLOWING REQUIREMENTS:

HE DEVELOPER COMPLIES AT ALL TIMES WITH THE

15. FILL MATERIAL ORIGINATING FROM THE LAND THAT IS

IMPORTED/PLACED TO SUPPORT GROWTH.

14. AREAS SHOWN FOR VEGETATIVE FILTER STRIPS SHALL BE INSPECTED FOR VIABILITY OF GROWTH IF PRESENT, ALL ROCKS THAT INTERFERE WITH VEGETATIVE FILTER STRIPS SHALL BE REMOVED AND FILL WATERIAL SHALL BE

PURPOSES ONLY, CONTRACTOR SHALL KEEP ALL CONSTRUCTION WITHIN THE PROPERTY BOUNDARY.

REMOVE INLET PROTECTION MEASURES UNTIL SUCH TIME AS THE WEATHER EVENT HAS PASSED. 13. LIMITS OF CONSTRUCTION IS FOR ILLUSTRATIVE

11. SILT FENCE PLACED ALONG FUTURE ROADWAY TO BE PLACED OUTSIDE OF RIGHT OF WAY TO ENSURE CONTINUED 12. IN THE EVENT OF INCLEMENT WEATHER THAT MAY RESULT IN A FLOODING SITUATION, THE CONTRACTOR SHALL

10 CONTRACTOR WILL CLEAN UP SPOILS THAT MIGRATE ONTO THE ROADS A MINIMUM OF ONCE DAILY.

9. THE CITY OF LEANDER ENVIRONMENTAL INSPECTOR HAS THE AUTHORITY TO ADD OR MODIFY EROSION/SEDIMENT CONTROLS ON SITE THROUGHOUT THE DURATION OF THE PROJECT

DETAIL ON SHEET 98 UPON COMPLETION OF THE INLETS. 8. CNSITE DUST CONTROL SHALL BE IN ACCORDANCE WITH THE CITY OF AUSTIN ENVIRONMENTAL CRITERIA MANUAL SECTION 1.4.5 D

5. ALL NATURAL GROUND SLOPES FOR THIS PHASE ARE BETWEEN 0% AND 15% 6. EXISTING CONTOUR INFORMATION SHOWN ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS. 7. INSTALL INLET PROTECTION PER GEO CURVE INLET FILTER.

SHOWN "TO BE PROTECTED" WHENEVER POSSIBLE IF SILT FENCE MUST CROSS THE CRZ, THEN ALTERNATE APPROVED METHODS FOR SECURING THE FABRIC SHALL BE USED IN LIEU OF THE SPECIFIED TRENCHING.

OUTSIDE THE CRITICAL ROOT ZONE (CRZ) OF ALL TREES

3. SEE SHEET 98 FOR EROSION AND SEDIMENTATION CONTROL DETAILS 4, EROSION & SEDIMENTATION CONTROLS SHALL BE LOCATED

RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY-LOCATE AND LOCATE AND PRESERVE ANY AND ALL 2. SPOILS & STAGING AREA TO BE GRADED TO NATURAL

REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE

A

304 GT U **Q**

 (\odot)

82

52

0F 2 ROL NON: Ō

T LL () က \triangleleft Ē RACT, F

SEDIMENTAT FB 8 NO S ШШ ADING,

CITY JOB No. 21-PICP-0/ 50816-23 MAY 2022. DATE RBB ESIGNER CKED REC DRAWN AD 8 of 83 SHEET

21-PICP-027

CITY OF LEANDER APPROV.



NOTES (CONT.): NOTES: LEGEND 13. FILL MATERIAL ORIGINATING FROM THE LAND THAT IS THE SUBJECT OF A SUBDIVISION APPLICATION MAY BE TEMPORARILY STORED ON SAID LAND PROVIDED THAT THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE PROPERTY BOUNDARY HOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS THE DEVELOPER COMPLIES AT ALL TIMES WITH THE REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXISTING CONTOUR FOLLOWING REQUIREMENTS: EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE (A) THE FILL MATERIAL SHALL BE STORED AT THE LOCATION SHOWN ON THE APPROVED COMMENCING WORK, AND AGREES TO BE FULLY PROPOSED CONTOUR RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE CONSTRUCTION PLANS. ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY (B) THE FILL MATERIAL SHALL CONSIST OF EARTHEN MATERIAL ORIGINATING FROM THE SUBDIVISION ONLY, SHALL REMAIN FREE FROM DEBRIS, AND SHALL BE SUITABLE FOR USE AS FILL MATERIAL ON THE FUTURE PHASES OF TH IN MAR AND LOC IN LIMITS OF CONSTRUCTION LOCATE AND LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES SILT FENCE SPOILS & STAGING AREA TO BE GRADED TO NATURAL GROUND AND VEGETATION ESTABLISHED PRIOR TO FINAL SUBDIVISION SUBDIVISION. THE FILL MATERIAL MAY NOT STABILIZED CONSTRUCTION ACCEPTANCE 0 2 . . . 0 ENTRANCE/EXIT SEE SHEET 76 FOR EROSION AND SEDIMENTATION CONTROL UBDIVISION TO BE FIELD LOCATED) DETAILS EROSION & SEDIMENTATION CONTROLS SHALL BE LOCATED TEMPORARY STAGING AND OUTSIDE THE CRITICAL ROOT ZONE (CRZ) OF ALL TREES HOWN "TO BE PROTECTED" WHENEVER POSSIBLE. IF SILT STORAGE AREA FENCE MUST CROSS THE CRZ, THEN ALTERNATE APPROVED (TO BE FIELD LOCATED) COMMISSION ON ENVIRONMENTAL QUALITY. METHODS FOR SECURING THE FABRIC SHALL BE USED IN LIEU OF THE SPECIFIED TRENCHING. CONCRETE TRUCK ALL NATURAL GROUND SLOPES FOR THIS PHASE ARE WASHOUT PIT BETWEEN 0% AND 15% (h: v) SLOPE. (TO BE FIELD LOCATED) EXISTING CONTOUR INFORMATION SHOWN ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS 7 INSTALL INLET PROTECTION PER GEO CURVE INLET FILTER VEGETATIVE FILTER STRIPS DETAIL ON SHEET 76 UPON COMPLETION OF THE INLETS. 8. ONSITE DUST CONTROL SHALL BE IN ACCORDANCE WITH THE GRATE INLET PROTECTION CITY OF AUSTIN ENVIRONMENTAL CRITERIA MANUAL SECTION FLOW ARROWS THE CITY OF LEANDER ENVIRONMENTAL INSPECTOR HAS THE AUTHORITY TO ADD OR MODIFY EROSION/SEDIMENT CURB INLET PROTECTION CONTROLS ON SITE THROUGHOUT THE DURATION OF THE ROJECT EXISTING CURB INLET 10 CONTRACTOR WILL CLEAN UP SPOILS THAT MIGRATE ONTO THE ROADS A MINIMUM OF ONCE DAILY. PROPOSED CURB INLET 11. SILT FENCE PLACED ALONG FUTURE ROADWAY TO BE PLACED OUTSIDE OF RIGHT OF WAY TO ENSURE CONTINUED USE CZP BOUNDARY 12 IN THE EVENT OF INCLEMENT WEATHER THAT MAY RESULT IN -A FLOODING SITUATION, THE CONTRACTOR SHALL REMOVE STREET FILL SPECIFICATIONS: INLET PROTECTION MEASURES UNTIL SUCH TIME AS THE WEATHER EVENT HAS PASSED. REFER TO MLA LABS, INC. GEOTECHNICAL INVESTIGATION PAVEMENT THICKNESS RECOMMENDATIONS FOR LIVELY TRACT, WILLIAMSON COUNTY, TEXAS

900

N/A.

885

LOT FILL SPECIFICATIONS: REFER TO GEOTECHNICAL INVESTIGATION REPORT.

TREE AND NATURAL AREA PROTECTION NOTES: ALL TREES AND NATURAL AREAS SHOWN ON PLAN TO BE PRESERVED SHALL BE PROTECTED DURING CONSTRUCTION WITH TEMPORARY FENCING. 2. PROTECTIVE FENCES SHALL BE ERECTED ACCORDING TO CITY OF AUSTIN STANDARDS FOR TREE

PROTECTION PROTECTIVE FENCES SHALL BE INSTALLED PRIOR TO THE START OF ANY SITE PREPARATION WORK (CLEARING, GRUBBING OR GRADING), AND SHALL BE MAINTAINED THROUCHOUT ALL PHASES OF THE CONSTRUCTION PROJECT.

4. EROSION AND SEDIMENTATION CONTROL BARRIERS SHALL BE INSTALLED OR MAINTAINED IN A MANNER WHICH DOES NOT RESULT IN SOIL BUILD-UP WITHIN TREE DRIP LINES. 5. PROTECTIVE FENCES SHALL SURROUND THE TREES OR GROUP OF TREES, AND WILL BE LOCATED AT THE OUTERMOST LIMIT OF BRANCHES (DRIP LINE), FOR NATURAL AREAS, PROTECTIVE FENCES SHALL FOLLOW THE LIMIT OF CONSTRUCTION LINE, IN ORDER TO PREVENT THE FOLLOWING: A SOIL COMPACTION IN THE ROOT ZONE AREA RESULTING FROM VEHICULAR TRAFFIC OR STORAGE OF EQUIPMENT OR MATERIALS;

B. ROOT ZONE DISTURBANCES DUE TO GRADE CHANGES (GREATER THAN 6 INCHES CUT OR FILL), OR TRENCHING NOT REVIEWED AND AUTHORIZED BY THE CITY ARBORIST, C. WOUNDS TO EXPOSED ROOTS, TRUNK OR LIMBS BY MECHANICAL EQUIPMENT. OTHER ACTIVITIES DETRIMENTAL TO TREES SUCH AS CHEMICAL STORAGE, CEMENT TRUCK CLEANING, AND FIRES. EXCEPTIONS TO INSTALLING FENCES AT TREE DRIP LINES MAY BE PERMITTED IN THE FOLLOWING

WHERE THERE IS TO BE AN APPROVED GRADE CHANGE, IMPERMEABLE PAVING SURFACE, TREE WELL, OR OTHER SUCH SITE DEVELOPMENT, ERECT THE FENCE APPROXIMATELY 2 TO 4 FEET

WHERE PERMEABLE PAVING IS TO BE INSTALLED WITHIN A TREE'S DRIP LINE, ERECT THE FENCE AT THE OUTER LIMITS OF THE PERMEABLE PAVING AREA (PRIOR TO SITE GRADING SO THAT THIS AREA IS GRADED SEPARATELY PRIOR TO PAVING INSTALLATION TO MINIMIZED ROOT AMAGE): WHERE TREES ARE CLOSE TO PROPOSED BUILDINGS, ERECT THE FENCE TO ALLOW 6 TO 10 FEET OF WORK SPACE BETWEEN THE FENCE AND THE BUILDING.

FEET OF WORK SPACE BETWEEN THE FENCE AND THE BUILDING, WHERE THERE ARE SEVERE SPACE CONSTRAINTS DUE TOTRACT SIZE, OR OTHER SPECIAL REQUIREMENTS, CONTACT THE CITY ARBORIST AT 974-1876 TO DISCUSS ALTERNATIVES. SPECIAL NOTE: FOR THE PROTECTION OF NATURAL AREAS, NO EXCEPTIONS TO INSTALLING LIMIT OF CONSTRUCTION LINE WILL BE PERMITTED.

TREE AND NATURAL AREA **PROTECTION NOTES (CONT.**

7. WHERE ANY OF THE ABOVE EXCEPTIONS RESULT IN A FENCE BEING CLOSER THAN 4 FEET TO A TREE TRUNK, PROTECT THE TRUNK WITH STRAPPED-ON PLANKING TO A HEIGHT OF 8 FT (OR TO THE LIMITS OF LOWER BRANCHING) IN ADDITION TO THE REDUCED FENCING PROVIDED 8. TREES APPROVED FOR REMOVAL SHALL BE REMOVED IN A MANNER WHICH DOES NOT INPACT REMOVED IN A MANNER WHICH DOES NOT IMPACT REES TO BE PRESERVED.

TREES TO BE PRESERVED. 9 ANY ROOTS EXPOSED BY CONSTRUCTION ACTIVITY SHALL BE PRUNED FLUSH WITH THE SOIL BACKFILL ROOT AREAS WITH GOOD QUALITY TOP SOIL AS SOON AS POSSIBLE IF EXPOSED ROOD QUALITY TOP SOIL AS SOON AS POSSIBLE IF EXPOSED ROOD REAS ARE NOT BACKFILLED WITHIN 2 DAYS. COVER THEM WITH ORGANIC MATERIAL IN A MANNER WHICH REDUCES SOIL TEMPERATURE AND MINIMIZES WATER LOSS DUE TO EVAPORATION 10. ANY TRENCHING REQUIRED FOR THE INSTALLATION OF LANDSCAPE IRRIGATION SHALL BE PLACED AS FAR FROM EXISTING TREE TRUNKS AS POSSIBLE 11. NO LANDSCAPE TOPSOIL DRESSING GREATER THAN 4 INCHES SHALL BE PERMITTED WITHIN THE DRIP LINE OF TREES. NO SOIL IS PERMITTED ON THE ROOT FLARE OF ANY TREE PRUNING TO PROVIDE CLEARANCE FOR STRUCTURES, VEHICULAR TRAFFIC AND

EQUIPMENT SHALL TAKE PLACE BEFORE DAMAGE OCCURS (RIPPING OF BRANCHES, ETC.) 13 ALL FINISHED PRUNING SHALL BE DONE ACCORDING TO RECOGNIZED, APPROVED STANDARDS OF THE INDUSTRY (REFERENCE THE NATIONAL ARBORIST ASSOCIATION PRUNING STANDARDS FOR SHADE TREES AVAILABLE ON REQUEST FROM THE CITY 14 DEVIATIONS FROM THE ABOVE NOTES MAY BE CONSIDERED ORDINANCE VIOLATIONS IF THERE IS SUBSTANTIAL NON-COMPLIANCE OR IF A TREE SUSTAINS DAMAGE AS A RESULT. 15. SEE TREE PLAN, SHEETS 11 - 14, FOR TREES TO BE REMOVED AND TO BE





	enne a				2-03	87
0.01 22		0 P	Ø		(1 , 1)	12
-						
		6	66	2]	
2	e Pos		75-	we-de	<u>1998</u>	P
602-	5	19 65	-	an south	司	0.0
	eretere R	-Q	75)	5 2 1 V		<u> </u>
				11.00		0
			"			
Gest	9783.8	2	SF		-	84
2	7	77)	777		5	20
	5		74		3	
2	\boxtimes				2	eff
6	<1		-	0g		
51	100 100	2.	Brindering	and the second	25 88 8	^b O
						0
2	22	6 \$	9		R	0
				6% ⁰	0040-000	0
0	0 2 2	9 9 10 10	i.	6	ථ යු	5
	0	0				





		μ	14, 1 () () () () () () () () () (
		DAT	
	SCALE: 1"= 100'		
		0. REVISIO	
n na serie de la companya de la comp No serie de la companya de la company No serie de la companya de la company	NOTES: 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY	Z	ann y commercial a
	VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY	DUSTIN J. GOSS 91805	an an taon an
	AND ALL UNDERGROUND UTILITIES. 2. EXISTING CONTOUR INFORMATION SHOWN IS AT 1 FOOT INTERVALS. THE CONTOURS ARE COMPUTER GENERATED USING CITY OF AUSTIN DATA.	The signal ensure On Gass 2/10/109	
815 11. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	LEGEND		a sa
	SD INLET	DDN I DALLAS 12.454.8711 #10028801	· · · · · · · · · · · · · · · · · · ·
	BOUNDARY DRAINAGE AREA BOUNDARY HEADWALL 786 PROPOSED CONTOUR LINE 786	DRT WORTH N, TX 78759 1 5 REGISTRATION	· · · · · · · · · · · · · · ·
3		E-D/ INEI HOUSTON I F STE 200 I AUSTI	
		PAP ENG ENG 3, 1 ISTRATION #470	······
		AUSTIN I SAN	
			·. · · · · · · · · · · · · · · · · · ·
8 1 875		Ш 5 0 П 5 0	
		HAS EXAS V SHEE	
		N PLAN	an a
	· · · ·	RAC DRAIN	
		TV OF TORM	
		IVEI CI CI	
		CITY JOB No JOB NO DATEFEBRUARY 2019	
	CITY OF LEANDER APPROVAL	DESIGNER RBB CHECKED S DRAWN TK SHEET 12 Of 83	·····
			····

 U Elekeristerziewenie/estate 		COMP	OSITE C	1			Cumulative	INTE	NSITY	DISCHARG		
DRAINAGE	AREA	C ₂₅	C ₁₀₀	A-C ₂₅	A.C.100	I.C.	Te	1 25yr	1 100yr	Q 25	Q 100	
A South and the second	acresi					70			((n/nr)	(CIS)	(CIS)	
					and working the			MURINE : H				
JLTIMATE CON	DITION D	RAINAG	E AREA	So				Et				
to ta	0.35	0.79	0.81	0 28	0.28	170%	5.00	10.1	12.5	2.9	36	
A1.02	0.71	0.69	0.72	0.49	0.51	53%	5.00	10.1	12.5	50	64	
A1.03	1.10	0.63	0.67	0.70	0.74	43%	5.00	10.1	12.5	7.0	9.3	
A1.04	1.46	0.64	0.68	0.94	0.99	44%	10.15	8,1	10.3	7.6	10.3	
A1.05	0.55	0.79	0.81	0.44	0.45	70%	5.00	10,1	12.5	4.4	5.6	
A1.06	1.89	0.64	0.68	1.21	1.29	44%	6.73	9.3	11.7	11.3	15.1	
A1.07	1.75	0.49	0.55	0.86	0.96	18%	6.73	9.3	11.7	8.0	11,2	
A1.09	0.38	0.79	0.81	0.30	0.31	70%	5.00	10.1	12.5	20	3.0	
A1.10	1.07	0.69	0.73	0.74	0.78	53%	5.00	10 1	12.5	7.5	9.8	
<u> </u>				pinove ar weeds						2		
A2.01	0.87	0.65	0.69	0.57	0.60	46%	5.00	10.1	12.5	5.7	7.5	
A2.04	4.24	0.70	0.72	0.04	0.00	0000			10.0		100	
A3.02	1.09	0.70	0.73	0.94	0.98	1000	8,69	8.5	10.8	0.6	10.6	
A3.03	0.58	0.80	0.82	0.47	0.48	72%	5.00	10.1	12.5	47	60	
A3.04	0.45	0.65	0.69	0.29	0.31	45%	5.00	10.1	12.5	2.9	3.9	
A3.05	0.24	0.81	0.83	0.19	0.20	73%	5.00	10.1	12.5	2.0	2.5	
A3.06	0,91	0.65	0.69	0.59	0.63	46%	6,24	9.5	11.9	5.7	7.5	
A3.07	0.61	0.63	0.67	0.38	0.41	41%	6.24	9.5	11.9	3.6	4.9	
A3.08	0.71	0.67	0.71	0.48	0.50	49%	5,00	10.1	12:5	4.8	6,3	
A4.01	1.57	0.62	0.66	0.98	1.04	41%	7.42	9.1	11.4	8.9	11.9	
A4.02	1.27	0.60	0.65	0.77	0.82	38%	7.48	9.0	11.4	6.9	9.4	
A4.03	0.53	0.64	0.68	0.34	0.36	44%	5.00	10,1	12.5	3.4	. 4.5	
A4.04	0.48	0.75	0.78	0.36	0.37	63%	5.00	10 1	12.5	3.6	4.7	
A4.05	1.20	0.70	0.73	0.83	0.87	54%	5:00	10,1	12.5	8,4	11.0	
A4.06	1.20	0.62	0.64	0.21	0.22	3002	5.00	1.01	12.5	2.2	2.1	
	(All Checks)	M.MA.	SANGAMANG	- AND		500.00						
A5.01	1.24	0.67	0.71	0.84	0.88	50%	5.81	9.7	12.1	8.1	10.7	
A5.02	0.77	0.68	0.72	0.53	0.55	51%	5.00	10.1	12.5	53	6.9	
A5.03	0.64	0.76	0.79	0.49	0.50	66%	5.72	9.8	12.2	4.8	6_1	
A5.04	0.82	0.66	0.70	0.54	0.57	48%	5,79	9.7	12.1	5.3	7.0	
A5.05	0.36	0.67	0.71	0.55	0.55	50%	5.00	9.6	12:0	5.1	6.6	
GOOD4	9.99		Mell_	Tate	0.201	5070			14.9	6.9		
AQ1.1	0.50	0.72	0,75	0.36	0.37	58%	5.49	9.9	12.3	3:6	4.6	
· - 243						{			я П		leanna ann an Aonailte I	
B11.1	1.09	0.66	0,70	0.72	0.76	48%	5.00	10,1	12.5	7.3	9.6	
B11.2	1.34	0.64	0.68	0.86	0.91	44%	5.00	10.1	12.5	8.7	11.4	
B11.3A	3.21	0.53	0.58	1.70	1.87	24%	9.34	8.4	10.6	14.2	19.8	
B11.4	0.79	0.4/	0.53	0.54	0.57	13%	6.00	1.5	9.6	10.3	7.4	
B11.5	1.14	0.64	0.68	0.73	0.78	44%	5.00	10.1	12.5	7.4	97	
B11.6	0.99	0.65	0.69	0.65	0.68	46%	5.19	10.0	12:4	6.5	8.5	
B11.7	0.11	0.79	0.81	0.09	0.09	69%	5:00	10.1	12.5	0.9	1.1	
								0				
B12.1	0.90	0.74	0.76	0.66	0.69	61%	5.00	10.1	12.5	6.7	8,6	
B12.2	1.04	0.73	0.76	1.05	1.12	26%	5.00	10.1	12.5	1.7	9.9	
B12.4	0.66	0.63	0.67	0.42	0.44	42%	500	10.4	10.4	0.0	6.6	
B12.5	0.66	0.75	0.77	0.49	0.51	62%	5.00	10.1	12.5	5.0	64	
B12.6	1.11	0.63	0.67	0,70	0.75	43%	5.30	10.0	12.4	7.0	9.3	
		a S	and a second		Contraction					percentral CONders R		
INT-1	1.80	0.39	0.46	0.70	0.83	0%	18.29	6.3	8,2	4.4	6.8	
INT-2	44.37	0.40	0.47	17.57	20.64	1%	30.64	4.8	6.4	84.9	131.1	

55

×.

ŝu

THIS DOQUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTROMICALLY AND MAT HAVE BEEN INADVERTENTLY ALTERED. HELY SALV ON FINAL HARDCOPY MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTROMICALLY AND MAT HAVE BEEN INADVERTENTLY ALTERED. HELY SALV ON FINAL HARDCOPY MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTROMICALLY AND MAT HAVE BEEN INADVERTENTLY ALTERED. HELY SALV ON FINAL HARDCOPY MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTROMICALLY AND MAT HAVE BEEN INADVERTENTLY ALTERED. HELY SALV ON FINAL HARDCOPY MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTROMICALLY AND MAT HAVE BEEN INADVERTENTLY ALTERED. HELY SALV ON FINAL HARDCOPY MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTROMICALLY AND MAT HAVE BEEN INADVERTENTLY ALTERED.

8

₩ ∰ X N = N Z	STREET FLOW	V AND INL	ETICALCUL	ATIONS			10 10 10 10				2011 1971	2.200	8 	I	1							ti in the second	n ⁰	n n	
ణి చి .ా	20 TEAR STU		1.31		Q spill	91	treet Crowi	STREET C.	APACITY	1	Ponded	Reduction	l Te	<i>12</i>	INLET	ON GRAI	DE CAPAC	NTY I	_g .	·····	Passto	SUMI Clogging	P INLET C	APACITY	
1	Inlet No.	Inlet Type	Drainage Area	Q 25 (Cfs)	Q pass Q (cfs) (t	total Wie :fs)	ith F-F Type (ft)	Slope (%)	a	-Yo (R)	Width (ft)	Factor (%)	Qa/La	La (ft)	Length (ft)	LLa	a/Yo (0/Qa	Qa (cfs)	Q pass (cfs)	iniet #	Factor (%)	Q total 1 (cfs)	ength (ft)	h ft)
a, g	ULTIMATE CO	NOTION L	ASE 2 DRAINAGE /	AREAS		51 52					Ng Persina							M							
یت دو دو دو ت ا	A1:01 " A1:02	G-1 G-1_₄	0.35	28	-	2.8	36 P 36 P	1.90%	0.42	0.30	5,49 8,10	0%	0.75	3.70 5.74	10 10	2.70	1.42 1.05	0.37	7.55 8.64	0.0					
	A1.03 A1.04	G-1	1.10	7.6			36 P 36 P	2.90%	0.42	0.45	9.64	0%	0.92	7.66	10 10	1.30	0.94	0.77	9.18 8.49	0.0 0.0	2 540 540		642 1961	u () 	201 201 1960 1960
	A1.03		1.89	4 4 11.3 6.0	4		36 P	8.30%	0.42	0.37	4/90 7/28	0%	0.73	6.05	10 15 5×5	1.65	1 56	0.60	7.28 12.48	0.0		а. ²			
*. 2 2	A1.08 A1.09	G-1 G-1=	0.48	2 7 3 0			36 P	2:10%	0.42	0.29	5.35 5.62	0%	0.75	3.67 3.99	10	2.72	1 45	0 37 0 40	7.48	0.0		2076 2			
	ALIO	G-1	1.07	7.5		45	36 P	2.00%	0.42	0.41	8:37	0%	0.87	8.60	10	1.18	1.03	0.86	8.74	0.0	27 (N (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1 (1	*		N 1	
SITE C Cumulative INTENSITY DISCHARGE	A3.01	G-1	4.34	8-0			30 P	1.50%	0.42	0.39	9.83	0%	0.85	8.69		1.49	0.92	0.67	8.57	0.0					
C100 A·C25 A·C100 I.C. Tc I 25yr I 100yr Q 25 Q 100 % (min) (in/hr) (in/hr) (cfs) (cfs)	A3.02 A3.03	G41 . G41	0.98	5.3 4:7		03 7	30 P 30 P	1.40%	0.42	0.40	7.92 7.45	0% 0%	0.87	6.12 5.53	10 10	1.63	1.04	0.61	8 68 8 51	0.0	: 140	·	387 190	B 0	
	A3.04 A3.05	G-1 G-1	0.45	2.9		20	30 P 30 P	1.40%	0.42	0.33	6.00 4.79	0%	0.79	3.72 2.66	10	2.69	1.27	0.37	7.92	0.0	<u>a.</u>				<u>Barra</u> <u>BR</u>
AREAS	A3.07 A3.08	G-1 G-1	0.61	3.6 4.8		8	30 P 30 P	2 00%	0.42	0.34	6.09 6.91	0%	0.83	4 58	10	2.18	1.25	0.46 0.58	7 96 8 30	D 0 0 0		2 	940 • 660		
0.81 0.28 0.28 70% 5.00 10.1 12.5 2.8 3.6 0.72 0.49 0.51 53% 5.00 10.1 12.5 5.0 6.4	A4 01	G-1	1.57	8.9		9	30 P	2.00%	0.42	0.45	9.54	0%	0.92,	9.64	10	1.04	0.93	0.96	9.20	0.0					
0.67 0.70 0.74 43% 5.00 10.1 12.5 7.0 9.3 0.68 0.94 0.99 44% 10.15 8.1 10.3 7.6 10.3	A4.03 A4.04	G-1 G-1	0.53	3.4 3.6			30 P 30 P 30 P	0.50%	0.42	0.41	8.68 8.24 8.52	0% 0%	0.89	7,77 3,89 4,10	10 10 10	1.29 2.57 2.44	0.99 1 1.02 1 1.00	0.39 0.41	8.79 8.79 8.89	0.0		206			
0.81 0.44 0.45 70% 5.00 10.1 12.5 4.4 5.6 0.68 1.21 1.29 44% 6.73 9.3 11.7 11.3 15.1	A4.05 A4.06	G-1 G-1	1.20	8.4 2.2		24 2	30 P 30 P	4.30%	0.42	0.39	7.53	0%	0.85	9.87 3.06	10 10	1.01	1.08 (1.70 °	0.99	8 54 7.05	0.0					-
0.55 0.86 0.96 18% 6.73 9.3 11.7 8.0 11.2 0.61 0.27 0.30 31% 5.00 10.1 12.5 2.7 3.7	A4.07	GI	1,27	<u>74.</u>		.4	30 <u>P</u>	1.60%	0.42		9	0%		141	10		FR.	8	NO	120	<u>e</u>	10%	7.4	10 0.	42
0.81 0.30 0.31 70% 5.00 10.1 12.5 3.0 3.9 0.73 0.74 0.78 53% 5.00 10.1 12.5 7.5 9.8	A5 02 A5 03	G-1 G-1	0.77	53 48		3	30 P 30 P	1.90%	0.42	0.44	9 21 7.34 10 01	0%	0.91	8.95 6.27	10	1.12	0.95 (0.89	9.10 8.47	0.0		214 	init Mit	creat in a local de la companya de l	
0.69 0.57 0.60 46% 5.00 10.1 12.5 5.7 7.5	A5:04 A5:05	G-1 G-1	0.82 0.78	5.3 5.1	5	3	30 P 30 P	0.50%	0.42	0.48	10.78	0% 0%	0.95	5.58	10	1.79	0.88	0.56	9.50 9.42	0.0					
0.73 0.94 0.98 55% 8.89 8.5 10.8 8.0 10.6	A5.06	G-1	0.36	2.5	2		30 P	0.50%	0.42	0.37	6.97	0%	0.83	2.94	10	3.40	114	0:29	8.33	0.0	90	1940	105		2
0.67 0.62 0.66 42% 8.69 8.6 10.9 5.3 7.1 0.82 0.47 0.48 72% 5.00 10.1 12.5 4.7 6.0	B11.1	G-1	0.50	38 73		3 3	30 P	× 0.50%	0.42	0.48	Line and Lin	0%		2.87	15	¥.07	0.00	370		0.0		10%	3.6	-15 0.2	21
0.69 0.29 0.31 45% 5.00 10.1 12.5 2.9 3.9 0.83 0.19 0.20 73% 5.00 10.1 12.5 2.0 2.5	B11.2 B11.3A	G-1 G-1	1 34 3.21	8.7 14.2	(B	7	30 P 30 P	4 60% 0.00%	0.42	0.39	7.51	0%: 0%:	0.85	10,15	10 5x5	0.98	1.08	1.02	8.53		P B11.5	10%	14.2	20 0.	45
0.69 0.59 0.63 46% 6.24 9.5 11.9 5.7 7.5 0.67 0.38 0.41 41% 6.24 9.5 11.9 3.6 4.9	B11 38 B11 4	G-1 G-1	2.90 0.79	10.3) 3 .5	30 P 30 P	0.00% 2.20%	0.42	0.69	7 19	0% 0%	0.84	6.52	5x.5 10	1.53	1.11 (0.65	त 8,41	0.0		10%	10.3	20 0.:	36
0.71 0.48 0.50 49% 5.00 10.1 12.5 4.8 6.3	B11.6 B11.7	G1 G1	0.99	6.5 0.9		.9	30 P	0.50%	0.42	0.51	MAX 4.48	0% 0%	0.39	8.90 6.56 1.21	10	1.12 1.52 8.25	1.08 0 0.82 0 1.60 0) 89) 66) 12	8.54 9.87 7.22	0.0					5
0.66 0.98 1.04 41% 7.42 9.1 11.4 8.9 11.9 0.65 0.77 0.82 38% 7.48 9.0 11.4 6.9 9.4	B12-1	G-1	0.90	8.7	6	17.	30 P	2.90%	0.42	0.39	7.41	0%	0.85	7 89	10	1.27	1.09	0.79	8.50	0.0		-16			
0.68 0.34 0.36 44% 5.00 10.1 12.5 3.4 4.5 = 0.78 0.36 0.37 63% 5.00 10.1 12.5 3.6 4.7	B12.2 B12.3 B12.4	G-1 G-1	1.77	8.6 4.2		5 2	30 P 30 P 30 P	2,70%	0.42	0:41	8.08	0% 0%	0.87	8.79 9.67 4.85	10	1.14	1.03 0 0.99 (0.88	8.74 8.91	0.0	47 G1				
0.73 0.83 0.87 54% 5.00 10,1 12.5 8.4 11.0 0.84 0.21 0.22 75% 5.00 10,1 12.5 2.2 2.7	B12.5 B12.6	G-1 G-1	0.66	5.0 7.0		0	30 · P 30 P	0.90%	0.42	0.42	8.60 10.64	0%	0.89	5.58 7.39	10 10 10	1.79	0.99 () 56	8.91 9.47	0.0			#		P
			E		ކ					ç	R 42			an 2000 (kan 1999)										*******************************	
0.72 0.53 0.55 51% 5.00 10.1 12.5 5.3 6.9 0.79 0.49 0.50 66% 5.72 9.8 12.2 4.8 6.1	STREET FLOW A	IND INLET	CALCULAT	IONS						U												Managaran (g			p p
0.70 0.54 0.57 48% 5.79 9.7 12.1 5.3 7.0 0.71 0.53 0.55 50% 6.12 9.6 12.0 5.1 6.6	Inlet	lolet F	Valpada	0.100	Q spill	Str	Seet Crown	Gutter	PACITY		Ponded	Reduction	Dealer		INLET	ON GRA	DE CAPA				Pass to	SU Clogging	MP INLET	CAPACITY	500 10 10 10 10 10 10 10 10 10 10 10 10 1
0.71 0.24 0.26 50% 5.00 10.1 12.5 2.5 3.2	No: LIVELY TR	Type ACT, PHAS	Area SE 2	(Cfs)	(cfs) (cf	s) ((%)	(ft)	(ft)	(ft)	(%)		(ft)	in (ft)		RUTO ²	-CrCa	i(cfs)	C pass (cfs)		ractor (%)	(cfs)	(ft)	n (ft)
0.75 0.36 0.37 58% 5.49 9.9 12.3 3.6 4.6	ULTIMATE CON	ITION DR/	AINAGE ARE	EAS								<u></u>]			Monorman and		10 10								
0.70 0.72 0.76 48% 5.00 10.1 12.5 7.3 9.6 0.68 0.86 0.91 44% 5.00 10.1 12.5 8.7 11.4	A1:01 A1:02 A1:03	G-1 G-1	0.35	3.6 6,4 9.3	3 6: 9	6 3 4 3	6 P	1.90%	0.42	0.32	8.07 9.21	0%	0.78	4.56 7.13	10 10	2.19	0.97	0.46	7.8 9.0	0.0			1990 		
0.58 1.70 1.87 24% 9.34 8.4 10.6 14.2 19.8 0.53 1.38 1.55 15% 12.63 7.5 9.6 10.3 14.8	A1.04 A1.05	Get Get u	1.46	10.3 5.6	10 10 15	3 3 6 3	8 P	2.90% 8.30%	0.42	0.43	8 90 5 40	0% 0%	0.89	11.50 7.46	-10 = 10	0.87	0.99	1.15 0:75	8.9 7.5	1.3	P A1.6				
0.72 0.54 0.57 52% 5:00 10:1 12:5 5:5 7:1 0.68 0.73 0.78 44% 5:00 10:1 12:5 7:4 9:7	A1:06 A1:07	G-1 G-1	1.89	15.1	1.3 16	4 3	6 P P	8.30%	0.42	0.42	8.65	0% 0%	0.88	18.54	16 5x5	0.81	101	1.24	13.3	8/1	P.A1.8	20%	11.2	20	0.41
0.69 0.65 0.68 46% 5.19 10.0 12.4 6.5 8.5 0.81 0.09 0.09 69% 5.00 40.4 42.5 0.9 1.1	A1.09 A1.10	G-1 G-1	0.38	3.9	201 D. 31 91	9 9 9 8 8 9		2.00%	0.42	0.39 0.33 0.45	6.21 9.54	0%	0.96	4.91	10	1.25 2.04 0.94	1.29	0.80	8.6 7.9	0.0	P Offsile	<u></u>	R. 171		
0.76 0.66 0.69 61% 5.00 10.1 12.5 6.7 8.6	(A2:01	· 61	0.87	7.6	* [4]	52° 🗾 9	0 IP	1.90%	0.42	0.43	8.50	0%	0.90	8.40	10	1.19	0.98	0.84	90	0.0				M	
0.76 0.76 0.79 60% 5.00 10.1 12.5 7.7 9.9 0.64 1.05 1.13 36% 10.01 8.2 10.4 8.6 11.8	A3.01	. G-1 2 1	1.34	10.6	10.	6 : 0	<u>e</u>	1.50%	0.42	0.50	MAX.	0%	0.98	10.88	10	0.92	0.84	1.09	9.8	09	PA3.2				
0.67 0.42 0.44 42% 5.00 10.1 12.5 4.2 5.5 0.77 0.49 0.51 62% 5.00 10.1 12.5 5.0 6.4	A3 03 A3 04	G-1 G-1	0.58	6.0 3.9	1.1 7	1 3		1.40%	0.42	0.44	9.27	0%	0.93	7.76 4.69	10	1 29	0.95	0.78	9.1 8.3	0.0		9465 54		in In Internet in the second s	
0.67 0.70 0.75 43% 5.30 10.0 12.4 7.0 9.3	A3.05 A3.06	G-1 G-1	0.24	2.5 7.5	2	5- 3 5- 3	D P	1.80% 1.80%	0.42 (0.42 (0.30	5.28 8.90	0% 0%	0.76 = 0.90	3.27 8.30 ×	10 10	3.06 1.20	1 40 0.97	0.33	7.6 9.0	0.0					
0.46 0.70 0.83 0% 18.29 6.3 8.2 4.4 6.8 0.47 17.57 20.64 1% 30.64 4.8 6.4 84.9 131.1	A3:07 A3:08	G-1 G-1	0.61	4 9 8:3	6	3 35 2 2		2.00%	0.42	0.37 0.40	6.94 7.88	0%: 0%:	0.83	5.84 7:28	10	1.71	1.14	0.58	8 3 8.7	0.0	1427 	2 19	825 380 1907	2	
در بالمربق (1997) (1997) در المربق (1997) در المربق (1997)	A4.01 A4.02	G-1 G-1	1.57 1.27	11.9 9.4	11 2.2 11	9 3 5 3	0 P) P	2.00% 1.70%	0.42 (0.42 (0.49 · 0.50	11.84 MAX	0% 0%	0 97 - 0 96	12.24 11.76	10 10	0.82	0.85	1.22	9.7 9.8	2.2 1.7	P A4.2 P A4.3				
	A4.03 A4.04	G-1 G-1	0.53	4.5	4		P	0.50%	0.42 (0.50	MAX 9.87	0% 0%	0.98	6.36 5.04	10 10	1.57 1.99	0.84	0.64 0.50	9.8 .9.3	0.0 0.0	Sala Inte	2	1223 1421	P. C	80 - Con B N
5	BANE	and the second se	and considered and the	CHUR AND D	1 11.	AN 11 🔝		4.30%	araz 8 (f	JAZ	0.04	0%	MARKED B	12.28	10	1581	0.99	1.23	.89	20	PA47	6		1 sa 1	1962 1962
5	A4.05 A4.06 A4.07	G-1 .	0.26	2.7 9.9	2.0 12	7 3 0 3	P P	4.50% 1.00%	0.42 (0/27	4.55	0% 0%	0.73	3.77	10 10	2.66	1.58	0.38	73	0.0		10%	12.0	10	0.58
5	A4.05 A4.06 A4.07 A5.01	641 . 641 . 641 .	0.26 1.27 1.24	2.7 9.9 10.7	2 1 2.0 12 10	7 3 0 3 7 3) Pl) Pl 	4.50% 1.00% 1.90%	0,42 (0,42 0,42 (0.27	4.55	0% 0% 0%	0.73	3.77	10 10 10	2.66	1.58 8 0.87	0.38 - 1.12	7.3 - 9.6	0.0 F	P A5/2	-10%	12.0	# 10	0.58
5	A4:05 A4:06 A4:07 A5:01 A5:02 A5:03 A5:04	G-1 G-1 G-1 G-1 G-1 G-1 G-1 G-1	1.20 0.26 1.27 1.24 0.77 0.64 0.89	2.7 9.9 10.7 6.9 6.1	2.0 12 10 11.1 8.0 10.5	7 3 9 3 7 9 9 3 1 9 1 9 1 9 1 9	P P P P P P P P P P P P	4.50% 1.00% 1.90% 1.90% 0.50%	0.42 0 0.42 0 0.42 0 0.42 0 0.42 0 0.42 0	0.27 0.48 0.44 0.50	4.55 11.04 9.14 MAX	0% 0% 0% 0%	0.73	3.77 11.17 8.85 6.29	10 10 10 10 10	2.66 0.90 1.13 1.59	1.58 8 0.87 0.96 0.84	0.38	73	0.0 1.1 0.0 0.0	P A52	4 10%	12.0 12.0	ni 10 Sala Nac Litte	0.58
5	A4.05 A4.07 A4.07 A5.01 A5.02 A5.03 A5.04 A5.04 A5.05 A5.06	6-1 6-1 6-1 6-1 6-1 6-1 6-1 6-1 6-1	0.26 1.27 1.24 0.77 0.64 0.82 0.78 0.36	2.7 9.9 10.7 6.9 6.1 7.0 16.6 3.2	2.0 12 10 11.1 80 6. -0.7 6. -0.4 6.		P P P P P P P P P P P P P P P P P P P P P P P P P P P P P P	4.50% 1.00% 1.90% 1.90% 0.50% 0.50% 0.50% 0.50%	0.42 0 0.42 0 0.42 0 0.42 0 0.42 0 0.42 0 0.42 0 0.42 0 0.42 0	0.27 0.48 0.44 0.50 0.50 0.50 0.50 0.40	4.55 2011.04 9.14 MAX MAX MAX 7.95	0% 0% 0% 0% 0% 0% 0%	0.73 =	3.77 11.17 8.85 6.29 6.40 6.37 3.68	10 10 10 10 10 10 10 10 10 10	2.66 	1.58 8 0.87 0.96 0.84 0.83 0.83 0.83 1.04	0 38 - 1.12 0.89 0.63 0.64 0.64 0.64 0.37	7.3 9.6 9.1 9.8 9.8 9.8 9.8 8.7	1.1 1.1 0.0 0.0 0.0 0.0	P A52 S A33 S A33			# _10 10 100 100 100 100 100 100	0.58

D

ŝ

0.0 0.0

STREET FLOW 100 YEAR STOP	and Inli M	ET CALCULA	TIONS							U U		F -						area ann an Aonaichtean ann ann ann ann ann ann ann ann ann		******	110				D.
		1						STREET CA	APACIT	Y	•• <u>201</u> 32				INLET	ON GRA	DE CAP	ACITY				SU	MP INLET	CAPACIT	Y
				Q spill		Street	Crown	Gutter	l l		Ponded	Reduction			v	2 2.2		8			Pass to	Clogging			
Inlet	Inlet.	Drainage	Q 100	Q pass	Q total	Width F-F	Type	Slope	a	Yo	Width	Factor	Qa/La	La	Length	L/La	a/Yo	Q/Qa	Qa	Q pass	Inlet	Factor	Q total	Length	h
No	Туре	Area	(cfs)	(cfs)	(cfs)	(11)		(%)	(ft)	(ft)	(ft)	(%)		(ft)	(ft)		ii		(cfs)	(cfs)	о ж	· (%)	(cfs)	(ft)	(ft)
LIVELY II	CAUL PE	ASE 2	DEAC					5 <u> </u>						1990)), 1999) 1990)											
OLTIMATE CON		RAINAGE AI	New States		18 V	January Mandalana and A	ll					50					1					L		L	hanna
A1:01	G-1	0.35	36	1	3.6	36	P	1,90%	0.42	0.32	6.07	0%	0.78	4.56	10	2.19	4 31	0.46	7.8	0.0	1941				
A1.02	G-1	0.71	6.4		6.4	36	P	1.00%	0.42	0.44	9.21	0%	0.90	7.13	10	1.40	0.97	0.71	9.0	0.0		1000			1051
A1.03	G-1	1-10	9.3	R	9,3	a 36	. P	1.00%	0,42	0.49	11.27	0%	0.97	9.60	10	1.04	0 85	0.96	9.7	0.0	*		171.		
A1.04	G-1	1.46	10.3		10.3	36	P	2.90%	0.42	0.43	8.90	0%	0.69	11.50	10	0.87	0.99	4,15	8.9	1.3	P A1.6	125	188 217.0		
A1-06	G 1 G	1 80	2.6		.5.6	36		8.30%	0.42	0.29	5.40	. 0%	0.75	7.46	s 10	134	1.44	0_75	7.5	0.0		GADE STATE - OF AD - AMPRICATION	1940. 		GED HIND HOUSEBOOK
A1-07	GI	1.75	11.2	<u>- 1-9</u>	11.2		P	0.00%	0.42	UAZ	0.03	0%	0.65	10.04	- 15 5x5	0.81	1.01	1.24	7,3.3	51	P A1.8	20%	14.2	20	0.44
A1.08	G-1	0.48	3.7	3.1	6.8	36	P	2.10%	0.42	0.39	7.91	0%	0.86	7.97	10	1 25	1 07	0.80	8.6	00		20%	11.4	20	9.41
A1.09	G-1	0.38	3.9		3.9	36	P	2.00%	0.42	0.33	6.21	0%	0.79	4.91	10	2.04	1.29	0.49	7.9	0.0		ing and the second s Second second s			
A1.10	G-1	1.07	9,8		98		P	2.00%	0.42	0.45	9.54	0%	0.91	10.67	10	0.94	0.94	1.07	9.1	0.6	P Offsite	Geo 1	145-	a	
-		0.07	-											4			11.11.11.11.11.11.11.11.11.11.11.11.11.		. 1						
AE UI	161	0.8/	<u>P</u>		A.5-	<u>v 30</u>		1.90%	0.42	0.43	8,50	0%	0.90	8.40	10	1:19	0.98	0.84	9.0	0.0		Service Charge of	10 10 10 10 10	M	
A3.01	. G-1	1.34	10.6		10.6	30	P	1 50%	0.42	0.50	ΜάΧ	n%	nca	10.88	10	0.02	0.84	1.00	0.9	no	0 4 2 2	ann an Anna an Anna Cailgeann an Anna			
A3.02	G-1	0.98	7.1	0.9	8.0	30	P	1.40%	0.42	0.46	10.01	0%	0.93	8.58	10	1.17	0.91	0.86	9.3	00	(F (59-6) (60		180 Sale - 1		
A3.03	G-1	0.58	6.0	1.1	7.1	30	P	1.40%	0.42	0.44	9.27	0%	0.91	7.76	10	1.29	0.95	0.78	9.1	0.0	entra de la composición de la composici Composición de la composición de la comp	14 14	(#5	ia i	963
A3.04	G-1	0.45	3.9		3.9	30	P	1.40%	0,42	0.36	6.79	0%	0.83	4.69	10	2 13	1.16	0.47	8.3	0.0	anna an		195		teleti
A3.05	G-1	0.24	2.5		2.5	-30	P	1.80%	0.42	0.30	5.28	0%	0.76	- 3.27	10	3.06	1.40	0.33	7.6	0.0		L		()	1999 1999
A3.00		0.91	1.5		1.5	30	<u> </u>	1.80%	0.42	0.43	8.90	0%	0.90	8.30	10	1.20	0.97	0.83	9.0	0.0	4				and the second
A3.08	G1	0.71	63	THE REPORT	63	30 7		2,00%	0.42	0.37	7.88	0%	0.83	5.84	10	1.20	1.14	0.58	83	0.0			125		<u></u>
						N DIS					1,00			1.60	10	0.00		0.15	9.2		1961 				
A4.01	G-1	1.57			11.9	30	. P	2.00%	0.42	0.49	11.84	0%	0.97-	12.24	10	0.82	0.85	1.22	9.7	2.2	P A4.2	5	1992		
A4 02	G-1	1.27	9.4	2.2	11.5	30	P	1.70%	0.42	0.50	MAX.	0%	0.96	11.76	10	0.85	0.83	1 18	9.8	1.7	P.A4.3			C. Berry	
A4.03	G-1	0.53	4.5	1.7	6.2	30	<u>.</u>	0.50%	0.42	0.50	MAX	0%	0.98	6.36	10	1.57	0.84	0.64	9.8	0.0		2	720	Rama	and the second
A4 04	01	1 20	4 / 44 0		4.7	30		0.50%	0.42	0.46	9.87	0%	0.93	5.04	10	1.99	0.92	0.50	.9.3	0.0		#	1982	200	N
A4.06	Gat	0.26	27		27	30	D	4.30%	0.42	0.42	0.04	0%	0.69	12.20	10	0.81	1.59	1.23		20	P A4./	8	1960 - 1960 2019 - 2019	Sile And the second	562 - 512 - 113 - 1166
A4.07	G-1	1.27	9.9	2.0	12.0	39	P	1.00%	0.42	stati	10000000000000000000000000000000000000	0%	San	(1977) (1977)	10	- 2002			1. 14 1 4 1 1 14	- 9.9		10%	12.0	10	0.58
anti-anti-anti-anti-anti-anti-anti-anti-					anadimontan pita	Paragram and a second	= 8		ļ						Contraction of the second s				U			jus var			endingen sine - States - States (
A5.01	G-1	1,24	10.7		10.7	30	P _	1.90%	0.42	0.48	11.04	0%	0.96	11.17	10	0.90	0.87	1.12	9.6	1.1	P A5.2	12	540 J	22	81
A5.02	<u>G-1</u>	0.77	6.9	1.1	80	30	P	1.90%	0.42	0.44	9.14	0%	0.91	8.85	10		0.96	0.89	9.1	0.0	9800 (1	NI III	1005 B	192	
A5 04	G-1	0.69	7.0	.07	63	30	6	0.50%	0.42	0.50	MAX	0%	0.96	6.29	10	1.59	0.84	0.63	9.8	00			1933	ESR.	*
A5 05	G-1	0.78	6.6	-0.4	6.2	30	P	0.50%	0.42	0.50	MAX	0%	0.98	6.37	10	1.57	0.83	0.64	9.8	0.0	S 433	100 870	n Administration of the second		<u>sein (</u>
A5.06	G-1	0.36	3.2		3.2	30	P	0.50%	0.42	0.40	7.95	0%	0.87	3.68	10	2.72	1.04	0.37	8.7	0.0	a	CZ	anna Miranad 22		
1			-		 Sindesza 				1					[]	1022001012002 DD105		pt.							1	
A01:1	<u>6-1</u>	0.50	4.6		4.6	30	P	0.50%	0.42	-157 - 17 E		0%			15						- <u>7</u> 4	10%	4,6	15	0.25
Bit.t.	Cal	1.09	9.6		9.6	30	Do	4.20%/	0.42	0.60	8.8 K.V	03/	0.00	0.70	20	6 00	0.04	0.00	0.0	0.0		l			
B11,2	G-1	1.34	11.4		11.4	30	P	4.60%	0.42	0.43	8-67	0%	0.90	12.77	10	0.78	0.04	1.28	89	2.5	P 911 6			mental Summer	and the second s
B11.3A	G-1	3.21	19.8		19.8	30	P	0.00%	0.42	100		0%	e		5x5	(M 22 M -	EL .	6	1000000	(March March 1997)	in the second se	10%	19.8	20	0.56
B11.3B	G-1	2.90	14.8	i:	14,8	30	P	0.00%	0.42		Harrison Harrison Harrison	0%	<u> </u>		6x5				ann an Anna Carl	and and the second	ausea 🕅	10%	14.8	20	0.46
B11.4	G-1	0.79	71	•	7.1	30	P	2.20%	0.42	0.41	• 8:21	0%	0.86	8.13	10	1.23	-1.02	0.81	8.8	0.0		Connect Manager	15 M	2963	e
BTI-5	Gel	1.14	9.7	2.5	12.2	30	P	3.50%	0.42	0,46	9 79	0%	0.93	13,19	10	0.76	0.92	1,32	9,3	3.0	P-11.7	: <u>8</u>		and the second second	ana Maria
B11.7	Gil	0.11	0.3	5.2	6.0	30		0.50%	0.42	0.50	MAX	0%	0.98	6.43	10	1.56	0.83	0.64	9.8	0.0	S 11.7	le.	R		
	<u></u>		1956 B	W cdu	194792			0.0078	0.42		- MIAUA	a 1779	0.00	0.08	10	1.00	0.03	1 1/104 0	3.0	0.0					
B12.1	G-f	0.90	8.6		8.6	30	P	2.90%	0.42	0.42	8.44	0%	0.89	9.74	10	1.03	1.00	0.97	8.9	0.0	energia di Constanti di Constanti Mi	State of the second	in the second	100	
812.2	Q-1	1.04	9.9	Ę.	9,9	30	9	2.70%	0.42	0.44	9.31	0%	0.91	10.84	10	0.92	0.95	1.08	9.1	0.8	P B12.5				
B12.3	<u>G-1</u>	4.72	11.8		11.8	30	P	2.70%	0.42	0,47	10.42	0%	0.94	12.49	10	0.80	0.89	41.25	9.4	2.3	P B12.4				
B12.4	6-1	0.66	0.5	2.3	7.9	30	<u>P</u> _	0.90%	0.42	0.49	. 11.73	0%	0.97	8.14	10	1.23	0.85	0.81	9.7	0.0	2500	390 	E	5520	E.
B12.5	G.1	1.11	04	0.8	0.2	20		0.90%	0.42	0.48	10.81	0%	0.95	1.52	10	1.33	88.0	0.75	9.5	0.0	2001	000	R.		
Carl March March 1				1	00		<u> </u>	0.30%	N.42	U.SC	ANN	076	1.00	<u>. a to</u>	<u></u>	1.00	0.01	0.99	10.0	0.0	1 W W 🕅	1985	e	680	300

د تو تو

7

ی چ ش ۸

6.4

· a

1 d

9

64

a

S	
	INTERNATION OF THE RESIDUAL OF
	THE FRANCTION I FORT I FORT I DALLARS
	<text><text></text></text>
	CITY JOB No. JOB NO: 50816-21 DATE DECEMBER 2018 DESIGNER RBB
CITY OF LEANDER APPROVAL	SHEET 13 Of 83

1

30

5a

1990 B

a t



5.

в

e 13





2

18

5 (S)

i^o

c

8<u>°</u>

<u>41</u>

2

 if
 if
 if
 if

 if
 if
 if
 if</th

• a

5 2 1

정 년 문 또 음

15 49 20 22 v2

69

12

78 5、195

51 51

2, 23

₽ *

¢)

2.

13

NOTE 1. THE UTIL WAY INDE OR CON LOC BEF(TO ALL ASS FAIL PRE UTIL 2. ALL NOT 3. THE 25 NOR SHO 4. EXIS HER AT COM LEA 5. ALL 95%	ES: LOCATIONS OF ITIES ARE SHOW ONLY AND HA PENDENTLY VEI TS REPRESENT TRACTOR SHAL ATION OF ALL I ORE COMMENCIN BE FULLY RESP DAMAGES WHIC OCIATED BY TH URE TO EXACTI SERVE ANY ANI ITIES. RCP IS CLASS ED. HYDRAULIC GR YEAR EVENT IS MAL DEPTH CA WIN OTHERWISE. TING CONTOUR E ON THIS PLA ONE (1) FOOT I IPUTER GENERA NDER DATA. FILL AREAS SE PRIOR TO UTIL	EXISTING UNDERGROUND WI IN AN APPROXIMATE VE NOT BEEN RIFIED BY THE OWNER ATIVE. THE L DETERMINE THE EXACT SISTING UTILITIES IG WORK, AND AGREES ONSIBLE FOR ANY AND H MIGHT BE E CONTRACTOR'S LY LOCATE AND D ALL UNDERGROUND HI UNLESS OTHERWISE ADE LINE (HGL) OF THE DEFINED BY THE LCULATION UNLESS INFORMATION SHOWN IN SHEET ARE SHOWN IN SHEET ARE SHOWN INTERVALS THEY ARE TED USING CITY OF IALL BE COMPACTED TO ITY INSTALATION.			
л л л л		WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE DOUBLE WW SERVICE SINGLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WATER LINE EXISTING STORM DRAIN LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE PROPOSED CONTOUR LINE PROPOSED CONTOUR LINE	<text></text>		TAPETERA REQUERTS ON FORT WORTH DALAXSON TANDAR IN ANTONIO FORT WORTH DALAXSON TAPETERA REQUERTS ANTONIO FORT WORTH DALAX TODOL N MODAG EXP. BLOG 3, STE 2001 AUSTRU, TX 178750 I ST2454 BT11
Velocity 12.37 8.34 8.37 6.93 13.54 13.55 Velocity (fi/s) 13.32 8.90 8.92 7.32 14.81 14.81 14.81	25 yr Stor Depth (Out) (ft) 1.50 0.76 0.74 1.22 3.03 1.58 1.58 1.58 0.90 0.88 1.41 2.55 0.90 0.88 1.41 1.90 0.88	Hydraulic Hydraulic Grade Line (in) (ft) 879.18 880.06 882.58 882.59 882.59 882.59 882.59 882.69 880.21 883.02 883.02 883.02 883.66 882.83 20NTAL CALES: ZONTAL CALES: 20NTAL 20NTAL 20NTAL 20NTAL 20NTAL 20NTAL 20NTAL 20NTAL 20NTAL 20NTAL <td>Kydraulic Grade Line (Out) (ft) 878.91 878.91 879.76 82.75 875.71 881.63</td> <td></td> <td>LIVELY TRACT, PHASE 2 OUTY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE B11, (2 OF 2) & LINE B11.34</td>	Kydraulic Grade Line (Out) (ft) 878.91 878.91 879.76 82.75 875.71 881.63		LIVELY TRACT, PHASE 2 OUTY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE B11, (2 OF 2) & LINE B11.34
	25-YR HGL 100-YR HGL 50/ HGL		e e e t z t t t t t t t t t t t t t t t	WAL	CITY JOB No JOB NO DECEMBER 2018 DESIGNER RBB CHECKED DRAWN TK SHEET 15 Of 833

8

In 182

7 // //

₽ 7.

招 际

1

1 B



I

а ч Л

B12.4 812.5 B12.6 Label B11.2 B11.3B **B11.4** B11.5

Label B11.2 B11.38

PROPOSED 25-YR HGL 100-YR HGL

S	CALES:
F	RIZONTAL
T	ICAL
í.	EGEND:
N	D

			ANNO DAVIS DISA Y
			si Marina da Marina da
STORM DRA	ÍN	-	
			2

=25yr HGL

BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S ala Managantawaa FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES. 2. ALL RCP IS CLASS III UNLESS OTHERWISE

55

NOTES:

e:

NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS

1. THE LOCATIONS OF EXISTING UNDERGROUND

UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT

LOCATION OF ALL EXISTING UTILITIES

- SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN
- AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING CITY OF LEANDER DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO

		ia.		95% PRIOR TO UTLET	INSTALATION.	M
			25 yr Stor	m Event	una de la companya de	
	Flow	Velocity	Depth	"Hydraulic "	Hydraulic	
_	(cfs)	-(ft/s)	(Out) (ft)	Hydraulic Grade Line (In) (ft)	Grade Line (Out) (tt)	
	8.8	8,18	1:50	8/0.30	875:43	
		8,69	Z.28	861.89 975.270	801.99	
-	5.5	9,59	0.01	01/000	90,70	
	70	° 0380 6 69	1 0.91 · · ·	861.57	863.61	948 N
	<u>7.0</u>	10.52	1.57	863.74	863.17	
	4.3	9.62	1.18	857.86	857.88	
1.520	5.0	6.72	1.77	856.87	856.82	
	7.0	3.98	1.84	856.42	856.37	
14		An an an a start of the start o	100 yr Sto	rm Event		
	Flow	Velocity	Depth	Hydraulic	Hydraulic	
	(cfs)	(ft/s)	(Out) (ft)	Hydraulic Grade Line (In) (ft)	Grade Line (Out) (ft)	
	.11.5	6.51	2.55	877.69	877,48	
	15.0	4.76	2.90	862.84	862.61	
	7.2	4.08	2.85	857.96	857.91	
-	9.9	5.58	1.74	852.34	:852:12	
	10.0	<u>\$.65</u>	1,98	864.37	864,21	
_	11.8	6.70	2,21	863.78	803/03	
08	5.6	3.15	3.04	859,70	0027.74	
uncli	0.5	5.05	3:29	857 6/.	857.54	
-100	870	-9151/		1007/057		
		14.1	4 LF 18" RCP		. 음 리 및	2
	000	II		968	e.	
	000			···	44 v d	
	to at state				p.	
	866			800		
		37 41			8	
	864			864	Ð	¢.
				anna ann a sua ann ann ann ann ann ann ann ann ann a		
	862			862		
	860	FINISHED	. 8	860	ĩ	
	000	GRADE	Ę.		14	U S E
		NATURAL		OP 0		
	828	100vr HCl		000		
55		SE NO			<i>u</i> *	
	856	20yr HGL		856		l L a d C
	W				21	L.≂H ZШ
	854	1 ²	Very N 1 1 1 1 1	854		
				67		
	852	6	01.	852		
	u testere					
	950				i.	
	000			and antipersected sector of the sector of th		
			and here and the second se			
	848			348		
					54	
	846			846	ų:	
						20
	844		- 10	844	70	
			2 <u>8 8</u>		σ	
	842		54.33	842	<u>.</u>	
	"MTA	× *	10 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)			
12		н	i Para ang			
	840	1.5	S OF L		r,	34 °
			2.6	NLE RUC	Š.	
Σ	838		****	838		
			o × 8 8 9	58.58	ο.	CITY JOB No.
	836		A C A A	836		JOB NO. 50816-21
	92 					DATE DECEMBER 2018
	ŕ.		9			DESIGNER RBB a
S	D-B12.6		4 2	**		
	HI H		82	¥.	т Т	
The second s	п			CITY OF	LEANDER APPROVAL	SHEET 16 Of 83
			0+00	0+75		

X 1 DUSTIN J. GOSS 91805 91805 15/15/18 0.AL LAS 454.8711 2 S ENGINEER STORMDRAIN PLAN & PROFILE LINE B11 LATERALS CITY OF LEANDER, TEXAS JOB No. _____ DECEMBER 2018 GNER RBB


8 8 E E E E E

C Frank Strand Strand Astor and

0° 07

Velo (ft. 8.9 7.3 6.4 8.0 13. 5.0 10. 13. 10. 13. 10. 13. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 13. 10. 13. 10. 10. 13. 10. 10. 13. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 13. 10. 13. 10. 13. 10. 13. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 13. 10. 10. 10. 10. 10. 10. 10. 10. 10. 10	city /s) 20 39 12 14 53 37 32 08 10 03 10 10 10 10 10 10 10 10 10 10	De (Ou 3 4 4 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	100 yr Stor pth 1) (ft) 35 01 29 82 54 62 71 98 74 34 34 34 34 34 34 34 34 34 34 34 34 34	m Event	Hydraulic Grade Line 856.95 857.98 859.15 860.18 862.73 863.81 867.28 871.03 872.49		Grade	Hydraulic Line (Out 856.53 857.54 859.15 859.74 860.18 863.63 864.21 866.88 871.23						A: 0+43.5 : 0+00.0 I4.14. "SE JRB INLET ND CONST 	0 "SD-B 0 "SD-B B12.6" RUCTION B 025 010 B 025 010 B 025 010 C 00 C 00 C 00 C 00 C 00 C 00 C 00					STA: 0+2 STA: 0+2 STA: 0+2 IO' CURB STA: 0+2 IO' COR STA: 0+2 IO' COR STA	ALLET BIT TRUCTION	SD-B12.1 SD-B12.1 SD-B12.5 B12.5 PVC - B12.5 B12.5 PVC - B12.5 SD-B12 SD	
				K	X					۶. ۲	20				X			Ś			Cont .		Symmetry and the second s
s 1 22	W.		2	243.0	3 LF 24"	RCP	= 40 T		T M		le le							335.	31 LF	18" RCP			5 25
	26.55 26.55				1											CINICUE			Sentines)				
	(out) 8														NAT	URAL GRO		A		E.			
	ے اور		S		1° 	· .97								·•				¥	Y			- 74 - 74	
- - -	0-812.	12	5 ;) s									L.	Ż					maanaaa		27 01	50%
	24***	X								1		<u>.</u>	đ			- martinera	and the second				mmentant	a 8 10 5	
	50.00	E BREJ			2			and the second second	-					ana	0 2	507 Star	and the second				PVC "W	LAST 0	2.50
	i Z	24 25 6 :			<u></u>			annui	(another the				RC-	BV6	and the second								
					1007 105	and the second second			*B12	0	eren eret			Turn A	3.1- 0.2	507							
			- HONY HOL-		-201 ²⁰	5073	nunnen en e	anananan an a					P	VC MM									
				B	nanananan Reference					T	.1	1		:							5		
0 1	.00%	and a second second	and the second se																				ľ
					,													j.					
F												1						et) 866		E.			
g	9								5						a svite or skilling with the first of a state of a			L L			Gen Dec vy Incidentia de Antinica		
2.4" 812-A	856.19 856.69 856.69	SMERSING - 2							2.3° 860.91 860.91	361.41	2.2 812-8	862.23						0.0					
B S S B S S S S S S S S S S S S S S S S	ieg.							-812.1	-50-8 FL (ou FL (n)	L (in))-812.1	SD-B							S.	li manananan reconstruction	р. 			
POCTON	12.01							JS. E1.	+00.00 12.01 12.01	12.3" F	NCTION	12.01 [°]	A STATE					32 18					
STA D								2+5 2+5	STA: 0. "SD-8	"SD-8	10 11 0	8-05. 1-05.		Para Para Para Para Para Para Para Para				Į					
	382							sts -	188	18" STA	1 20 2	88						STA	8				
856.30	856.55	857.18	857.80	858.43	859.06	859.68	860.31	860.93		861.56	862.68		863.31	863.93	864-56	REST	20 81 81 80	10-000	866.43	867.06	867.68	868 31	

7.58

10 ve







| T FLOW AND | INLETCALCUL

 | |

 | | Crown

 | Curb
 |
 | арасіту | | Ronded
 | | 9
0
11
 | | INLET C
 | N GRADE | CAPACITY | | |
 | S | UMP IN LI
CURB | T CAPA
(with De | CITY |

--
--|--
--
--
--|---
--

--
--	--

--
--
--|--|--|--|---|---|--
--|-----------------|--|---|--|
| det link
lo Tyr | et Drainage
pe Area

 | Q 25
(cfs) | Q pass Q tot
(cfs) (cfs

 | e Width F-F
(ft) | Туре

 | Height
(ft)
 | Slope
(%)
 | a ''Yo
(ft) (ft) | Height
(R) | Width
(ft)
 | Eo | SW
 | Sx | Se – L
 | ti di | | QÌ | Opass
(cfs) | Pass to Inlet
 | Qtotal
(cfs) | Length
(ft) | -d (ft) | d
(d 5 |
| E CONDITIO
91 - State
92 - Condition
93 - Condition
93 - Condition
93 - Condition
94 - Condition
95 - Condition
96 - Condition
97 - Condition | N DRAINAGE A
1.08
1.089
1.023

 | 6 58
5 11
1 96 |)) 6.6
.02. (153
.20

 | 27
27
27 |

 | 0.50
0.50
0.50
 | 0.60% 0
1.00% 0
0.60% 0 | 0.42 = 0.5
0.42 0.4
0.42 0.3
 | 04 == 0.50
2 1210.50
34 110.50 |
 | 0.34 | 0.28
 | 0.04 | 0 13 11
0 19 9
0 27 4 | 48 10
39 10
47 1 10
 | 0.97 | 6.4
5.3
2.0 | 0.2 | | |
 | | |
| 4 | 1 0.71
1 0.72
1 0.61
1 0.37

 | 3.96
4.23
4.09
(3.01) |

 | 27
21 | P
P
P

 | 0.50
 | 0
 | 0 42 0 0 0 4
0 42 0 0 0 4
0 42 0 0 4
0 42 0 0 4 | i 10.50
i 0.50 | 973
7.32
 | 0.49
0.51
10.63 | 0.28
 | 0.04 (
0.02 (
0.04 (
0.04 (| 0 17 7
0 18 7
0 21 5
 | 8 10
6 10 | 1.00
1.00
1.00 | 4.2
4.1
- 3.0 | 00 |
 | | | | |
| 8 G
9 G
0 S | 1 09
0.40
1 0.55

 | 7,99
3,20
3,51 | 8.0
37
3.5

 | 2
7 | P
P U

 | 0.50
 | 190%
 | 0.42 0.4 | 4 0.50
2 0.50 | 8 74
5.48
 | 0.85 | 0.28
 | 0.04 | 0.18 14
 | 76 10
76 10
10 | 1.00 | 3.2 | 0.0 |
 | 35 | 10 | 0.24 | |
| и | 1 0.63
1 1.03

 | 3 49 6 84 | 3.6
0 8.8

 | 21 | R

 | 0.50
 |
 | 0.42 0.4 | 0 0.50
3 0.50 | 7 55
 | 0.60 | 0.28
 | 0.04 | 0.20 6
 | 77 10
15
39 10 | 1.00 | 3.5
5.6 | 0.0 |
 | | 15 | 0.30 | |
| 12 G
13 G | 1 077

 | 1.09 | 6 (35.1
1737
1737

 | 1 <u>2</u> |

 | 0.50
 | 1.00%
 | 042 04 | 2 0.50
9 0.50 | 8 12
4 78
 | 0.55 | 0.28
 | 0.04 | 0.19 9
 | 89 10
89 10 | 1.00 | 51
1.7
61 | 0.0 |
 | | | | |
| 01 G
02 G
03 G
04 G | 1 0.40/
1 0.83
1 0.31

 | 6.71
3.02
4.72
2.44 | Det () 36

 | 27
27
21
27 | 1

 | 0.50
0.50
0.50
 | 1 90%
 | 0.42 0.3
0.42 0.4
0.42 0.3 | 4 0.50
5 0.50
6 0.50 | 1. 579
- 902
- 4.88
 | 0.84
0.49
0.85 | 0.28
0.28
0.28
 | 0.04 | 0 27 8
0 17 8
0 27 8
 | 21 10
51 10
92 10 | 1.00 | 3.6
4.7
2.4 | 0.0 |
 | | | | |
| 05 G
06 G
07 G | 067
071
3 0401

 | 4.58
4.42
-3.25 |

 | 27
21
27
27 | (P)
(P)
(P)

 | 0.50
 | 2 20% 1
1 80%
1 00%
 | 0.42 0.3
0.42 0.3
0.42 0.3 | 6 0.50
6 0.50
6 0.50
6 0.50 | 6.25
6.44
6.40
6.47
 | 0.76 | 0.28
0.28
0.28
0.28
 | 0.04 | 0.24 9
0.24 8
0.24 7
 | 43 10
92 10
03 10 | 1 00 | 4.4
3.2
3.3 | 0.0
0.0
0.0 |
 | | | | |
| L 00 G
L 00 G
L 10 G
L 11 G | 1 0.58
-1 0.63
-1 0.61

 | 3 97
4 35
4 30 |

 | 27 | P
IP
IP

 | 0.50
0.50
0.50
 | 1.00%
1.00%
1.00%
 | 0.42 0.3
0.42 0.4
0.42 0.4 | 9 0.50
0 0.50
0 0.50 | 7,07
7,41
1,7,36
 | 0.65 | 0.28
 | 0.04 | 0.22 B
0.21 B
0.21 B
 | 01 10
56 10
49 10 | 1.00 | 4.0
4.3
4.3 | 0.0 |
 | | | | |
| 012 G | -1 0.75

 | 4.93 | μμ 4.9
γ/]

 | 27 |

 | 0.50
 | 1.00%
 | 0.42 0.4
0.42 0.3 | 1 0.50
4 0.50
8 0.50 | - 17.93
- 15.90
- 17.00
 | 0.57 | 0.28
 | 0.04 | 0.26 6
 | 10 10
81 10 | 1 00 | 2.7 | 0.0 |
 | С.
 | | | |
| 02 G
03 G
04 G | 1 0.92
1 0.42
1 1.06

 | 5.93
2.76
5.69 | 16.9
2.6
1.57

 | 27
27
27
27 | I P

 | 0.50
 | 1 90%
 | 0.42 0.4 | 0 0 50
2 0 50
4 0 50 | 7.37
5.34
8.64
 | 0.62 | 0.28
0.28
0.28
 | 0.04 | 0.21 11
0.27 6
0.18 10
0.22 7
 | 79 10
93 - 10
48 10
90 10 | 0.97
 | 5.7
2.8
5.7
3.9 | 0.2 |
 | | | | |
| .05 G | -1 0.50
-1 1.13
-1 0.64

 | 5 30
3 05 |

 | 27
1 27
1 271 | P

 | 0.50
 | 0.60%
 | 0.42 0.4 | 6 0.50
8 0.50 | (9.60
-7.03
 | 0.44 | 0.28
0.28
 | 0.04 | 016 9
 | 34 10
13 10 | 1.00 | <u>53</u>
30 | 0 0
0 0 | 1
1
 | | | | |
| 2.03 G
2.04 G
2.05 G | -1 0.77
-1 1.24
-1 0.79

 | <u>4 62</u>
<u>6 71</u>
<u>4 74</u> | (

 | 21
27
21
21 | P
P
P

 | 0.50
 | 0 70%
 | 0.42 0.4
0.42 0.4
0.42 0.3 | 4 0.50
23 0.50
8 10.50 | 8 71
2 8 00
1 6 97
1 6 70
 | 0.51
0.56
0.66
0.70 | 0.28
0.28
0.28
0.28
 | 0.04 | 0.19 12
0.22 129
0.23 29
 | 62
81 10
66 10
10 | 0.93 | 4 8
 | 0.4 |
 | | | | |
| .07 | 0.53

 | 3 70
3.37 | 2

 | 21 | С.
Р.

 | 0.50
 | 1.60%
 | 0.42 | 4 0.50 |
 | 0.83 | 0.28
 | 0.04 | 0 27 7
 | 61 (1) 10
01 | 100 | 3.4 | 0.0 |
 | | 10 | 0.25 | |
| 3,04 G | 1 (0.66
1 1.75

 | 4.04
1 7.38
-3.37 | 1

 | - 136 | P

 | 0.50
 | 2.00%
 | 0.42 0.
0.42 0. | 11-12-20-50
A-21-20-50 | 10.17
 | 0.45 | 0.28
 | - 10:03 1
- 10:03 1 | 0.15
 | 92 15
86 1 10 | 1 1 0 99
1 1 0C | 107,3
-(3,4 | |
 | | | | |
| 1:03 G |

 | 5.79
6.42 |

 | 36
27 | Р

 | 0.50
0.50
0.50
 | 0.80%
2.00%
 | 0.42 0.
0.42 0.
0.42 0. | 0.50
0.50
0.50
0.50
0.50 |) 8.67
17.18
∩ 6.82
19.05
 | 0.64 | 0.28
 | 0.04 | 0.18 7
0.22 1
0.23 1
0.17 1
 | 90 | 1.00
1.00
11 1.00
1.00 | 3.4
5.8
6.1 | 0.0 |
 | |) 김 사람은
1914년 - 1914
1914년 - 1914년 - 191 | | |
| | a wa manai a a a a

 | |

 | 077 | D D

 | 0.60
 | 1 0004
 | | |
 | | I CO CO I
 | 0.04 | 0.20 1 9
 | 19 10-10 | 1.00 | 4.8 | 0.0 |
 | di jihas shia | | (<u>E</u> 040 | 16 |
| 11.061 C | 1120
111061
111093

 | 1 1 6 12
A 78
3 5 06 |

 | 27
27
27
27 | P
P
P

 | 0.50
 | 1009
- 009
- 709
- 110
 | 0.42 0 0 | 1 - 0.50
8 - 0.50 | - 7.60
- 6.99
 | 0.58 | 0.28
 | | 0.22
 | 24111140 | 1.00 | 6.4 | 0.0 |
 | | |)
10 | 補約
以此
例例 |
| 1106 C | 1 120
1 0.81
1 0.93
1 0.99
21 0.99
21 0.99
21 0.11
51 0.45

 | 6.76
6.76
70.91
2.90 |

 | 27
- 27
- 27
- 27
- 27
- 27
- 21 | P
P
P
P
P
P

 | 0.50
0.50
0.50
0.50
0.50
 | 1.00%
1.00%
1.70%
1.20%
0.60%
 | 0.42 0.0
0.42 0.0
0.42 0.0
0.42 0.0
0.42 0.0
0.42 0.0 | 1 0.50
16 0.50
15 1 0.50
16 0.50
16 0.50
18 1 0.50 | 6.96
6.96
 | 0.58
0.96
0.48
0.85
10.68 | 0.28
 | 0.04 | 0221 11
0174 11
0277 13
0234 5
 | 2331 10

 243 10
 245 10
 21-1 10 | 00
0.95
00
00 | 6.4
 | 0.0 |
 | | | | |
| 106 0
107 0
108 0
1108 0
1 | 1 120
1 0.93
1 0.93
1 0.99
1 0.99
1 0.11
1 0.45
NLETCALCULA

 | ATONS |

 | 27 | P
P
P
P
P

 | 0.50
 | 1.00%
1.00%
1.70%
1.20%
0.60% | 0.42 0 0
0.42 0
0
0.42 0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
 | 1 = 1 = 0.50
8 = 1 = 0.50
15 = 1 = 0.50
16 = 1 = 0.50
18 = 1 = 0.50
18 = 1 = 0.50 | 8.10
4.12
6.86
 | 0.58 | 0.28
 | 0.04 | 0.221 11 |) 33 1 (= 10
2243) 24 1 (
24 = 40
24 = 40
27 1 (= 37
 | | 64
09
29 | 0.0 | | |
 | | |
| 106 C | 1 120
1 0.81
1 0.93
1 0.99
1 0.99

 | 6 76
6 76
0 91
2 90
ATIONS |

 | 27
27
27
27
27
27
27
27
27
27 | P
P
P
P
P
P
Crown Cu

 | 0.50
0.50
0.50
0.50
10.50
10.50
10.50
 | 1.00%
1.00%
1.70%
1.20%
0.60%
0.60% | 0.42 0.
0.42 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | 0 50
0 50
15 1 0 50
15 1 0 50
15 1 0 50
16 0 50
18 1 0 50
19 1 0 50
10 50
1 | Ponded
Width (c)
 | 0.58
0.66
0.85
10.68
 | 0.28
0.28
0.28
0.28
0.29
 | 0.04
0.04
0.04
0.04 | 0.221 41
0.17 41
0.27 143
0.23 4 5
0.23 4 5
0.24 5
0 |) 33) 10
24 10
24 10
91 17
91 17
911 | | 64
09
29 | 0.0
0.0
0.0
0.0 | | | SUMP
CU
 | NLET CA
RB (w/h | APAC |
| 1.06 0
1.07 0
1.07 0
1.08 0
11.08 0 | 1 120
1 0.93
1 0.95
1 0.95
1 0.45
1 0.45
1 0.95
1 0.45
1 0.45
1 0.95
1 0.45
1 0.45
1 0.95
1 0.95
1 0.45
1 0.95
1 0.95
 | 6.72
4.78
5.00
2.90
ATONS
0.100
CdS
9.82
7.85
 | 0 15
15
15
15
15
15
15
15
15
15

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P
P
P
P
P
Crown Cu
Typs Hei
P
 | 0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50

 | 1.00%
1.00%
1.70%
1.20%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60% | 0.42 0.
0.42 0.
0.
0.42 0.
0.
0.
0.
0.
0.
0.
0.
0.
0.
0.
0.
0.
0 | 0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
 | Ponded
(1)
(1)
(1)
(1)
(1)
(1)
(1)
(1)
(1)
(1) | 0.58
0.66
0.85
0.85
0.068
 | 0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0.04 | 0.22
0.17
0.27
0.23
0.23
1.380 |) 331 10
244 11
24 11
31 13
31 13
31 13
31 10
31 10
31 10
31 10
30 | CAPACITY
6 85
0 72
 | 64
0.9
29
0
0
0
0
5
0
5
0
5
0
5
0
5
0
5
0
5
0
5 | | | | SUMP
CU
cts) (| NLETCA
RB (with
R) d | APAC
Dep |
| 1.06
1.07
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1.09
1 | 1 0.93
1 0.93
1 0.99
1 0.99
1 0.99
1 0.99
1 0.45
NLET CALCUL
0 45
NLET CALCUL
0 45
0 4
0 45
0 4

 | ATONS
2 90
ATONS
0 100
2 90
ATONS
0 100
(cfs)
REAS
9 82
7 85
2 89
5 91
6 32
6 10 | 2 pass Q total
(cfs) (cfs)
(cfs) (cfs) (cfs)
(cfs) (cfs) (cfs)
(cfs) (cfs) (cf

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P
P
P
P
P
P
Crown Cu
Type Hei
P
P
D
P
D
P
D
P
D
P
 |
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10
 | 1100%
1100%
1100%
120%
0.60%
0.60%
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60%
1
0.60% | 0.42 0.
0.42 0.
0.43 0.
0.49 0.
0.49 0.
0.49 0.
0.49 0.
0.49 0.
0.49 0.
0.50 0.
0.5 |
Crown
Height
(t)
(0.50
(0.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)
(1.50)(| Ponded
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1):50
(1
 | 0.58
0.06
0.06
0.085
0.063
0.063
0.063
0.063
0.063
0.02
0.02
0.02
0.02
0.02
0.02
0.02
0.0 | 0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0:04
0:04
0:04
0:04
0:04
0:04
0:12
0:12
0:12
0:12
0:12
0:12
0:12 | 0.222 11
0.17 11
0.27 12
0.23 15
0.23 15
10.23 15
11.02
13.80
10.22
11.07
11.02
10.99 |) 33 10
24 10
24 10
31 10
31 10
31 10
30 |
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
2.9
00ass
(cfs)
0.3
0.5
0.0
0.1
0.1 | | | | SUMP
CU
cotal Lier | NUETCA
RB (with
spin | apa(
Dep |
| 1.06 C | 1 120
1 0.93
1 0.93
1 0.99
1 0.99
1 0.45
INLET CALCULD
INLET CALCULD
1 0.45
INLET CALCULD
1 0.45
1

 | 6.76
6.76
0.91
2.90
ATONS
0.100
(cfs)
7.65
2.89
5.91
6.10
4.46
11.92
4.76 | 1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
100
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1000
1

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P
P
P
P
P
P
P
Crown Cu
Type Hei
P
D
D
D
D
D
D
D
D
D
D
D
D
D
D
D
D
D
D

 | (0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.50
 | 1100%
1100%
1100%
120%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.10%
0.10%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.12%
0.1 | 0.42 0
0.42 0
0.40 0
0.45 0
0.5 0 |
Crown
Height
(1)
0,50
15
10,50
15
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10,50
10 | Porided
(1) 50
(1) 50
(| 0.58
0.66
0.66
0.85
0.85
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.068
0.00
0.00
 | 0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0:04
0:04
0:04
0:04
0:04
0:04
0:04
0:12
0:12
0:12
0:12
0:12
0:12
0:12
0:12 | 0.22
0.17
0.27
0.27
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23 | 1331 10
244 10
24 | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
29
0pass
(cb)
03
08
0.0
01
01
01
01
01
01
01
01
01
01
01
01 | |
 | | SUMP
CU
CU
COLAI
LUEY | NLETCA
RB (with
opth
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c | APAC
Dep
(m) |
| 1.05
1.07
1.07
1.08
1.07
1.08
1.07
1.08
 | 1 0.93
1 0.93
1 0.93
1 0.99
1 0.99
1 0.99
1 0.99
1 0.99
1 0.45
INLET CALCULU
et Drainage
per Area
NI DRAINAGE AF
1 08
1 08

 | 6.12
4.78
5.06
0.91
2.90
ATONS
0.290
ATONS
0.290
C(c5)
REAS
0.82
7.85
2.89
5.91
6.32
6.10
4.46
11.92
4.74
5.24
10.21 | 2 pass 2 total
(cfs)

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P
P
P
P
P
P
P
Crown Cu
Type Hei
P
0
P
0
P
0
P
10
P
10
P
10
P
10
P
10
P

 | 0.50
0.50
0.50
0.50
0.50
0.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
0.6
50
0.6
50
0.6
50
0.5
0.5
0.5
0.5
0.5
0.5
0.5
 | 1100% | 0.42 0.
0.42 0.
0.40 0.
0.50 0.
0.5 | Crown
Height
(1)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5
 | 7.60 6.99/J 4.12 6.96/J 8.10 4.12 6.96/J 8.10 13.50 13.50/III 13.50/III 13.50/III 13.50/III 13.50/III 13.50/III 13.50/III 13.50/IIII 13.50/IIII 13.50/IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII | 0.58
0.06
0.48,
0.85
0.06
0.048,
0.05
0.05
0.05
0.05
0.02
0.02
0.02
0.02
 | 0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 | 0.22 11
0.17 11
0.27 13
0.23 3
0.23 3 | 133 10 124 10 24 10 24 10 24 10 24 10 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 0.9 10 11 10 11 10 11 10 11 | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
29
29
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
 | | Loss to Intel =
1054 Pass (G
2074 Pass (G | | SUMP
CU
cotal Lei
cfs) 1
7.3 | NLET CA
RB (with
h) d
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c
c | APA(
Dep
(ft) |
| 1.06 | 120 1 0.93 1 0.93 1 0.93 1 0.93 1 0.93 1 0.93 1 0.93 1 0.45 INLET CALCULY et Drainage pe Area N DRAINAGE AV 1 0.89 1 0.72 0 0.11 1 0.72 0 0.11 1 0.72 0 0.13 1 0.40 0.55 1.03 0.80 1.03 0.80 1.03

 | 6.12
4.78
5.00
2.90
ATONS
2.90
ATONS
9.82
7.65
2.89
5.91
6.10
4.46
11.92
4.74
5.24
11.92
4.74
5.24
11.92
4.74
5.24
11.92
10.21
6.10 | 100
100
100
100
100
100
100
100

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P
P
P
P
P
P
P
Crown Cu
P
P
P
0
P
P
0
P
0
P
0
P
0
P
0
P
0
P
0

 | 10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10
 | 1100%
120%
120%
0.60%
0.60%
0.60%
0.60%
0.60%
0.12
0.60%
0.12
0.60%
0.12
0.60%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.12
0.50%
0.50%
0.12
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.
 | 0.42 0.
0.42 0.
0.40 0.
0. | Crown
Height
(1)
0.50
25
10.50
25
10.50
25
0.50
0.50
0.50
0.50
0.50
0.50
0. | Porided
Watth (-)
13 50
13 50
10 10
10 10 | 0.58
0.06
0.06
0.085
0.068
0.085
0.068
0.085
0.068
0.068
0.085
0.068
0.02
0.02
0.02
0.02
0.02
0.02
0.02
0.0
 | 0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0:04
0:04
0:04
0:04
0:04
0:04
0:04
0:12
0:12
0:12
0:12
0:12
0:12
0:12
0:12 | 0.22 11
0.17 11
0.27 13
0.23 15
13
0.23 15
13
10.22
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
10.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02
11.02 | |
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
2.9
0pass
(cfs)
0.3
0.6
0.0
0.1
0.1
0.1
0.1
0.1
0.1
0.1
0.1
0.1 | 0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0 | ass to link a second se | | SUMP
CU
cotal Ler
cotal Ler
cotal Cu
cotal Cotal Cu
cotal Cotal Co | NLETCA
RB (with
syth
n) - d
s
 | 40
40 |
| 1.05
1.07
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.07
1.08
1.07
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.07
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08
1.08 | 120 0.93 0.93 0.93 0.10 0.11 0.45 INLET CALCULU et Drainage ps: NDRAINAGE AF NORAINAGE AF 0.63 1.03 0.63 1.03 0.63 1.03 0.63 1.03 0.63 1.03 0.63 1.03 0.63 1.03 0.63 1.03 0.80 0.77 0.80 0.77 0.80 0.77 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80 0.80

 | 6.12
4.78
5.06
0.91
2.90
ATONS
0.91
2.90
(cfs)
REAS
0.82
7.65
2.89
5.91
6.32
6.10
4.46
11.92
4.74
5.22
10.21
8.38
7.66
2.50
10.03
4.50
2.50 | 2 pess 2 total
(cfs) (cfs)
(cfs) (cfs) (cfs)
(cfs) (cfs) (cfs)
(cfs) (cfs) (cfs)
(cfs) (cfs) (cfs)
(cfs) (cfs) (cfs) (cfs)
(cfs) (cfs) (cf

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P
P
P
P
P
P
P
P
P
P
P
P
P
P
P
P
P
P
P

 | 0.50
0.50
0.50
0.50
0.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
 | 1100% | 0.42 0.
0.42 0.
0.50 0.
0.5 | Crown
Height
(1)
0.50
15 (
0.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.5 | 7.60 6.99// 4.12 6.96// 4.12 6.96// 8.00 4.12 6.96// 8.00 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 0.15 0 0.15 0 0.15
 | 0.58
0.048,
0.85
0.065
0.065
0.048,
0.055
0.055
0.055
0.055
0.055
0.055
0.02
0.02 | 0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12 | 0.22
0.17
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27 |
 | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
29
000000
00000
001
001
001
01
01
01
01
01 | | Los Pas G
1074 Pa | | SUMP
CU
otal Loi
7.3 | | 40
40 |
| 1.05 .05 1.07 .05 1.08 .05 1.08 .05 11.07 .05 11.08 .05 11.08 .05 11.08 .05 11.08 .05 11.08 .05 11.08 .05 11.08 .05 10.102 .05 10.2 .05 10.2 .05 10.2 .05 10.3 .05 10.4 .05 10.7 .05 10.8 .05 10.7 .05 10.8 .05 10.7 .05 10.8 .07 10.8 .07 10.9 .05 10.05 .05 10.07 .05 10.08 .07 10.09 .05 10.01 .05 10.02 .05 10.03 .05 10.04 .05 10.05 .05< | 1 0.93 1 0.93 1 0.93 1 0.93 1 0.93 1 0.45 INLET CALCUL et Drainage pri 1.08 0.39 0.23 1 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.73 1.09 1 0.83 0.73 0.20 1.03 0.83 0.40 0.83 0.40 0.83 0.31 0.57 0.40 0.57 0.31 0.57 0.40 0.33

 | 6.12
4.78
5.06
0.91
2.90
ATONS
0.100
(cfs)
REAS
9.82
7.65
2.89
5.91
6.10
4.46
11.92
4.74
5.22
5.22
5.22
5.22
5.021
8.38
7.66
2.50
10.03
4.55
2.50
10.03
4.55
2.50
10.03
4.55
2.50
10.03
4.55
2.50
10.03
4.55
2.50
10.03
4.55
2.50
10.03
4.55
2.55
10.21
1.55
2.55
10.21
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
1.55
2.55
2 | 100
150
150
150
150
150
150
150

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P
P
P
P
P
P
P
Crown CU
Type Hei
P
0
P
0
P
0
P
0
P
0
P
0
P
0
P
0
P
0
P
0
P
0
P
0
0
P
0
0
P
0
0
P
0
0
P
0
0
P
0
0
P
0
0
P
0
0
P
0
0
P
0
0
0
P
0
0
0
P
0
0
0
0
0
0
0
0
0
0
0
0
0

 | (0.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10
 | 1100%
120%
120%
0.60%
0.60%
0.60%
0.60%
0.60%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20%
0.20
 | 0.42 0
0.42 0
0.43 0
0.49 0
0.40 0
0. | Crown
Height
(1)
0.50
25
10.50
25
10.50
25
10.50
0.50
0.50
10.50
0.50
0.50
10.50
0.50 | Porided
Watth (-)
13 50
13 50
10
13 50
10
13 50
10
13 50
10
13 50
10
13 50
10
13 50
10
10
13 50
10
10
13 50
10
10
10
10
10
10
10
10
10
10
10
10
10
 | 0.58 0.66 0.48, 0.85 10.68 10.78 10.73 10.73 10.73 10.73 10.74 10.75 10.76 10.76 11.77 11.78 12.77 13.79 14.79 10.75 10.76 10.76 10.76 10.77 10.76 10.77 10.76 < | 0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 | 0.22
0.17
0.27
0.27
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23
0.23 |
 | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACI | 64
0.9
2.9
(cpass
(cfs)
0.1
0.1
0.1
0.1
0.1
0.1
0.1
0.1
0.1
0.1 | 0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0 | Cos Control Co | | SUMP
CU
cotal Ler
cotal 2
2
2
2
2
2
2
2
2
2
2
2
2
2
2
2
2
2
2 | NUETCA
RB (with
ypth
1
3
4
5
5
10
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
0 | 40
40 |
| 1.06 1.07 1.07 1.03 1.08 1.03 1.08 1.03 1.08 1.03 1.08 1.03 1.08 1.03 1.08 1.03 1.08 1.03 1.08 1.03 1.08 1.03 1.08 1.04 1.01 1.02 1.02 1.03 1.04 1.05 1.05 1.05 1.06 1.05 1.07 1.05 1.08 1.05 1.09 1.05 1.09 1.05 1.09 1.05 3.01 1.05 3.02 3.03 3.03 1.05 3.04 1.05 3.02 1.05 3.03 1.05 3.04 1.05 4.03 1.05 4.04 1.05 4.05 1.05 4.06 1.05 | 1 0.93 1 0.93 1 0.93 1 0.93 1 0.93 1 0.45 INLET CALCULU et Drainage pe Arag NORAINAGE AJ 1 0.61 0.23 1 0.72 0.61 0.72 0.63 0.71 0.72 0.63 0.71 0.72 0.63 0.71 0.72 0.63 0.73 0.740 0.75 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.70 0.71<

 | 6.12
4.78
5.06
0.91
2.90
ATONS
0.91
2.90
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
0.0
(100
(10 | IB 15 61 15 61 2 2 2 2 15 2 2 2 15 2 2 2 15 2 15 <td>27
27
27
27
27
27
27
27
27
27
27
27
27
2</td> <td>P P P P P P P P P P P P P</td> <td>0.50
0.50
0.50
0.50
0.50
0.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
1</td> <td>1100%</td> <td>0.42 0
0.42 0
0.45 0
0.45 0
0.50 0
0.</td> <td>Crown
Height
(1)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5</td> <td>7,60 6,99// 4,12 6,96// 8,10,1 4,12
 6,96// 9,10,1 4,12 6,96// 9,10,1 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 0 13,50// 13,50// 0 13,50// 13,50// 0 13,50// 0 13,50// 0 13,50// 0 7,951// 0 7,951// 0 7,951// 0 7,951// 0 7,951// 0</td> <td>0.58
0.048,
0.85
0.065
0.055
0.055
0.055
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0
2
31
0.2
31
0
2
2
31
0.2
31
0</td> <td>0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28</td> <td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12</td> <td>0.221 11
0.271 13
0.271 13
13.802 14
13.802 14
14.802 14</td> <td></td> <td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td> <td>64
0.9
29
000000
000
000
000
001
01
01
01
01
01
0</td> <td></td> <td>Los Color
Cos Color</td> <td></td> <td>SUMP
CO
CO
CO
CO
CO
CO
CO
CO
CO
CO
CO
CO
CO</td> <td></td> <td>40
40
40</td> | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P P P P P P P P P P P P P

 | 0.50
0.50
0.50
0.50
0.50
0.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
1
 | 1100%
 | 0.42 0
0.42 0
0.45 0
0.45 0
0.50 0
0. | Crown
Height
(1)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | 7,60 6,99// 4,12 6,96// 8,10,1 4,12 6,96// 9,10,1 4,12 6,96// 9,10,1 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 13,50// 0 13,50// 13,50// 0 13,50// 13,50// 0 13,50// 0 13,50// 0 13,50// 0 7,951// 0 7,951// 0 7,951// 0 7,951// 0 7,951// 0
 | 0.58
0.048,
0.85
0.065
0.055
0.055
0.055
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0.2
31
0
2
31
0.2
31
0
2
2
31
0.2
31
0 | 0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12 | 0.221 11
0.271 13
0.271 13
13.802 14
13.802 14
14.802 14 |
 | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
29
000000
000
000
000
001
01
01
01
01
01
0 | | Los Color
Cos Color | | SUMP
CO
CO
CO
CO
CO
CO
CO
CO
CO
CO
CO
CO
CO | | 40
40
40 |
| 1.06 0.0 1.07 0.0 1.08 0.0 1.08 0.0 1.08 0.0 1.08 0.0 1.08 0.0 1.08 0.0 1.08 0.0 1.08 0.0 1.08 0.0 AR STORM 0.0 1.02 1.0 1.02 1.0 1.02 1.0 1.02 1.0 1.03 0.0 1.04 0.0 1.05 1.0 1.06 0.0 1.07 0.0 1.08 1.0 1.09 0.0 1.07 0.0 1.08 1.0 1.09 0.0 1.07 0.0 1.08 0.0 1.09 0.0 1.01 0.0 3.02 0.0 3.03 0.0 4.03 0.0 4.04 0.0 4.05 0.0 | 1 0.61 0.93 0.93 1 0.93 1 0.93 1 0.93 1 0.45 INLET CALCULU et Drainage pe Arage pe 0.89 pe 0.83 1.03 1 pe 0.80 pe 0.80 pe 0.80 pe 0.80 pe 0.80 pe 0.80 pe

 | ATONS
6.76
0.91
2.90
ATONS
0.100
(cfs)
REAS
9.82
7.85
2.89
5.91
6.32
6.10
4.46
11.92
4.74
5.22
10.21
8.38
7.65
2.59
10.03
4.50
7.05
3.62
5.91
6.32
6.10
4.46
11.92
4.74
5.22
10.21
8.38
7.65
2.59
10.03
4.50
7.05
3.62
5.91
6.32
6.10
4.46
11.92
6.32
6.10
4.46
11.92
6.32
6.10
4.46
11.92
6.32
6.10
7.05
3.52
10.03
6.57
7.05
3.62
5.91
6.32
6.10
7.05
7.65
2.59
10.03
6.57
7.05
3.62
5.91
6.32
6.10
7.05
7.65
7.65
7.65
7.65
7.65
7.65
7.55
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.65
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.55
7.5 | C 1000
C 100

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P P P Crown Crown Crown Crown Crown Crown P P P P P P P P P P P P P
 |
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10.50
10
 | 1100%
1100%
1100%
120%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.6 |
 | Crown
Height
(1)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | 7,60 6,99/J 4,12 6,96/J 4,12 6,96/J 7,60 4,12 6,96/J 7,60 4,12 6,96/J 7,60 7,60 4,12 6,96/J 7,60 7,70 13,50
 | 0.58
0.66
0.66
0.66
0.65
0.65
0.65
0.65
0.65 | 0.20
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 | 0.22
0.17
1.0
0.27
1.3
0.23
1.3
1.2
1.2
1.2
1.3
1.2
1.1
1.4
1.1
1.4
1.1
1.4
1.1
1.4
1.1
1.4
1.1
1.4
1.1
1.4
1.1
1.4
1.1
1.4
1.4 | | | |
 | CAPACITY
CAPACITY
GI
CAPACITY
GI
CAPACITY
GI
CAPACITY
GI
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY | 64
0.9
2.9
(cpass
(cfs)
0.1
0.1
0.1
0.1
0.1
0.1
0.1
0.1
0.1
0.1 | 0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0 | A C C C C C C C C C C C C C C C C C C C | |
 | | 40
40 |
| 1.06 | 1 0.03 1 0.93 1 0.93 1 0.93 1 0.45 INLET CALCUL et Drainage pr Area N DRAINAGE AF 0.89 1 0.72 0.71 0.72 0.61 0.72 0.71 0.72 0.71 0.72 0.71 0.72 0.71 0.72 0.71 0.72 0.71 0.72 0.73 0.73 0.83 0.73 0.73 0.73 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75

 | ATONS
6.76
0.91
2.90
ATONS
0.91
2.90
ATONS
0.91
2.90
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.0 | 18 15

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P P <t< td=""><td>10.50 50 50<!--</td--><td>1100% 170% 170% 170% 170% 170% 170% 170%</td><td>0.42 0
0.42 0
0.45 0
0.45 0
0.45 0
0.45 0
0.50 0</td><td>Crown
Height
(1)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5</td><td>7.60 6.99// 4.12 6.96// 4.12 6.96// 7.60 4.12 6.96// 7.60 4.12 6.96// 7.60 7.60 4.12 6.96// 7.60 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 7.901 0 6.41 0 7.901 0 7.901 0 7.901 0 7.901 0 7.901</td><td>0.58 0.66 0.48, 0.85 10.68 10.73 10.23 10.02 10.02
 10.02 10.02 10.02 10.02 10.02 10.02 11.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02</td><td>0.20 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04</td><td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td><td>0.22 1
0.17 1
0.27 3
0.23 3
0.25 3
0.25</td><td></td><td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td><td>64
0.9
29
29
0000
01
01
01
01
01
01
01
01
01
01
01
0</td><td></td><td>a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a</td><td></td><td>Cotal Lier
Cotal Cotal Lier
Cotal Cotal Lier
Cotal Cotal Lier
Cotal Cotal Co</td><td></td><td>40
40
40
40
40
40
40
40
40
40
40
40
40
4</td></td></t<> | 10.50 50 50 </td <td>1100% 170% 170% 170% 170% 170% 170% 170%</td> <td>0.42 0
0.42 0
0.45 0
0.45 0
0.45 0
0.45 0
0.50 0</td> <td>Crown
Height
(1)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5</td> <td>7.60 6.99// 4.12 6.96// 4.12 6.96// 7.60 4.12 6.96// 7.60 4.12 6.96// 7.60 7.60 4.12 6.96// 7.60 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 7.901 0 6.41 0 7.901 0 7.901 0 7.901 0 7.901 0 7.901</td> <td>0.58 0.66 0.48, 0.85 10.68 10.73 10.23 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 11.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02</td> <td>0.20 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04</td> <td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td> <td>0.22 1
0.17 1
0.27 3
0.23 3
0.25 3
0.25</td> <td></td>
<td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td> <td>64
0.9
29
29
0000
01
01
01
01
01
01
01
01
01
01
01
0</td> <td></td> <td>a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a</td> <td></td> <td>Cotal Lier
Cotal Cotal Lier
Cotal Cotal Lier
Cotal Cotal Lier
Cotal Cotal Co</td> <td></td> <td>40
40
40
40
40
40
40
40
40
40
40
40
40
4</td> | 1100% 170% 170% 170% 170% 170% 170% 170% | 0.42 0
0.42 0
0.45 0
0.45 0
0.45 0
0.45 0
0.50 0 | Crown
Height
(1)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | 7.60 6.99// 4.12 6.96// 4.12 6.96// 7.60 4.12 6.96// 7.60 4.12 6.96// 7.60
 7.60 4.12 6.96// 7.60 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 7.901 0 6.41 0 7.901 0 7.901 0 7.901 0 7.901 0 7.901 | 0.58 0.66 0.48, 0.85 10.68 10.73 10.23 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 11.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02 10.02
 | 0.20 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04
 | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 | 0.22 1
0.17 1
0.27 3
0.23 3
0.25 | | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
29
29
0000
01
01
01
01
01
01
01
01
01
01
01
0 | | a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a:
a
 | | Cotal Lier
Cotal Cotal Lier
Cotal Cotal Lier
Cotal Cotal Lier
Cotal Cotal Co | | 40
40
40
40
40
40
40
40
40
40
40
40
40
4 |
| 1.06 | 1 0.93 1 0.93 1 0.93 1 0.93 1 0.45 INLET CALCULA et Drainage prime Areas prime 100 0.11 0.45 et Drainage prime Areas prime 100 0.23 0.71 0.72 0.63 0.73 1.09 0.740 0.55 0.63 1.03 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.77 0.73 0.76 0.30 0.75 0.40 0.75 0.40 0.75 0.40 0.75 0.42 0.75 0.42 0.75 0.42 0.75 0.42 </td <td>ATONS
0.76
0.91
2.90
ATONS
0.91
2.90
ATONS
0.91
0.91
2.90
4.76
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.9</td> <td>18 15 61 15 61 2 2 15 15 61 2 15 <t< td=""><td>27
27
27
27
27
27
27
27
27
27
27
27
27
2</td><td>P P Crown Crown</td><td>10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 50 10.6 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50</td></t<><td>1100%
120%
120%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0%
0.12
0%
0%
0%
0%
0%
0%
0%
0%
0%
0%</td><td>0.42 0 0
0.42 0
0.49 0
0.40
0</td><td>Crown
Height
(H)
050
050
050
050
050
050
050
050
050
05</td><td>7.60 6.99// 4.12 6.96// 4.12 6.96// 8.00 4.12 6.96// 8.00 8.00 8.90 9.10 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50</td><td>0.58 0.48, 0.85 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.7 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31</td><td>0.20 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 <td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td><td>0.22
0.17
1.0
0.27
1.3
0.23
1.3
0.23
1.3
1.0
1.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.5
1.5
1.5
1.5
1.5
1.5
1.5
1</td><td></td><td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td><td>64
0.9
29
29
00
00
01
01
01
01
01
01
01
01
01
01
01</td><td>0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0</td><td></td><td></td><td></td><td></td><td>40
40
40
40</td></td></td> |
ATONS
0.76
0.91
2.90
ATONS
0.91
2.90
ATONS
0.91
0.91
2.90
4.76
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.91
0.9 | 18 15 61 15 61 2 2 15 15 61 2 15 <t< td=""><td>27
27
27
27
27
27
27
27
27
27
27
27
27
2</td><td>P P Crown Crown</td><td>10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 50 10.6 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50</td></t<> <td>1100%
120%
120%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0%
0.12
0%
0%
0%
0%
0%
0%
0%
0%
0%
0%</td> <td>0.42 0 0
0.42 0
0.49 0
0.40 0</td> <td>Crown
Height
(H)
050
050
050
050
050
050
050
050
050
05</td> <td>7.60 6.99// 4.12 6.96// 4.12 6.96// 8.00 4.12 6.96// 8.00 8.00 8.90 9.10 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50</td> <td>0.58 0.48, 0.85 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.7 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31</td> <td>0.20 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04
<td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td><td>0.22
0.17
1.0
0.27
1.3
0.23
1.3
0.23
1.3
1.0
1.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.5
1.5
1.5
1.5
1.5
1.5
1.5
1</td><td></td><td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td><td>64
0.9
29
29
00
00
01
01
01
01
01
01
01
01
01
01
01</td><td>0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0</td><td></td><td></td><td></td><td></td><td>40
40
40
40</td></td>
 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P P Crown
 | 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 50 10.6 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50 10.5 50
 | 1100%
120%
120%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0.12
0%
0%
0.12
0%
0%
0%
0%
0%
0%
0%
0%
0%
0%
 | 0.42 0 0
0.42 0
0.49 0
0.40 0 | Crown
Height
(H)
050
050
050
050
050
050
050
050
050
05 | 7.60 6.99// 4.12 6.96// 4.12 6.96// 8.00 4.12 6.96// 8.00 8.00 8.90 9.10 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50
 | 0.58 0.48, 0.85 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.7 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 | 0.20 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 <td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td>
<td>0.22
0.17
1.0
0.27
1.3
0.23
1.3
0.23
1.3
1.0
1.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.5
1.5
1.5
1.5
1.5
1.5
1.5
1</td> <td></td> <td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td> <td>64
0.9
29
29
00
00
01
01
01
01
01
01
01
01
01
01
01</td> <td>0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0</td> <td></td> <td></td> <td></td> <td></td> <td>40
40
40
40</td> | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 |
0.22
0.17
1.0
0.27
1.3
0.23
1.3
0.23
1.3
1.0
1.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.2
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.4
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.1
0.5
1.5
1.5
1.5
1.5
1.5
1.5
1.5
1 | | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
29
29
00
00
01
01
01
01
01
01
01
01
01
01
01 | 0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0
0.0 |
 | | | | 40
40
40
40 |
| 1.06 | 1 0.093 1 0.93 1 0.93 1 0.93 1 0.45 INLET CALCUL et Drainage pt Area DY ARAGE AU 0 0.39 0 0.39 0 0.39 0 0.72 0 0.71 0 0.72 0 0.31 0 0.33 0

 | ATONS
6.76
0.91
2.90
ATONS
2.90
ATONS
0.100
0.05
2.90
0.05
2.90
0.05
2.90
0.05
2.90
0.05
2.90
0.05
2.90
0.05
2.90
0.05
2.90
0.05
2.90
0.05
2.90
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0.05
0. | 10 15 100 15 100 15 100 15 100 15 15 15 15 15 15

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P P Crown

 | 10.50 50
 | | 0.42 0
0.42 0
0.45 0
0. | Crown
Height
(1)
()
()
()
()
()
()
()
()
()
()
()
()
()
 | 7.60 6.99// 4.12 6.96// 4.12 6.96// 9.10.1 4.12 6.96// 9.10.1 4.12 6.96// 9.10.1 13.50// 0 4.10// 13.50// 0 5.861// 0 5.79// 0 3.79// 0 3.79// 0 < | 0.58 0.48, 0.85 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68
 10.68 10.7 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 55 0.2 50 0.2 50 0.2 50 0.2 50 0.2 50 | 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.000 </td <td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td> <td>0.22 1
0.17 1
0.27 3
0.23 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25</td> <td></td> <td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td> <td>64
0.9
29
29
009
29
009
29
009
001
01
01
01
01
01
01
01
01
01
01
01
01</td> <td></td> <td></td> <td></td>
<td>SUMP
CU
CU
COLAI
UP
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLA</td> <td></td> <td>1
PAC
Des
40
40
40
40
40
40
40
40
40
40</td> | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 | 0.22 1
0.17 1
0.27 3
0.23 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 3
0.25 | | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP |
64
0.9
29
29
009
29
009
29
009
001
01
01
01
01
01
01
01
01
01
01
01
01 | | | | SUMP
CU
CU
COLAI
UP
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLAI
COLA | | 1
PAC
Des
40
40
40
40
40
40
40
40
40
40 |
| 1.06 | 1 1.20 1 0.93 1 0.93 1 0.93 1 0.45 INLET CALCUL et Drainage pe Arage NO RAINAGE AF NO RAINAGE AF 0.31 0.031 0.032 0.031 0.032 0.33 0.031 0.63 1.03 0.63 1.03 0.63 1.03 0.63 1.03 0.63 1.03 0.63 0.63 0.63 0.63 0.61 0.77 0.77 0.77 0.77 0.77 0.75 0.75 0.75 0.75 0.75 0.76 0.77 0.78 0.79 0.79 0.79 <

 | ATONS
6.76
0.91
2.90
ATONS
4.78
0.91
2.90
ATONS
0.91
2.90
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.0 | 18 15

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P P <td< td=""><td>10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 50 0.6 50 0.5 50 0.5 50 1.9 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0<!--</td--><td></td><td>0.42 0
0.42 0
0.40 0
0.</td><td>Crown Height (1) Crown Height (1) Crown Height (1) Crown Crown Height (1) Crown Crown</td><td>7.60 6.99// 4.12 6.96// 4.12 6.96// 8.00// 4.12 6.96// 9.10 4.12 6.96// 9.10 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 7.901 0 13.50 0 7.901 0 13.50 0 7.901 0 13.50 0 13.50 0 13.50 <td>0.58 0.48, 0.85 0.06 0.085 0.06 0.085 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.07
 0.07 0.07 0.07 0.07 0.07 <</td><td>0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.040 0.041 0.041 0.042 0.043 0.044<!--</td--><td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td><td>0.22 1
0.17 1
0.27 13
0.23 5
 1023 5
 1014
 1209
 13.80
 1022
 1074
 1024
 1024
 1024
 1034
 104
 104
 104
 104
 104
 104
 109
 104
 104
 109
 104
 104
 104
 109
 104
 105
 104
 104
 105
 104
 105
 104
 105
 107
 107</td><td></td><td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td><td>64
0.9
29
00000
000
001
01
01
01
01
01
01
01
01
0</td><td></td><td></td><td></td><td></td><td></td><td>APAC
Dep
(II)</td></td></td></td></td<> | 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 10.50 50 0.6 50 0.5 50 0.5 50 1.9 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 50 1.0 </td <td></td> <td>0.42 0
0.42 0
0.40 0
0.</td> <td>Crown Height (1) Crown Height (1) Crown Height (1) Crown Crown Height (1) Crown Crown</td> <td>7.60 6.99// 4.12 6.96// 4.12 6.96// 8.00// 4.12 6.96// 9.10 4.12 6.96// 9.10 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 7.901 0 13.50 0 7.901 0 13.50 0 7.901 0 13.50 0 13.50 0 13.50 <td>0.58 0.48, 0.85 0.06 0.085 0.06 0.085 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.07 0.07 0.07 0.07 <</td><td>0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.040 0.041 0.041 0.042 0.043 0.044<!--</td--><td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td><td>0.22 1
0.17 1
0.27 13
0.23 5
 1023 5
 1014
 1209
 13.80
 1022
 1074
 1024
 1024
 1024
 1034
 104
 104
 104
 104
 104
 104
 109
 104
 104
 109
 104
 104
 104
 109
 104
 105
 104
 104
 105
 104
 105
 104
 105
 107

107</td><td></td><td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td><td>64
0.9
29
00000
000
001
01
01
01
01
01
01
01
01
0</td><td></td><td></td><td></td><td></td><td></td><td>APAC
Dep
(II)</td></td></td> | | 0.42 0
0.42 0
0.40 0
0. | Crown Height (1) Crown Height (1) Crown Height (1) Crown Crown Height (1) Crown | 7.60 6.99// 4.12 6.96// 4.12 6.96// 8.00// 4.12 6.96// 9.10 4.12 6.96// 9.10 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 13.50 0 7.901 0 13.50 0 7.901 0 13.50 0 7.901 0 13.50 0 13.50 0 13.50 <td>0.58 0.48, 0.85 0.06 0.085 0.06 0.085 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.07 0.07 0.07 0.07 <</td> <td>0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.040 0.041 0.041 0.042 0.043 0.044<!--</td--><td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td><td>0.22 1
0.17 1
0.27 13
0.23 5
 1023 5
 1014
 1209
 13.80
 1022
 1074
 1024
 1024
 1024
 1034
 104
 104
 104
 104
 104
 104
 109
 104
 104
 109
 104
 104
 104
 109
 104
 105
 104
 104
 105
 104
 105

104
 105
 107
 107</td><td></td><td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td><td>64
0.9
29
00000
000
001
01
01
01
01
01
01
01
01
0</td><td></td><td></td><td></td><td></td><td></td><td>APAC
Dep
(II)</td></td> | 0.58 0.48, 0.85 0.06 0.085 0.06 0.085 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.065 0.07 0.07 0.07 0.07 < | 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.040 0.041 0.041 0.042 0.043 0.044 </td <td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td> <td>0.22 1
0.17 1
0.27 13
0.23 5
 1023 5
 1014
 1209
 13.80
 1022
 1074
 1024
 1024
 1024
 1034
 104
 104
 104
 104
 104
 104
 109
 104
 104
 109
 104
 104
 104
 109
 104
 105
 104
 104
 105
 104
 105
 104
 105
 107
 107</td> <td></td>
<td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td> <td>64
0.9
29
00000
000
001
01
01
01
01
01
01
01
01
0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>APAC
Dep
(II)</td> | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 | 0.22 1
0.17 1
0.27 13
0.23 5
 1023 5
 1014
 1209
 13.80
 1022
 1074
 1024
 1024
 1024
 1034
 104
 104
 104
 104
 104
 104
 109
 104
 104
 109
 104
 104
 104
 109
 104
 105
 104
 104
 105
 104
 105
 104
 105
 107
 107 |
 | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
29
00000
000
001
01
01
01
01
01
01
01
01
0 | | | | | | APAC
Dep
(II) |
| 1.06 | 1 0.93 1 0.93 1 0.93 1 0.93 1 0.45 MILET CALCULA et Drainage pe Areas NORAINAGE AJ 0.39 0.23 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.73 1.03 1.03 0.72 0.73 1.03 0.73 0.740 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 0.75 <td< td=""><td>ATONS
6.76
0.91
2.90
ATONS
4.78
0.91
2.90
ATONS
4.76
1.00
4.45
1.02
4.76
1.02
4.76
1.02
4.76
1.02
4.76
1.02
4.76
1.02
4.76
1.02
4.76
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.0</td><td></td><td>27
27
27
27
27
27
27
27
27
27
27
27
27
2</td><td>P P <t< td=""><td>10.50 10.50</td><td></td><td>0.42 0
0.42 0
0.43 0
0.43 0
0.45 0
0.</td><td>Crown Height (1) Crown Crown Height (1) Crown Cro Crown Crown Cro Crown Crown Cro Crow</td><td>7.60 6.99/0 4.12 6.96.0 4.12 6.96.0 9.10.1 4.12 6.96.0 9.10.1 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 0.13.500 13.500 0.13.500<</td><td>0.58 0.48. 0.85 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.7 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 35 0.2 36 0.2 37 0.2 38 0.2 31 0.2 31 0.2 31 0.</td><td>0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200
0.200 0.200 0.200 0.200 0.200 0.000<!--</td--><td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td><td>0.22 1
0.17 1
0.27 3
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
12.09 1
0.27 1
0.27 1
12.09 1
13.02 1
14.02 1
0.27 1
15.74 1
0.27 1
15.74 1
0.22 1
15.75 1
0.22 1
15.75 1
0.22 1
10.22 1
1</td><td></td><td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td><td>64
0.9
29
29
000
01
01
01
01
01
01
01
01
01
01
01
01</td><td></td><td></td><td></td><td></td><td></td><td>APAC
Dep
(ff) 40</td></td></t<></td></td<> | ATONS
6.76
0.91
2.90
ATONS
4.78
0.91
2.90
ATONS
4.76
1.00
4.45
1.02
4.76
1.02
4.76
1.02
4.76
1.02
4.76
1.02
4.76
1.02
4.76
1.02
4.76
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.02
1.0 |

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P P P
 P P <t< td=""><td>10.50 10.50</td><td></td><td>0.42 0
0.42 0
0.43 0
0.43 0
0.45 0
0.</td><td>Crown Height (1) Crown Crown Height (1) Crown Cro Crown Crown Cro Crown Crown Cro Crow</td><td>7.60 6.99/0 4.12 6.96.0 4.12 6.96.0 9.10.1 4.12 6.96.0 9.10.1 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 0.13.500 13.500 0.13.500<</td><td>0.58 0.48. 0.85 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.7 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 35 0.2 36 0.2 37 0.2 38 0.2 31 0.2 31 0.2 31 0.</td><td>0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.000<!--</td--><td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td><td>0.22 1
0.17 1
0.27 3
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
12.09 1
0.27 1
0.27 1
12.09 1
13.02 1
14.02 1
0.27 1
15.74 1
0.27 1
15.74 1
0.22 1
15.75 1
0.22 1
15.75 1
0.22 1
10.22 1
1</td><td></td><td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td><td>64
0.9
29
29
000
01
01
01
01
01
01
01
01
01
01
01
01</td><td></td><td></td><td></td><td></td><td></td><td>APAC
Dep
(ff) 40</td></td></t<> | 10.50

 | | 0.42 0
0.42 0
0.43 0
0.43 0
0.45 0
0. | Crown Height (1) Crown Crown Height (1) Crown Cro Crown Crown Cro Crown Crown Cro Crow | 7.60 6.99/0 4.12 6.96.0 4.12 6.96.0 9.10.1 4.12 6.96.0 9.10.1 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 13.500 0.13.500 13.500 0.13.500<
 | 0.58 0.48. 0.85 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.68 10.7 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 31 0.2 35 0.2 36 0.2 37 0.2 38 0.2 31 0.2 31 0.2 31 0. | 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.000 </td <td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td> <td>0.22 1
0.17 1
0.27 3
0.23 5
0.23
5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
12.09 1
0.27 1
0.27 1
12.09 1
13.02 1
14.02 1
0.27 1
15.74 1
0.27 1
15.74 1
0.22 1
15.75 1
0.22 1
15.75 1
0.22 1
10.22 1
1</td> <td></td> <td>CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP</td> <td>64
0.9
29
29
000
01
01
01
01
01
01
01
01
01
01
01
01</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>APAC
Dep
(ff) 40</td> | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 | 0.22 1
0.17 1
0.27 3
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
0.23 5
12.09 1
0.27 1
0.27 1
12.09 1
13.02 1
14.02 1
0.27 1
15.74 1
0.27 1
15.74 1
0.22 1
15.75 1
0.22 1
15.75 1
0.22 1
10.22 1
1 |
 | CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAPACITY
CAP | 64
0.9
29
29
000
01
01
01
01
01
01
01
01
01
01
01
01 | | | |
 | | APAC
Dep
(ff) 40 |
| 1.06 | 1 1.20 0.93 0.93 1 0.93 0.11 0.45 et Drainage pri 0.45 et Drainage pri 0.81 0.93 0.31 0.72 0.61 0.89 0.23 0.71 0.72 0.63 0.71 0.72 0.61 0.83 0.31 0.83 0.31 0.83 0.31 0.77 0.72 0.83 0.33 0.83 0.33 0.83 0.31 0.75 0.33 0.75 0.33 0.75 0.33 0.75 0.33 0.76 0.72 0.75 0.33 0.76 0.75 0.75 0.33 0.76 0.72 0.75 0.33 0.76 0.72 0.77 0.72 0.78 0.75 0.79

 | ATONS
6.76
0.91
2.90
ATONS
2.90
ATONS
0.91
2.90
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.0 | 10 15 15 01 01 01 01 01 01 01 01 01 01 01 01 01 01 01 02 03

 | 27
27
27
27
27
27
27
27
27
27
27
27
27
2 | P P P <td>10.50 50 50</td> <td></td> <td>0.42 0
0.42 0
0.45 0
0.</td> <td>Crown Height (1) Crown Height (1) Crown Height (1) Crown Height (1) Crown Crown Height (1) Crown Crown</td> <td>0.760 0.101 4.12 6.99/ 4.12 6.96. Ponded Math (2) 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0.13.50 13.50 0.790 0.841 0.13.50 0.790 0</td> <td>0.58 0.66 0.85 0.85 0.66 0.85 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.60 0.60 0.70 0.70 0.70 0.70
0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.71 0.72 0.71 0.72 0.71 0.72 0.71 0.72 0.73 0.74 0.75 0.75 0.75 0.76 0.77 0.76 0.77 0.76</td> <td>0.20 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04</td> <td>0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04</td> <td>0.22 1
0.17 1
0.27 3
0.23 3
1.2 3
0.23 3
0.23 3
1.2 3
1.5 74 1
0.24 3
0.23 3
1.5 74 1
0.24 1
0.25 3
1.5 74 1
0.25 1
1.5 74 1
0.25 1
0.25 1
1.5 74 1
0.25 1
0.25 1
1.5 74 1
1.</td> <td></td> <td>100 0.96 0.00 1.00 1.00 0.96 0.00 1.00 0.96 0.96 0.96 0.96 0.96 0.96 0.97 0.96 0.97 0.96 0.97 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 <</td> <td>64 0.9 2.9 0.03 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.0 .14 1.5 0.0 .24 0.0 .14 1.5 0.0 0.1 0.2 0.2 0.2 0.2 0.3 0.4 0.5 0.5 0.5 0.5 0.5 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>APAC
Dep
(II)
40
40
40
40
40
40
40
40
40
40
40
40
40</td> | 10.50 50
 |
 | 0.42 0
0.42 0
0.45 0
0. | Crown Height (1) Crown Height (1) Crown Height (1) Crown Height (1) Crown Crown Height (1) Crown | 0.760 0.101 4.12 6.99/ 4.12 6.96. Ponded Math (2) 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 0.13.50 13.50 0.790 0.841 0.13.50 0.790 0
 | 0.58 0.66 0.85 0.85 0.66 0.85 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.60 0.60 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.71 0.72 0.71 0.72 0.71 0.72 0.71 0.72 0.73 0.74 0.75 0.75 0.75 0.76 0.77 0.76 0.77 0.76 | 0.20 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.28 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04 8 0.04
 | 0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04 | 0.22 1
0.17 1
0.27 3
0.23 3
1.2 3
0.23 3
0.23 3
1.2 3
1.5 74 1
0.24 3
0.23 3
1.5 74 1
0.24 1
0.25 3
1.5 74 1
0.25 1
1.5 74 1
0.25 1
0.25 1
1.5 74 1
0.25 1
0.25 1
1.5 74 1
1. |
 | 100 0.96 0.00 1.00 1.00 0.96 0.00 1.00 0.96 0.96 0.96 0.96 0.96 0.96 0.97 0.96 0.97 0.96 0.97 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.96 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 < | 64 0.9 2.9 0.03 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.0 .14 1.5 0.0 .24 0.0 .14 1.5 0.0 0.1 0.2 0.2 0.2 0.2 0.3 0.4 0.5 0.5 0.5 0.5 0.5 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 | | | | | | APAC
Dep
(II)
40
40
40
40
40
40
40
40
40
40
40
40
40
 |

THIS DOCIMENT HAS BEEN PRODUCED FROM WATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND WAY HAVE BEEN IND/VERTENTLY ACTERED. RELY ONLY ON FINAL HARDOOPY WATERIALS BEARING THE CONSULTANT'S ORIGINAL SIGNATURE AND SEAL

RAINAGE AREA		AREA (acros)	COMPOSITE C	A-Cai	w Length (ft)	SHEET FLOW Manning's Slope (n) ft/ft	To (min)	SHALLO Length (ft)	W CONCI Paved/ Unpaved	Slope ft/ft	FLOW Tc (min)	Length (ft)	CHANNI Manning's (n)	ELIZED FLO Slope fuft	Velocity ft/s	Tc (min)	Cumulative Tc (min)	INTENS 125yr (in/hr) (100yr 100 in/hr) (g	ISCHARGE 25 Q 100 fs) (cfs)
TIMATE CO G1 01 G1 02	G1.01 G1.02	RAINAGE AR 1.08 0.89	EAS 0.64 0.72 0.62 0.70	0.6941 1/0 78		0.24 10.030 0.24 10.030	2 7 77 7 87	-1301 		0.024	- 1087. - 1101 - 100	*160,70* *160,1	0.015		3.0 3.8 3.0	0.313 0.693 2.355	8.95 () 9.57 5.00 ()	9 48 9 25 511 30 5	12-57-1 - 6 12-27 16 15-00 - 1-12	6 98 1 76 0 29
G1 04 G1 05 G1 06 C1 07	G1 04 G1 05 G1 05	0.77	0.61 0.69 0.64 0.72 0.64 0.72 0.64 0.72	0.433 0.48 0.4610 0.5 0.392 0.44 0.266 0.25	19 1 = 5 = - 19 1 = 5 C - 11 U = 2 C 1 = 7 / 1 = - 0 1 = -	0241 0.00 024 0.00 1024 0.00 024 0.00	16.40 7.09 1.4.10 1.000	129 1147 2001 0			0.67	44514 201915 1910 161914	0.015 0.015 0.015 0.015 0.015		2.7 2.7 2.7 2.7 2.7	0.888 1.232 0.674 13.762	9.96 9.77 6.66 5.00	9 12 9 19 10 45 11 30 - 5	12:00 12:18:1.114 13:85:1.114 15:00:111	9 - 59 2 - 63 1 - 61 1 - 61 - 45
G1 08 G1 09 G1 10		1 09 0:40 0:55	0.65 0.73 0.71 0.79 0.64 0.72	0 707 1 0 79 0 283 - 0 39 0 353 1 0 39	95 (100) 161 (100) 98 (100) 162 (100)	- 1024 1,1, 20010 - 2024;=, 100010 - 2024;= 100010 - 2024;= 100010 - 2025;= 2025	0.00 0.00 6.49	- 180 - 51 - 518 (- 5 - 70 (1-10 - 0.00 - 10.00		0.015		53 53/4 53/4	10.566 -2.012 -1.306 1	5 00 - 5 00 - 7 80	11.30 11.30 9.94	15 00,1 1-4 15 00,1 1-4 13 18 1,	10 - 1119 12 47 15 52
G2.01 G2.02	162.01 (62.02)	0.63 - 1.03	0.61 0.68 0.64 0.72 -0.67 0.75	0.382 0.43	22 (1993) (1993) 33 (1993) (1995) 74 (1993) (1995)	0.24 0.02 0.24 0.02 1 0.24 0.02 0.24 0.01	8 25 4 57 3 89	196 196 17276		0.022 0.0018 1.0015	1.60		0.015		3.0 3.0 3.8	0.431	6.85	10.36 10.36 10.58	12 (10 5) 18 744 (10 6) 14 (03) (10 6)	10.2 16 8.4
G3 02 G3 03		0.77	0 64 0 73 0 75 0 83 0 62 0 70	0.496 0.55		120243 10001 1202425 2000 12024 2000	3 99 0 00 8 49			0.015	2.60 2.000 3.21.11	64 13/360 73 U	0.015		3.8 3.8 1 6.2	10.277 -1.560 1.0.196	6 87 5 00	10.35 11.30 – 9.18 – L	13-72 (m) 15:00 (m) 12:16 (m)	17 2.5 37 10.0
G4.02 G4.03 G4.04 G4.05	GA 02 GA 03 GA 04 GA 04	0.40 0.83 0.31 0.67	0.67 0.75 0.62 -0.70 - 0.70 0.78 0.65 0.73	0 267 0.3 0 518 0.5 0 216 0.2 0 437 °0.4	001 (2760) (27 941 (2760) (2 411 (2770) (2 91 (2770) (20) (20)	024	0.00 8.57 0.00 4.52				0.29 1.04 1.04 1.04 1.044	11160 172 ²¹ 1-283 1-1801-1	0.015		53 3.0 53 7 5.7	0.403 0.905 0.234	5.00) 10.01 5.00 6.56 (-) -	11 30/- - 9 10 - 11 30 - 10 49 -	15:00 12:00 15:00 15:00 15:91	30 4.5 47 7.1 2.4 3.6 4.6 6.8
G4.06 G4.07 G4.08 G4.09		0.71 0.40 0.40 0.58	0.67 0.75 0.72 0.80 0.73 0.82 0.67 0.75	0 474 0.5 0 287 0.3 0 294 0 3 0 390 0.4	521 (2014) (1994) 2111 (2014) (2014) 2712 (2014) (2014) 2713 (2014) (2014)	1024 012 024 012 10024 012 10024 012 10024 012	8 17 0 0 00 0 0 00 4 89	100 200 200 200		12-01030 11-0020 U 11-01620 11-01620	0.99 0.00 1.200 1.76	78 694 1694 130	0.015 0.015 0.015 0.015 0.015		5.2 3.8 3.8 1.3.8	0.252 3.007 3.007 0.563	9.42 5.00 5.00 7.21	9 31 - 11/30 - 11/30 - 10/19	15:00 15:00 15:00 13:51	12 - 48 13 - 49 10 - 59
G4 10 G4 11 G4 12 G4 13	G410 G411 G412 G412	0.63 0.61 0.75 0.33	0.66 0.74 0.67 0.75 0.61 0.69 0.73 0.82	0.416 0.4 0.408 0.4 0.459 0.5 0.241 0.2	575 - 729 - 7 581 - 729 - 7 191 - 102 - 7 591 - 107 - 1	0.24 0.02 0.24 0.02 0.24 0.02 0.24 0.02	2 4 64 3 4 53 7 4 60 7 0 00		12 N 3 - 2 1 - 10 7 - 1 1 - 10 - 1 1 - 10 - 1	1 - 20 6922 1 - 20 6223 1 - 20 6273 - 1 - 20 6274	1.67 1.62 0.84 0.00		0.015 0.015 0.015 0.015		3.6 3.8 3.8 (* 3.8	0.347 0.347 0.637 2.461	6.66 6.50 6.07 5.00	10.45 10.52 10.73 11.30	13.65 13.96 14.23 15.00	13
.01.01 .01.02 		1.08 0.92 0.42 1.06	0.59 0.67 0.66 0.74 0.67 0.75 0.57 0.65	0.637 0.7 0.607 0.6 0.280 0.3 0.603 0.6	21.0 152 82 1 050 14 51 85 69	0.24 0.02 0.24 0.02 0.24 0.02 0.24 0.02	49 77 00 6 66 5 6 66	218		1230-00152 1230-020 1400-20 1230-020 1230-020	0.90		0.015 0.015 0.015 0.015 0.015		5.7 1 5.3 - 4.9 - 3.8 - 3.8	0 745 0 299 0 360 11 382 2 786	10.08 8.20 7.94 9.05 5.00	9.08 9.78 9.88 9.45	12:03 12:96 13:10 12:52 15:00	58 87 59 88 28 41 57 86 39 58
J1.05 J2.01 J2.02	U2.01	0.50	0.69 0.77 0.57 0.64 0.57 0.64	0.641 0.7	80 4 29 75 12 70	0.24 0.01 0.24 0.01	10 60 1 9 89			10.0192	187		0.015		30 30	10.201 (0.531 0.880	12.75 12.24 5.00	5 8 26 1 1 8 10 1	10.96	53 80 30 46 48 73
J2.03 J2.04 J2.05 J2.06 J2.06 J2.07 J2.08	<u>J2:03</u> <u>J2:04</u> <u>J2:05</u> J2:06 <u>J2:07</u> 42:08	0.77 1.24 0.79 0.58 0.53 0.64	0 55 0 63 0 59 0 67 0 62 0.70 0 67 0.75 0 69 0.77 0 54 0.61	0 427 .004 0 732 0 8 0 488 0 5 0 386 0 4 0 365 0 4 0 345 0 3	80 0 29 51 50 72 34 0 99 56 93 55	0.24 0.02 0.24 0.02 0.24 0.05 0.24 0.05 0.24 0.04 0.24 0.04	1 7 38 7 6 76 2 0.00⊤ 9 5,67 4 93				174 126 079 129 062		0.015 0.015 0.015 0.015 0.015 0.015		52 47 47 47 47 49	10.720 0.318 - 1.981 -	19.84 8.36 5.00 7/36 8.22	9 16 9 71 11 30 10 13 9 77	12 14 12 87 15 00 13 43 12 95	67 7404 47 71 44 65 37 55 34 51
J3.04 B1.01		0.66	0.67 0.75	0.443	97 39 89 100	024-1.000	4 7.00 - 7_ 9.16 -	- 172 - 1126 I II - 1226 I II - 1226 I II	- - 	9 - 1-10-011 1-0-0264	1.24		0.015		3 0	1 678 0 613	9.92 11.61	9 13	12 10 1	4.0 6.0 7.4 11.3
81.02 81.03 81.04 81.05 81.05 81.06 81.07		0.63 -0.53 -123 -146 -120 -0.61	0.51 0.59 0.57 0.65 0.53 0.60 0.56 0.64 0.61 0.68 0.69 0.78	0.322 0.3 0.303 0.3 0.650 0.7 0.817 0.9 0.726 0.8 0.423 0.4	70- 1930 441 - 23 291 - 70 - 21 - 109 745 - 0	0.24 0.01 0.24 0.02 0.24 0.02 0.24 0.02 0.24 0.03 0.24 0.03 0.24 0.01	3			- 10 000 - 10 0013 - 20 0015 - 20 0015 - 20 0015 - 21 00015	0.53 0.00 1.29 1.90 1.32 1.0.00		0.015 0.015 0.015 0.015 0.015 0.015	= 100003 = 100003 = 100000 = 100000 = 100000 = 1000000	3.4 13.4 15.4 16.7 3.8 3.8	0 262 2 364 0 919 0.538 0 672 3 033	5.00 10.63 - 14.33 - 12.19 1- 5.00	11.30 8.89 7.86 8.42 11.30	15:00 11:79 10:42 11:61 15:00 (1)	34 152 58 88 64 197 61 192 48/ 71
B1:08 B11:06 B11:07	B1 08	0.93	0.60 0.68	0.556 0.0 6	29) = 6) 89) /	0.24 0.02 0.24 0.064 0.24 0.04	5 8.25 6 3.53 6 0.00	234 U		0.023 0.023	1.18 1.59 0.00		0.015		(4.2 3-0)	0.285	9.98 6.41 5.00	11 08 1/1 11 30 1/1	12.08 14.70 15.00	6 8 // 10 1 0 9 13
B11.08	B11.05	0.45	0.63 0.71	0.282 10 3	18	0.24	51/114.50			0.023	2.20		0015			0 2961 39 7	1. 17.00		10.01	2 al 10 4 9
		2					_ل ې			C			00							
			00																	
															G					
				00					00											
																в.			0	

同 つ

°₽

2 P

м м ථ 121 00 95

8

a

	0	
C	0.0	
00		
		10

LIVELY IFACI, FHASE 4 OITY OF LEANDER, TEXAS	PAPE-DAWSON ENGINEERS	DUST	
DRAINAGE CALCULATIONS	AUSTIN A SAN AMTONIO I HOUSTON I FORT WORTHIE DALLAS 10801 M MOPAC EXPY, BLDG 3, STE 2001 AUSTIN, TX 78756 I 512 454 8711 TBRE FIRM REGISTRATION #420 I TBPLS FIRM REGISTRATION A 10028001		

CHECKED PS DRAWN F

SHEET 19 of 83



BLOCK NI			
ET 38)	NC I. TA POSEA OCP 2. A 3. T	DIES: HE LOCATIONS OF EXISTING UNDERGROUND UTILITIES RE SHOWN IN AN APPROXIMATE WAY ONLY AND AVE NOT BEEN INDEPENDENTLY VERIFIED BY THE " WNER OR ITS REPRESENTATIVE." THE CONTRACTOR HALL DETERMINE THE EXACT LOCATION OF ALL XISTING UTILITIES BEFORE COMMENCING WORK, AND OREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL AMAGES WHICH WIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND RESERVE ANY AND ALL UNDERGROUND UTILITIES ALL ROP IS CLASS III UNLESS OTHERWISE NOTED HE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR VENT IS DEFINED BY THE NORMAL DEPTH	DUSTINA GOSS BIBDS
842 840 44 838 100 YR 838 838 838 834 42* 834 100 YR 836 834 100 YR 836 834 834 834		CALCULATION UNLESS SHOWN OTHERWISE EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING SELD SURVEY DATA ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALATION.	TABLE DANSON TABLE DANSON
52 0 50 48 48 44 46 444 44 44 44 338 536 536 536 536 536 536 536 536 536 536		Image: state of the	CITADE A TRACT, PHASE 4 CITADE TRACT, PHASE 4 CITADE A DE RACT, PHASE 4 CITADE A DE RACTOR 4 CITADE A DE RA
		BARSE DE SEPTERATORIED DE SEPTERATORIED DE SETERATORIED DE SET	CITY JOB NO. JOB NO. SOBIE-23 JOB NO. SOBIE-23 DATE MAY 2022 DESIGNER REB CHECKED PS DRAMALABO AD OF 83





(n)

0.00

14

0

d⁰ 0



21-PICP-027

0 00

8 0

8



80 E 110 c E 2

0

Ξ. ...

	0 1964-1915 92		7				Surger State			41				c 2 4	₩	A C			
	60		1 1	20 2 2 9	0 0		K			STA: 1.	3+96.42	SD-B1.01*		F *	BLOCK I				
ř.		SCALE 40"	€ ***	80*	120 [*]	HIS SHEET			Ì	$\left \right $	STA: 14+ = STA: 0 4 X 4' JI STA: =STA:	22.02 "SD +00.00 "SC UNCTION BC 16 0+10.00 "S 22+49.79	B1.01" 		15			Ş Ç	552
SHEET) ~~		σ	9 ² 5	\hat{b}_{j}^{α}	à	INE (SEE 1		$\langle \rangle$		\langle / \rangle		A: 0+20.00 CURB INLI ID CONSTRU	о "SD-В ЕТ "В1.0 ИСПОМ	MAGNO	UA FAR	M, WAY	NY RVC "WT-4E		
(SEE THIS	0				OO MATCH			14,00		24 5(0.1 1.05 5 6.4 0 9.4	2\$D-181	-01° & "				16+00	W-47-		Baio
IAT CHLINE				8	TA: 13+25.		28 28	ſ		29		30			а 31 ⁰		, ⊂ 32.		
13+25.00 M	81 81 81 81	abel 1-48 1-4C 1-4D	Flow (cfs) 159.9 32.1 28.8 23.2	Velocity (ft/s) 15.27 6.54 5.87 4.73		25 yr St Depth lut) (ft) 4 50 3 49 3 63 3 87	orm Event	Hydraulic Grade Line 846.28 848.16 848.45 848.83	(n) (ft)	Hydrau Grade Line (844.4 848.0 848.4 848.7	lic Out) (ft) 9 5 3 3	() (a) (b) (c) (c) (c) (c) (c) (c) (c) (c) (c) (c	5el 48 4C - 4 40 42	Flow (cfs) 179.95 48.38 43.48 35.07	8 10 10 10 10 10 10 10 10 10 10 10 10 10	ocity (5) 31 85	100 y Depth (Out) (ft) 5,51 4,33 4,95 5,56	Storm Even	nt Hydra aulic Grad 847 849 849 850
STA:	81 81 81 8 8	1-4F -4G 1-4H 1-4I 1-4I 1-4I 1-4I 1-4I	23.3 23.3 17.4 17.6 12.33	13.74 13.75 12.85 9.93 9.08		3 56 1 17 1 72 1 11 2 07		850.54 851.24 854.76 856.48 858.77		848.8 850.0 	3 7 2 6 4	-B1 61 61 81 81 81 81	4f	35 37 35 4 26 58 26 73 18 78		21	5.38 2.52 2.32 1.49 2.64		851 851 855 856 859
	208	35 LF 30*	RCP					INISHED GRADE Vatural Ground Select Fill				355.	18 LF 24						
												House Strings B1-41 4	11.503		4			B1-4J	011507
		DDye HGL						101-411.9 BT-411.9	3.00%							11 11 11 12 12			
X		B1	AF 0 3.0											2) 					
31.01° FL 845.27					31.01* FL 848.90					31.00* FL 853.25						855.01 55.07 55.47			
2+75.39 30* 50-8 ADE BREAK					3+96.42 30 SD-E	4+22.02 SD-BI:01	C+00100 SD-B1.C LUNCTION BOX #8 SD-B1.01 FL (out) 8 SD-B1.01 FL (in) 855			5+24.86 24 50-E					6+42.02 "SD_B1.01"	88 (u) 13 .4018-05. 89-81.01 - FL (out) (85-81.01 - FL (u) 85 85-81.01 - FL (u) 85			
SR S	1907 (2) 14				STA: B PT	STÀ.	0 × 1 + 8 N	9		STA: GR					STA:	24 24			

00

۳ ۹ ^{۱۱}

0

23 28 원

0 P 0

8.0



21;PICP-027





A SERVER	51.0Z	34n -	6.8	1.22	
B	31.03	3.45	5.65	1.22	860.22
B	81.04	5.83	8.56	1.57	857
E	81.05	6.47	6.65	1,22 🗉	851.78
B	81.06	6.16	3,49,	2.26	- 9 848.81
Lunger I	31.07	4.8	2.73	1,99 -	848.45
2000-000000000000000000000000000000000	10= = 110 -944 10= = 110 -944			= 100 yr Sto	™ FM Event
ļ	abel	Plow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Hydraulic Grade Line (Ir
	81.02	5.17	7.63	L1,7 ² r	860,75
6	81.03	5.22	2.95	1.7	
B	1.04	8,84	5	2.14	857,78
B	1.05	9.76	5.52	1.82	852.56
В	1.06	9.24	5.23	3.96	850.61
E	31.07	7.2	4.06	3.30	849.80
					D 11 D D
0		c o	X R	24 J E	5 7
	00 <3	0	0		9 - 2





U 2₁₁

21-PICP-027



9 E

đ





	25 yr Storm Event											
o Label	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Hydraulic Grade Line (In) (ft)	-3P.0							
B11-A	130.3	8.19	5.49	848.23	1000							
811-B	127.8	8.04	5.45	848.62	1							
811-C	127.0	7.99	5,49	848.94	0							
B11-D	127.1	7,99	5.36		and the second s							
B11-E	120.3	12,50	4.36	850-19	040.79							
811.06	6.8	3.85	2.36	849.55								
B11.07	0.9	0.52	2.49	848.88								
811.08	29	1.66	2.44	848.53	-							

8 6	ۍ . 		100 yr St	orm Event	70 800
Label	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Hydraulic Grade Line ((n) (ft)	D TIPE D
811-A	135.3	8,51	6.33	849.08	
B11 B	131,7	8.28	6.34	849.52	
B11-C	130.4	8.20	6.41	849.87	のでし
B11-D	130.5	8.20	6.29	850.06	「日本
B11-E	120.3	12,50	5.35	851.17	「小小」
B11.06	10.2	5.78	3.35	850.58	の中山
B11.07	1.4	0.77	3.41	849.80	にいいた
B11.08	4.4	2.47	3,33	- 849.43	

e= :9

(2)

G

-q₂ ОО

6

S 00 0

⁵⁰ 00

	ana an ann a' ann an ann ann ann ann an ann an	
55 00 SO SO	SLE: $1^* = 40^{1}$	
NOTES: THE LOCATIONS O ARE SHOWN IN AN HAVE NOT BEEN I OWNER OR ITS RE SHALL DETERMINE EXISTING UTILITIES AGREES TO BE FL DAMAGES WHICH CONTRACTOR'S F/ PRESERVE ANY A 2. ALL RCP IS CLAS 3. THE HYDRAULIC	F EXISTING UNDERGROUND UTILITIES APPROXIMATE WAY ONLY AND NDEPENDENTLY VERIFIED BY THE PRESENTATIVE. THE CONTRACTOR THE EXACT LOCATION OF ALL BEFORE COMMENCING WORK, AND JULY RESPONSIBLE FOR ANY AND ALL MIGHT BE ASSOCIATED BY THE JULVE TO EXACTLY LOCATE AND ND ALL UNDERGROUND UTILITIES. S III UNLESS OTHERWISE NOTED. RADE LINE (HGL) OF THE 25 YEAR	DUSTIN J GOSS BIBOS CENSE ONAL DISTORES DUSTIN J GOSS
EVENT IS DEFINED CALCULATION UNL 4. EXISTING CONTOUT THIS PLAN SHEET INTERVALS THEY FIELD SURVEY DA 5. ALL FILL AREAS A TO UTILITY INSTAL 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	BY THE NORMAL DEPTH ESS SHOWN OTHERWISE. R INFORMATION SHOWN HERE ON ARE SHOWN AT ONE (1) FOOT ARE COMPUTER GENERATED USING TA. SHALL BE COMPACTED TO 95% PRIOR ATION. WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE DOUBLE WW SERVICE SINGLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE PROPOSED CONTOUR LINE	<text><text><text></text></text></text>
PROFILE S PROFILE S T = 40' HOR T = 4' VERTI PROFILE L NATURAL GROUNI FINISHED GRADE SUBGRADE PROPOSED STOR 25-YR HGL 100-YR HGL	INLET # / CAPTURE DALES: IZONTAL CALES: IZONTAL EGEND: IZONTAL IZONTAL IZONTAL IZONTAL <td>LIVELY TRACT, PHASE 4 DUTY OF LEANDER, TEXAS STORMDRAIN PLANDER, TEXAS LINE SDB11,01 & B11,06-B11,08 LINE SDB11,01 & B11,06-B11,08</td>	LIVELY TRACT, PHASE 4 DUTY OF LEANDER, TEXAS STORMDRAIN PLANDER, TEXAS LINE SDB11,01 & B11,06-B11,08 LINE SDB11,01 & B11,06-B11,08
	TTY OF LEANDER APPROVAL	CITY JOB No. 21-PICP-027 JOB NO. 50816-23 DATE WAY 2022 DESIGNER RBB CHECKED PS DRAWN ABC 25 of 83

21-PICP-027

Hydraulic
Grade Line (Out) (ft)
848.05
848.52
848.88
. 848.94
849/51
849.51
848.52

	Hydraulic	1
Grad	le Line (Out) (ft)	
	848.89	
	849.41	Contage (Inc.
20030 - 2-824	849.80	E LE POESCEL
	849.87	
	850.50	
an en Forde Startific	850.50	
্রুলায়ের রবাগজন্য	849.80	
	849.41	

and a

0 D



			00	E DATE		
			۲' ۲	REVISION		
	o" 40 ¹	11 40) 80 ¹	120 7	N		
	NOTES: 1. THE LOCATIONS OF E ARE SHOWN IN AN A HAVE NOT BEEN INDE OWNER OR ITS REPRI SHALL DETERMINE TH EXISTING UTILITIES BE AGREES TO BE FULLY DAMAGES WHICH MIG CONTRACTOR'S FAILU PRESERVE ANY AND 2. ALL RCP IS CLASS III	XISTING UNDERGR PPROXIMATE WAY PENDENTLY VERIF SENTATIVE. THE E EXACT LOCATIO FORE COMMENCIN RESPONSIBLE FO T BE ASSOCIATED RE TO EXACTLY L ALL UNDERGROUN UNLESS OTHERW	OUND UTILITIES ONLY AND IED BY THE CONTRACTOR N OF ALL G WORK AND OR ANY AND ALL O BY THE OCATE AND D UTILITIES. ISE NOTED:		DUSTIN J BIB SOONA	6055 5 5 05 09 2022
	EVENT IS DEFINED BY CALCULATION UNLESS 4. EXISTING CONTOUR IN THIS PLAN SHEET AF INTERVALS THEY AR FIELD SURVEY DATA 5. ALL FILL AREAS SHA TO UTILITY INSTALAT	THE NORMAL DE SHOWN OTHERW FORMATION SHOW E SHOWN AT ON E COMPUTER GEN LL BE COMPACTED ON	N HERE ON EE (1) FOOT ERATED USING) TO 95% PRIOR		ERS	FORT WORTH I DALLIAS TM, TX 78759 I 512454.8711 M REGISTITATION & LODDBOD
DD		WATER LINE WASTEWATER LIN STORM DRAIN LIN CURB INLET SINGLE WATER S DOUBLE WATER S DOUBLE WW SERV DOUBLE WW SERV GATE VALVE FIRE HYDRANT EXISTING GATE A EXISTING FIRE H EXISTING WATER EXISTING WATER EXISTING STORM EXISTING CONTOL PROPOSED CONT	E & MH NE & MH ERVICE SERVICE ICE VICE VICE VICE VICE VICE VICE V			AUSTIM J ISAN ANTONIO I HOUSTON I 10001 N MOPAC EXPY, BLDG JS, STE 2001 AUS 18PE FIRM REGISTRATION (178PLS FIR
	PROFILE SC Disciplination PROFILE SC Disciplination PROFILE LEC NATURAL GROUND FINISHED GRADE SUBGRADE PROPOSED STORM D 25-YR HGL	NLET # / CAPT O= 25/100 YEA			CITY OF LEANDER, TEXAS	STORMDRAIN PLAN & PROFILE
		D B B B B B B B B B B B B B B B B B B B	DER APPROVA	CITY JOB N DATE DESIG CHECI SHEE	JOB No 6 MI NER KED PS 26	-PICP-027 50816-23 AY 2022 RBB DBAWN ABC OF 83

21-PICP-027

30

\$3

M

Ш



æ



120

21-PICP-027





0.0

æ

00 0 5 0 00 0 5 0 00 60 60

0.0

8

00 00 0

				đ o			
		e e e e e e e e e e e e e e e e e e e				- Marine	
	200 200	ی م	w ⁴ 5	0 00 00		00 F3	
				1Ē		2	
	0		œ				E
		00	6	ی ۵	0		
				O M	0	ථ	
		ත ව		0	α	в о	
CURB INLET "J2.01" CONSTRUCTION 0+84.44 "SD-J2.01"			a,				
						e ع	Ш
	25 yr S	torm Event Hydraulic		Hydraulic			
870 Label (cfs) (ft)	(Out) (ft) 52 1.32 72 0.97 07 1.12 53 1.54 54 1.45 34 1.02	Hydraulic Grade Line 860.27 861.4 862.06 862.53 862.66 862.8	• ((n) (ft) 'Grad	de Line (Out) (ft) 857.75 860.02 861.78 862.5 862.53 862.79	0	Ø	
B64 Flow Vela R 12.00 17.54 12.54	100 yr : Depth (/s)(Out) (ft) .871.65	Storm Event Hydraulic Hydraulic Grade Lini 860:87	e ((n)) (ft)	Hydraulic de Line (Out) (ft) 857-19 860-63		3	
12-N 17-03 0 12-0 12-4 7 858 12-P 7.94 4 12-Q 8.04 4 12-R 8.05 4	49 1.56 °. 49 2.29 °. 55 2.25 °. 56 2.17 °.	862.71 863.33 863.83 864.01		862 23 863 24 863 33 863 94			
854	6					0	
852						0	
848				9	00		
846 ra ∞	0		Ū	00			
844	5	æ	12				
042 3 3 840	0		Ð	الآم			
838 836 836			0		2		
	00						
) 11+25 		SCRONNELLER (NULL) AND SCROP (SERVICE (SERVICE))					400777018080 00 200 2778 7477∓00
CE CE		ථ		0 0		ଥା କ୍ର ଅ	ъ О

90 aa

13

3	∞ 00 0	00 🛥 0	2			
	0	в				
	ц. Э		1 40			
						1949. 1949.
	00 10	UTES: THE LOCATIONS OF E ARE SHOWN IN AN A HAVE NOT BEEN INDE OWNER OR ITS REPRI SHALL DETERMINE TH EXISTING UTILITIES BI AGREES TO BE FULL	XISTING UNDERGROUND UTIL PPROXIMATE WAY ONLY AN PENDENTLY VERIFIED BY TO ESENTATIVE. THE CONTRAC IE EXACT LOCATION OF ALL FORE COMMENCING WORK. Y RESPONSIBLE FOR ANY A	LTIES DE TOR AND ND ALL	DUSTIN J 9180 0C EN 0C EN 0C	GOSS 5 6 8 0 5 0 5 0 5 0 8 0 5 0 8 0 7 0 7 0 7 0 7 7 7 7 7 7 7 7 7 7 7
-	n ⁴ 2 2. 3.	DAMAGES WHICH MIG CONTRACTOR'S FAILU PRESERVE ANY AND ALL RCP IS CLASS II THE HYDRAULIC GRAV EVENT IS DEFINED B CALCULATION UNLES	AT BE ASSOCIATED BY THE RE TO EXACTLY LOCATE AN ALL UNDERGROUND UTILITIE I UNLESS OTHERWISE NOTEI DE LINE (HGL) OF THE 25 Y THE NORMAL DEPTH S SHOWN OTHERWISE	D S.o YEAR		
D	00 5.	EXISTING CONTOUR IN THIS PLAN SHEET AF INTERVALS THEY AF FIELD SURVEY DATA. ALL FILL AREAS SHA TO UTILITY INSTALLAT	LL BE COMPACTED TO 95%	DT JSING PRIOR	son	08114 1 DALLAS
		LEGEND W O W SO SO	WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE		PE-DAW GINEER	10 HOUSTON 1 FORT W 06 3 STE 200 AUSTIN, TX 78 N AAZD TBPLS FIRMIREGIST
			SINGLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE			AUSTIN I SAN ANTON 10801 N MOPAC EXPY BL 18PF FIRM REGISTRATIO
	U		EXISTING STORM DRAIN LI EXISTING CONTOUR LINE PROPOSED CONTOUR LINE INLET # / CAPTURE Q= 25/100 YEAR			
		PROFILE SC 1" = 40' HORIZ(1" = 4' VERTICA PROFILE LE	ALES: <u> </u>	00 90	SE 4	
		NATURAL GROUND FINISHED GRADE SUBGRADE			, PHA	N & PRO (2 OF 2)
		PROPOSED_STORM_C	<mark>JRAIN</mark>] 25уг нбі		FLEANDE	RAIN PLAI SD-J2:01
20	CURVE #	CUR RADIUS DELTA 330.00" 044'48'58	IVE TABLE CHORD BEARING CHORD S35'06'29"W; 251:59	LENGTH 258.12		STORMD
	٥	-				5
					1076337620 07276 012255 12000	
	0				CITY JOB NO JOB NO DATE M DESIGNER	PICP-027 50816-23 AY 2022 RBB

.....

οD



8a - E -

8







		25 yr Storm Event				
Label	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Hydraulic Grade Line (in) (ft		
12.02	3.07	6.76	1.54	862.5		
12.03	4.87	6.43	1.12	861.74		
12.04	6.76	9.91	1.58	852.14		
12.05	.4.78	8.03	1.06	849.52		
12.06	4.4	11.08	1,16	848.89		
12.07-A	3.71	7.28	1.22	847.07		
J2.07-B	3.73	7.29	0.94	847.49		
12 08	3.4	13 35 R	073	848.37		

III ~

			100 yr Storm Event				
0	Label	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Hydraulic Grade Line (In) (f		
38	J2.02	4.63	2.62	2.29	863,27		
10	J2.03	7.35	7 13	1,56	862.3		
	J2.04	10.15	5.74	3.54	854-113		
	J2:05	7.14	74.04	3.79	852.14		
1	J2.06	6.56	3.71	4.1	851.47		
-	12.07-A	5.47	1.74	4.84	850.75		
	J2.07-8	5,54	1.76	4,6	850.78		
1	12:08	5.13	2.9	4.17	850.26		





R - 200

ß

Label	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
J3-A	_ 15.71	12.94	0.92	845:28	843.33
J3-8	12.21	12.08	1.91	846 15	845.76
J3-C4	12,34	6.43	1.18	846.76	846.07
J3-C5	12.5	6.46	1.18	847.5	846.68
J3.04	4.08	12.59	1.41	846.29	845.76

2

070

070

8

0.0

2

•

M

ъ О

0.0

0

2

œ

- P

-

PLUDDZ IDANS SHITAND-PRO	100 yr Storm Event				
Label	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
J3·A	23:44	14.34	2.98	845.76	845:39
13-8	18.22	13;46	2.41	846.43	846.26
J3-C4	18.41	6,89)	1.55	847.09	846,44
J3-C5	18.63	6.9	1.59	847.83	847.09
13.04	6.06	14 12	1.91	846 46	846.76

102 308 ST	-	250005 39-5	CORDER OF STREET,
21-	$\mathbf{P}(\mathbf{c})$	P_f	197
		1 - 6	ICI
	S		

р. 11			DATE	
Ŭ.		120*		
00	NOTES: 1. THE LOCATIONS OF EXISTING UNDE ARE SHOWN IN AN APPROXIMATE HAVE NOT BEEN INDEPENDENTLY OWNER OR ITS REPRESENTATIVE. SHALL DETERMINE THE EXACT LOC EXISTING UTILITIES BEFORE COMME AGREES TO BE FULLY RESPONSIBL DAMAGES WHICH MIGHT BE ASSOC CONTRACTOR'S FAILURE TO EXACT PRESERVE ANY AND ALL UNDERGR 2. ALL ROP IS CLASS III UNLESS OTH THE HYDRAULIC CRATE UNLESS OTH	RGROUND UTILITIES WAY ONLY AND VERIFIED BY THE THE CONTRACTOR ATION OF ALL NCING WORK, AND E FOR ANY AND ALL VATED BY THE LY LOCATE AND ROUND UTILITIES HERWISE NOTED.	DUSTIN 918	
	UEGEND	LINE & MH	-DAWSON VEERS	ITON (1) FORT WORTH I DAULAS 001 AUSTIN TX 78759 I 512 454 8711 PLS FIRM REGISTRATION #10020901
=0	CURB INLET SINGLE WATE DOUBLE WAT SINGLE WW SATE VALVE FIRE HYDRAN EXISTING GA EXISTING FIRI EXISTING WA SD SD SD 286 200 200 200 200 200 200 200 200 200 20	R SERVICE ER SERVICE SERVICE SERVICE IT TE VALVE E HYDRANT TER LINE STEWATER LINE ORM DRAIN LINE NTOUR LINE		AUSTIN, I, SAN, ANTONIO, I, HOUS 10801 M, MOPAC, EXPY, BLDS, 3, STE, 20 THEE FIRM HEGISTBATION #470, 1, TB
9 9	PROFILE SCALES: 1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND: NATURAL GROUND	ONTOUR LINE APTURE YEAR	ASE 4 (AS	OFILE
	FINISHED GRADE SUBGRADE PROPOSED STORM DRAIN 25-YR HGL 25-YR HGL 25-YR HGL 25-YR HGL 00-YR HGL		Y TRACT, PH	RMDRAIN PLAN & PRI LINE SD-J3.01
				STOF
Đ		NDER APPROVAL	CITY JOB NO 21- JOB NO 50 DATE MA DESIGNER CHECKED PS SHEET 31	PICP-027 1816=23 2022 RBB DRAWN ABC OF 83





- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION LINESS SHOWN OTHERWISE
- CALCULATION UNLESS SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING
- FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALATION.

LEGEND

	WATER LINE
— o ——ww —	WASTEWATER LINE & MH
- 0	STORM DRAIN LINE & MH
	CURB INLET
0	SINGLE WATER SERVICE
D	DOUBLE WATER SERVICE
\	SINGLE WW SERVICE
<u>}</u>	DOUBLE WW SERVICE
	GATE VALVE
-⊗()	FIRE HYDRANT
8 1	EXISTING GATE VALVE
- <u>8</u> -(+)-	EXISTING FIRE HYDRANT
	EXISTING WATER LINE
	EXISTING WASTEWATER LINE
SD	EXISTING STORM DRAIN LINE
	EXISTING CONTOUR LINE
	PROPOSED CONTOUR LINE







- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH
- CALCULATION UNLESS SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING
- FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALATION.

LEGEND

	WATER LINE
— • ww —	WASTEWATER LINE & MH
- 0	STORM DRAIN LINE & MH
	CURB INLET
0	SINGLE WATER SERVICE
D	DOUBLE WATER SERVICE
\	SINGLE WW SERVICE
	DOUBLE WW SERVICE
í Ø	GATE VALVE
-⊗(-)	FIRE HYDRANT
8 1	EXISTING GATE VALVE
-84 +}	EXISTING FIRE HYDRANT
wi/	EXISTING WATER LINE
	EXISTING WASTEWATER LINE
SD	EXISTING STORM DRAIN LINE
<u> </u>	EXISTING CONTOUR LINE
786	PROPOSED CONTOUR LINE





- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- ALL RCP IS CLASS III UNLESS OTHERWISE NOTED.
 THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING
- FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALATION.

LEGEND

	WATER LINE
— ww —	WASTEWATER LINE & MH
	STORM DRAIN LINE & MI
	CURB INLET
0	SINGLE WATER SERVICE
	DOUBLE WATER SERVICE
\	SINGLE WW SERVICE
	DOUBLE WW SERVICE
í Ø	GATE VALVE
-⊗()	FIRE HYDRANT
8	EXISTING GATE VALVE
-8-(+)-	EXISTING FIRE HYDRANT
	EXISTING WATER LINE
	EXISTING WASTEWATER L
SD	EXISTING STORM DRAIN I
— — —786— — —	EXISTING CONTOUR LINE
	PROPOSED CONTOUR LIN

NE



-۲ ۲ THIS DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANT'S ORIGINAL SIGNATURE AND SEAL

· · · · · · · · · · · · · · · · · · ·	I		COM	POSITE C		Ī		SHEET	FLOW	w	SUALI	OW CONC			T	CLIANIN		A 111	T					6 6 MM - 40 MM
DRAINAGE	INLET	AREA	C ₂₅	C100	A.C25	A.C100	Length	Manning's	Slope	Tc	Length	Paved/	Slope	Tc	Length	Manning's	Slope	Velocity	Тс	Cumulative Tc	e INTEL I 25yr	I 100yr	DISCH Q 25	Q 100
AREA	NUMBER	(acres)					(ft)	(n)	ft/ft	(min)	(ft)	Unpaved	ft/ft	(min)	(ft)	<u>(n)</u>	ft/ft	ft/s	(min)	(min)	(in/hr)	(in/hr)	(cfs)	(cfs)
ULTIMATE CO	ONDITION D	RAINAGE A	REAS			ĺ						1												
B1.08	B1.08	0.93	0.66	0.74	0.616	0.691	50	0.24	0.030	6.30	145	<u> </u>	0.020	1.06	197	0.015	0.017	50	0.655	8.01	0.85	13.06	R1	
B1.09	B1.09	0.53	0.64	0.72	0.338	0.381	27	0.24	0.023	4.29	90	U	0.016	0.73	266	0.015	0.005	2.7	1.630	6.66	10.45	13.85	3.5	5.3
B1.10 B1.11	B1.10 B1.11	0.84	0.76	0.84	0.356	0.396	23	0.24	0.020	0.00	0		0.020	0.00	783	0.015	0.005	2.7	4.798	5.00	11.30	15.00	4.0	5.9
B1.12	<u>B1.12</u>	0.50	0.67	0.75	0.335	0.376	20	0.24	0.021	3.56	157		0.015	1.91	202	0.015	0.005	2.7	1.238	<u> </u>	10.26	13,61	<u>5.7</u> 3.5	8.5
B1.13 B1.14	B1.13 B1.14	0.29	0.67	0.75	0.194	0.217	<u>0</u> 15	0.24	0.036	0.00	137		0.017	0.00	351	0.015	0.005	2.7	2.151	5.00	11.30	15.00	2.2	3.3
B1.15	B1.15	0.46	0.67	0.75	0.307	0.345	10	0.24	0.036	1.62	148		0.020	0.98	56	0.015	0.005	5.3	0.176	<u> </u>	11.30	15.00	<u>3.4</u> 3.5	5.1
B1.16	B1.16	0.79	0.66	0.75	0.524	0.589	0	0.24	0.015	0.00	80	U	0.015	0.67	492	0.015	0.019	5.3	1.538	5.00	11.30	15.00	5.9	8,8
		0.01	1 0.00	0.74	1 0.557	0.002	90	0.24	0.049	8.32	110	<u> </u>	0.015	0.93	56	0.015	0.043	8.0	0.117	9.36	9.33	12.37	5.0	7.5
B2.01	B2.01	1.06	0.66	0.74	0.699	0.785	20	0.24	0.022	3.42	290	U	0.024	1.93	90	0.015	0.016	4.8	0.312	5.67	10.94	14.51	7.6	11.4
B2.02 B2.03	B2.02	0.74	0.66	0.74	0.522	0.586	20	0.24	0.026	<u>3.20</u> 3.16	290		0.023	1.96 2.18	78	0.015	0.019	5.3	0.245	5.40	11.08	14.70	5.4	8.1
B2.04	B2.04	0.88	0.66	0.74	0.584	0.655	20	0.24	0.015	3.99	290	Ŭ	0.015	2.45	80	0.015	0.014	4.6	0.201	6.73	10.98	13.81	6.1	9.0
B2.05 B2.06	B2.05 B2.06	0.51	0.67	0.75	0.342	0.384	20	0.24	0.072	2.13	185		0.020	1.37	90	0.015	0.016	4.9	0.304	5.00	11.30	15.00	3.9	5.8
B2.07	B2.07	0.63	0.68	0.76	0.426	0.477	20	0.24	0.028	3.10	134	U	0.020	1.12	173	0.015	0.019	5.3	0.544	5.00	11.30	15.00	4.8	4.9
B3.01	B3.01	0.70	0.67	0.75	0.466	0.523	17	0.24	0.077	1.82	271		0.014	234	42	0.015	0.014	A	0.476	E 00	44.00	45.00		
B3.02	B3.02	0.71	0.67	0.75	0.473	0.530	17	0.24	0.044	2.27	275	U	0.014	2.34	43 87	0.015	0.020	<u>4.1</u> 5.4	0.176	<u> </u>	11.30	15.00 15.00	<u>5.3</u> 5.3	7.8
B3.03 B3.04	B3.03 B3.04	0.75	0.66	0.75	0.498	0.560	17	0.24	0.054	2.10	281	U	0.015	2.36	85	0.015	0.020	5.4	0.260	5.00	11.30	15.00	5.6	8.4
B3.05	B3.05	0.53	0.69	0.70	0.366	0.410	0	0.24	0.024	0.00	0		0.001	2.78	78 510	0.015	0.020	<u> </u>	0.239	5.94	10.80	14.32	5.1	7.6
B3.06	B3.06	0.67	0.66	0.74	0.444	0.499	17	0.24	0.027	2.77	288	U	0.011	2.84	84	0.015	0.020	5.4	0.257	5.86	10.84	14.37	4.8	7.2
B3.08	B3.08	0.51	0.66	0.73	0.338	0.379	0	0.24	0.028	2.74	317		0.011	3.12	206	0.015	0.020	5.4	0.631	6.50	10.53	13.96	7.4	11.1
	0101	4.00	0.50	0.04			20				· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·	0.010	0.020	0.7	10.007	0.00	1 11.00	<u>10.00</u>	<u> </u>	0.1
B4.01 B4.02	B4.01 B4.02	0.61	0.66	0.61	0.646	0.738	<u>80</u> 17	0.24	0.021	10.54	277		0.015	1.45	65 40	0.015	0.006	3.0	0.364	12.35	8.37	11.10	5.4	8.2
B4.03	B4.03	0.28	0.75	0.84	0.211	0.235	0	0.24	0.020	0.00	0	Ŭ	0.020	0.00	398	0.015	0.006	3.0	2.224	5.00	11.30	15.00	2.4	<u> </u>
B4.04 B4.05	B4.04 B4.05	0.66	0.66	0.74	0.435	0.489	17	0.24	0.054	2.11	280	U	0.015	2.36	85	0.015	0.006	3.0	0.475	5.00	11.30	15.00	4.9	7.3
B4.06	B4.06	0.39	0.69	0.77	0.270	0.302	0	0.24	0.070	0.00	109		0.016	2.24	60	0.015	0.006	3.0	0.336	5.00	11.30	15.00	5.9	8.8
B4.07 B4.08	B4.07 B4.08	0.70	0.66	0.74	0.462	0.519	17	0.24	0.044	2.28	270	U	0.018	2.09	86	0.015	0.006	3.0	0.481	5.00	11.30	15.00	5.2	7.8
B4.09	B4.09	0.75	0.66	0.74	0.494	0.555	20	0.24	0.022	2.97	312		0.022	2.63	57 88	0.015	0.006	<u>3.0</u> 41	0.319	<u> </u>	11.30	15.00	2.7	4.0
B4.10 B4.11	B4.10 B4.11	0.61	0.68	0.76	0.412	0.462	10	0.24	0.020	2.04	116	U	0.020	0.85	165	0.015	0.014	4.6	0.604	5.00	11.30	15.00	4.7	6.9
		0.00		U.I.Y	0.000	0.407	2.0	0.24	0.042	2.00	140		0.015	1.22	141	0.015	0.014	4.6	0.516	5.00	11.30	15.00	4.4	6.5
B12.1 B12.2	B12.1 B12.2	0.66	0.69	0.77	0.454	0.509	30	0.24	0.036	3.90	148		0.024	0.98	215	0.015	0.006	3.0	1.203	6.09	10,72	14.22	4.9	7.2
B12.3	B12.3	0.31	0.69	0.77	0.213	0.239	0	0.24	0.020	0.00	0		0.010	0.00	436	0.015	0.006	<u>3.0</u> 3.0	2.439	<u>8.78</u> 5.00	9.55	<u>12.66</u> 15.00	3.5	5.2
B12.4 B12.5	B12.4 B12.5	0.79	0.63	0.71	0.494	0.557	90	0.24	0.016	13.06	147	U	0.020	1.07	436	0.015	0.006	3.0	2.439	16.57	7.35	9.75	3.6	5.4
B12.6	B12.6	0.73	0.67	0.76	0.492	0.552	20	0.24	0.100	1.87	302	U	0.010	2.17	100	0.015	0.045	<u>8.2</u> 8.2	0.216	<u>5.18</u> 5.00	11.20	14.86	4.7	7.0
B12.7 B12.8	B12.7 B12.8	0.39	0.67	0.75	0.260	0.292	20	0.24	0.100	1.87	0	U	0.021	2.04	43	0.015	0.020	5.4	0.132	5.00	11.30	15.00	2.9	4.4
B12.9A	B12.9A	0.89	0.66	0.74	0.583	0.655	20	0.24	0.100	1.87	302	U	0.020	2.55	180	0.015	0.020	<u> </u>	1.443	<u> </u>	11.30	15.00	2.2	<u>3.3</u> 9.8
B12.9B B12.9	B12.9B B12.9	0.12	0.61	0.69	0.073	0.082	0	0.24	0.100	0.00	0	U	0.015	0.00	141	0.015	0.020	5.4	0.432	5.00	11.30	15.00	0.8	1.2
r		· · · · · · · · · · · · · · · · · · ·	·						-ll.								0.020	**	1 - 1	5.00	11.30	15.00	1.4	
B5.01 B5.02	B5.01 B5.02	0.49	0.68	0.76	0.331	0.371	20	0.24	0.015	3.99	120	U	0.015	1.01	145	0.015	0.006	3.0	0.811	5.81	10.86	14.41	3.6	5.4
					9.201	0.202	<u> </u>	<u>v.24</u>	0.010	0.00	00		0.010	U.0/	194	0.015	0.006	3.0	1.085	5.00	11.30	15.00	2.8	4.2
B7.01	B7.01	0.73	0.65	0.73	0.474	0.533	20	0.24	0.032	2.96	275	U	0.013	2.49	75	0.015	0.009	3.7	0.339	5.79	10.87	14.42	5.2	7.7
B7.02 B7.03A	B7.03A	0.66	0.67	0.75	0.435	0.488	20	0.24	0.028	3.10	270		0.016	2.18	138	0.015	0.005	2.7	0.846	6.13	10.70	14.19	4.7	6.9
B7.03B	B7.03B	0.75	0.66	0.74	0.495	0.556	20	0.24	0.043	2.63	280	U	0.015	2.36	0	0.015	0.000	3.8	0.021	<u>0.17</u> 5.00	11.30	15.00	4./	<u> </u>
B7.03 B7.04	B7.03 B7.04	<u> </u>	0.67	0.75	0.938	1.053	<u> </u>	0.94	0.020	-	-	n en	0.000	-		0.010	0.010			6.17	10.68	14.17	10.0	14.9
B7.05	B7.05	0.86	0.68	0.76	0.583	0.653	20	0.24	0.020	3.99	0		0.020	0.00	561	0.015	0.019	<u> </u>	2.115	5.00	11.30	15.00	3.7	5.5
B7.06	B7.06	0.35	0.67	0,75	0.235	0.264	20	0.24	0.044	2.60	226	U	0.025	1.46	10	0.015	0.019	5.3	0.031	5.00	11.30	15.00	2.7	4.0
B8.01	B8.01	0.78	0.67	0.75	0.524	0.588	20	0.24	0.015	3.99	125	UT	0.015	1.05	179	0.015	0.019	53	0.563	5.61	10.97	14.55	57	86
B8.02	B8.02	0.54	0.67	0.75	0.361	0.405	0	0.24	0.015	0.00	266	U	0.015	2.24	50	0.015	0.005	2.7	0.306	5.00	11.30	15,00	4.1	6.1
J1.04	J1.04	0.82	0.64	0.72	0.526	0.593	20	0.24	0.028	3.11	128	UI	0.020	0.93	340 1	0.015	0.010	30	1 172	5 57	1100	1/ 62	50 T	071
J1.05	J1.05	0.51	0.70	0.78	0.355	0.397	0	0.24	0.028	0.00	0		0.020	0.00	655	0.015	0.010	3.8	2.838	5.00	11.30	15.00	4.0	6.0
J1.07	J1.07	0.68	0.67	0.75	0.457	0.513	20	0.24	0.028	3.99	00 105		0.015	0.51	<u>380</u> 90	0.015	0.020	<u>5.4</u> 5.1	1.164	5.00	11.30	15.00	5.5	8.2
J1.08	J1.08	0.51	0.75	0.83	0.381	0.424	0	0.24	0.028	0.00	0	U	0.015	0.00	444	0.015	0.008	3.5	2.099	5.00	11.30	15.00	4.3	6.4
J3.01	J3.01	1.26	0.66	0.74	0.835	0.938	20	0.24	0.020	3.56	250	UT	0.022	1.74	171	0.015	0.019	53	0.537	5.84	10.85	11 20	<u>a1</u>	125
J3.02	J3.02	0.39	0.67	0.75	0.262	0.294	20	0.24	0.015	3.99	115	U	0.015	0.97	88	0.015	0.019	5.3	0.277	5.24	11.17	14.82	2.9	4.4
J3.04	J3.04	0.66	0.68	0.76	0.446	0.500	0	0.24	0.015	0.00	60		0.015	0.00	300	0.015	0.019	<u>5.3</u> 3.0	0.927	<u>5.00</u> 5.00	11.30	15.00	2.5	3.7

PICP-24-0120

Cay of Barr		
	RMG	estrature a biologickus 1
CITY OF LE	EANDER APPRO)VAI



STREET FLOW 25 YEAR STORM	AND INLET CALCULATIONS			STREET FLOW AND INLET CALCULATIONS	
	Street Crown Curb Gutter Crown Ponded	INLET ON GRADE CAPACITY	SUMP INLET CAPACITY CURB (with Depression)	INLET ON GRADE CAPACITY INLET ON GRADE CAPACI	SUMP INLET CAPACITY
Inlet No. ULTIMATE CON B1.08	InletDrainageQ 25Q passQ totalWidth F-FTypeHeightSlopeaYoHeightWidthITypeArea(cfs)(cfs)(cfs)(cfs)(ff)(ff)(ff)(ff)(ff)(ff)DITION DRAINAGE AREAS6.076.127P0.501.70%0.420.410.507.680	Eo S'w Sx Se LT L E Qi Qpass Pass to inlet Qi	totalLengthd (ft)cfs)(ft)d (ft)(d \leq h + a)	Inlet Inlet Drainage Q 100 Q pass Q total Width F-F Type Height Slope a Yo Height Width (-) Eo S'w Sx Se LT L E Qi Qpass Pass to Inlet Qto No. Type Area (cfs) (cfs) (ft) (CORB (with DepressiontotalLengthd (ft)d (ft)cfs)(ft)d (ft)d (ft)
B1.09 B1.10 B1.11 B1.12 B1.13 B1.14 B1.15 B1.16 B1.17	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		B1.09 G-1 0.80 5.03 2.7 P 0.30 1.70% 0.42 0.46 0.50 9.89 0.44 0.28 0.04 0.16 16.04 15 0.99 9.0 0.1 Pass B1.09 - B1.09 G-1 0.633 5.28 0.8 6.0 27 P 0.50 0.50% 0.42 0.50 0.50 12.60 0.34 0.28 0.04 0.13 10.56 10 0.99 6.0 0.0 -	- · · · · · · · · · · · · · · · · · · ·
B2.01 B2.02 B2.03 B2.04 B2.05 B2.06 B2.07	G-1 1.06 7.65 7.6 27 P 0.50 1.56% 0.42 0.45 0.50 9.06 0. G-1 0.74 5.43 5.4 27 P 0.50 1.96% 0.42 0.45 0.50 9.06 0. G-1 0.79 5.73 5.7 27 P 0.60 1.88% 0.42 0.40 0.50 7.04 0. G-1 0.79 5.73 5.7 27 P 0.60 1.68% 0.42 0.40 0.50 7.48 0. G-1 0.88 6.08 6.1 27 P 0.50 1.40% 0.42 0.42 0.50 8.12 0. G-1 0.61 3.87 3.9 27 P 0.50 1.64% 0.42 0.35 0.50 6.18 0. G-1 0.40 3.31 3.3 27 P 0.50 1.90% 0.42 0.33 0.50 5.56<	49 0.28 0.04 0.17 13.91 10 0.90 6.9 0.8 - 66 0.28 0.04 0.22 11.04 10 0.99 5.4 0.1 - 61 0.28 0.04 0.21 11.29 10 0.98 5.6 0.1 - 55 0.28 0.04 0.19 11.51 10 0.97 5.9 0.2 - 77 0.28 0.04 0.25 8.45 10 1.00 3.9 0.0 - 85 0.28 0.04 0.27 7.86 10 1.00 3.3 0.0 - 71 0.28 0.04 0.23 10.11 15 1.00 4.8 0.0 -		B2.01 G-1 1.06 11.39 -0.3 11.1 27 P 0.50 1.56% 0.42 0.50 13.50 0.31 0.28 0.04 0.12 19.76 10 0.72 8.0 3.1 split 82.06 / pass 82.02 - B2.02 G-1 0.74 8.09 3.1 11.2 27 P 0.50 1.90% 0.42 0.49 0.50 11.55 0.37 0.28 0.04 0.14 19.61 10 0.72 8.1 3.1 pass 82.02 - B2.03 G-1 0.79 8.54 3.0 11.5 27 P 0.50 1.68% 0.42 0.50 13.50 0.31 0.28 0.04 0.12 20.55 10 0.70 8.1 3.5 split 82.06 / pass 82.02 - B2.04 G-1 0.88 9.05 1.6 0.42 0.50 0.50 13.50 0.31 0.28 0.04 0.12 18.74 10 0.75	
B3.01 B3.02 B3.03 B3.04 B3.05 B3.06 B3.07 B3.08	G-1 0.70 5.27 5.3 27 P 0.50 1.12% 0.42 0.42 0.50 7.98 0 G-1 0.71 5.34 5.3 27 P 0.50 2.00% 0.42 0.42 0.50 7.98 0 G-1 0.71 5.34 5.3 27 P 0.50 2.00% 0.42 0.38 0.50 6.89 0 G-1 0.75 5.63 5.6 27 P 0.50 2.00% 0.42 0.39 0.50 7.08 0 G-1 0.71 5.09 5.1 27 P 0.50 2.00% 0.42 0.37 0.50 6.73 0 G-1 0.53 4.14 4.1 27 P 0.50 2.00% 0.42 0.35 0.50 6.09 0 0 G-1 0.67 4.81 4.8 27 P 0.50 2.00% 0.42 0.37 0.50	56 0.28 0.04 0.19 10.03 10 1.00 5.3 0.0 - 67 0.28 0.04 0.22 10.99 10 0.99 5.3 0.1 - 65 0.28 0.04 0.22 11.43 10 0.98 5.5 0.1 - 69 0.28 0.04 0.23 10.61 10 0.99 5.1 0.0 - 79 0.28 0.04 0.26 9.13 10 1.00 4.1 0.0 - 72 0.28 0.04 0.24 10.19 10 1.00 4.8 0.0 - 54 0.28 0.04 0.19 14.04 15 1.00 7.4 0.0 - 82 0.28 0.04 0.27 8.62 10 1.00 3.8 0.0 -	····································	B3.01 G-1 0.70 7.84 7.8 27 P 0.50 1.12% 0.42 0.47 0.50 10.47 0.41 0.28 0.04 0.15 13.73 10 0.90 7.1 0.8 pass B3.02 - B3.02 G-1 0.71 7.96 0.8 8.7 27 P 0.50 2.0% 0.42 0.45 0.50 9.09 0.48 0.28 0.04 0.17 15.86 10 0.83 7.3 1.4 pass B3.03 - B3.03 G-1 0.75 8.39 1.4 9.8 27 P 0.50 2.0% 0.42 0.47 0.50 9.93 0.44 0.28 0.04 0.16 17.50 10 0.78 7.7 2.1 pass B3.03 - B3.04 G-1 0.71 7.58 2.1 9.7 27 P 0.50 2.0% 0.42 0.40 0.50 7.41 0.62 0.28 0.04	
B4.01 B4.02 B4.03 B4.04 B4.05 B4.06 B4.07 B4.08 B4.09 B4.10 B4.11	G-11.225.415.427P0.500.60%0.420.470.509.960.G-10.614.564.627P0.500.60%0.420.440.508.830.G-10.282.382.427P0.500.60%0.420.360.506.240.G-10.664.924.927P0.500.60%0.420.450.509.280.G-10.795.895.927P0.500.60%0.420.480.5010.720.G-10.393.053.027P0.500.60%0.420.390.507.030.G-10.705.235.227P0.500.60%0.420.460.509.700.G-10.755.335.327P0.500.60%0.420.370.506.600.G-10.755.335.327P0.501.16%0.420.370.507.950.G-10.614.664.727P0.501.40%0.420.380.507.030.G-10.594.394.427P0.501.40%0.420.380.507.030.G-10.614.664.727P0.501.40%0.420.380.507.030.<	44 0.28 0.04 0.16 9.49 10 1.00 5.4 0.0 - 50 0.28 0.04 0.18 8.29 10 1.00 4.6 0.0 - 76 0.28 0.04 0.25 5.13 10 1.00 2.4 0.0 - 47 0.28 0.04 0.17 8.79 10 1.00 4.9 0.0 - 40 0.28 0.04 0.15 10.22 10 1.00 5.9 0.0 - 66 0.28 0.04 0.15 10.22 10 1.00 5.9 0.0 - 45 0.28 0.04 0.16 9.23 10 1.00 5.2 0.0 - 71 0.28 0.04 0.16 9.23 10 1.00 5.3 0.0 - 71 0.28 0.04 0.19 10.16 10 1.00 5.3 0.0 - 66 0.28 0.04 0.22 9.45 10 1.00 </td <td></td> <td>B4.01 G-1 1.22 8.20 -1.3 6.9 27 P 0.50 0.60% 0.42 0.50 0.50 13.50 0.31 0.28 0.04 0.12 12.15 10 0.96 6.6 0.3 spill B4.03 / pass B4.02 - B4.02 G-1 0.61 6.80 0.11 6.9 27 P 0.50 0.60% 0.42 0.50 0.60 13.50 0.31 0.28 0.04 0.12 12.16 10 0.96 6.6 0.3 spill B4.03 / pass B4.02 - B4.03 G-1 0.28 3.62 1.5 5.0 27 P 0.50 0.60% 0.42 0.50 0.50 0.31 0.28 0.04 0.12 12.10 10 0.96 6.6 0.3 spill B4.03 / pass B4.02 - B4.05 G-1 0.79 8.78 -1.9 6.9 27 P 0.50 0.60% 0.42 0.50 0.50 13.50 0.31<!--</td--><td></td></td>		B4.01 G-1 1.22 8.20 -1.3 6.9 27 P 0.50 0.60% 0.42 0.50 0.50 13.50 0.31 0.28 0.04 0.12 12.15 10 0.96 6.6 0.3 spill B4.03 / pass B4.02 - B4.02 G-1 0.61 6.80 0.11 6.9 27 P 0.50 0.60% 0.42 0.50 0.60 13.50 0.31 0.28 0.04 0.12 12.16 10 0.96 6.6 0.3 spill B4.03 / pass B4.02 - B4.03 G-1 0.28 3.62 1.5 5.0 27 P 0.50 0.60% 0.42 0.50 0.50 0.31 0.28 0.04 0.12 12.10 10 0.96 6.6 0.3 spill B4.03 / pass B4.02 - B4.05 G-1 0.79 8.78 -1.9 6.9 27 P 0.50 0.60% 0.42 0.50 0.50 13.50 0.31 </td <td></td>	
B12.1 B12.2 B12.3 B12.4 B12.5 B12.6 B12.7 B12.8 B12.9A B12.9B B12.9	G-1 0.66 4.87 4.9 27 P 0.50 0.60% 0.42 0.45 0.50 9.22 0.4 G-1 0.55 3.50 3.5 27 P 0.50 0.60% 0.42 0.45 0.50 9.22 0.4 G-1 0.55 3.50 3.5 27 P 0.50 0.60% 0.42 0.40 0.50 7.57 0.6 G-1 0.31 2.41 2.4 27 P 0.50 0.60% 0.42 0.36 0.50 6.27 0.7 G-1 0.79 3.63 3.6 27 P 0.50 0.60% 0.42 0.41 0.50 7.72 0.6 G-1 0.63 4.71 4.7 27 P 0.50 4.50% 0.42 0.32 0.50 5.38 0.6 G-1 0.73 5.56 5.6 27 P 0.50 2.00% 0.42 0.34 0.50 5.79 0.6 G-1 0.39 2.94 2.9 27 P <t< td=""><td>48 0.28 0.04 0.17 8.73 10 1.00 4.9 0.0 - 60 0.28 0.04 0.20 6.79 10 1.00 3.5 0.0 - 76 0.28 0.04 0.25 5.17 10 1.00 2.4 0.0 - 59 0.28 0.04 0.20 6.97 10 1.00 3.6 0.0 - 59 0.28 0.04 0.20 6.97 10 1.00 3.6 0.0 - 85 0.28 0.04 0.27 11.82 10 0.97 4.5 0.2 - 84 0.28 0.04 0.27 12.76 10 0.94 5.2 0.4 - 85 0.28 0.04 0.27 7.60 10 1.00 2.9 0.0 - 35 0.28 0.04 0.27 6.73 10 1.00 2.2 0.0 - 35 0.28 0.04 0.27 4.46 15 1.00</td></t<> <td></td> <td>B12.1 G-1 0.66 7.23 -0.4 6.8 27 P 0.50 0.60% 0.42 0.50 13.50 0.31 0.28 0.04 0.12 12.10 10 0.96 6.5 0.3 pass B14.14 - B12.2 G-1 0.55 5.21 0.3 5.5 27 P 0.50 0.60% 0.42 0.47 0.50 10.10 0.43 0.28 0.04 0.16 9.63 10 1.00 5.5 0.0 -</td> <td></td>	48 0.28 0.04 0.17 8.73 10 1.00 4.9 0.0 - 60 0.28 0.04 0.20 6.79 10 1.00 3.5 0.0 - 76 0.28 0.04 0.25 5.17 10 1.00 2.4 0.0 - 59 0.28 0.04 0.20 6.97 10 1.00 3.6 0.0 - 59 0.28 0.04 0.20 6.97 10 1.00 3.6 0.0 - 85 0.28 0.04 0.27 11.82 10 0.97 4.5 0.2 - 84 0.28 0.04 0.27 12.76 10 0.94 5.2 0.4 - 85 0.28 0.04 0.27 7.60 10 1.00 2.9 0.0 - 35 0.28 0.04 0.27 6.73 10 1.00 2.2 0.0 - 35 0.28 0.04 0.27 4.46 15 1.00		B12.1 G-1 0.66 7.23 -0.4 6.8 27 P 0.50 0.60% 0.42 0.50 13.50 0.31 0.28 0.04 0.12 12.10 10 0.96 6.5 0.3 pass B14.14 - B12.2 G-1 0.55 5.21 0.3 5.5 27 P 0.50 0.60% 0.42 0.47 0.50 10.10 0.43 0.28 0.04 0.16 9.63 10 1.00 5.5 0.0 -	
B5.01 B5.02 B7.01	G-1 0.49 3.60 3.6 27 P 0.50 0.60% 0.42 0.41 0.50 7.68 0.5 G-1 0.37 2.84 2.8 27 P 0.50 0.60% 0.42 0.41 0.50 7.68 0.5 G-1 0.37 2.84 2.8 27 P 0.50 0.60% 0.42 0.38 0.50 6.79 0.6 G-1 0.73 5.16 5.2 27 P 0.50 0.92% 0.42 0.43 0.50 8.35 0.6	59 0.28 0.04 0.20 6.93 10 1.00 3.6 0.0 - 39 0.28 0.04 0.23 5.82 10 1.00 2.8 0.0 - 53 0.28 0.04 0.19 9.61 10 1.00 5.2 0.0 -		B5.01 G-1 0.49 5.35 5.4 27 P 0.50 0.60% 0.42 0.46 0.50 9.88 0.44 0.28 0.04 0.16 9.41 10 1.00 5.4 0.0 - - B5.02 G-1 0.37 4.23 4.2 27 P 0.50 0.60% 0.42 0.43 0.50 8.42 0.53 0.28 0.04 0.16 9.41 10 1.00 5.4 0.0 - - - B5.02 G-1 0.37 4.23 4.2 27 P 0.50 0.60% 0.42 0.43 0.50 8.42 0.53 0.28 0.04 0.16 9.41 10 1.00 4.2 0.0 - - - B5.02 G-1 0.73 7.69 7.7 27 P 0.50 0.42 0.42 0.42 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.50	
B7.02 B7.03A B7.03B B7.03 B7.04 B7.05 B7.06 B7.07 B7.08 B7.09 B7.10 B7.11 B7.12	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		B7.02 G-1 0.10 1.1 2.1 P 0.50 0.42 0.42 0.42 0.50 11.35 0.38 0.28 0.04 0.14 13.36 10 0.92 7.0 0.6 pass B7.02 - B7.03A G-1 0.66 7.05 -0.8 6.3 27 P 0.50 0.50% 0.42 0.50 0.50 13.50 0.31 0.28 0.04 0.12 11.02 10 0.99 6.1 0.1 pass B7.02 - B7.03B G-1 0.75 8.33 0.3 8.6 27 P 0.50 1.00% 0.42 0.50 12.90 0.33 0.28 0.04 0.13 15.24 15 1.00 8.6 0.0 - </td <td> .9 15 0.51 0.51 </td>	 .9 15 0.51 0.51
B8.01 B8.02	G-1 0.78 5.75 5.7 27 P 0.50 1.90% 0.42 0.39 0.50 7.25 0.6 G-1 0.54 4.08 4.1 27 P 0.50 0.50% 0.42 0.39 0.50 7.25 0.6 G-1 0.54 4.08 4.1 27 P 0.50 0.42 0.44 0.50 8.72 0.5	53 0.28 0.04 0.21 11.52 10 0.97 5.6 0.1 - 51 0.28 0.04 0.18 7.44 10 1.00 4.1 0.0 -		B8.01 G-1 0.78 8.55 8.6 27 P 0.50 1.90% 0.42 0.45 0.50 9.14 0.48 0.28 0.04 0.17 15.54 10 0.84 7.2 1.3 pass B8.02 - B8.02 G-1 0.54 6.08 1.3 7.4 27 P 0.50 0.42 0.53 0.50 13.50 0.31 0.28 0.04 0.17 15.54 10 0.84 7.2 1.3 pass B8.02 -	
J1.05 J1.06 J1.07 J1.08	G-1 0.62 5.60 5.8 2/ P 0.50 1.00% 0.42 0.44 0.50 8.74 0.55 G-1 0.51 4.01 4.0 27 P 0.50 1.00% 0.42 0.39 0.50 7.10 0.6 G-1 0.73 5.53 5.5 27 P 0.50 2.00% 0.42 0.38 0.50 7.10 0.6 G-1 0.68 5.13 5.5 27 P 0.50 1.76% 0.42 0.38 0.50 7.01 0.6 G-1 0.68 5.13 5.1 27 P 0.50 1.76% 0.42 0.38 0.50 6.97 0.6 G-1 0.51 4.30 4.3 27 P 0.50 0.84% 0.42 0.41 0.50 7.72 0.5	0.28 0.04 0.18 10.63 15 1.00 5.8 0.0 - 0.5 0.28 0.04 0.22 8.06 10 1.00 4.0 0.0 - - 0.6 0.28 0.04 0.22 11.27 10 0.98 5.4 0.1 - 0.6 0.28 0.04 0.22 10.47 10 1.00 5.1 0.0 - 0.28 0.04 0.20 8.29 10 1.00 4.3 0.0 -		J1.04 G-1 0.82 8.66 0.8 9.5 27 P 0.50 1.00% 0.42 0.51 0.50 13.50 0.31 0.28 0.04 0.12 16.22 15 0.99 9.4 0.1 - <th< td=""><td></td></th<>	
J3.01 J3.02 J3.03 J3.04	G-1 1.26 9.06 9.1 27 P 0.50 1.90% 0.42 0.46 0.50 9.51 0.4 G-1 0.39 2.93 2.9 27 P 0.50 1.90% 0.42 0.31 0.50 5.28 0.8 G-1 0.33 2.51 2.5 27 P 0.50 1.90% 0.42 0.31 0.50 5.28 0.8 G-1 0.33 2.51 2.5 27 P 0.50 1.90% 0.42 0.30 0.50 4.94 0.8 G-1 0.66 5.05 5.0 27 P 0.50 0.60% 0.42 0.46 0.50 9.45 0.4	6 0.28 0.04 0.16 16.27 10 0.82 7.4 1.6 -		J3.01 G-1 1.26 13.50 -1.2 12.3 27 P 0.50 1.90% 0.42 0.50 13.60 0.31 0.28 0.04 0.12 21.90 10 0.67 8.2 4.1 spiil J3.03 / pass J3.02 - J3.02 G-1 0.39 4.36 4.1 8.5 27 P 0.50 1.90% 0.42 0.45 0.50 9.07 0.49 0.28 0.04 0.17 15.41 10 0.67 8.2 4.1 spiil J3.03 / pass J3.02 - J3.03 G-1 0.33 3.73 1.2 4.9 27 P 0.50 1.90% 0.42 0.37 0.50 6.71 0.70 0.28 0.04 0.17 15.41 10 0.85 7.2 1.3 pass J3.04 - J3.04 G-1 0.66 7.51 1.3 8.8 27 P 0.50 0.50 0.50 13.50 0.31 0.28 0.04 0.12 13.59 10 0.91 8.0 0.8 pass J1.04 - -	

9, 2024, 10:14am User ID: tkrause vjects\508\16\24\301 Construction Documents\Civil

THIS DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANT'S ORIGINAL SIGNATURE AND SEAL

•

PICP-24-0120

San Jor	APPROVED
	RMG
A Approximation	

CIT JOE DAT DES CHE SHE					
Y 3 N TE			N	U. REVISION DAT	E
NO. 10. NEI KED			*** PRO	-	
SE R	CITY OF LEANDED TEYAS				
Р .РТ СК			TE.		
1CP 502 EME _ D					
-2 B16 BER AE RA		ALICTIN I CAN ANTONIO I HOUSTON I FORT WITCH	J. G J. G J. G		
4-(-2 3C WN					
012 5 024 Al	DRAINAGE CALCHI ATIONS /2 OF 2)	10801 N MUPAG EXPY, BLDG 3, SIE 200 I AUSTIN, TX 78759 I 512.454.8711			
о + ЗС 3		TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801			
		4 1/			



. Ŷ

818.42		
		drau ine 17.1 8.5 324 29.5 30.3 30.9 30.3 30.9 30.3 30.9 30.3 30.9 30.3 30.9 30.3 30.9 30.3 30.9 4 4
		Ilic (In) 9 9 6 7 5 9 6 8 1 1 31 1 7 1
818.69	<u>-100</u> "B1-	(ft)
818.07		Gra 28.10 JUNC
	<u>5' E</u>	Hade STAF10'EN 4.000
		Ivdr. Line 817 817 821 825 827 830 830 830 830 80 800 800 800
4+ 819.25		aulic (OL 16 .72 .37 .29 .64 .52 .7 .35 .42 .35 .42 .35 .42 .35 .42 .35 .42 .35 .42 .35 .42 .35 .42 .35 .42 .35 .42 .35 .42 .42 .42 .42 .42 .42 .42 .42
	400% -25%	
L L L L L L L L L L L L L L L L L L L	HGL	
013.33 STA: 4+28.14 "SD-B1.01"		
= 21A: 0+0000 20+B1.1/ 9' x 9' JUNCTION BOX #B1-B		
822.55 7' × 5' "SD-B1.01" FL (out) \$19.56		
7 x 5 * SD-B1.01 FL (in) 822.22 18 *SD-B1.17* FL (in) 823.24	D" (ESM. P
822.92	50%	STA: AY 60 60 A:AP
314 312 310 308 306 306 304 302 302 202 51	834 834 830 830 826 826 824 822 822 822 818 818	
82 82 82 82 82 81 81 81 81 81	84 84 83 83 83 83 83 83 84 84 84 84 84 84 84 84 84 84 84 84 84	
24 22 20 18 6 4 2	14 12 10 38 36 34 30 28 28	
823.67		*SD B1.0 115 16"
834 D5		
		All
STA: 5+60.01 84* "Sh-B1.01" FI 824 20		
824.36		
*8		
1 ⁺⁹ 824.64	52 I	
824.91		
825.19 STA: 6+47.40 "SD-B1.01"	2057 F	A 2 A A A A A A A A A A A A A A A A A A
= STA: 0+00:00 "SD+B1.16"		
7' x 5' "SD-B1.01" F1 (in) 825.16		
825.46 18" "SD-B1.16" FL (in) 828.66		
v-4F		
825.74	л л нGL л	
STA: 7+15.33 7' x 5' *SD-B1.01* FL825.91 %	G"	BLOOK MM DI PLOOK MI PLOOK MI PLOOK MI PLOOK MININ PLOOK M PLOOK MININ PLOOK M
826.01		
		L'ANDTCHLINE (SEE SUICE
826.29	byr HQ Harl	STA: 8+25.00 Min.
826.56 STA: 7+73.17 7 × 51 *SD-B1.01* FL826.54		
STA: 7+87.66 "SD-B1.01"	37.: 37.: 31-1	
B27.76 STA: 0+00/00 "SD+B5.01" 0 9' x 9' JUNCTION BOX #B1-C		entropy of the second s
0 7' x 5' "SD-B1.01" FL (out) \$26.70	F 7'	
7' x 5' "SD-B1.01" FL (in) 827.70 18" "SD-B5.01" FL (in) 831.20	× 5'	3'
		TR
		2 ²⁸ RICK

					DATE
				SCALF: $1'' = 40'$	
	- 5			0' 40' 80' 120'	NISION
					NO. R
				NOTES: 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN ARPROVIMATE WAY ONLY AND	
				HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND	SATE OF TELE
				AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.	DUSTIN J. GOSS 91805
				2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.	09/21/2024
				4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.	
				 ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION. EXPOSED CONCRETE THAT IS VISIBLE IS REQUIRED TO BE MADE OF STONE OR CLAD IN STONE INCLUDING 	AS 711 801
		·		BUT NOT LIMITED TO LEDGESTONE, FIELDSTONE, CAST STONE, OR OTHER DECORATIVE MATERIALS SUCH AS STAMPED AND TINTED CONCRETE THAT RESEMBLES STONE OR BRICK. THE CONCRETE TRICKLE CHANNEL IS NOT SUBJECT TO THIS REQUIREMENT.	SOC TH 1 DALL 9 1 512.454.8 TION #10028
	12%	- X		LEGEND	FORT WOR A REGISTRA
FT	RICKI	F	- CLASS "A" CONCRETE W/ 6X6X#6 W.W.F. PROVIDE TOOLED JOINTS	WATER LINE WASTEWATER LINE & MH	USTON I USTON I USTON I USTON I AUST
L D	ETAIL		© 10' O.C. WITH DOWELS AND EXPANSION JOINTS © 40' O.C.	SINGLE WATER SERVICE DOUBLE WATER SERVICE SINGLE WWW SERVICE	APP VGI NIO 1 HO BLDG 3, STE ION #470 1
LE CH E REC	IANNEL QUIREMEI	IS NOT NTS FOR		DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT	SAN ANTC
		-		EXISTING GATE VALVE 	AUSTIN I 10801 N MO TBPE FIRM
5' 10	X	844			
122		842		$\frac{\#01}{Q_{25}; Q25}$ INLET # / CAPTURE Q= 25/100 YEAR	
		838		Q ₁₀₀ : Q100	
	() 	836		$\frac{PROFILE SCALES:}{1" = 40' HORIZONTAL}$ $1" = 4' VERTICAL$	О Ш
		834		PROFILE LEGEND:	ASI (AS 0FIL 3)
	Ш	832		FINISHED GRADE	PH PH OF OF
	Е S 	830		SUBGRADE	DER DAN
		828		25-YR HGL	AC -EAN -B1.
	ATCI	824		100-YR HGL 100yr HGL	OF L DRA E SC
l	≥	822		CURVE TABLE	
		820		""""""""""""""""""""""""""""""""""""	
(III) 041.	ΤΑ: ε	818			
	ທ —	816			
, 		812			CITY NO PICP-24-0120
2				APPROVED DMM/A	JOB NO. 50816-25 DATE SEPTEMBER 2024
827.89	828.01				DESIGNER RBB CHECKED TCK DRAWN ADS
	8+	-50		CITY OF LEANDER APPROVAL	SHEET 37 of 83



~____

2 "SD-B1.0 0 "WW-5D" 7.66 "SD-B 00.00 "SD- +14.38 "SD RB INLET "E DNSTRUCTIO 31.14 5: 3.4 0: 5.4 A FARM W 8" A 8" A 8" A 8" X 8	1.01" B1.14" B1.14" B1.14" B1.14" B1.14" Construction Constructio	OCK W BAO STA: BAO STA: PC STA: PC STA: S	14 11+92.59 "SD-B1.01" A: 12+25.12 "SD-B1.01" A: 0+00.00 "SD-B1.1 TA: 0+14.14 "SD-B1.12" VD CONSTRUCTION 13+34.62 "SD-B1.01" STA: 0+10.00 "WW-5C" "SD-B1.01" STA: 0+10.00 "WW-5C" CURB INLET "B1.12" ND CONSTRUCTION		MAGNOLIA MAGNOLIA	A: 0+16.00 "SD-E TA: 7+22.88 "WT A: 13+62.57 "SD-PC 17 17 840 FARM WAY	19 33.01" -5A" BLO -B1.01" STA: 14+8 =STA: 0+1 STA: 14+8 =STA: 0+1 C END END C END END END END END END END END	16 18.98 "SD-B1.01" 00.00 "SD-B1.11" 0+13.92 "SD-B1.11" 0+13.9		STA. 15 5.00 15 5.00 15 5.00 15 5.00 15 15 5.00 15 15 0 15 15 15 15 15 15 15 15 15 15	
Flow (cfs) 354.86 355.01 352.15 316.89 312.73 310.54 310.8 307.06 253.89 254.62 247.38	Velocity (ft/s) 13.13 13.13 10.06 10.56 10.42 10.35 10.36 10.24 8.46 8.49 8.25	Depth (Out) (ft) 5.13 4.82 5.32 6.36 6.69 7.08 6.88 6.77 7.7 7.61 7.32	Hydraulic Grade Line (In) (ft) 833.38 833.31 834.35 835.71 836.24 836.96 837.11 837.65 839.06 839.45 840.14 840.16	Hydraulio Grade Line (Ou 832.83 833.38 833.99 835.49 836.18 836.68 836.68 836.96 837.11 839 839.06 839.78		24	STA:	16+12.56 "SD-B1 (TA: 16+19.37 "SD STA: 0+00.00 "SD STA: 16+29.37 3+65.26 (EXISTING (STA: 0+ 10' CL EN	.01" PC -B1.01" -B1.10" "SD-B1.01" "WW-4F" 28.28 "SD-B1.10" JRB INLET "B1.10" JRB INLET "B1.10" ID CONSTRUCTION	21	
242.75	8.09	6.95	840.69	840.45		Ha 1-S" ● 0.80%	330.38 L	E 6' x 5' BOX	HGL 25	25yr HGL	CHLINE (SEE SHEET 41)
829.95 STA: 11+92.59 6' x 5' "SD-B1.01" FL830.09		$830.55 6' \times 5' \ \text{*SD-B1.0'} \ \text{FL (in)} \ 833.85 \ \text{or} \ \text{*SD-B1.12'} \ \text{FL (in)} \ 833.85 \ \text{or} \ \text{or} \ \text{*SD-B1.12'} \ \text{FL (in)} \ \text{B33.85} \ \text{or} \ \text{or}$	<u>VC *WW-4F* € C.60%</u> <u>VC *WW-4F* € C.60%</u> <u>VC *WW-4F* € C.60%</u>	B31.15 STA: 13+44.62 "SD-B1.01" B31.35 = STA: 0+00.00 "SD-B1.01" B' x 8' JUNCTION BOX #B1-E 6' x 5' "SD-B1.01" F1 (out) 831.30	831.55 6' x 5' "SD-B1.01" FL (in) 831.30 831.55 42" "SD-B3.01" FL (in) 832.80 831.75 6 x 5' "SD-B1.01" FL 831.45 831.75 6 PC	832.15 832.15	832.35 STA: 14+88.98 "SD-B1.01" = STA: 0+00000 "SD-B1.11" = STA: 0+00000 "SD-B1.11" = STA: 0+00000 "SD-B1.11" = 332.46 m m m m m m m m m m m m m m m m m m m	0 6 ** 3 30 - B1.01 FL (in) 832.46 832.75 832.75 832.75 832.75 832.75 832.75 96 832.75 832.75 96 97 97 97 96 97 97 97 97 97 97 97 97 97 97	833.15 833.15 833.15 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.35 833.45 83	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	833.95 B34.15 B34.15

		DATE
		NOI
		SENS
	SCALE: $1'' = 40'$ 0' 40' 80' 120'	<u>0</u>
	NOTEO	STATE OF TELAS
	INDIES: 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES	DUSTIN J. GOSS
	ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR	91805 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL	SSIONAL ENG
- -	DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND	- (
	2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED.	
	3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.	
THE SECOND	4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT	AS AS 111
-+ m	FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR	DALL 2.454.87
	TO UTILITY INSTALLATION.	B I 511 ATION #
1-	LEGEND	7 7 7 7 7 7 7 7 7 7
		LE FOR USTIN, TENRING
		STON BPLS F
	CURB INLET	Н НОЦ
and the second se		
		I SAM
		JSTIN B01 N
850		AL AL
850		AL AL
850		A A
850	=	A A
850 848 846 846 844	EXISTING WATER LINE EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE PROPOSED CONTOUR LINE #01 $a_{28}:a_{25}$ $a_{100}:a_{100}$ INLET # / CAPTURE Q = 25/100 YEAR	THE GOLD AND AND AND AND AND AND AND AND AND AN
850 848 846 844 844 844 842	EXISTING WATER LINE EXISTING WATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE PROPOSED CONTOUR LINE #01 $a_{22}: a_{25}$ $a_{100}: a_{100}$ INLET # / CAPTURE q = 25/100 YEAR PROFILE SCALES:	
850 848 846 844 844 842 840	$\frac{1}{1} = 4^{\circ} \text{ VERTICAL}$ EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE EXISTING CONTOUR LINE $\frac{\#01}{\alpha_{28}:\alpha_{25}}$ PROPOSED CONTOUR LINE $\frac{\#01}{\alpha_{28}:\alpha_{25}}$ INLET # / CAPTURE $Q = 25/100 \text{ YEAR}$	
850 848 846 844 844 842 840	=	AS AS SFILE
850 848 846 844 844 842 840 840 838		HASE 5 EXAS FOFILE T 3)
850 848 846 844 844 842 840 840 838 11 838 11 838 11 836		R PHASE 5 , TEXAS & PROFILE & PROFILE OF 3)
850 848 846 844 844 842 840 840 838 11 838 836 836 836 836		T, PHASE 5 ER, TEXAS IN & PROFILE I (2 OF 3)
850 848 846 844 844 842 840 838 836 836 834	=	CT, PHASE 5 NDER, TEXAS PLAN & PROFILE 1.01 (2 OF 3)
	EXISTING WATER LINE EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE PROPOSED CONTOUR LINE PROPOSED CONTOUR LINE #01 0283:0225 0100:0100 INLET # / CAPTURE Q = 25/100 YEAR PROFILE SCALES: 1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND: NATURAL GROUND FINISHED GRADE SUBGRADE PROPOSED STORM DRAIN 25-YR HGL	RACT, PHASE 5 EANDER, TEXAS N PLAN & PROFILE -B1.01 (2 OF 3)
850 848 846 844 844 842 840 838 838 836 836 834 834 832 830	EXISTING WATER LINE EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE III = 786 PROPOSED CONTOUR LINE III = 786 PROPOSED CONTOUR LINE III = 786 III = 786 IIII = 786 IIIII = 786 IIIIII = 786 IIIII = 786 IIIII = 786 IIIII = 786 IIIII = 786 IIIII = 786 IIIII = 786 IIIIII = 786 IIIIII = 786 IIIIIIIII = 786 IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	F LEANDER, TEXAS F LEANDER, TEXAS AIN PLAN & PROFILE SD-B1.01 (2 OF 3)
850 848 846 844 844 842 840 838 836 836 836 836 834 832 830 830		/ TRACT, PHASE 5 OF LEANDER, TEXAS ADRAIN PLAN & PROFILE JE SD-B1.01 (2 OF 3)
850 848 846 844 842 840 838 838 838 836 836 834 832 830 830 830 828	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	LY OF LEANDER, TEXAS ITY OF LEANDER, TEXAS RMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3)
850 848 846 844 842 840 838 838 836 836 836 834 832 830 830 830 828 826		/ELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS TORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3)
850 848 846 844 842 840 838 838 836 836 836 836 834 832 830 832 830 832 830 828 828 828 828 826	$= - WV = EXISTING WATER LINE \\ = - WV = EXISTING WASTEWATER LINE \\ = - SD = EXISTING STORM DRAIN LINE \\ = - 786 = - EXISTING CONTOUR \\ = - 786 = - EXISTING CONTOUR \\ = - 78$	-IVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3)
850 848 846 844 842 840 838 838 838 836 834 836 834 832 830 830 832 830 832 830 834 832 830 834 834 832 830 834 834 832 830 834 834 834 834 834 834 834 836 836 836 837 836 836 836 837 836 837 838 838 838 836 836 836 837 838 838 836 837 838 838 836 836 836 837 838 838 838 838 836 836 836 836 837 837 838 838 838 838 836 836 836 836 837 837 838 838 838 836 836 836 836 836 836 836	$ \begin{array}{c} \hline \\ \hline $	LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3)
850 848 846 844 844 844 842 840 838 838 838 838 838 838 838 83	$ \begin{array}{c} \hline \\ \hline $	LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3)
850 848 848 846 844 844 842 840 838 838 838 836 836 834 832 830 834 832 830 828 828 828 826 826 824 822 820	EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE FROPOSED CONTOUR LINE FROPOSED CONTOUR LINE #011 $g_{asc} cosc}$ INLET # / CAPTURE $g_{asc} cosc}$ $g_{asc} cosc}$	LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3)
850 848 848 844 844 844 844 844 84	EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE FROPOSED CONTOUR LINE PROPOSED CONTOUR LINE #01 g_{12} g_{12} g	LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3)
850 848 846 844 844 842 840 838 838 838 836 838 836 834 832 830 834 832 830 834 832 830 834 832 830 834 832 830 834 832 830 834 832 830 834 832 830 834 836 836 836 837 838 836 837 838 838 836 838 836 836 837 838 836 836 836 836 837 838 836 836 836 836 836 836 836	EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING WASTEWATER LINE EXISTING CONTOUR LINE $\overrightarrow{\mu}$ = 30 EXISTING CONTOUR LINE $\overrightarrow{\mu}$ = $\overrightarrow{\mu}$ PROPOSED CONTOUR LINE $\overrightarrow{\mu}$ = $\overrightarrow{\mu}$ MILET # / CAPTURE $\overrightarrow{\mu}$ = $25/100$ YEAR $\overrightarrow{\mu}$ = $40'$ HORIZONTAL 1'' = 40' HORIZONTAL 25-YR HGL 25-YR HGL 25-YR HGL 25-YR HGL 100-YR HGL	LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3) LINE SD-B1.01 (2 OF 3)
850 848 846 844 844 842 840 838 836 836 836 836 834 836 836 834 832 830 834 832 830 828 830 828 828 828 826 828 826 828 828 826 828 826 828 826 828 826 828 826 828 826 828 826 830 836 836 836 836 836 836 836 836 836 836		LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3) VIENTIFICATION (2 OF 3)
850 848 846 844 842 840 838 838 836 838 836 834 832 830 834 832 830 828 830 828 830 828 830 828 830 828 830 828 830 828 830 828 830 828 830 834 832 830 834 832 830 834 834 832 830 834 836 834 836 836 837 838 836 837 838 838 836 836 837 838 836 837 838 838 836 837 838 838 836 837 838 838 836 837 838 838 836 837 838 838 836 837 838 836 836 837 838 838 836 836 837 838 836 836 837 838 838 836 836 836 837 838 838 836 838 836 836 837 838 838 836 836 838 836 836 836 836 836		LIVELY TRACT, PHASE 5 LIVELY TRACT, PHASE 5 LIVE SD-B1.01 (2 OF 3) DEPLOSENT TEXAS LINE SD-B1.01 (2 OF 3) DET SED-EMBER 2024 DESIGNERRBB
850 848 848 846 844 844 842 840 838 838 838 838 838 838 838 83		LINE SD-B1.01 (2 OF 3) CITA NOF LEANDER, TEXAS CITA NOF LEANDER, TEXAS STORMDRAIN PLAN & PROFILE LINE SD-B1.01 (2 OF 3) DATE SED-EMBER 2024 DESIGNER RBB CHECKED TCK DRAWN ADS

17+00



-



NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES. 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED.
- 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.



NO. REVISION DATE NO. REVISION DATE NO. REVISION	J. GOSS 105 NSEQ.144 09/21/2024
Engineers	AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10801 N MOPAC EXPY, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711 TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801
LIVELY TRACT, PHASE 5	STORMDRAIN PLAN & PROFILE
CITY OF LEANDER, TEXAS	LINE SD-B1.01 (3 OF 3) & LATERALS B1.08-B1.09
CITY NO	CP-24-0120
JOB NO	50816-25
DATESEPTE	EMBER 2024
DESIGNER	RBB
CHECKED TCK	DRAWN ADS
SHEET	Of 83

PICP-24-0120

CITY OF LEANDER APPROVAL

Bight APPROVED

pmg



~

• -



			25 yr Sto	rm Event	
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
Laber	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
B1.10	4.06	6.4	0.61	838.13	837.61
B1.11	5.72	11.55	1.19	837.57	837.15
B1.12	3.57	13.13	1.53	836.04	835.38
B1.13	2.21	9.71	2.01	835.46	835.1
B1.14	3.48	13.91	1.8	835.5	834.78
B1.15	3.5	17.51	1.14	836.39	833.31
B1.16	5.97	23.71	1.24	835.03	829.9
B1.17	5.05	17.98	0.43	825.99	823.66

	100 yr Storm Event					
labol	Flow	Velocity	Depth	Hydraulic	Hydraulic	
Lavei	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)	
B1.10	5.99	3.39	3.45	840.53	840.45	
B1.11	8.52	4.82	3.82	839.86	839.78	
B1.12	5.31	3.01	3.27	837.14	837.11	
B1.13	3.28	1.86	3.58	836.7	836.58	
B1.14	5.19	15.63	3.19	836.2	836.18	
B1.15	5.22	19.68	1.82	836.55	833.99	
B1.16	8.91	26.64	1.86	835.24	830.52	
B1.17	7.5	20.16	1.45	826.19	824.68	

NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

PROFILE SCALES:	
1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND:	
NATURAL GROUND	

FINISHED GRADE

SUBGRADE ______

PROPOSED STORM DRAIN

25-YR HGL -25yr HGL----

100-YR HGL 00vr HGL---

NO. REVISION	
DUSTII BUSTII	OF TETTS NJ. GOSS 1805 ENSE AL 09/21/2024
FAPE-DAWSON ENGINEERS	AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10801 N MOPAC EXPY, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512,454.871 TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801
LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS	STORMDRAIN PLAN & PROFILE LINE SD-B1.01 LATERALS B1.10-B1.17
CITY NO. <u>PICE</u> JOB NO. <u>50</u> DATE <u>SEPTEN</u> DESIGNER CHECKED <u>TCK</u> SHEET <u>40</u>	P-24-0120 0816-25 MBER 2024 RBB DRAWN ADS Of 83

PICP-24-0120

CITY OF LEANDER APPROVAL

stephnder APPROVED

RMG

Y (4382 ----



PICP-24-0120

Depth	Hydraulic	Hydraulic
)ut) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
3.41	841.99	841.81
3.21	842.41	842.38
2.61	842.34	842.41
2.5	842.92	842.91
2.32	844.74	842.92
1.81	845.13	844.4
2.82	845.95	845.81
2.58	846.99	845.95
1.55	847.93	847.01
1.53	848.73	847.64
2.7	850.07	849.61
2.25	851	850.73
0.95	851.32	850.74
1.4	852.31	851.49
1.4	852.31	851.49

<u>Leamder</u>	APPROVED).
	RMG	an Carry Sam Sector -
i china -		

00 yr Storm Event					
epth	Hydraulic	Hydraulic			
ut) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)			
3.41	841.99	841.81			
3.21	842.41	842.38			
2.61	842.34	842.41			
2.5	842.92	842.91			
2.32	844.74	842.92			
L.81	845.13	844.4			
2.82	845.95	845.81			
2.58	846.99	845.95			
L.55	847.93	847.01			
1.53	848.73	847.64			
2.7	850.07	849.61			
2.25	851	850.73			
).95	851.32	850.74			
1 /	957 21	851 40			

	NATURAL	GROUND					
	FINISHED	GRADE					
	SUBGRAD	<u>E</u>	· · · · ·				
	PROPOSED STORM DRAIN						
	8			· .	0		
	25-YR H	GL	-25yr	HGL			
	100-YR	HGL 100yr HGL			—100yr HGL-	· ·	
Hydra	ulic						
e Line	(Out) (ft)						
841.8	81						
842.3	38						
842.4	41						
842.9	91						
842.9	92						
011	л						

TABLE			
ORD BEA	RING	CHORD	LENGTH
S78'46'51"	V .	214.64'	216.29'
N79'37'23"	Ē	180.30'	181.50'

E TABLE			
CHORD BEARIN	G СНС	DRD LE	NGTH

0.77	850.27
1.09	850.54
2.08	851.22

fraulic	Hydraulic
ine (In) (ft)	Grade Line (Out) (ft)
1.08	840.76
1.59	841.62
1.68	841.36
2.38	842.23
4.38	841.85
4.77	844.02
5.04	845.31
6.63	844.55
7.66	846.65
8.46	847.29
9.78	849.04
0.77	850.27
1.09	850.54
2.08	851.22

0'	40'	80'	120'
		· · · · · · · · · · · · · · · · · · ·	
NOTES:			
1. THE LOCA ARE SHOW	TIONS OF EXI	STING UNDERGRO PROXIMATE WAY	OUND UTILITIES

SCALE: 1"= 40'

- HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL
- DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED.
- 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT
- INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

-SD ---- STORM DRAIN LINE & MH CURB INLET

SINGLE WATER SERVICE

DOUBLE WATER SERVICE

SINGLE WW SERVICE

DOUBLE WW SERVICE

EXISTING GATE VALVE EXISTING FIRE HYDRANT

GATE VALVE

EXISTING WATER LINE

----- EXISTING WASTEWATER LINE

----- EXISTING STORM DRAIN LINE

#01 INLET # / CAPTURE $q_{28}:q_{25}$ Q= 25/100 YEAR $q_{100}:q_{100}$

PROPOSED CONTOUR LINE

FIRE HYDRANT

LEGEND

-2-4-

PROFILE SCALES:

1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND:

--0--



SHEET 41 of 83



~

~

2

~



	25 yr Storm Event					
Labol	Flow	Velocity	Depth	Hydraulic	Hydraulic	
Label	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)	
B2.02	5.47	9.07	1.28	850.26	850.27	
B2.03	5.78	7.63	1.63	849.08	849.04	
B2.04	6.13	9.43	0.74	847.13	846.7	
B2.05	3.9	10.2	1.32	845.4	845.31	
B2.06	3.34	5.88	0.83	842.33	842.23	
B2.07	4.85	8.44	0.95	841.85	841.62	

	100 yr Storm Event						
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic		
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)		
B2.02	8.15	10.08	1.75	850.8	850.73		
B2.03	8.6	4.87	2.2	849.69	849.61		
B2.04	9.12	10.47	0.94	847.34	846.9		
B2.05	5.81	11.43	1.82	845.73	845.81		
B2.06	4.93	6.53	1.5	842.92	842.91		
B2.07	7.21	9.39	1.71	842.43	842.38		

NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH
- CALCULATION UNLESS SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON
- THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

PROFILE SCALES:		
1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND:		<u> </u>
NATURAL GROUND	÷	
FINISHED GRADE		
SUBGRADE		

PROPOSED STORM DRAIN

25-YR HGL

100-YR HGL

		μ	
raulic ne (In) (ft)	Hydraulic Grade Line (Out) (ft)	Ž <u>A</u>	
0.26 9.08	850.27 849.04		
7.13 5.4	846.7 845.31		
2.33	842.23	7	
1.85	841.62		
		KEV	
raulic	Hydraulic	<u>o</u>	
ne (In) (ft)	Grade Line (Out) (ft)		
9.69	849.61		
7.34	846.9 845.81	TE OF	TEN
2.92	842.91	S S P	T TAS
2.43	842.38	DUSTIN J.	GOSS
		면. 9180 이 · · · · ·	5
		KSSIONAL	SENGIN
			09/21/2024
NO UN EXISTI IN AN APPRO	NG UNDERGROUND UTILIT XIMATE WAY ONLY AND DENTLY VERIEIED BY THE	°	
S REPRESENT	ATIVE. THE CONTRACTO		
LITIES BEFORE	COMMENCING WORK, AN PONSIBLE FOR ANY AND	ALL	
ICH MIGHT BE	ASSOCIATED BY THE D EXACTLY LOCATE AND	2	LLAS 4.8711 28801
NY AND ALL U	JNDERGROUND UTILITIES. ESS OTHERWISE NOTED	Ō	I DA 112.454 #100
LIC GRADE LIN	NORMAL DEPTY	N N N	RTH 59 I 5 Ation
UNLESS SHO	WN OTHERWSE.		г W0 X 787 зізтв <i>і</i>
HEET ARE SI	HOWN AT ONE (1) FOOT		FORT TIN, T M REG
Y DATA.	COMPACTED TO 95% DE		n I I AUS S FIRI
ISTALLATION.	COMPACIED 10 33% Pr)UST(200 TBPL
		22	Н Н(3, STI 470 1
SCALES	•		ONIO BLDG
RIZONTAL			ANT(EXPY, STRAT
	:		SAN)PAC I REGIS
			n MC Firm
IAN			AUST 10801 TBPE
· · · · · · · · · · · · · · · · · · ·			
RM DRAIN			
	6		
	100yr HGL	S	.07
			ЩŴ
		SS	2-E
		A	0.0
		ΤÜ	Р Н В З В З
		□ □ [~.	လ လ
			AN
		59	IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII<
		A V V	d II
		三化	
			45
			MD Z.
			ЧЧ Н Н Н Н С Н С
			ST(ES
			STC INE S
			STC LINE S
			STC LINE S
			STC LINE S
			STC LINE S
			STC LINE S
			-24-0120
City of L.P. (H.I) (GY	APPROVED	CITY NO. PICP JOB NO. 50	-24-0120 B16-25 BFR 2024
City of	APPROVED	CITY NO JOB NO DATESEPTEMI DESIGNER	-24-0120 B16-25 BER 2024 RBB
Ciny d	APPROVED	CITY NO JOB NO DATE DESIGNER CHECKED TCK	-24-0120 B16-25 BER 2024 RBB
City of	APPROVED PMG	CITY NO. PICP JOB NO. 50 DATE SEPTEM DESIGNER CHECKED TCK D	-24-0120 B16-25 BER 2024 RBB WRAWN ADS

PICP-24-0120



-

~

845 STA: 5+35.34 "SD-B3.01" STA: 0+00.00 "SD-B3.02" STA: 0+14.14 "SD-B3.02" STA: 0+14.14 "SD-B3.02" IO IO IO IO IO IO IO IO IO	
SD-B3.05" STA: 3+59.37 "SD-B3.01" T,63 "SD-B3.05" STA: 3+59.37 "SD-B3.01" STA: 3+59.37 "SD-B3.04" STA: 3+59.37 "SD-B3.04" ************************************	25 yr Storm Event owVelocityDepthHydraulicHydraulicfs)(ft/s)(Out) (ft)Grade Line (In) (ft)Grade Line (Out) (ft).8812.683.92836.74836.72.2311.762.77838.44836.99.3311.771.27839.33837.97.3911.312.25839.79839.83.7510.692.31840.88840.0511.020.98843.56841.39.559.861.99844.61844.11.579.860.83845.27844.28.38.121.17847.02845.27
B3.04 B3.04 C25: 5.1 C100: 9.7 B3.04 B3.04 B3.04 B3.04 C25: 5.1 C100: 9.7 B3.04 B3.04 B3.04 C100: 9.7 B3.04 C100: 9.7 B3.04 C100: 9.7 B3.04 C100: 9.8 C100: 7 C100: 9.8 C100: 7 C100: 7	31 7.26 0.92 847.24 847.13 100 yr Storm Event 100 yr Storm Event ow Velocity Depth Hydraulic Hydraulic fs) (ft/s) (Out) (ft) Grade Line (In) (ft) Grade Line (Out) (ft) .21 6.15 6.2 839.16 839 .57 6.16 5.38 840.13 839.6 .57 6.16 5.38 840.23 840.13 .84 12.6 3 840.58 840.58 0.9 11.94 3.12 841.22 840.82 .96 12.13 1.26 843.85 844.62 .71 10.96 2.51 844.88 844.62 .75 10.97 1.05 845.54 844.5 .9 9.09 1.82 847.21 845.93 91 8.12 1.14 847.43 847.35
Image: Constraint of the second se	
ВЗ-G [*] © 2.10% ВЗ-G [*] © 2.10%	
1073 1073 840 1073 1073 836 1073 1073 836 1073 1073 836 1073 1073 1073	
000000000000000000000000000000000000	

	DATE				
	REVISION				
SCALE: $1'' = 40'$ 0' 40' 80' 120'	NON NON				
mining mining mining mining <td< th=""><th>PAPE-DAWSON</th><th>DUSTIN SOLO</th><th>AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS</th><th>TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801</th><th>24</th></td<>	PAPE-DAWSON	DUSTIN SOLO	AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS	TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801	24
PROPOSED CONTOUR LINE PROPOSED CONTOUR LINE #01 g_{st} (225 g_{st} (225) g_{st} (25) g_{st} (27) g_{st} (2	LIVELY TRACT, PHASE 5	CITY OF LEANDER, TEXAS	STORMDRAIN PLAN & PROFILE	LINE SD-B3.01	
Stednoer APPROVED PMG	CITY NO. JOB NO. DATE DESIGNED CHECKED	5 5 R 0тск	P-24- 0816-2 MBER 2 RBB DRAWN	0120 25 2024 1 AD:	

draulic	Hydraulic
Line (In) (ft)	Grade Line (Out) (ft)
36.74	836.72
38.44	836.99
39.33	837.97
39.79	839.83
40.88	840
43.56	841.39
44.61	844.11
45.27	844.28
47.02	845.27
47.24	847.13

NO. REVISION DUSTIN 91 Signal 91 Signal 91	J. GOSS 805 NSE 09/21/2024
FAPE-DAWSON ENGINEERS	AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10801 N MOPAC EXPV, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711 TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801
LIVELY TRACT, PHASE 5	STORMDRAIN PLAN & PROFILE
CITY OF LEANDER, TEXAS	LINE SD-B3.01
CITY NO. PIC	P-24-0120
JOB NO. 5	0816-25
DATE SEPTE	MBER 2024
DESIGNER	RBB
CHECKED TCK	DRAWN ADS
SHEET 43	Of 83



.





	25 yr Storm Event					
label	Flow	Velocity	Depth	Hydraulic	Hydraulic	
Lavel	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)	
B3.02	5.39	7.52	0.71	845.73	845.32	
B3.03	5.67	8.8	1.49	844.04	844.11	
B3.04	5.13	8.59	0.67	842.02	841.58	
B3.05	4.17	6.29	0.62	840.19	839.7	
B3.06	4.85	6.39	0.72	840.19	839.91	
B3.07	7.49	14.81	1.27	837.58	836.99	
B3.08	3.85	9.57	1.27	837.27	836.99	

	100 yr Storm Event						
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic		
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)		
B3.02	8.01	8.32	1.32	845.93	845.93		
B3.03	8.47	4.79	2.01	844.7	844.62		
B3.04	7.64	9.55	0.85	842.22	841.76		
B3.05	6.2	6.98	1.5	840.57	840.58		
B3.06	7.23	4.09	1.62	840.87	840.82		
B3.07	11.15	6.31	3.88	839.7	839.6		
B3.08	5.73	3.24	3.88	839.65	839.6		

NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

PROFILE SCALES:

1" = 40' HORIZONTAL1" = 4' VERTICAL PROFILE LEGEND: ------NATURAL GROUND

FINISHED GRADE

SUBGRADE

PROPOSED STORM DRAIN

25-YR HGL

100-YR HGL

<u>Leander</u>	APPROVED
	RMG
7 C.222 -	
CITY OF LEA	ANDER APPROVAI



NO. REVISION DUSTIN DUSTIN DUSTIN DUSTIN DUSTIN DUSTIN DUSTIN DUSTIN	DF 7.5-70 J. GOSS 805 N.S.E.O. MA AL ENGLAND
REPEDAWSON ENGINEERS	AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10801 N MOPAC EXPY, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711 TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801
LIVELY TRACT, PHASE 5	STORMDRAIN PLAN & PROFILE
CITY OF LEANDER, TEXAS	LINE SD-B3.01 LATERALS B3.02-B3.08
CITY NO. PICH	2-24-0120
JOB NO. 50	0816-25
DATE SEPTEM	MBER 2024
DESIGNER	RBB
CHECKED TCK	DRAWN ADS



/ >	1 11 1-	1.						-)			25 vr Str	orm Event	
			26	1				, J Labe	Flow	Velocity	Depth	Hydraulic	Hydraulic
D-B4.06 T "B4.06" 3 TPUCTION		25		< ib	T.t		i \``	B4-A	(cts) 36.18	(ft/s) 12.45	(Out) (ft) 3.22	Grade Line (In) (ft) 834.4	Grade Line (Out) (ft) 834.35
	1.1-, / 1			X		$\sqrt{1}$	1	<u> В4-В</u>	33.06	12.15	2.99	834.57	834.57
				~ 1	STA: 6+8	35.71 "SD-E	34.01"	078 B4-C	29.92	<u> </u>	2.83	835.99 837.17	834.57 836.49
	/\\		X	1		D CONSTRU	CTION X X2	B4-E	24.11	11.15	2.06	837.76	837.58
								/ <u>B4-F</u> B4-G	24.12	<u> </u>	1.4 1.56	837.83	837.58 838.3
	вгоск х	STA: 0+14.14 "SD 10' CURB INLET	-B4.03" "B4.03"	STA: 6+5	57.42 "SD-B4.0 PI 45'00'00"	1" " <u> 1</u> " "		B4-1	16.16	7.31	2.02	839.26	839.26
		END CONST	RUCTION		1		T e	B4-J B4-K	14.06	6.57	2.09 1.02	839.29 840.15	839.37 839.54
	845 STA:	5+62.82 "SD-B4.01		$\langle \rangle$	\sim			A B4-L	10.52	6.57	1.08	840.2	840.06
X I	=STA:	0+00.00 "SD-B4.03		1	8-1-		T	B4-N	5.44	5.94	1.55 1.59	840.6 840.57	840.6 840.67
M	STA: 5+49	9.21 "SD-B4.01"	\ ₉ 2	()				B4-0	5.45	8.47	0.93	841.22	840.67
	11	10					MT_	F^{-}	Y				
	STA: 4+83.6	1 "SD-B4.01"			B4 03		-+=		T T	A T			
	= STA: 0+00.00 4' X 4' JUNCTION	0 "SD-B4.04" N BOX #B4-B			Q25: 2.4	t		T	1	THE STATE			
	STA: 0+10.00 "SD)-B4.04")	+ h	ノ井	<u></u>			H.J.	MMM -				
	=STA: 7+81.58 *	<u>'WW-5A"</u>			6+01		HHH	6×86	B4.01	12			
	Q25: 3.0		A Contraction of the second se			H DVC "WY	1-50°		Q25: 5.4 Q100: 6.9				
And the second s	Q100: 6.8		-5+00		OX 2	8			TA: 6+71.56	/ /SD-B4.01")			
the second secon	4+00 30" R.C.P.	"SD-B4.01"	, For	H	BZ BZ	1.02			STA: 6+82.36	<u>"WW-5D"</u>			
				1	Q25: Q100	4.6	N	A				 	an an an ann an Aonaichtean an Aona Ann an Aonaichtean an
1		Ī	B4.04	511	= 7/ -					Viele -**	100 yr Ste	orm Event	likelaa fi
24	H B4.05	The second secon	- Q25: 4.9 T		$I \setminus I$			Labe	I Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
	Q25: 5.9 Q100: 6.9	— — — — Y			1-+-1			28 B4-A	54.18	7.66	4.36	835.64	835.49
				<u>k-1</u>		27	-+	B4-B	49.52	7.01	4.4	836.03 836.4	835.98 836.03
	(STA: 0+2	20.00 "SD-B4 04"	//		1	¥ F-		B4-D	38.93	12.7	2.84	837.56	837.06
		RB INLET "B4.04"	25		1		\	B4-E	36.1	12.44	2.57 1.75	838.13 838.2	838.1 837.93
22	23-	24		XI	! · · · · · · · · · · · · · · · · · · ·	1	$\langle \rangle$	B4-G	30.61	8.46	2.12	839.13	838.87
82.54 "SD-B4.01"		STA: 5+57.4	2 "SD-B4.01" 0 "SD-B4.02"	TAL		1-00-		B4-1 B4-J	24.23	4.94	2.52 2.67	839.78 840.1	839.77 839.95
3+94.27 "WW-5D"		(CTA.)+14.14 "SD_B4					B4-K	15.78	7.2	1.83	840.42	840.36
TA: 0+28.80 "SD-B4	4.05"	=STA:	<u>5+82.36 *WW-</u>	50"	BLOCK W			B4-L B4-N	<u> </u>	6.61	1.36 1.96	840.48 841.01	840.35
END CONSTRUC		ST	A: 0+28.28 "SD	-B4.02"	1	F	SIT	B4-N	8.25	6.17	2.04	841.15	841.12
			10' CURB INLET END CONST	"B4.02" RUCTION		+		<u> </u>	8.26	9.53	1.4/	841.42	<u> </u>
	B1-0-0-0-0-2-0-0-0-2-0-0-0-2-0-0-0-2-0-0-0-2-0-0-0-2-0-0-0-2-0-0-0-2-0-0-0-2-0-0-0-2-0-0-0-0-2-0			214 214 214 214 215 215 214 214 214 214 214 214 214 214 214 214	333.5 33.5 3.5 </th <th></th> <th></th> <th></th> <th></th> <th>852 850 848 848 846 844 842 840 838 838 836</th> <th></th> <th></th> <th></th>					852 850 848 848 846 844 842 840 838 838 836			
36" "SD-B4.01" FL (out) 836.24 30" "SD-B4.01" FL (in) 836.74 30" "SD-B4.07" FL (in) 837.74 18" "SD-B4.07" FL (in) 837.74 7.09 18" "SD-B4.07" FL (in) 837.74 7.27 STA: 3+72.02 "SD-B4.01"	7.62 7.62 8.00 50 - 64.05 7.24 8.37 24 9.00 50 * 8.00 55 7.24 9.05 7.24 9.05 7.24 9.05 7.24 9.05 7.24 9.05 7.24 18" * 80-84.05 7.24 9.05 7.24 7.24 7.24 7.25 7.24 7.25 7.24 7.25 7.24 7.25 7.24 7.25 7.24 7.25 7.24 7.25 7.24 7.25 7.24 7.25 7.24 7.25 7.25 7.25 7.25 7.25 7.25 7.25 7.25	37.79 57.97 57.97 57A: 4+83.61 "SD-B4.01" = STA: 0+00.00 "SD-B4.04"	58.64 4' x 4' JUNCTION BOX #84-B 50.85 30" *5D-B4.01" FL (out) 838.03 24" *5D-B4.01" FL (in) 838.53 18" *5D-B4.04" FL (in) 839.03 58.82	38.99 STA: 5+49.21 24" "SD-B4.01" FL83898 @ PT	39.17 STA: 5+57.42 "SD-B4.01" 39.17 = STA: 0+00100 "SD-B4.02" 24" "SD-B4.01" 24" "SD-B4.01" 24" "SD-B4.01" 18" "SD-B4.02" 39.34 18"	-5D* @ 0.5	39.69 STA: 6+57.42 "SD-B4.01"	P. 15 24" "SD-B4.01" FL 839.74 P. 15 24" "SD-B4.01" FL 839.74 STA: 6+85.71 "SD-B4.01" 24" "SD-B4.01" FL (out) 840[40	10° CURB INLET B4.01 END CONSTRUCTION	830 832 832 830 830 828 828 828 828 828 828 828 828 828 828 828 828 828 828 828 828 822			



- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

LEGEND	
	WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE SINGLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE
	EXISTING CONTOUR LINE PROPOSED CONTOUR LINE
#01 Q25:Q25 Q100:Q100	INLET # / CAPTURE Q= 25/100 YEAR

$\frac{PROFII}{1" = 40'}$ $\frac{1" = 40'}{PROFII}$ $\frac{1" = 4'}{PROFII}$ $\frac{100}{100}$ $\frac{100}{100}$ $\frac{100}{100}$	ESC/ HORIZO VERTICA ELEC ROUND RADE STORM DI STORM DI CUR DELTA 025*23*31*	ALES: NTAL SEND: RAIN 5yr HGL- 100yr HGL- VE TABLE CHORD BEARING \$79'22'22"W	CHORD 250.55'	LENGTH 252.61'	LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS	STORMDRAIN PLAN & PROFILE LINE SD-B4.01
	CI	Freduder AP	PRC	NED	CITY NO JOB NO DATE DESIGNER CHECKED TO SHEET	PICP-24-0120 50816-25 PTEMBER 2024 RBB K DRAWN ADS 5 Of 83

~~~~~ × DUSTIN J. GOSS 91805 ON CENSED IN 110000 09/21/2024 al 5355 DALLAS 2**454.8711** 2 0 SS 3 X AU PAPE-DA ENGINEE ZZ STORMDRAIN PLAN & PROFILE LINE SD-B4.01 -24-0120

28.28 LF 18" RCP 14.14 LF 18" RCP 354 839.67 834.80 85 852 리더 <u>. 2 6</u> 850 850 848 2 m +14.14 5+82.3 846 FINISHED-GRADE 844 844 SELECT-----FILL SELECT-FILL FINISHED-842 100 YR HGL 842 GRADE 100 YR HGL----840 25 YR HGL 25 YR HGL-840 838 838 .838 836 836 836 834 834 832 832 832 830 H 830 830 830 828 <u>8 4 4</u> 828 0 8 8 839 839 839 50000 826 826 -1826 826 ट ट ट ् त त त 00000 824 824 4.14 " 34.03" INLET -1824 -1824 255 4 4 4 4 4 4 4 <u> 19 28</u> <u>ੜ ਲੇ ਲੇ ਲੇ</u> <u>אַ אַ אַ ד</u> 822 822 - 822 24 °S 24" STA: 24" STA: 18" EN1 8" STA 18" END SD-B4.02 SD-B4.03 SD-B4.04 0+00 0+75 0+00 0+75 20 LF 18" RCP 854 <u>B4-A</u> FL 837.91 FL 831.03 854 852 852 852 <u>0 ₹</u>| 850 850 850 848 848 848 <u>* 1 04</u> 846 846 846 S IS 844 844 FINISHED GRADE 842 842 842 842 840 840 100 YR HGL 840 100 YR HGL-838 25 YR HGL 838 838 838 25 YR HGL-836 836 836 836 834 834 834 832 832 832 830 830 830

 STA:
 3+00.65
 "SD-B4.01"

 =
 STA:
 0+00.00
 "SD-B4.01"

 +'
 ×
 +'
 JUNCTION
 BOX #B4-A

 36"
 "SD-B4.01"
 FL
 (out)
 B36.74

 36"
 "SD-B4.01"
 FL
 (out)
 B36.74

 36"
 "SD-B4.01"
 FL
 (in)
 B35.74

 30"
 "SD-B4.07"
 FL
 (in)
 B37.74

 18"
 "SD-B4.07"
 FL
 (in)
 B35.74

 18"
 "SD-B4.07"
 FL
 (out)
 B35.774

 18"
 "SD-B4.07"
 FL
 (out)
 B357.74

 10"
 CURB
 NLET
 B4.07"
 END
 END

 10"
 CURB
 NLET
 B4.07"
 END
 END
 END

 10"
 CURB
 NLET
 B4.07"
 END
 END
 END

 < .01" -B4.08" ut) 835.53) 835.53) 837.02 828 828 -826 H 826 --1826 ू _ट ट ट ट STA: 0+14.14 "S 18" "SD-B4.08" 10' CURB INLET END CONSTRUCT 824 824 -1824 <u>אַאַ</u>אַאַ אַאָּאַאַאַאַ 822 822 -1822 18° × SD-B4.07 SD-B4.08 SD-B4.09 0+00 0+00 0+75 0+75 THIS DOCUMENT HAS BEEN PRODUCED FROM MATERIAL THAT WAS STORED AND/OR TRANSMITTED ELECTRONICALLY AND MAY HAVE BEEN INADVERTENTLY ALTERED. RELY ONLY ON FINAL HARDCOPY MATERIALS BEARING THE CONSULTANT'S ORIGINAL SIGNATURE AND SEAL.



			· · · · · · · · · · · · · · · · · · ·	25 yr Sto	rm Event	
854	Labol	Flow	Velocity	Depth	Hydraulic	Hydraulic
	Laber	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
852	B4.02	4.6	5.86	1.05	840.62	840.6
002	B4.03	2.4	5.67	1.09	840.65	840.67
	B4.04	4.96	6.52	0.71	840.09	839.74
850	B4.05	5.94	7.59	1.02	839.62	839.26
	B4.06	3.08	7.72	1.09	839.31	839.37
0.40	B4.07	5.26	8.3	0.65	839.01	838.4
848	B4.08	2.7	10.21	0.36	838.55	837.38
	B4.09	5.37	12.31	0.49	838.36	836.21
846	B4.10	4.69	15.26	1.33	835.87	834.57
	B4.11	4.43	12.14	1.49	835.85	834.57
011				-	· · · · · ·	
044				100 yr Sto	orm Event	
	Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
842		(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
	B4.02	6.85	6.47	1.46	841.03	841
010	B4.03	3.55	6.32	1.54	841.12	841.12
040	B4.04	7.39	7.2	1.33	840.28	840.36
	B4.05	8.84	8.37	1.52	839.83	839.77
838	B4.06	4.57	8.63	1.67	839.95	839.95
	B4.07	7.85	9.22	1.12	839.21	838.87
000	B4.08	4.02	11.46	1.07	838.7	838.1
836	B4.09	8.01	13.76	1.34	838.56	837.06
	B4.10	6.98	17.1	2.78	836.06	836.03
001	R/ 11	6.61	13.6	20	836.03	925.09

NOTES:

832

-1824

-1822

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH THE ASSOCIATED BY THE DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION. SUBGRADE PROPOSED STORM DRAIN

100-YR HGL

city of Leander	APP	RON	/ED
	1-1	- 0	
	pr	NG	
r Qizzina			

		NO.	REVISION
PAPE_DAWSON			- - -
ENGINEERS	TE DUS Solution		
	F J. O 305		
I ANTONIO I HOUSTON I FORT WORTH I DALLAS			-
EXPY, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711	S		
ISTRATION #470 I TBPLS FIRM REGISTRATION #10028801	*****		

2

PICP-24-0120

1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND:	
NATURAL GROUND	······
FINISHED GRADE	

25-YR HGL

-25yr HGL-

CITY NO). <u>PI(</u>	CP-24-	-0120
JOB NO		50816-	25
DATE	SEPTE	MBER	2024
DESIGNE	.R	RBE	3
CHECKE	<u>D_тск</u>	DRAW	N_ADS_
	10	_ f	
SHEET	40	OT	_





25 yr Storm Event									
Labol	Flow	Velocity	Depth	Hydraulic	Hydraulic				
Label	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)				
B5-A	6.25	9.9	0.61	833.49	831.81				
B5-B	3.55	8.45	1.33	833.85	833.85				
B5-C	3.6	8.49	1.29	837.44	833.85				
B5-D	3.62	7.84	0.47	838.67	837.19				
B5-E	3.63	5.57	0.83	838.8	838.77				
B5.02	2.86	17.94	1.33	837.55	833.85				

		100 yr Storm Event					
Label	Flow	Velocity	Depth	Hydraulic			
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)			
B5-A	9.31	11.01	1.63	833.7			
B5-B	5.29	3	1.68	834.2			
B5-C	5.36	9.49	1.64	837.61			
B5-D	5.38	8.76	0.59	838.84			
B5-E	5.39	6.18	1.02	838.97			
B5.02	4.26	20.2	1.68	837.7			



Hydraulic
Grade Line (Out) (ft)
 832.83
 834.2
 834.2
 837.31
 838.97
834.2

NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

LEGEND	
W O WW O SD O SD SQ SQ <t< td=""><td>WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE SINGLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE</td></t<>	WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE SINGLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE
#01 925:925 9100:9100	INLET # / CAPTURE Q= 25/100 YEAR

	Ρ	ROFIL	E SC	ALES:				
	1" 1" P	= 40' = 4' \ ROFIL	HORIZO	NTAL GEND:			S Е С	0
	NA	TURAL G	ROUND	······································	· · · · · · · · · · · · · · · · · · ·		A	ζ
	FIN	ISHED G	RADE					Ĺ
	SU	BGRADE						Ĺ
	PR	OPOSED	STORM DI	RAIN				L L
	25	-YR HGL	25	övr HGL				ļ
	100	0-YR HG	L /r HGL	100	yr HGL	_		-
<u></u>	_		• •)
	· · ·		CUR	VE TABLE	·			
CUR	RVE #	RADIUS	DELTA	CHORD BEAR	RING CHORD	LENGTH	I Ш I ()
	C10	295.00'	026'54'34"	N8312'48"E	137.28	138.55'		
			F					

City of Leander	APPROVED	
	pmg	
CITY OF LE	EANDER APPROVA	L

111100 × 91805 FNS 110000 09/21/2024 an Looss -AS Z 0 APE-DAWS

PA Z Z

STORMDRAIN PLAN & PROFILE LINE SD-B5.01 & LATERAL B5.02 -

CITY NO. PICP-24-0120 JOB NO. 50816-25 DATE SEPTEMBER 2024 DESIGNER RBB CHECKED_TCK_DRAWN_ADS_ SHEET 47 of 83



~

BLOCK MM BLOCK MM 21 =STA: 8+ 22 SD-B6.09" CR FUTURE SD-B6.09" STRUCTION B6.09" W-3A" STA: 6+59.64 "SD STRUCTION B6.09" W-3A" STA: 6+59.64 "SD STRUCTION B6.09" STA: 6+59.64 "SD STRUCTION B6.09" STA: 6+59.64 "SD STRUCTION B6.09" STA: 6+59.64 "SD STRUCTION B6.09" STA: 6+59.64 "SD STRUCTION B6.09" STA: 6+59.64 "SD STRUCTION B6.09" STA: 6+59.64 "SD STRUCTION STA: 6+59.64 "SD STA: 6+59.64 "SD	STA: 0+28.28 "SD-B6.07" CAP STUB FOR FUTURE 10' CURB INLET "B6.07" END CONSTRUCTION STA: 0+14.14 "SD-B6.07" 50.15 (FUTURE) "WW-3A" : 6+99.59 "SD-B6.01" 0+00.00 "SD-B6.07" -B6.01" • PT	18 16 STA: 8+44 = STA: 0+00 8' x 6' JUNCT 8' x 8' 8' x 8' 820 7 6' JUNCT 8' x 8' 820 7 8' x 8' 820 7 8' x 8' 8 8' x 8' 8 <tr< th=""><th>4.95 "SD-B6.01" 0.00 "SD-B7.01" TION BOX #B6-C</th><th>A HUODI - +ISYILIY 14 14 14 14 14 14 14 14 14 14</th><th>13 11 13 11 0 0 0 0 0 0 0 0 0 0 0 0 0</th><th></th></tr<>	4.95 "SD-B6.01" 0.00 "SD-B7.01" TION BOX #B6-C	A HUODI - +ISYILIY 14 14 14 14 14 14 14 14 14 14	13 11 13 11 0 0 0 0 0 0 0 0 0 0 0 0 0	
1		TO BE PART OF FUTU	IN PHASE 5. RE PHASE 6 Label FI	25 ow Velocity Dep	yr Storm Event oth Hydraulic	Hydraulic
		25' OFFSITE DRAINAGE E	ASEMENT B6-A 14	:fs) (ft/s) (Out) 0.18 10.2 2.7 1.00 10.21 2.7	(ft) Grade Line (In) (ft) 77 815.79 815 79	Grade Line (Out) (ft) 815.84
STA: 0+13.98 " CAP STUB FOR	SD-B6.10"	0x 02 22	X B6-C 14 B6-C 14 B6-D 14	1.99 10.24 2.7 2.37 9.26 3.3 0.03 10.36 3.5	3 816.55 1 817.52 2 817.95	815.88 817.52 917.99
10' CURB INLET END CONSTRUCT	"B6.10" <u>10N</u> / 7		B6-E 13 B6-F 13	5.81 10.27 3.6 3.77 10.23 3.4	817.85 63 818.11 18 818.25	818.17 818.42
820 STA: 5+49.48 "SD- =STA: 0+00.00 "SI	-B6.01" D-B6.10"	STA: 7+31.40 "SD-BO 18" TEMPORARY SLOP	6.01" ING HEADWALL B6-G 12 B6-H 12	5.0810.043.34.310.023.7	11 818.8 75 819.29	818.81 819.34
STA: 0+13.98 "SD-B6.11" CAP STUB FOR FUTURE 20		TA: 0+14.14 "SD-B6.08" UTURE 10' CURB INLET "B6.08"	B6-I 12 B6-J 12	4.4110.023.21.79.963.4	3 819.27 1 819.52	819.29 819.53
10' CURB INLET "B6.11" END CONSTRUCTION			B6-K 12 B6-L 12	0.33 9.93 3.4 0.88 11.2 3.1	819.69 1 819.47	819.73 819.69
6.12" RE	STA: 6 =STA: 6	6+72.95 "SD-B6.01" 0+00.00 "SD-B6.08") yr Storm Event	······································
·B6.12"				ow Velocity Dep ifs) (ft/s) (Out)	(ft) Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
			BG-R 20 B6-B 20 B6-C 20	4.36 11.38 3.0 6.67 11.41 3.1 7.25 8.64 4.2	3 810.13 3 817.21 2 818.58	816.28
		24	B6-D 20 B6-E 19	3.98 8.5 4.5 8.02 8.25 4.8	819.04 819.64	818.89 819.36
			B6-F 19 B6-G 18	5.358.144.92.77.615.1	8 820.31 .6 820.71	819.93 820.66
+			B6-H 18 B6-I 18	1.97.585.82.17.595.6	8 821.67 1 821.7	821.39 821.67
			B6-J 17 B6-K 17	8.22 7.43 5.8 6.49 7.35 6	<u>3 822.03</u> 822.44	821.96 822.26
				1.1 1.4 5.8 No: 11 FX	<u>5 822.66</u>	822.44
285.64 LF 6' × 4' BOX			280.7 LF 6' x 4' BOX			
					712	
			· · · · · · · · · · · · · · · · · · ·		8 8	832
					817.07 H-5F" FL 80	832
					I" FL 817.07 C) "WW-5F" FL 80	832 830 828
Image: Section of the section of th					-B6.01" FL 817.07 XISTING) "WW-5F" FL 80	832 830 828
					85 "SD-B6.01" FL 817.07 85 "SD-B6.01" FL 817.07 0.00 (EXISTING) "WW-5F" FL 80	832 830 828 826
					84-3495 "SD-B6.01" FL 817.07 64-3495 "SD-B6.01" FL 817.07 64-3495 "SD-B6.01" FL 817.07 64 64 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	832 830 828 828 826 826 824
				H04	1000000000000000000000000000000000000	832 830 828 826 826 824 824 822
					P 2774. 84-34 95 "SD-B6.01" FL 817.07 274. 04.00.00 (EXISTING) "WW-5F" FL 80 274. 04.00 (EXISTING)	832 830 828 826 826 824 824 822 822
				H0+ 105+ H	HGL HGL HGL HGL HGL HGL HGL HGL HGL HGL	832 830 828 826 826 824 822 822 820
		2000r AG		25yr	HGL PUTURE BG-M* 0.70%	832 830 828 826 824 824 822 822 820 818
		"B6-H" @ 0.50% "В6-	-l [*] "B6J" "B6-K" ● 0.5	25yr 30% "B6-L" (HGL 0.70%	832 830 828 826 824 824 822 822 820 818 818 818
		"B6-H" @ 0.50% "В6-	1000 Het 1000	HGL	HGL 000 000 000 000 000 000 000 000 000 0	832 830 828 828 826 824 822 822 820 818 818 818 816 814
			1009- Met 1009- Met	HO2 HO2 DO3 BG-L" C	HGL 000 1000 1000 1000 1000 1000 1000 100	832 830 828 828 826 824 822 820 818 818 816 814 814 812
		"B6-H" @ 0.50% "B6-	100, Ma 100, Ma 10	25yr	HGL 900 HGL 9000 HGL 900 HGL 900 HGL 900 HGL 900 HGL 900 HGL 900 HG	832 830 828 826 824 824 822 820 818 818 818 816 814 814 812
		на советски странации и советски советски советски советски советски советски советски советски советски советс и советски советс в советски сове в советски со в советски советс	-1° "B6J" "B6K" ● 0.5		HGL	832 830 828 826 824 822 822 820 818 818 816 816 814 812 812 810
		ВС-Н" @ 0.50% "ВС- "ВС-Н" @ 0.50% "ВС- "ВС-И" "ВС-И" "ВС- "ВС-И" "ВС-И" "ВС- "ВС-И" "ВС-И" "ВС- "ВС-И" "ВС-И" "ВС- "ВС-И" "ВС-И" "ВС- "ВС-И" "ВС-И" "ВС- "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-"ВС-"ВС-" "ВС-""""""""""	" " " " " " " " " " " " " "		HGL 60 HGL 61 HGL 61 HGL 61 HGL 70% HGL 70%	832 830 828 828 826 824 822 822 820 818 818 818 818 816 814 814 812 810
Index Index <t< td=""><td>0.50% 100x 80x 100x 80x</td><td>ці </td><td>1000 1000</td><td>HON HOOMER HOOME</td><td>HGL</td><td>832 830 828 828 826 824 822 820 818 818 818 816 814 814 812 810 812 810 810</td></t<>	0.50% 100x 80x 100x 80x	ці 	1000 1000	HON HOOMER HOOME	HGL	832 830 828 828 826 824 822 820 818 818 818 816 814 814 812 810 812 810 810
Image: 100 million Image: 100 million Image: 100 mil	Be di "Fil. (m) Bi5.55 Bio. 01" Fil. (m) Bi5.51 1000 Box #B6 0. "Syb-#6.01" Bis.01 Bis.01" Bis.01" Bis.01" Bis.55 Bis	B6 -H" ● 0.50% "B6- "B6 - "B6 -	0000 "50-186.08" B6.01" FL ((n)) 816.13 B6.01" FL ((n)) 816.13 B6.01" FL ((n)) 816.13 B6.01" FL ((n)) 818.13 B6.01" FL ((n)) 816.26 B16.07"	25yr 25yr	HGL	832 830 828 828 826 824 822 820 818 818 818 818 818 818 818 818 818 81
$ \begin{array}{c} & & & & & & & & & & & & & & & & & & &$	0.202 	"B6-H"	· * * * * * * * * * * * * * * * * * * *		HGL	832 830 830 828 828 826 824 822 820 818 818 818 816 814 812 810 808 808 808 806 804
100 1	STA: 5+49.48 "SD-B6.01" = STA: 0+00.00 "SD-B6.01" = STA: 0+00.00 "SD-B6.10" 72" "SD-B6.01" FL (n) 815.51 72" "SD-B6.01" FL (n) 815.51 72" "SD-B6.01" FL (n) 815.51 72" "SD-B6.01" FL (n) 815.51 72" "SD-B6.01" FL (n) 815.51 86" × 4" "SD-B6.01" FL (n) 815.58 60" FL (n) 815.58 88" × 6" "D-B6.01" FL (n) 815.58 60" FL (n) 815.58 88" × 6" "SD-B6.01" FL (n) 815.58 60" FL (n) 815.58 80" × 4" "SD-B6.01" FL (n) 815.58 60" FL (n) 815.58 80" × 4" "SD-B6.01" FL (n) 815.58 81" × 4" "SD-B6.01" FL (n) 81" × 4" "SD-B6.01" FL (n) 81" * 8"	X × X, 20 B6.00° BC-H* ● 0.50% BC-H* ● 0.50% B	6 ° × 4 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	25yr 25yr 30% "B6−L" (25yr 30% "B6−L" (25yr 30% "B6−L" (30% "B6+L")	HGL	832 830 830 828 828 826 824 822 820 818 818 818 816 812 810 810 808 808 808 804 802
100x	STA: 5+49.48 "SD-B6.01" = STA: 5+49.48 "SD-B6.01" = STA: 5+49.48 "SD-B6.01" = STA: 55-B6.01" "I. 72" "SD-B6.01" "I. (out) 172" "SD-B6.01" "I. (in) 172" "SD-B6.01" "I. (in) 172" "SD-B6.01" "I. (in) 18" "SD-B6.01" "I. (in) 18" "SD-B6.01" "I. (in) 8" X 6" JUNCTION BOX #B6-B "MARCHINAN BOS 6" * "SD-B6.01" "I. 8" X 6" JUNCTION BOX #B6-B "MARCHINAN BOS 6" * "SD-B6.01" "I. 6" * "SD-B6.01" "MARCHINAN BOS	× X, 2000 × 1/4 *B6 -H [*] ● 0.50% *B6- *B6 -H [*] ● 0.50% *B6- 1.000 × 1/4 9000 × 1/4 1.000 × 1/4 1.0000 × 1/4 1.0000 × 1/4 1.0000 × 1/4 1.0000 × 1/4 1.0000 × 1/4	= 517: 0+0000 50 - 86.08" = 517: 0+0000 50 - 86.08" = 517: 0+0000 50 - 86.08" = 517: 0+0000 50 - 86.01" Fl. (n) 816.13 = 517: 0+0000 *50 - 86.01" = 517: 0+00000 *50 - 86.01" = 516: 0* * * * * * * * * * * * * * * * * * *	H04 H04 H04 H06 H04 H06 50% "B6-1" 60% "B6-1" 70% "B6-1" 70% "B6-1" 70% "B6-1" 70% "B6-1"	08 1 1 1 <td< td=""><td>832 830 828 828 826 824 822 820 818 816 814 812 810 812 808 808 808 808 808 808 808 808 808 808 808 808 808 808 808 808 802</td></td<>	832 830 828 828 826 824 822 820 818 816 814 812 810 812 808 808 808 808 808 808 808 808 808 808 808 808 808 808 808 808 802
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	B17.90 S17.55 *\$0-86.01* = STA: 0+00.00 "Sp-86.10" = STA: 0+00.00 "Sp-86.10" T2" "S0-86.01" FL (ni) 815.51 72" "S0-86.01" FL (ni) 815.51 72" "S0-86.01" FL (ni) 815.51 317.90 STA: 5+64.25 "\$0-86.01" STA: 5+64.25 "	2' × 2' "50-86.00" F1 (ir) 817.58 2' × 2' "50-86.00" F1 (ir) 817.58 =	319.49 6' × 4' * * * * * * * * * * * * * * * * * *	HOR 25yr HOR 25yr SO "B6-L" GO	319.64 319.6	832 830 828 828 826 824 822 820 818 818 816 814 812 810 812 810 812 810 812 810 812 808 812 808 808 808 808 808 808 808 80

	Hydrauli
)	Grade Line (O
	815.84
	815.84 815.88
	815.84 815.88 817.52
	815.84 815.88 817.52 817.88
	815.84 815.88 817.52 817.88 818.17
	815.84 815.88 817.52 817.88 818.17 818.42
	815.84 815.88 817.52 817.88 818.17 818.42 818.81

		834
		832
		830
		828
		826
		824
		822
UTURE		820
'B6-M"		818
	-	816
		814
	10 Konstanti (140	812
•		810
-C t) 817.1 818.14 817.14		808
80X #86 전 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		806
ACTION E - B6.01 - B6.01 - B6.01		804
× × × × × × × × × × × × × × × × × × ×		802
819.42	818.35	



NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.



CURVE	#	RADIUS	DELTA	CHORD BEARING	CHORD	LENGTH
C11		420.00'	051*58'48"	N4417'19"E	368.10'	381.03'



1	T	O I	TI IT	1.1.1	1 11	T T.	1

Z Parinter DUSTIN J. GOSS 91805 CENSE (10000) 09/21/2024 22000 All mars Z 0 WS - ¥ d L PE-D/ 200 BPL STE — **ຕ**໌ 50 PA S , PHASE R, TEXAS PROFILE STORMDRAIN PLAN & LINE SD-B6.01 LIVELY TRACT, F CITY NO. _____PICP-24-0120 JOB NO. 50816-25

DATE SEPTEMBER 2024

CHECKED_TCK_DRAWN_ADS_

SHEET 48 of 83

RBB

DESIGNER



v



- 830

826

-1814

-1810

808

- 806

-1804



				and the second			
	25 yr Storm Event						
Labol	Flow	Velocity	Depth	Hydraulic	Hydraulic		
Laver	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)		
B6.07	2.3	4.18	0.97	819.72	819.73		
B6.08	3.46	4.6	0.91	819.52	819.53		
B6.09	1.88	6.35	1.75	819.33	819.34		
B6.10	10.84	6.13	1.26	819.49	819.27		
B6.11	3.68	12.72	0.98	819.46	818.42		
B6.12	5.38	17.02	1.13	820.1	818.17		
B6.13	3.32	12.16	1.03	820.12	817.88		

100 yr Storm Event						
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic	
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)	
B6.07	3.39	1.92	3.5	822.28	822.26	
B6.08	5.16	2.92	3.33	821.99	821.96	
B6.09	2.78	0.89	3.8	821.39	821.39	
B6.10	16.15	9.14	2.66	820.95	820.66	
B6.11	5.49	14.28	2.48	819.89	819.93	
B6.12	8.01	19.08	2.32	820.31	819.36	
B6.13	4.88	13.61	2.04	820.27	818.89	

NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

PROFILE SCALES:	
1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND:	
NATURAL GROUND	
FINISHED GRADE	
SUBGRADE	· · · · · · · · · · · · · · · · · · ·
PROPOSED STORM DRAIN	
8	
25-YR HGL25yr HGL	

100-YR HGL

00vr HGL----







-

* 2

ESHEET	³¹ 53) ; ; ;	
3 3 3 3 3 3 3 3 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5	B7.01"	SCALE: 1"= 40' 0' 40' 80' 120'
STA: 0+10.11 "SD- 15' CURB INLET "B7 END CONSTRUCTION	-5F" B7.03"	NOTES: 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND
: 7+83.22 SD-B7. STA: 0+00.00 SD-E STA: 0+00.00 SD-E (4' JUNCTION BOX	01" 37.03" 38.01" #B7-C	AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES. 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION LINESS SHOWN OTHERWISE
Event Hydraulic Grade Line (In) (ft) 823.43 823.61 823.91	Hydraulic Grade Line (Out) (ft) 823.37 823.59 823.77	 4. EXISTING CONTOUR INFORMATION SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.
823.93 824.16 824.6 824.68 825.61 826.2 827.31	823.91 824.09 824.22 824.6 825.18 826.06 826.2	W WATER LINE WW WASTEWATER LINE & MH WASTEWATER LINE & MH CURB INLET
827.54 829.34 830.52 832.04 832.48 834.85	826.2 826.89 828.75 830.39 831.09 832.04 833.05	DOUBLE WATER SERVICE DOUBLE WATER SERVICE SINGLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE
844 RCF		EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE CONTOUR LINE PROPOSED CONTOUR LINE
842 840 838		$\frac{\#01}{\substack{q_{28}: q_{25} \\ q_{100}: q_{100}}}$ INLET # / CAPTURE Q= 25/100 YEAR $\frac{PROFILE SCALES:}{1" = 40' HORIZONTAL}$
		1" = 4' VERTICAL PROFILE LEGEND:
		SUBGRADE PROPOSED STORM DRAIN
HOTHER 828 826 826 824		25–YR HGL 25yr HGL 100–YR HGL 100yr HGL 100yr HGL
00.9 57 822 820		CURVE TABLE CURVE # RADIUS DELTA CHORD BEARING CHORD LENGTH C12 295.00' 022'33'55" S31'00'14"E 115.43' 116.18' C13 305.00' 018'55'39" S32'49'23"E 100.30' 100.76'
818 816 814		
812		Statuter APPROVED
837.39 837.39		CITY OF LEANDER APPROVAL
		PICP-24-0120





÷ .

2





	-		25 yr Storm Event			
Labol	Flow	Velocity	Depth	Hydrau		
Laber	(cfs)	(ft/s)	(Out) (ft)	Grade Line (
B7-S	5.1	6.15	1.12	835.18		
B7-T	5.19	6.19	0.62	836.52		
B7-U	5.2	5.48	0.91	836.62		
B7.02	4.69	6.98	0.67	835.69		
B7.03	10.1	14.96	1.58	835.55		
B7.04	3.75	12.05	1.5	832.07		

	100 yr Storm Event						
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic		
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)		
B7-S	7.62	2.43	2.28	836.46	836.44		
B7-T	7.74	6.91	2.07	836.71	836.46		
B7-U	7.75	6.12	1.12	836.81	836.85		
B7.02	6.98	3.95	1.78	836.49	836.44		
B7.03	15.04	8.51	2.28	836.12	835.94		
B7.04	5.56	3.15	2.83	833.09	833.05		



THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

LEGEND	
→ W → SD − 786	WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE SINGLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE PROPOSED CONTOUR LINE
#01 q ₂₈ : q25 q ₁₀₀ : q100	INLET # / CAPTURE Q= 25/100 YEAR
PROFILE SCA	ALES:

120'

1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND:	
NATURAL GROUND	 ·
FINISHED GRADE	
SUBGRADE	
PROPOSED STORM DRAIN	

PROPOSED STORN	A DRAIN	
8		
25-YR HGL	—25yr HGL	
100-YR HGL 100yr HGL	48-14-14-16-14-14-14-14-14-14-14-14-14-14-14-14-14-	-100yr HGL

CURVE TABLE						
CURVE #	JRVE # RADIUS DELTA CHORD BEARING CHORD LENGTH					
C14	295.00'	025*55'07*	N79"36'00"E	132.31'	133.45'	



PE-DAWSON GINEERS	10 I HOUSTON I FORT WORTH I DALLAS DG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711 N #470 I TBPLS FIRM REGISTRATION #10028801	
LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS	STORMDRAIN PLAN & PROFILE 10801 N MOPAG EXPY, BLD LINE SD-B7.01 (2 OF 2) & LATERALS B7.02-B7.04 TBPE FIRM REGISTRATION	

CHECKED_TCK_DRAWN_ADS_

SHEET 51 of 83

PICP-24-0120

Hydraulic e (In) (ft) Grade Line (Out) (ft) 18 835.27 835.01 836.63 835.32 835.25 831.72



-

-

834	14.14	LF 18" RCP	834	834	28.	28 LF 18" RCP	834
		GRAD					
832		SIHED SIHED	832	832			832
830	FUTURE-		830	830			830
828	GRADE		828	828		ATUR ATUR	828
020	SELECT			020	FINISHED GRADE		ULU ULU
826	100 YR HGL		826	826	SELECT-FILL		826
824	25 YR HGL-		824	824	100 YR HGL	A Statement	824
		₿7.07" Ф 5.78%				-	
822			822	822			822
820			820	820	· ·	"B7.08"	820
818			818	818			818
816			816	816			816
014			014	014	adara dalahan judi di sebahan arangka mang dalam dal a dalam dara jugi kamalah di kapanangka di papangga judi p		
814			814	814			814
812		<u> </u>	812	812		8	812
<u>8</u> 10		ET 87	810	810			010
010			010			N	010
808		7" 21.26 3.76 3.76 24.57 CURI	808	808	8* 19.74	9.74 2.24 CURE CURE	808
806	5	-B7.0 ut) 8 1) 82 1) 82 10 10 10	806	806	.01") 815) 825 (08° (10' E 10'	806
000		C 다 다 다 더 이 다 단정 이 이 이 이 이 이 이 이 이 이 이 이 이 이 이 이 이 이 이			50-87 SD-87		500
804	°,	00.00 7.01 7.07 7.07 7.07 7.07 7.07	804	804	7.01*	7.01 7.08 7.08 7.08	804
802	2+1 2	+ 0 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1	802	802	2+49 	SD-B7 SD-B7 SD-B7 SD-B7 SD-B7 SONST	802
	SIA	END END END END END END			81 STA: 8 STA: 8 ST/	END 0.0	
				[
SD-B7.07	5.61			SD-B7.08	4.57	5.19	
	82				80	82	
·····	0+	-00 0+	75	L	0+	-00	0+75
	14 14				00	09 15 10" DOD	
834			834	834			834
832			832	832			832
830		Щ	830	830	- 	<u> </u>	830
828		GRAD	828	828		GRA	828
826	FUTURE		826	826	FUTURE-		826
824	GRADE		824	824	GRADE		824
. · · ·	100 YR HGL				100 YR HGL		
822	FILL 25 YR HGL		822	822	SELECT FILL	All and a second second	822
820			820	820	25 YR HGL	0.91%	820
		☐"B7.11"	010		UNUUNU		
818	7		010	818			818
816			816	816			816
041			814	04 /			044
014	en nation million à la recomme caractéricade en manufacture montant en citar comma avant			014		N	014
812		1	812	812	· · · · · · · · · · · · · · · · · · ·	10 309.2	812
810			810	810	**********		
	7.38 38 38				32 32 82		
808	t) 817. 817. 819.8	220.01 CUR	808	808	12" (1) 81 819	EI	808
806		7.11 **	806	806	(in)	712" 712" 711NG) 8F 10' 8F 10'	806
	0 "SD-B 0 "SD 01" F 11" F				0 "SD-E 0 "SD-E 12" F		NOL
804	9.50 100.00 0-87.0 0-87.0 0-87.0	7.11 [*]	804	804 -	8.50 1 - 87 1 - 87 1 - 87 1 - 87 1 - 87	.15 ": 75.50 3.28 7.12" FOR	804
802	<u>+ 7 4 4</u> + 7 7 4 4		802	802 -	* * <u>*</u> 0 <u>* * * 0</u>	STUB STUB STUB	SNO 802
	18" × × SI 18" × × SI	END END		-	ع × × ۲۵ ۵۳ × × ۲۵ ۵۳ × × ۲۵	STA: STA: STA: 18" ;	EB
					~		
SD-B7.11	20.25			SD-B7.12	20.06	20.50	
	8				8	8	
	0+	00 0+7	75	l	. 0+	00	0+75

Lak B7. B7. B7. B7.0 B7. B7. B7. B7.

Lab B7.0 B7.(B7.(B7.(B7.0

B7.1 B7.1 B7.1

			25 yr Sto	orm Event	
	Flow	Velocity	Depth	Hydraulic	Hydraulic
bei	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
.05	6.4	9.43	1.84	829.15	829.28
.06	2.68	8.39	1.95	829.61	829.61
.07	3.63	10.74	0.95	825.3	824.71
.08	4.03	7.91	1.05	823.65	823.29
.09	3.5	7.26	0.55	821.64	821.28
.10	6.03	6.29	0.82	821.66	821.26
.11	4.13	6.67	0.92	820.85	820.79
.12	3.01	5.25	0.85	820.73	820.67

	·		100 yr Sto	orm Event	
bel	Flow	Velocity	Depth	Hydraulic	Hydraulic
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
05	9.51	5.38	2.94	830.58	830.39
06	3.99	2.26	3.43	831.11	831.09
07	5.41	3.06	2.3	826.09	826.06
08	6	3.4	2.94	825.26	825.18
09	5.2	2.94	3.5	824.24	824.22
10	8.98	5.08	3.65	824.27	824.09
11	6.13	3.47	3.89	823.81	823.77
12	4.47	2.53	3.78	823.64	823.59

NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

PROFILE SCALES:
1" = 40' HORIZONTAL
PROFILE LEGEND:
NATURAL GROUND
FINISHED GRADE
SUBGRADE
PROPOSED STORM DRAIN
25-YR HGL25yr HGL
100-YR HGL 100yr HGL

<u>Lednder</u>	APPROVED
	RMG
7 - Lighter 1	

STORMDRAIN PLAN & PROFILE	EXAS
NE SD-B7.01 LATERALS B7.05-B7.12 TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801	POFILE AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10801 N MOPAC EXPY, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711 37.05-B7.12 TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801

CITY NO. PICP-24-0120 JOB NO. 50816-25 DATE SEPTEMBER 2024 DESIGNER RBB

CHECKED_TCK_DRAWN_ADS_

_{SHEET} 52 of 83


С С



25 yr Storm Event						
Label	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Grade Line (In) (ft)		
B8-A	9.67	8.94	1.58	835.73		
B8-B	5.79	7.87	1.71	837.14		
B8-C	5.79	7.61	1.07	837.36		
B8.02	4.11	2.33	1.71	836.26		

		rm Event		
Label	Flow (cfs)	Velocity (ft/s)	Depth (Out) (ft)	Hydraulic Grade Line (In) (ft)
B8-A	14.3	8.09	2.28	836.75
B8-B	8.6	4.87	2.96	838.06
B8-C	8.63	4.88	1.97	838.27
B8.02	6.12	3.47	2.96	837.53



Hydraulic	
Grade Line (Out) (ft)	
835.25	
835.24	
836.24	
······································	
Hydraulic	
Grade Line (Out) (ft)	
835.94	
837.49	
838.18	
	NOTES
	1. THE LOCATIONS OF EXISTING LINDERGROUND LITUTES
	ARE SHOWN IN AN APPROXIMATE WAY ONLY AND
	OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR
	EXISTING UTILITIES BEFORE COMMENCING WORK, AND
	AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE
	CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERCROUND LITUTES
	2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED.
	3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH
	CALCULATION UNLESS SHOWN OTHERWISE.
	4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT
	INTERVALS THEY ARE COMPUTER GENERATED USING
	5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR
	TO UTILITY INSTALLATION.
	LEGEND
	STORM DRAIN LINE & MH
	SINGLE WW SERVICE
	FIRE HYDRANT
	EXISTING GATE VALVE
	#01 INLET # / CAPTURE
	$Q_{28}: Q25 Q= 25/100 \text{TEAR}$ $Q_{100}: Q100$
	PROFILE SCALES:
	$1^{"} = 40^{'} \text{HORIZONTAL}$
	PROFILE LEGEND
	NATURAL GROUND
	FINISHED GRADE
	SUBGRADE
	PROPOSED STORM DRAIN
	<u>v </u>
	25-YR HGL 25vr HGI-
	100-YR HGL
	100yr HGL



PICP-24-0120

CITY OF LEANDER APPROVAL

APPROVED

pmg



			25 yr Sto	orm Event	
Inhol	Flow	Velocity	Depth	Hydraulic	Hydraulic
Lapei	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft
B12-A	25.58	3.62	3.85	815.88	815.84
B12-B	25.75	3.64	3.67	816.01	815.95
B12-C	21.06	4.29	2.85	816.21	816.15
B12-D	21.0 9	11.32	2.62	816.2	816.21
B12-E	21.13	11.33	2.24	816.73	816.33
B12-F	19.75	11.12	1.96	817.5	817.13
B12-G	17.86	10.82	1.91	817.72	817.91
B12-H	17.88	14.28	0.87	819.29	817.16
B12-I	14.34	13.41	1.86	824.12	819.72
B12-J	11.25	12.5	1.28	824.71	824.12
В12-К	11.3	12.52	1.17	829.98	824.75
B12-L	9.81	7.88	0.93	830.67	830.28
B12-M	9.9	7.9	1.17	831.92	830.72
B12-N	7.87	7.42	1.47	832.12	832.26
B12-0	7.89	7.42	1.17	832.3	832.24
B12-P	4.86	6.49	1	833.67	832.3
	· · · ·	i in constantin	· ·		······································
	· · · · · · · · · · · · · · · · · · ·		100 yr Sto	orm Event	
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft

		(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
	B12-A	38.29	5.42	4.11	816.18	816.1
	B12-B	38.45	5.44	4.07	816.49	816.34
	B12-C	31.4	6.4	3.49	816.93	816.79
	B12-D	31.46	6.41	3.34	817.07	816.93
	B12-E	31.53	12.57	3.2	817.55	817.29
	B12-F	29.47	12.36	2.62	817.85	817.79
	B12-G	26.65	12.04	2.38	818.28	818.38
	B12-H	26.68	15.97	1.99	819.62	818.28
	B12-I	21.39	15.02	2.34	824.41	820.19
	B12-J	16.78	14.03	1.57	824.97	824.41
	B12-K	16.86	14.04	1.44	830.24	825.03
. · ·	B12-L	14.61	8.73	1.17	830.93	830.52
~	B12-M	14.72	8.74	1.44	832.18	830.99
	B12-N	11.71	8.25	1.83	832.59	832.63
	B12-0	11.73	8.25	1.63	832.53	832.71
	B12-P	7 24	7 25	1 57	833.85	837.88

NOTES:

- 3'

 $\overline{}$

836

 \sim

5

9+00

SiO 3

тш ^{- 1}832

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND
- PRESERVE ANY AND ALL UNDERGROUND UTILITIES. 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED.
- 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

LEGEND		
W WW SD SD WW SD WW SD WW SD WW SD WW SD WW SD T86	WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE SINGLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE PROPOSED CONTOUR LINE	TRACT, PHASE 5
#01 925: 925	INLET # / CAPTURE Q= 25/100 YEAR	

		830	>	DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE	CT, P NDER, T PLAN & F 2.01 (1 0
		- 826		EXISTING WATER LINE EXISTING WATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE PROPOSED CONTOUR LINE	FRA AIN F SD-B1
	AM -	824		#01 INLET # / CAPTURE	
	-0	822		g_{00} : Q100	
	3+75	820	PROFILE SCALES:		ST ST
	LA: 8	- 818	1" = 40' HORIZONTAL 1" = 4' VERTICAL		
	-'v 	816	NATURAL GROUND		
		814	FINISHED GRADE		
		812	SUBGRADE	12 dailer APPROVED	CITY NO. <u>PICP-24-0120</u> JOB NO. 50816-25
 	2			pmg	DATE SEPTEMBER 2024 DESIGNER RBB
832.4	832.7		25-YR HGL 25yr HGL 100-YR HGL	-	CHECKED_TCK_DRAWN_ADS
	9+	_ ⊦00	100yr HGL	· CITY OF LEANDER APPROVAL	SHEET 54 OT 83

PICP-24-0120

10000 09/21/2024 m las WS PAPE-DAV ENGINEEI

0

Ш

PROFIL OF 2)

00011111

 \bigstar

ISTIN J. GOS

9180





	·							
	25 yr Storm Event							
Labal	Flow	Velocity	Depth	Hydraulic	Hydraulic			
Laper	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)			
B12-P	4.86	6.49	1	833.67	832.3			
B12-Q	4.9	6.5	0.58	834.36	833.48			
B12-R	4.91	6.11	0.88	834.53	834.47			
B12.02	3.53	8.9	0.45	833.32	832.26			
B12.03	2.43	11.02	0.97	832.92	832.26			
B12.04	3.66	5.74	0.61	830.78	830.46			

100 yr Storm Event						
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic	
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)	
B12-P	7.24	7.25	1.57	833.85	832.88	
B12-Q	7.28	7.27	0.73	834.54	833.63	
B12-R	7.3	6.83	1.09	834.71	834.67	
B12.02	5.26	9.96	1.08	833.49	832.88	
B12.03	3.61	12.38	1.33	833.05	832.63	
B12.04	5.48	6.38	0.77	830.95	830.62	

	DATE	
	VOISION	
SCALE: 1"= 40' 0' 40' 80' 120'	40. REV	
NOTES	STATE OF	TETAS
INCITES. 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES. 2 ALL RCP IS CLASS III UNLESS OTHERWISE NOTED	DUSTIN J. G 91805 SS/ONAL	OSS
 ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION. 	wson RS	T WORTH I DALLAS TX 78759 I 512.454.8711 GISTRATION #10028801
W WATER LINE WW WASTEWATER LINE & MH SO STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE DOUBLE WATER SERVICE DOUBLE WW SERVICE SINGLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WATER LINE WW EXISTING STORM DRAIN LINE PROPOSED CONTOUR LINE PROPOSED CONTOUR LINE	FAPE-DA ENGINEE	AUSTIN I SAN ANTONIO I HOUSTON I FOR 10801 N MOPAC EXPY, BLDG 3, STE 200 I AUSTIN, TBPE FIRM REGISTRATION #470 I TBPLS FIRM RE
#01 INLET # / CAPTURE Q= 25/100 YEAR Q= 25/100 YEAR 1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND: NATURAL GROUND FINISHED GRADE	HASE 5 TEXAS	PROFILE ALS B12.02-B12.04
SUBGRADE PROPOSED STORM DRAIN 25-YR HGL 25yr HGL	RACT, P	AIN PLAN & = 2) & LATEF
IUU-TK HGL 100yr HGL	LIVELY T CITY OF	STORMDR INE SD-B12.01 (2 OF
Stater APPROVED	CITY NO. PICP-	24-0120



1 L

ц.,



	25 yr Storm Event						
Label	Flow	Velocity	Depth	Hydraulic			
Laper	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)			
B12.05A	4.75	8.79	0.6	825.07			
B12.05B	4.75	8.79	0.87	825.44			
B12.06A	5.6	6.73	0.79	819.87			
B12.06B	5.61	6.73	0.95	820.03			
B12.07	2.96	5.77	0.91	817.82			
B12.08	2.22	4.95	0.96	817.06			
B12.09	7.47	8.53	2.35	816.17			

	100 yr Storm Event						
Label	Flow	Velocity	Depth	Hydraulic			
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)			
B12.05A	7.06	9.79	0.76	825.26			
B12.05B	7.07	9.8	1.08	825.63			
B12.06A	8.33	7.39	1.34	820.16			
B12.06B	8.35	7.4	1.25	820.24			
B12.07	4.41	6.44	1.38	818.38			
B12.08	3.28	5.52	1.62	817.81			
B12.09	11.16	3.55	2.99	816.84			

		DAT
		X
		South 1
		STATE OF TETTS
	NOTES:	DUSTIN J. GOSS
	1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE	CENSE SOLONIN ENG
	OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND	09/21/2024 92 09/21/2024
	AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND	
	2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR	
	EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON	AS 711 801
	THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.	D I DALL 512.454.8 4 #10028
	5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.	VORTH VORTH VORTH TRATION
		FORT V IIN, TX 7 A REGIS
	PROFILE SCALES:	DO I AUS PLS FIR
	1" = 40' HORIZONTAL 1" = 4' VERTICAL	NO I TB
	PROFILE LEGEND:	NG NID I ONID I DIAG
	NATURAL GROUND	AN ANT
		IN I S N MOP
	PROPOSED STORM DRAIN	AUST AUST TBPE
	6	
	25-YR HGL 25yr HGL 100-YR HGL	
	100yr HGL100yr HGL	
		60
Hydraulic Grade Line (Out) (ft)		2
824.44 825.1		S-B 5-B
819.65 819.91		
817.91 817.13 916.15		
		ALSS T
Hydraulic Grade Line (Out) (ft)		ON JE
824.6 825.31		
820.19 820.21		
818.38 817.79		
816.79		
	APPROVED	CITY NO. <u>PICP-24-0120</u> JOB NO. <u>50816-25</u>
	Rma	DATE <u>SEPTEMBER 2024</u> DESIGNER RBB
		CHECKED TCK DRAWN ADS
	CITY OF LEANDER APPROVA	L I_{current} 56 of 83





×

91805

111110

SS

CENSE

09/21/2024

en lisss

- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH
- CALCULATION UNLESS SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.
- 6. EXPOSED CONCRETE THAT IS VISIBLE IS REQUIRED TO BE MADE OF STONE OR CLAD IN STONE INCLUDING BUT NOT LIMITED TO LEDGESTONE, FIELDSTONE, CAST STONE, OR OTHER DECORATIVE MATERIALS SUCH AS STAMPED AND TINTED CONCRETE THAT RESEMBLES STONE OR BRICK. THE CONCRETE TRICKLE CHANNEL IS NOT SUBJECT TO THIS REQUIREMENT.

|--|

		WATER LINE WASTEWATER LI STORM DRAIN L CURB INLET SINGLE WATER DOUBLE WATER DOUBLE WATER DOUBLE WW SER DOUBLE WW SER FIRE HYDRANT EXISTING GATE EXISTING GATE EXISTING FIRE H EXISTING WASTE EXISTING WASTE EXISTING WASTE EXISTING CONTO PROPOSED CON	INE & MH JNE & MH SERVICE SERVICE RVICE VALVE HYDRANT R LINE EWATER LINE M DRAIN LINE DUR LINE TOUR LINE TURE AR		ENGINEER	AUSTIN I SAN ANTONIO I HOUSTON I FORT 10801 N MOPAC EXPY, BLDG 3, STE 200 I AUSTIN, TX TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGI
CURVE C15 C16	PROFILE S 1" = 40' HOF 1" = 4' VERT PROFILE L NATURAL GROUN FINISHED GRADE SUBGRADE PROPOSED STOR 25-YR HGL 100-YR HGL 100-YR HGL 100yr HGL CC # RADIUS DEL 370.00' 05313 370.00' 026'08	SCALES: RIZONTAL ICAL EGEND: D M DRAIN -25 yr HGL 	CHORD LENGTH 331.83' 344.10' 167.50' 168.97'		LIVELY TRACT, PHASE 5 CITY OF LEANDER, TEXAS	STORMDRAIN PLAN & PROFILE LINE J1.01 (1 OF 2)
		CITY OF LEAN	PROVED 2MG DER APPROVA	Ci Ju Di Ci L	ITY NO. PICF DB NO. 50 ATE SEPTEM ESIGNER HECKED TCK HEET 57	2-24-0120 0816-25 IBER 2024 RBB DRAWN ADS Of 83



						1				1
	123	<u>5.9 L</u>	48″	RCP	}	<u> </u>				852
.										002
			[ļ	ļ			850
					A contract of the second se					
						ļ			Lingen 2	848
					Section 20	1.111	111	<u>UINII</u>	AIIIII	
<u>i</u>	77.77	111D		ĴΠ)	iiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiii	1111	111	NY .		
<u>`</u>			17		<u>httilli</u>			<u></u>		846
					MIIIII	())))	[]]]	N		
	GV-				<u> </u>			Y		
<u></u>	n Tali			mìt	million	HUHH	ANIIKI			844
A.						[]]]]				
25yr	HGL				25yr HGL		NY.	25yr HGL		
ᡟ─		· .			k.	(111)	Ň			842
						111	¥			- -
							Ø			~ ~
			01-N"	0 (.50%					840
XIII							1			
							Y			000
Π			" .11	-0*	@ 0.50%					838
	*****		U I	-0	W 0.30%					
				م	SVAT "WW=	5A"-C	1.0	0%		200
4 -		(EXIS	TING)		-					030
4 -				19. a. in 49						
										831
										004
										832
\mathbf{N}										002
	/	i			e e e e e e e e e e e e e e e e e e e	1994 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -				
	<u> </u>	}		· ·						830
							m			000
			-			1997 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 - 1998 -	6			
		ļ					Ň B			828
										020
			an "Adda a an tao (A. A) ai tao	al da i a adalah ya ata a		e para de la composition de la composi				
╔═╾┥		22	10 ID				¥0	<u> </u>		826
0.1		4 8	9.2				٩. ٣	4 12	vo del comente	
80	3	0.0	833			2	用 4	S Z		
<u>م</u>	— <u> </u>	₹ ŧ	22			<u> </u>	* 0	<u>72</u>		824
Ð	Ĭ	ର ୍	.55			Í	4 F	-ш 		
E	្តរី	° E	ट ट		and the advertised base to a strategy of Variaties of the state of the	รั	S S S S S	NO N		
6	6						E E			822
0.	80		50.5			4	ΧP	γġ		
ĩ	±	ļó j	ÍÌ	Alar		÷	Ŀн	Щú		
8	<u>7</u>	<u>₹</u> 3	ង់ស្			<u>u</u>)	漢필			820
	ž	ທຸ			frantises on a set of the second s	¥.	XX	ц <u>.</u>		
10	S	1 4	¥₽			S	2 2	Ϋ́β		
		L					L			
_										
28		4		53	66		78	6	F) O	
တ္တ်		39.		<u>છ</u> .	<u>3</u> 9.		တ္တ်	39.	호	
8		ŵ		8	8		ώ	ŵ	8	
l					15-	-00			15+	75

25 yr Storm Event										
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic					
Laper	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)					
J1-1	66.75	16.15	3.54	839.17	836.93					
J1-K	66.80	11.91	2.08	839.52	838.77					
J1-L	67.13	11.93	1.87	841.58	838.92					
J1-M	63.56	9.07	3.4	842.52	842.51					
J1-N	58.31	8.88	3.5	842.77	842.75					
J1-0	58.36	8.88	3.05	842.77	842.77					

Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
J1-I	99.03	17.96	4.46	839.71	837.85
J1-K	99.11	13.12	2.62	840.07	839.32
J1-L	99.55	13.13	2.38	842.13	839.43
J1-M	94.3	7.5	4.29	843.5	843.4
J1-N	86.58	6.89	4.57	844.12	843.82
J1-0	86.66	6.9	4.39	844.21	844.12



NOTES:

1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES. 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED.

Parilin'

*

DUSTIN J. GOSS 91805

100000

09/21/2024

an 1 == ass

- 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

IHIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION. UILITY INSTALLATION. W WATER LINE W WATER LINE W WATER LINE UILITY INSTALLATION. UILITY INSTALLATION. UILITY INSTALLATION. UILITY INSTALLATION. W WATER LINE WW WASTEWATER LINE & MH UILITY INSTALLATION. SINGLE WATER SERVICE DOUBLE WATER SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING WATER LINE WW EXISTING WASTEWATER LINE WW EXISTING STORM DRAIN LINE UILITY STORE CONTOUR LINE	EL PAPE-DAWSON ENGINEERS	AUSTIN I SAN ANTONIO I HOUSTON I FORT WORTH I DALLAS 10801 N MOPAC EXPV, BLDG 3, STE 200 I AUSTIN, TX 78759 I 512.454.8711 TBPE FIRM REGISTRATION #470 I TBPLS FIRM REGISTRATION #10028801
$ \begin{array}{c} \#01\\ g_{26}: q_{25}\\ g_{100}: q_{100}\\ \end{array} \\ \hline PROFILE SCALES: \\ \hline 1'' = 40' HORIZONTAL \\ 1'' = 4' VERTICAL \\ PROFILE LEGEND: \\ \hline NATURAL GROUND \\ \hline HNISHED GRADE \\ \hline SUBGRADE \\ \hline 25-YR HGL \\ \hline 25-YR HGL \\ \hline 100-YR HGL \\ \hline 100yr HGL \\ \hline 100yr HGL \\ \hline \end{array} $	Y OF LEANDER, TEXAS	MDRAIN PLAN & PROFILE LINE J1.01 (2 OF 2)
CURVE IABLE CURVE # RADIUS DELTA CHORD BEARING CHORD LENGTH C17 505.00' 040'45'34" N01'28'51"E 351.72' 359.25'		STOF
APPROVED 2MG CITY OF LEANDER APPROVAL	CITY NO JOB NO DATE DESIGNER CHECKED TCK SHEET	2P-24-0120 50816-25 MBER 2024 RBB DRAWN ADS Of 83



~



	· · · · · · · · · · · · · · · · · · ·		25 yr Sto	rm Event	· · · · · · · · · · · · · · · · · · ·						
Labol	Flow	Velocity	Depth	Hydraulic	Hydraulic						
Laper	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)						
J1.04	5.84	13.82	1	843.82	842.75						
J1.05	4.05	10.15	0.9	843.28	842.51						
J1.06	5.57	6.69	1.04	837.03	836.93						
J1.07	5.16	2.92	2.11	829.1	829.07						
J1.08	4.34	2.46	2.3	828.85	828.82						
J1.09	4.13	2.34	2.84	828.6	828.58						
		· · · · · · · · · · · · · · · · · · ·	100 yr Sto	orm Event							
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic						
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)						
J1.04	8.74	15.47	2.07	844.04	843.82						
J1.05	6	11.35	1.79	843.46	843.4						
J1.06	8.3	4.7	1.96	837.96	837.85						
J1.07	7.69	4.35	3.54	830.57	830.5						
J1.08	6.41	3.63	3.42	830	829.94						
		1	1		T						

NOTES:

829.45

J1.09 6.14 3.47 3.67

1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.

829.41

- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH CALCULATION UNLESS SHOWN OTHERWISE.
- 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.

5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.

PROFILE S	CALES:		
1" = 40' HORD	ZONTAL		
1" = 4' VERTIC	CAL		
PROFILE LE	EGEND:		
NATURAL GROUND	· · · · ·		········
FINISHED GRADE			
SUBGRADE			
PROPOSED STORM	DRAIN		
	. ·		
0		0	
25-YR HGL			
· · · · · · · · · · · · · · · · · · ·	-25yr HGL		
100-YR HGL 100yr HGL			



PICP-24-0120

APPROVED

PMG

XSKOST -



10 A

ب ب

25 yr Storm Event Depth Hydra (Out) (ft) Grade Line 1.29 847. 1.57 847 1.66 848.3 1.91 848.8 1.69 849. 1.61 849. 850.5 1.19 849.0 1.41 848. 846.38

100 yr Storm Event Depth Hydra (Out) (ft) Grade Line 1.83 848.3 848. 849.0 2.44 2.66 849.7 2.67 850.0 850.1



iulic	Hydraulic
e (In) (ft)	Grade Line (Out) (ft)
58	846.79
.8	847.79
36	847.97
82	848.92
08	849.08
89	849.08
58	850.04
06	849.08
91	848.92
38	845.95

nt	
Hydraulic	Hydraulic
de Line (In) (ft)	Grade Line (Out) (ft)
848.14	847.33
848.5	848.4
849.07	848.75
849.79	849.66
850.08	850.07
850.14	850.08
850.83	850.35
850.09	850.07
849.68	849.66
846.58	846.47





The Docient His Been PROUGD From Material. THAT was stored and/or Transmitted Electromodally and may have been individually a clear and a construction of Society 2025, 40 court particular storem and the store and

Debandar Example Community Perturbation Biges To Light Allow Other Harmings Begs Dist Harmings																									
DRAMAC Number Con Con Con Party Name Number Steps Ter Length Name Number Ter Terget Name Terget				COMP	OSITE C				SHEET FL	ow		SHALL	OW CONCE	ENTRATE	FLOW		CHANN	ELIZED FL	ow		Cumulative	INTEN	ISITY	DISCH	IARGE
AREA NUMBER Learners Image: Arrow and any and any and any and any and any and any	DRAINAGE	INLET	AREA	C25	C100	A.C ²⁵	A.C100	Length	Manning's	Slope	Tc	Length	Paved/	Slope	Tc	Length	Manning's	Slope	Velocity	Tc	Tc	l 25yr	I 100yr	Q 25	Q 100
ULTIWE CONDITION DRAIMAGE REALS b b b b b c <t< th=""><th>AREA</th><th>NUMBER</th><th>(acres)</th><th>- 4.5</th><th>- 100</th><th></th><th></th><th>(ft)</th><th>(n)</th><th>ft/ft</th><th>(min)</th><th>(ft)</th><th>Unpaved</th><th>ft/ft</th><th>(min)</th><th>(ft)</th><th>(n)</th><th>ft/ft</th><th>ft/s</th><th>(min)</th><th>(min)</th><th>(in/hr)</th><th>(in/hr)</th><th>(cfs)</th><th>(cfs)</th></t<>	AREA	NUMBER	(acres)	- 4.5	- 100			(ft)	(n)	ft/ft	(min)	(ft)	Unpaved	ft/ft	(min)	(ft)	(n)	ft/ft	ft/s	(min)	(min)	(in/hr)	(in/hr)	(cfs)	(cfs)
ULTMATE CONDITION DRAINAGE REFAS I <																									
Bit Bit <td>ULTIMATE CO</td> <td>DNDITION DR</td> <td>RAINAGE AR</td> <td>EAS</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>b</td> <td></td>	ULTIMATE CO	DNDITION DR	RAINAGE AR	EAS									b												
B1.10 B1.10 B1.10 B1.10 B1.10 B1.10 B1.10 B1.10 B1.11 D81 D81.11	54.40		0.70	0.00	0.77	0.544	0.007		0.04	0.000	1.05	-		0.045	0.00	400.00	0.045	0.040		0.000	0.05	10.00	40.70	5.0	
B117 D181 Outs Outs <thouts< th=""> Outs Outs <tho< td=""><td>B1.16</td><td>B1.16</td><td>0.79</td><td>0.69</td><td>0.77</td><td>0.541</td><td>0.607</td><td>34.83</td><td>0.24</td><td>0.028</td><td>4.85</td><td>0</td><td>U</td><td>0.015</td><td>0.00</td><td>462.02</td><td>0.015</td><td>0.010</td><td>3.8</td><td>2.002</td><td>6.85</td><td>10.36</td><td>13.73</td><td>5.6</td><td>8.3</td></tho<></thouts<>	B1.16	B1.16	0.79	0.69	0.77	0.541	0.607	34.83	0.24	0.028	4.85	0	U	0.015	0.00	462.02	0.015	0.010	3.8	2.002	6.85	10.36	13.73	5.6	8.3
Bolt Bolt Dot Dot <thdot< t<="" td=""><td>B1.17</td><td>B1.17</td><td>0.81</td><td>0.67</td><td>0.75</td><td>0.544</td><td>0.611</td><td>84.01</td><td>0.24</td><td>0.045</td><td>8.11</td><td>202.14</td><td>0</td><td>0.027</td><td>1.27</td><td>65.74</td><td>0.015</td><td>0.034</td><td>7.1</td><td>0.154</td><td>9.53</td><td>9.27</td><td>12.28</td><td>5.0</td><td>1.5</td></thdot<>	B1.17	B1.17	0.81	0.67	0.75	0.544	0.611	84.01	0.24	0.045	8.11	202.14	0	0.027	1.27	65.74	0.015	0.034	7.1	0.154	9.53	9.27	12.28	5.0	1.5
B&00 0.02 <th< td=""><td>DC 01</td><td>DE 01</td><td>0.72</td><td>0.67</td><td>0.75</td><td>0.496</td><td>0.540</td><td>00.40</td><td>0.24</td><td>0.017</td><td>12.24</td><td>172.20</td><td></td><td>0.000</td><td>1.07</td><td>100.02</td><td>0.015</td><td>0.005</td><td>27</td><td>0.779</td><td>45.00</td><td>7.64</td><td>10.00</td><td>27</td><td>5.5</td></th<>	DC 01	DE 01	0.72	0.67	0.75	0.496	0.540	00.40	0.24	0.017	12.24	172.20		0.000	1.07	100.02	0.015	0.005	27	0.779	45.00	7.64	10.00	27	5.5
Box Box <td>B0.01</td> <td>B0.01</td> <td>0.73</td> <td>0.67</td> <td>0.75</td> <td>0.460</td> <td>0.040</td> <td>30.10</td> <td>0.24</td> <td>0.017</td> <td>10.04</td> <td>173.30</td> <td>0</td> <td>0.020</td> <td>1.27</td> <td>120.93</td> <td>0.015</td> <td>0.005</td> <td>2.1</td> <td>1 200</td> <td>10.30</td> <td>7.01</td> <td>0.75</td> <td>3.1</td> <td>0.0</td>	B0.01	B0.01	0.73	0.67	0.75	0.460	0.040	30.10	0.24	0.017	10.04	173.30	0	0.020	1.27	120.93	0.015	0.005	2.1	1 200	10.30	7.01	0.75	3.1	0.0
B604 B804 B805 CAR B804	B0.02	B0.02	0.85	0.66	0.73	0.550	0.010	100	0.24	0.017	12.64	1/4.2/		0.010	1.42	107.25	0.015	0.000	4.2	0.424	14.15	7.00	9.75	4.0	6.6
B060 B060 C17 C031 C370 C11 C22 C22 C23 C11 C22 C23 C23 C11 C22 C24 C02 C23 C01 C03 C24 C02 C23 C01 C13 C11 C13 C10 C13 C13 C11 C13 C13 C11 C13 C11	B6.03	B6.03	0.88	0.00	0.74	0.500	0.650	81.11	0.24	0.021	11 13	171.52	U	0.020	1.00	138.38	0.015	0.012	4.2	0.424	13.20	8.14	10.40	4.4	7.0
bb0 bb bb0 bb 0.53 0.66 0.74 0.344 0.002 1.28 20.72 U 0.000 0.15 0.33.4 0.0015 0.000 3.7 0.242 1.12 0.71 2.8 4.2 B6.07 0.266 0.75 0.234 0.224 0.28 0.002 2.88 0.00 0.034 0.0015 0.0005 2.7 1.120 5.60 0.130 5.60 1.130 15.00 0.07 1.180 5.60 0.07 1.180 5.60 0.77 1.98 0.99 0.76 0.940 0.085 0.77 0.18 0.26 0.941 0.002 2.8 0 U 0.024 0.0015 0.005 2.6 0.911 1.30 15.00 0.77 1.30 15.00 1.01 1.50 0.10 1.30 15.00 1.01 1.50 0.002 2.6 0.0015 0.0005 2.7 5.00 11.30 15.00 1.83 1.50 1.30 15.00 1.30	B6.05	B6.05	0.00	00.00	0.74	0.331	0.000	11.0	0.24	0.013	2 35	0	U U	0.024	0.00	644 17	0.015	0.007	3.2	3 384	5.73	10.01	14.47	3.6	5.4
b807 b807 b807 b807 b807 b807 b807 b808 b008 b008 <thb008< th=""> b008 b008 <thb< td=""><td>B6.06</td><td>B6.06</td><td>0.40</td><td>0.66</td><td>0.74</td><td>0.348</td><td>0.301</td><td>100</td><td>0.24</td><td>0.020</td><td>12.80</td><td>20.72</td><td>U U</td><td>0.024</td><td>0.15</td><td>53.43</td><td>0.015</td><td>0.007</td><td>37</td><td>0.242</td><td>13.29</td><td>8.12</td><td>10.77</td><td>2.8</td><td>4.2</td></thb<></thb008<>	B6.06	B6.06	0.40	0.66	0.74	0.348	0.301	100	0.24	0.020	12.80	20.72	U U	0.024	0.15	53.43	0.015	0.007	37	0.242	13.29	8.12	10.77	2.8	4.2
B6.08 B6.08 0.03 0.07 0.75 0.24 0.03 0.24 0.002 0.23 0.005 2.7 1.722 8.84 0.94 1.365 2.3 3.4 B6.09A B6.09A 0.067 0.72 0.80 0.066 0.072 11.86 0.024 0.002 2.36 0 U 0.024 0.001 140.7 0.015 0.006 2.6 0.947 6.00 11.30 15.00 1.0 15. B6.09B B6.08 0.12 0.74 0.84 0.066 0.022 2.46 0 0.0024 0.000 140.7 0.015 0.006 3.7 0.990 5.00 11.30 15.00 10.7 11.8 0.024 0.002 2.17.4 0.015 0.004 2.4 0.041 2.4 0.015 0.004 2.4 0.011 1.0 0.020 1.2 0.020 0.2 0.23 0.011 1.0 0.024 0.000 0.015 0.011 0.01	B6.07	B6.07	0.26	0.00	0.81	0.189	0.001	12.02	0.24	0.022	2.28	0	U U	0.020	0.00	439.48	0.015	0.006	2.9	2 551	5.00	11.30	15.00	2.0	32
B6:09A B6:09A 0.09 0.72 0.80 0.005 0.005 0.005 2.6 0.947 5.00 1130 1500 0.7 1130 1500 0.7 1130 1500 0.7 1130 1500 0.7 1130 1500 0.7 1130 1500 0.7 1130 1500 0.7 1130 1500 0.7 1130 1500 0.7 1130 1500 0.7 1130 1500 10.7 1500 10.7 130 1500 10.7 1130 1500 10.7 1130 1500 10.7 1130 1500 10.7 1130 1500 10.7 1130 1500 10.7 1130 1500 10.7 1500 10.7 1130 1500 10.7 1130 1500 10.7 10.7 10.7 10.7 10.7 10.7 10.7 10.7 10.7 10.7 10.7 1130 1500 10.7 1130 1500 10.7 1130 150	B6.08	B6.08	0.35	0.67	0.75	0.234	0.263	33.04	0.24	0.013	6.32	0	U U	0.024	0.00	283.81	0.015	0.005	27	1.722	8.04	9.84	13.05	2.3	3.4
B6:09B B6:09B 0.12 0.76 0.44 0.021 0.74 0.002 0.003 3.7 0.990 5.00 11.30 15.00 10 15.2 B6:09 B6:10 B6:09 0.21 0.74 0.890 5.00 11.30 15.00 16.0 15.2 B6:10A B6:10A 0.07 0.86 0.75 0.485 0.822 15 0.24 0.044 21.347 U 0.043 15.1 39.88 0.015 0.009 3.6 0.471 9.98 9.11 12.08 6.5 6.7 B6:10 0.47 0.67 0.75 0.485 0.77 0.24 0.044 8.47 21.347 U 0.045 1.04 1032 0.050 . . 0.020 . 0.020 . 0.024 0.024 0.026 . 0.024 0.020 . 0.024 0.020 . 0.020 . 0.020 . 0.024 0.024 0.025 <	B6.09A	B6.09A	0.09	0.72	0.80	0.065	0.072	11.98	0.24	0.020	2.36	0	Ŭ	0.024	0.00	149.7	0.015	0.005	2.6	0.947	5.00	11.30	15.00	0.7	1.1
B6:09 B6:09 O.21 O.74 O.74 O.82 O.75 O.173 O.75 O.75 O.76 O.86 O.820 O.76 O.800 O.76 O.86 O.822 O.75 O.020 O.76 O.800 O.76 O.866 O.522 O.76 O.486 O.221 O.76 O.486 O.221 O.76 O.486 O.221 O.76 O.800 O.776 O.820 O.776 O.820 <tho.77< th=""> O.77 O.77 <th< td=""><td>B6.09B</td><td>B6.09B</td><td>0.12</td><td>0.76</td><td>0.84</td><td>0.091</td><td>0.101</td><td>13.18</td><td>0.24</td><td>0.022</td><td>2.45</td><td>0</td><td>Ŭ</td><td>0.024</td><td>0.00</td><td>217.42</td><td>0.015</td><td>0.009</td><td>3.7</td><td>0.990</td><td>5.00</td><td>11.30</td><td>15.00</td><td>1.0</td><td>1.5</td></th<></tho.77<>	B6.09B	B6.09B	0.12	0.76	0.84	0.091	0.101	13.18	0.24	0.022	2.45	0	Ŭ	0.024	0.00	217.42	0.015	0.009	3.7	0.990	5.00	11.30	15.00	1.0	1.5
B6:10A B6:10A 0.70 0.66 0.75 0.465 0.24 0.045 2.04 304.09 U 0.043 1.51 39.88 0.015 0.004 2.4 0.273 5.00 11.30 15.00 5.3 7.8 B6:10 14.4 0.67 0.75 0.483 0.553 7.6 - - - - 0.020 - 9.98 9.11 12.08 4.5 6.7 B6:10 1.44 0.67 0.75 0.386 100 0.24 0.039 9.97 208.86 U 0.042 1.05 67.44 0.015 0.020 - 0.015 0.020 - 0.015 0.022 6.55 11.30 15.00 3.0 4.5 B6:12 0.80 0.68 0.76 0.586 100 0.24 0.031 10.55 162.00 U 0.020 0.68 1.4 0.550 11.30 15.00 13.0 4.50 11.30 15.00 13	B6.09	B6.09	0.21	0.74	0.82	0.155	0.173	-	-	-	-	-	-	-	-	-	-	0.020	-	-	5.00	11.30	15.00	1.8	2.6
B6.108 B6.108 0.74 0.75 0.493 0.553 87.76 0.24 0.044 8.47 213.47 U 0.045 1.04 103.22 0.015 0.009 3.6 0.471 9.98 9.11 12.08 4.5 6.7 B6.10 B6.10 0.44 0.67 0.75 0.386 100 0.24 0.039 9.87 208.86 U 0.042 10.5 67.84 0.015 0.021 4.0 0.284 11.21 8.7 11.28 8.7 11.28 8.7 11.28 8.7 11.28 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208 8.7 11.208	B6.10A	B6.10A	0.70	0.66	0.75	0.465	0.522	15	0.24	0.045	2.04	304.09	U	0.043	1.51	39.88	0.015	0.004	2.4	0.273	5.00	11.30	15.00	5.3	7.8
B6.10 B6.10 1.44 0.67 0.75 0.988 1076 - - - - - - 0.020 - - 9.88 9.11 12.08 8.7 13.0 B6.11 B6.12 0.49 0.68 0.76 0.24 0.033 10.55 162.03 U 0.042 1.05 67.44 0.015 0.027 6.3 0.550 12.09 8.45 11.20 4.6 6.8 B6.12 B6.12 0.30 0.76 0.586 0.014 0.015 0.027 6.3 0.550 12.09 8.45 11.20 4.6 6.8 B6.13 B.13 0.38 0.76 0.586 0.68 0.76 0.586 0.627 31.19 0.24 0.001 9.61 14.4 0 0.020 10.08 0.015 0.015 0.015 0.015 0.015 0.024 0.037 16.0 0.024 0.023 0.26 16.0 0.035 0.66	B6.10B	B6.10B	0.74	0.67	0.75	0.493	0.553	87.76	0.24	0.044	8.47	213.47	U	0.045	1.04	103.22	0.015	0.009	3.6	0.471	9.98	9.11	12.08	4.5	6.7
B6.11 B6.11 0.49 0.67 0.75 0.326 0.366 100 0.24 0.039 9.87 208.86 U 0.042 1.05 67.84 0.015 0.015 0.027 6.3 0.550 1.20 8.45 11.20 8.46 11.20 4.6 6.8 B6.13 B6.13 0.38 0.71 0.76 0.541 0.666 100 0.24 0.033 10.55 162.03 U 0.029 0.98 208.71 0.015 0.027 6.3 0.550 12.09 8.45 11.20 4.6 6.8 B7.05 0.86 0.68 0.76 0.586 0.657 31.19 0.24 0.017 9.56 14.80 U 0.020 1.08 3 0.015 0.019 5.3 1.690 5.90 10.82 14.35 6.3 9.4 B7.06 B7.06 0.36 0.76 0.386 0.637 10.49 0.022 10.26 6.015 0.133 1	B6.10	B6.10	1.44	0.67	0.75	0.958	1.076	-		-	-	-		-	-	-	-	0.020	-	-	9.98	9.11	12.08	8.7	13.0
B6.12 B6.12 0.80 0.68 0.76 0.541 0.606 100 0.24 0.031 10.55 162.03 U 0.029 0.98 208.71 0.015 0.027 6.3 0.550 12.09 8.45 11.20 4.6 6.8 B6.13 0.38 0.71 0.79 0.270 0.301 10.32 0.24 0.019 2.14 0 U 0.015 0.0025 6.1 1.785 5.00 11.30 15.00 3.0 4.5 B7.06 B7.06 0.36 0.66 0.74 0.221 6.3 164.89 U 0.020 1.00 0.883 0.015 0.014 6.0 3.4 6.3 9.48 B7.06 B7.06 0.66 0.74 0.38 0.376 61.33 0.24 0.023 11.40 0.022 10.883 0.015 0.016 4.9 0.727 9.63 9.23 12.24 3.1 4.6 B7.09 B7.09 0.60 <td>B6.11</td> <td>B6.11</td> <td>0.49</td> <td>0.67</td> <td>0.75</td> <td>0.326</td> <td>0.366</td> <td>100</td> <td>0.24</td> <td>0.039</td> <td>9.87</td> <td>208.86</td> <td>U</td> <td>0.042</td> <td>1.05</td> <td>67.84</td> <td>0.015</td> <td>0.011</td> <td>4.0</td> <td>0.284</td> <td>11.21</td> <td>8.71</td> <td>11.55</td> <td>2.8</td> <td>4.2</td>	B6.11	B6.11	0.49	0.67	0.75	0.326	0.366	100	0.24	0.039	9.87	208.86	U	0.042	1.05	67.84	0.015	0.011	4.0	0.284	11.21	8.71	11.55	2.8	4.2
B6.13 B6.13 0.38 0.71 0.79 0.270 0.301 10.32 0.24 0.019 2.14 0 U 0.015 0.00 651.47 0.015 0.025 6.1 1.785 5.00 11.30 15.00 3.0 4.5 B7.05 B7.05 0.86 0.68 0.76 0.586 0.657 31.19 0.24 0.032 4.21 0 U 0.020 1.00 10.82 14.35 6.3 9.4 B7.06 B7.06 0.35 0.66 0.74 0.232 0.281 63.46 0.24 0.017 9.56 164.89 U 0.020 1.20 108.83 0.015 0.024 6.0 0.304 11.07 8.75 11.60 2.0 3.0 B7.07 0.48 0.70 0.78 0.449 0.024 0.037 10.08 10.92 257.53 0.015 0.024 5.90 11.30 15.00 6.0 8.9 3.3 4.26 3.3 </td <td>B6.12</td> <td>B6.12</td> <td>0.80</td> <td>0.68</td> <td>0.76</td> <td>0.541</td> <td>0.606</td> <td>100</td> <td>0.24</td> <td>0.033</td> <td>10.55</td> <td>162.03</td> <td>U</td> <td>0.029</td> <td>0.98</td> <td>208.71</td> <td>0.015</td> <td>0.027</td> <td>6.3</td> <td>0.550</td> <td>12.09</td> <td>8.45</td> <td>11.20</td> <td>4.6</td> <td>6.8</td>	B6.12	B6.12	0.80	0.68	0.76	0.541	0.606	100	0.24	0.033	10.55	162.03	U	0.029	0.98	208.71	0.015	0.027	6.3	0.550	12.09	8.45	11.20	4.6	6.8
B7.05 B7.05 0.86 0.68 0.76 0.586 0.657 31.19 0.24 0.032 4.21 0 U 0.020 0.00 537.74 0.015 0.019 5.3 1.690 5.90 10.82 14.35 6.3 9.4 B7.06 B7.06 0.35 0.66 0.74 0.232 0.261 63.46 0.24 0.017 9.56 164.89 U 0.020 1.20 106.83 0.015 0.024 6.0 0.304 11.07 8.75 11.60 2.0 3.0 B7.08 B7.08 0.60 0.70 0.78 0.419 0.469 100 0.24 0.022 7.26 160.36 U 0.020 1.17 139.95 0.015 0.024 5.9 3.868 11.50 3.6 5.4 B7.09 B52 0.66 0.74 0.444 0.387 51.2 0.24 0.022 7.26 160.36 U 0.020 1.17 139.95 0.0	B6.13	B6.13	0.38	0.71	0.79	0.270	0.301	10.32	0.24	0.019	2.14	0	U	0.015	0.00	651.47	0.015	0.025	6.1	1.785	5.00	11.30	15.00	3.0	4.5
B7.05 B7.05 0.86 0.68 0.76 0.586 0.687 31.19 0.24 0.032 4.21 0 U 0.020 5.07.74 0.015 0.019 5.3 1.690 5.90 10.82 14.35 6.3 9.4 B7.06 B7.07 0.48 0.774 0.232 0.261 63.46 0.24 0.017 9.56 164.89 U 0.020 1.20 108.83 0.015 0.016 4.0 0.727 9.63 9.23 12.24 3.1 4.6 B7.08 B7.09 0.52 0.66 0.74 0.344 0.387 51.2 0.40 0.022 1.71 139.95 0.015 0.029 6.6 0.655 11.33 8.68 11.50 3.6 5.4 B7.09 B7.09 0.52 0.66 0.74 0.344 0.387 51.2 0.276 72 U 0.004 1.43 50.17 0.015 0.024 5.00 11.30 15.00 6.0 8.9 3.169 0.245 5.00 11.30 15.00 5.2 7.8 <td></td>																									
B7.06 B7.06 0.35 0.66 0.74 0.222 0.216 63.46 0.24 0.017 9.56 164.89 U 0.020 1.20 108.83 0.015 0.024 6.0 0.304 11.07 8.75 11.60 2.0 3.0 B7.07 B7.07 0.48 0.70 0.78 0.336 0.376 61.33 0.24 0.022 8.25 114 U 0.032 0.66 212.36 0.015 0.024 6.0 0.655 11.33 8.68 11.50 3.6 5.4 B7.09 B7.09 0.52 0.66 0.74 0.344 0.387 51.2 0.24 0.002 7.26 160.36 U 0.020 1.17 139.95 0.015 0.024 5.00 11.30 15.00 6.0 8.9 B7.10 B7.10 0.80 0.66 0.75 0.531 0.596 0 2.4 0.033 0.00 276.72 U 0.0010 3.0 0.2	B7.05	B7.05	0.86	0.68	0.76	0.586	0.657	31.19	0.24	0.032	4.21	0	U	0.020	0.00	537.74	0.015	0.019	5.3	1.690	5.90	10.82	14.35	6.3	9.4
B7.07 B7.07 0.48 0.70 0.78 0.336 0.336 0.336 0.336 0.336 0.336 0.336 0.336 0.336 0.336 0.336 0.336 0.336 0.336 0.24 0.037 10.08 109.89 U 0.037 0.59 257.53 0.015 0.024 5.9 0.336 8.68 11.50 3.6 5.4 B7.09 B7.09 0.52 0.66 0.74 0.344 0.337 512 0.24 0.022 7.26 160.36 U 0.020 1.17 139.95 0.015 0.024 5.9 0.386 8.83 9.53 12.63 3.4 4.9 B7.10 B7.10 0.80 0.66 0.74 0.460 0.517 0 0.24 0.033 0.00 276.72 U 0.040 1.43 50.17 0.015 0.006 3.0 0.245 5.00 11.30 15.00 5.2 7.8 B7.11 B7.12 D.44 D.67 <td>B7.06</td> <td>B7.06</td> <td>0.35</td> <td>0.66</td> <td>0.74</td> <td>0.232</td> <td>0.261</td> <td>63.46</td> <td>0.24</td> <td>0.017</td> <td>9.56</td> <td>164.89</td> <td>U</td> <td>0.020</td> <td>1.20</td> <td>108.83</td> <td>0.015</td> <td>0.024</td> <td>6.0</td> <td>0.304</td> <td>11.07</td> <td>8.75</td> <td>11.60</td> <td>2.0</td> <td>3.0</td>	B7.06	B7.06	0.35	0.66	0.74	0.232	0.261	63.46	0.24	0.017	9.56	164.89	U	0.020	1.20	108.83	0.015	0.024	6.0	0.304	11.07	8.75	11.60	2.0	3.0
B7.08 B7.08 0.60 0.70 0.78 0.449 100 0.24 0.037 10.08 109 0.57 3 0.015 0.029 6.6 0.655 11.33 8.68 11.50 3.6 5.4 B7.09 0.52 0.66 0.74 0.344 0.387 51.2 0.24 0.002 7.26 160.36 U 0.020 1.17 139.95 0.015 0.024 5.9 0.396 8.83 9.53 12.63 3.3 4.9 B7.10 B7.10 0.66 0.74 0.460 0.517 0 0.24 0.003 0.00 276.72 U 0.040 1.43 50.17 0.015 0.006 3.0 0.245 5.00 11.30 15.00 6.6 8.9 B7.11 B7.12 0.44 0.67 0.75 0.296 0.332 100 0.24 0.033 0.00 3.66 9.03 0.015 0.006 3.0 0.245 5.00 11.30	B7.07	B7.07	0.48	0.70	0.78	0.336	0.376	61.33	0.24	0.023	8.25	114	U	0.032	0.66	212.36	0.015	0.016	4.9	0.727	9.63	9.23	12.24	3.1	4.6
B7.09 B7.09 0.52 0.66 0.74 0.344 0.387 51.2 0.24 0.022 7.26 160.36 U 0.020 1.17 139.95 0.015 0.024 5.9 0.386 8.83 9.53 12.63 3.3 4.9 B7.10 B7.10 0.80 0.66 0.75 0.531 0.596 0 0.24 0.043 0.00 276.72 U 0.040 1.43 50.17 0.015 0.016 5.00 11.30 15.00 6.0 8.8 B7.11 B7.10 0.70 0.66 0.74 0.460 0.517 0 0.24 0.043 0.00 306.93 U 0.021 1.9 43.76 0.015 0.006 3.0 0.245 5.00 11.30 15.00 6.0 7.8 B7.12 B7.12 0.44 0.67 0.75 0.296 0.332 100 0.24 0.045 9.32 87.9 U 0.023 0.60 99.03	B7.08	B7.08	0.60	0.70	0.78	0.419	0.469	100	0.24	0.037	10.08	109.89	U	0.037	0.59	257.53	0.015	0.029	6.6	0.655	11.33	8.68	11.50	3.6	5.4
B7.10 B7.10 0.80 0.66 0.75 0.531 0.596 0 0.24 0.043 0.00 276.72 U 0.040 1.43 50.17 0.010 3.9 0.216 5.00 11.30 15.00 6.0 8.9 B7.11 B7.11 0.70 0.66 0.74 0.460 0.517 0 0.24 0.033 0.00 306.93 U 0.021 2.19 43.76 0.015 0.006 3.0 0.245 5.00 11.30 15.00 5.2 7.8 B7.12 0.44 0.67 0.75 0.296 0.332 100 0.24 0.045 9.32 87.9 U 0.023 0.60 99.03 0.015 0.006 3.0 0.554 10.47 8.85 11.86 2.6 3.9 B9.01 0.71 0.66 0.74 0.460 0.517 67.52 0.24 0.018 3.9 2.64.03 U 0.023 1.61 141.57 0.015	B7.09	B7.09	0.52	0.66	0.74	0.344	0.387	51.2	0.24	0.022	7.26	160.36	U	0.020	1.17	139.95	0.015	0.024	5.9	0.396	8.83	9.53	12.63	3.3	4.9
B7.11 B7.11 0.70 0.66 0.74 0.460 0.517 0 0.24 0.033 0.00 306.93 U 0.021 2.19 43.76 0.015 0.006 3.0 0.245 5.00 11.30 15.00 5.2 7.8 B7.12 B7.12 0.44 0.67 0.75 0.296 0.332 100 0.24 0.045 9.32 87.9 U 0.023 0.60 99.03 0.015 0.006 3.0 0.554 10.47 8.95 11.86 2.6 3.9 B9.01 0.71 0.66 0.74 0.466 0.524 49.56 0.24 0.016 8.04 351.78 U 0.020 2.57 29.71 0.015 0.007 3.2 0.154 10.76 8.85 11.73 4.1 6.1 B9.02 D.70 0.66 0.74 0.460 0.517 67.52 0.24 0.018 9.82 264.03 U 0.015 0.007 3.1 <td>B7.10</td> <td>B7.10</td> <td>0.80</td> <td>0.66</td> <td>0.75</td> <td>0.531</td> <td>0.596</td> <td>0</td> <td>0.24</td> <td>0.043</td> <td>0.00</td> <td>276.72</td> <td>U</td> <td>0.040</td> <td>1.43</td> <td>50.17</td> <td>0.015</td> <td>0.010</td> <td>3.9</td> <td>0.216</td> <td>5.00</td> <td>11.30</td> <td>15.00</td> <td>6.0</td> <td>8.9</td>	B7.10	B7.10	0.80	0.66	0.75	0.531	0.596	0	0.24	0.043	0.00	276.72	U	0.040	1.43	50.17	0.015	0.010	3.9	0.216	5.00	11.30	15.00	6.0	8.9
B7.12 B7.12 0.44 0.67 0.75 0.296 0.32 100 0.24 0.045 9.32 87.9 0 0.023 0.60 99.03 0.015 0.006 3.0 0.554 10.47 8.95 11.86 2.6 3.9 B9.01 0.71 0.66 0.74 0.466 0.524 49.56 0.24 0.016 8.04 351.78 U 0.020 2.57 29.71 0.015 0.007 3.2 0.154 10.76 8.85 11.73 4.1 6.1 B9.02 0.70 0.66 0.74 0.460 0.517 67.52 0.24 0.018 9.82 264.03 U 0.015 0.007 3.1 0.597 10.27 9.01 11.95 5.8 8.5 B9.03 B9.04 0.59 0.66 0.74 0.391 0.439 100 0.24 0.021 12.64 179 U 0.027 1.13 102.8 0.015 0.006 3.0 <td>B7.11</td> <td>B7.11</td> <td>0.70</td> <td>0.66</td> <td>0.74</td> <td>0.460</td> <td>0.517</td> <td>0</td> <td>0.24</td> <td>0.033</td> <td>0.00</td> <td>306.93</td> <td>U</td> <td>0.021</td> <td>2.19</td> <td>43.76</td> <td>0.015</td> <td>0.006</td> <td>3.0</td> <td>0.245</td> <td>5.00</td> <td>11.30</td> <td>15.00</td> <td>5.2</td> <td>7.8</td>	B7.11	B7.11	0.70	0.66	0.74	0.460	0.517	0	0.24	0.033	0.00	306.93	U	0.021	2.19	43.76	0.015	0.006	3.0	0.245	5.00	11.30	15.00	5.2	7.8
B9.01 B9.01 0.71 0.66 0.74 0.466 0.524 49.56 0.24 0.016 8.04 351.78 U 0.020 2.57 29.71 0.015 0.007 3.2 0.154 10.76 8.85 11.73 4.1 6.1 B9.02 B9.02 0.70 0.66 0.74 0.460 0.517 67.52 0.24 0.018 9.82 264.03 U 0.015 0.006 3.0 0.792 12.77 8.26 10.95 3.8 5.7 B9.03 B9.03 0.84 0.76 0.84 0.640 0.712 53.27 0.24 0.020 7.79 276.32 U 0.023 1.88 112.71 0.015 0.006 3.0 0.575 14.34 7.85 10.41 3.1 4.6 B9.04 B9.04 0.59 0.66 0.74 0.391 0.439 100 0.24 0.021 12.64 179 U 0.027 1.13 102.8 0	B7.12	B7.12	0.44	0.67	0.75	0.296	0.332	100	0.24	0.045	9.32	87.9	U	0.023	0.60	99.03	0.015	0.006	3.0	0.554	10.47	8.95	11.86	2.6	3.9
B9.01 B9.01 0.71 0.66 0.74 0.466 0.324 49.56 0.24 0.016 8.04 351.76 0 0.020 2.57 29.71 0.015 0.007 3.2 0.154 10.76 8.85 11.73 4.1 6.1 B9.02 0.70 0.66 0.74 0.460 0.517 67.52 0.24 0.018 9.82 264.03 U 0.016 2.16 141.57 0.015 0.006 3.0 0.792 12.77 8.26 10.95 3.8 5.7 B9.03 0.84 0.76 0.84 0.640 0.712 53.27 0.24 0.020 7.79 276.32 U 0.023 1.88 112.71 0.015 0.006 3.0 0.575 14.34 7.85 10.41 3.1 4.6 B9.04 B9.04 0.59 0.66 0.74 0.391 0.439 100 0.24 0.018 2.69 U 0.027 1.13 102.8	D0.01	DO 01	0.74	0.00	0.74	0.466	0.524	40.50	0.04	0.040	0.04	254 70		0.000	0.57	00.74	0.015	0.007	20	0.454	40.70	0.05	44.70	4.4	6.4
B9.02 B9.02 0.70 0.66 0.74 0.460 0.517 67.32 0.24 0.018 9.82 264.03 0 0.016 2.16 141.37 0.013 0.006 3.0 0.792 12.77 8.26 10.95 3.8 5.7 B9.03 0.84 0.76 0.84 0.640 0.712 53.27 0.24 0.020 7.79 276.32 U 0.023 1.88 112.71 0.015 0.007 3.1 0.597 10.27 9.01 11.95 5.8 8.5 B9.04 B9.04 0.59 0.66 0.74 0.391 0.439 100 0.24 0.021 12.64 179 U 0.027 1.13 102.8 0.015 0.006 3.0 0.575 14.34 7.85 10.41 3.1 4.6 B9.05 0.22 0.72 0.80 0.158 0.176 13.39 0.24 0.018 2.69 0 U 0.015 0.005 3.0 </td <td>B9.01</td> <td>B9.01</td> <td>0.71</td> <td>0.00</td> <td>0.74</td> <td>0.460</td> <td>0.524</td> <td>49.00</td> <td>0.24</td> <td>0.016</td> <td>8.04</td> <td>301.78</td> <td></td> <td>0.020</td> <td>2.0/</td> <td>29.71</td> <td>0.015</td> <td>0.007</td> <td>3.2</td> <td>0.104</td> <td>10.70</td> <td>0.00</td> <td>11.73</td> <td>4.1</td> <td>5.7</td>	B9.01	B9.01	0.71	0.00	0.74	0.460	0.524	49.00	0.24	0.016	8.04	301.78		0.020	2.0/	29.71	0.015	0.007	3.2	0.104	10.70	0.00	11.73	4.1	5.7
B9.03 B9.03 0.84 0.76 0.84 0.64 0.712 53.27 0.24 0.020 7.79 276.32 0 0.023 1.86 112.71 0.015 0.007 3.1 0.397 10.27 9.01 11.95 5.8 6.3 B9.04 B9.04 0.59 0.66 0.74 0.391 0.439 100 0.24 0.021 12.64 179 U 0.027 1.13 102.8 0.015 0.006 3.0 0.575 14.34 7.85 10.41 3.1 4.6 B9.05 0.22 0.72 0.80 0.158 0.176 13.39 0.24 0.018 2.69 0 U 0.015 0.006 3.0 1.095 5.00 11.30 15.00 1.8 2.6 U U 0.035 0.98 43.24 0.015 0.013 4.4 0.164 13.56 8.05 10.67 6.6 9.9 B10.03 B10.03 1.20	B9.02	B9.02	0.70	0.00	0.74	0.460	0.517	62.0Z	0.24	0.018	9.62	204.03		0.010	1 00	141.07	0.015	0.000	3.0	0.792	10.07	0.20	10.95	5.0	0.6
B3.04 B3.05 B3.04 B3.04 B3.04 B3.04 B3.04 B3.04 B3.04 B3.04 B3.04 B3.05 B3.04 B3.04 B3.04 B3.05 B3.05 <th< td=""><td>B9.03</td><td>B9.03</td><td>0.64</td><td>0.70</td><td>0.04</td><td>0.040</td><td>0.712</td><td>100</td><td>0.24</td><td>0.020</td><td>12.64</td><td>170</td><td>0</td><td>0.023</td><td>1.00</td><td>102.0</td><td>0.015</td><td>0.007</td><td>3.0</td><td>0.597</td><td>14.24</td><td>7.05</td><td>10.41</td><td>2.1</td><td>0.0</td></th<>	B9.03	B9.03	0.64	0.70	0.04	0.040	0.712	100	0.24	0.020	12.64	170	0	0.023	1.00	102.0	0.015	0.007	3.0	0.597	14.24	7.05	10.41	2.1	0.0
B9.05 B9.05 0.22 0.72 0.80 0.186 0.176 13.39 0.24 0.016 2.69 0 0.015 0.006 3.0 1.095 5.00 11.30 13.00 1.8 2.6 B10.01 B10.01 1.25 0.66 0.74 0.823 0.924 100 0.24 0.022 12.41 177.68 U 0.035 0.98 43.24 0.015 0.013 4.4 0.164 13.56 8.05 10.67 6.6 9.9 B10.03 B10.03 1.20 0.66 0.74 0.798 0.895 100 0.24 0.026 11.61 214.16 U 0.038 1.13 39.02 0.013 4.4 0.148 12.89 8.22 10.90 6.6 9.8	B9.04	B9.04	0.09	0.00	0.74	0.391	0.439	12.20	0.24	0.021	2.60	179		0.027	0.00	102.0	0.015	0.000	3.0	1.005	5.00	11.00	10.41	0.1	4.0
B10.01 B10.01 1.25 0.66 0.74 0.823 0.924 100 0.022 12.41 177.68 U 0.035 0.98 43.24 0.013 4.4 0.164 13.56 8.05 10.67 6.6 9.9 B10.03 B10.03 1.20 0.66 0.74 0.798 0.895 100 0.24 0.026 11.61 214.16 U 0.038 1.13 39.02 0.013 4.4 0.148 12.89 8.22 10.90 6.6 9.8	09.00	D9.00	0.22	0.72	0.00	0.136	0.170	15.59	0.24	0.016	2.09	U	0	0.015	0.00	199.20	0.015	0.000	3.0	1.095	5.00	11.30	10.00	1.0	2.0
B10.03 B10.03 1.20 0.66 0.74 0.798 0.895 100 0.24 0.026 11.61 214.16 U 0.038 1.13 39.02 0.015 0.013 4.4 0.148 12.89 8.22 10.90 6.6 9.8	B10.01	B10.01	1.25	0.66	0.74	0.823	0.924	100	0.24	0.022	12.41	177 68	Ш	0.035	0.98	43.24	0.015	0.013	44	0 164	13.56	8.05	10.67	66	99
	B10.03	B10.03	1.20	0.66	0.74	0.798	0.895	100	0.24	0.026	11.61	214 16	U U	0.038	1 13	39.02	0.015	0.013	4.4	0.148	12.89	8.22	10.90	66	9.8
B10.04 B10.04 0.25 0.70 0.78 0.174 0.195 11.79 0.24 0.019 2.38 0 U 0.020 0.00 352.86 0.015 0.013 4.4 1.341 5.00 11.30 15.00 2.0 2.9	B10.04	B10.04	0.25	0.70	0.78	0.174	0.195	11 79	0.24	0.019	2.38	0	U U	0.020	0.00	352.86	0.015	0.013	4.4	1.341	5.00	11.30	15.00	2.0	2.9
	0.0.01	010.01	0.20	0.10	0.10	0.114	0.100		0.21	0.010	2.00	· · ·		0.020	1 0.00	002.00	0.010	0.010			0.00		10.00	2.0	2.0
J1.09 J1.09 0.57 0.68 0.76 0.385 0.432 56.63 0.24 0.036 6.47 123.45 U 0.020 0.90 169.19 0.015 0.006 3.0 0.946 8.31 9.73 12.90 3.7 5.6	J1.09	J1.09	0.57	0.68	0.76	0.385	0.432	56.63	0.24	0.036	6.47	123.45	U	0.020	0.90	169.19	0.015	0.006	3.0	0.946	8.31	9.73	12.90	3.7	5.6



The Docient His Been PROUGD From Material. THAT was stored and/or Transmitted Electromodally and may have been individually a clear and a construction of Society 2025, 40 court particular storem and the store and

| | | | | | |

 | | |
 |
 | | | | |
 | | | |
 | | | | | | | | | _ | |
|---|--|---|---|---|---
--
---	--
--
---|---|--|--|---
--|--|---|---
--|--|--|---|--|---|-------------------------------|---|---|--|--|
| STREET FLOW
25 YEAR STOR | | ET CALCUL | ATIONS | | |

 | | | CIDE
 |
 | | | | |
 | | | FTONC | DADE C
 | | | | | | | ET CADA | | _ | |
| | | | | | | Street

 | Crown | Curb | Gutter
 | CAPAC
 | | Crown | Ponded | |
 | | INL | ETONG | RADE C
 | | | | | 5 | | (with De | pression | 1) | |
| Inlet | Inlet | Drainage | Q 25 | Q pass | Q total | Width F-F

 | Туре | Height | Slope
 | a
 | Yo | Height | Width | Eo | S'w
 | Sx | Se | LT | L
 | E | Qi | Qpass | Pass to Inlet | Qtotal | Length | 1.00 | d (ft) | | |
| JLTIMATE CON | DITION D | Area
RAINAGE A | (CIS)
REAS | (CIS) | (CIS) | (π)

 | | (π) | (%)
 | (π)
 | (π) | (π) | (ft) | | | | | | | |
 | | | |
 | | | (CIS) | # | (CIS) | (π) | α (π) | (a ≤ n + | · a) | |
| B1.16
B1.17 | G-1
G-1 | 0.79 | 5.61
5.05 | | 5.6
5.0 | 27
27

 | P | 0.50 | 1.00%
 | 0.42
 | 0.43 | 0.50 | 8.56
5.91 | 0.52 | 0.28
 | 0.04 | 0.18 | 10.36 | 10
10
 | 1.00
0.98 | 5.6
4.9 | 0.0 | -
pass B6.12 | - | - | - | - | | |
| B6.01 | G-1 | 0.73 | 3.70 | | 3.7 | 27

 | P | 0.50 | 0.50%
 | 0.42
 | 0.42 | 0.50 | 8.21 | 0.54 | 0.28
 | 0.04 | 0.19 | 6.90 | 10
 | 1.00 | 3.7 | 0.0 | - | | - | - | | | |
| B6.02 | G-1 | 0.82 | 4.05 | | 4.0 | 27

 | P | 0.50 | 0.64%
 | 0.42
 | 0.42 | 0.50 | 8.07 | 0.56 | 0.28
 | 0.04 | 0.19 | 7.62 | 10
 | 1.00 | 4.0 | 0.0 | - | - | - | - | - | | |
| B6.03
B6.04 | G-1
G-1 | 0.85 | 4.43 | | 4.4 | 40

 | P | 0.50 | 0.80%
 | 0.42
 | 0.37 | 0.50 | 9.85 | 0.48 | 0.28
 | 0.03 | 0.16 | 10.80 | 10
 | 0.99 | 4.4 | 0.0 | - | - | - | - | - | | |
| B6.05 | G-1 | 0.48 | 3.61 | | 3.6 | 27

 | Р | 0.50 | 0.68%
 | 0.42
 | 0.40 | 0.50 | 7.43 | 0.61 | 0.28
 | 0.04 | 0.21 | 7.06 | 10
 | 1.00 | 3.6 | 0.0 | - | | | - | - | | |
| B6.06
B6.07 | G-1
G-1 | 0.53 | 2.82 | | 2.8 | 27

 | P | 0.50 | 0.92%
 | 0.42
 | 0.35 | 0.50 | 6.11 | 0.78 | 0.28
 | 0.04 | 0.25 | 6.17
4.68 | 10
 | 1.00 | 2.8 | 0.0 | - | - | - | - | - | | |
| B6.08 | G-1 | 0.35 | 2.30 | | 2.3 | 27

 | Р | 0.50 | 0.51%
 | 0.42
 | 0.36 | 0.50 | 6.38 | 0.74 | 0.28
 | 0.04 | 0.24 | 4.88 | 10
 | 1.00 | 2.3 | 0.0 | - | | | - | - | | |
| B6.09A
B6.09B | G-1
G-1 | 0.09 | 1.02 | | 1.0 | 27

 | P | 0.50 | 0.91%
 | 0.42
 | 0.25 | 0.50 | 3.96 | 0.85 | 0.28
 | 0.04 | 0.27 | 3.85 | 10
 | 1.00 | 1.0 | 0.0 | - | - | - | - | - | | |
| B6.09 | S-1 | 0.21 | 1.75 | | 1.8 | - 07

 | - | - | -
 | -
 | - | - | - | - | -
 | - | - | - | 10
 | - | - | - | - | 1.8 | 10 | 0.15 | 0.15 | | |
| B6.10A
B6.10B | G-1 | 0.70 | 4.49 | | 4.5 | 27

 | P | 0.50 | 0.40%
 | 0.42
 | 0.49 | 0.50 | 7.76 | 0.58 | 0.28
 | 0.04 | 0.14 | 8.64 | 15
 | 1.00 | 4.5 | 0.0 | - | - | | - | | | |
| B6.10 | S-1 | 1.44 | 8.73 | | 8.7 | - 27

 | -
D | - | -
 | -
 | - 0.24 | - 0.50 | - 5.01 | - | - 0.28
 | - | - 0.26 | - 6.34 | 15
 | - 1.00 | - | - | - | 8.7 | 15 | 0.36 | 0.36 | | |
| B6.12 | G-1 | 0.49 | 4.57 | 0.1 | 4.7 | 27

 | P | 0.50 | 2.70%
 | 0.42
 | 0.34 | 0.50 | 6.01 | 0.80 | 0.28
 | 0.04 | 0.26 | 10.42 | 10
 | 1.00 | 4.7 | 0.0 | - | | - | - | - | | |
| B6.13 | G-1 | 0.38 | 3.05 | | 3.0 | 27

 | Р | 0.50 | 2.50%
 | 0.42
 | 0.30 | 0.50 | 5.06 | 0.85 | 0.28
 | 0.04 | 0.27 | 8.25 | 10
 | 1.00 | 3.0 | 0.0 | - | | - | - | - | | |
| B7.05 | G-1 | 0.86 | 6.34 | | 6.3 | 27

 | Р | 0.50 | 1.90%
 | 0.42
 | 0.41 | 0.50 | 7.64 | 0.59 | 0.28
 | 0.04 | 0.20 | 12.38 | 10
 | 0.95 | 6.0 | 0.3 | pass B6.08 | - | - | - | - | | |
| B7.06 | G-1 | 0.35 | 2.03 | | 2.0 | 27

 | P | 0.50 | 2.40%
 | 0.42
 | 0.27 | 0.50 | 4.31 | 0.85 | 0.28
 | 0.04 | 0.27 | 6.87
7.27 | 10
 | 1.00 | 2.0 | 0.0 | - | - | - | - | - | | |
| B7.08 | G-1 | 0.60 | 3.63 | 0.3 | 3.9 | 27

 | P | 0.50 | 2.90%
 | 0.42
 | 0.32 | 0.50 | 5.47 | 0.85 | 0.28
 | 0.04 | 0.27 | 9.60 | 10
 | 1.00 | 3.9 | 0.0 | - | - | - | - | | | |
| B7.09
B7.10 | G-1
G-1 | 0.52 | 3.28 | | 3.3 | 27

 | P | 0.50 | 2.35%
 | 0.42
 | 0.32 | 0.50 | 5.29 | 0.85 | 0.28
 | 0.04 | 0.27 | 8.35 | 10
 | 1.00 | 3.3 | 0.0 | -
pass B7 12 | - | - | - | - | | |
| B7.11 | G-1 | 0.70 | 5.20 | | 5.2 | 27

 | P | 0.50 | 0.60%
 | 0.42
 | 0.46 | 0.50 | 9.67 | 0.45 | 0.28
 | 0.04 | 0.16 | 9.20 | 10
 | 1.00 | 5.2 | 0.0 | - | | - | - | - | | |
| B7.12 | G-1 | 0.44 | 2.65 | 0.1 | 2.7 | 27

 | Р | 0.50 | 0.60%
 | 0.42
 | 0.37 | 0.50 | 6.68 | 0.70 | 0.28
 | 0.04 | 0.23 | 5.68 | 10
 | 1.00 | 2.7 | 0.0 | - | - | - | - | | | |
| B9.01 | G-1 | 0.71 | 4.13 | | 4.1 | 48

 | Р | 0.50 | 0.70%
 | 0.42
 | 0.39 | 0.50 | 12.74 | 0.36 | 0.28
 | 0.02 | 0.12 | 10.41 | 10
 | 1.00 | 4.1 | 0.0 | - | | - | - | - | | |
| B9.02
B9.03 | G-1
G-1 | 0.70 | 3.80 | | 3.8
5.8 | 48

 | P | 0.50 | 0.60%
 | 0.42
 | 0.39 | 0.50 | 12.71 | 0.36 | 0.28
 | 0.02 | 0.12 | 9.59 | 10
 | 1.00 | 3.8
5.8 | 0.0 | - | - | - | - | - | | |
| B9.04 | G-1 | 0.59 | 3.07 | | 3.1 | 27

 | P | 0.50 | 0.60%
 | 0.42
 | 0.39 | 0.50 | 7.06 | 0.65 | 0.28
 | 0.04 | 0.22 | 6.17 | 10
 | 1.00 | 3.1 | 0.0 | | | | - | - | | |
| B9.05 | G-1 | 0.22 | 1.78 | | 1.8 | 27

 | Р | 0.50 | 0.62%
 | 0.42
 | 0.32 | 0.50 | 5.42 | 0.85 | 0.28
 | 0.04 | 0.27 | 4.34 | 10
 | 1.00 | 1.8 | 0.0 | - | | | - | | | |
| B10.01 | G-1 | 1.25 | 6.62 | | 6.6 | 48

 | Р | 0.50 | 1.30%
 | 0.42
 | 0.41 | 0.50 | 14.02 | 0.32 | 0.28
 | 0.02 | 0.11 | 16.20 | 10
 | 0.82 | 5.4 | 1.2 | pass B10.03 | | | - | - | _ | |
| B10.03
B10.04 | G-1
G-1 | 1.20
0.25 | 6.56 | 1.2 | 7.8 | 27 48

 | P | 0.50 | 1.30%
 | 0.42
 | 0.46 | 0.50 | 9.76 | 0.45 | 0.28
 | 0.04 | 0.16 | 13.79
6.52 | 15
 | 1.00 | 7.8 | 0.0 | - | - | - | - | - | | |
| | | | | | |

 | | |
 |
 | | | | | | | | | | |
 | | | |
 | | | | | | | | | | |
| J1.09 | G-1 | 0.57 | 3.75 | | 3.7 | 27

 | Р | 0.50 | 0.60%
 | 0.42
 | 0.41 | 0.50 | 7.85 | 0.58 | 0.28
 | 0.04 | 0.20 | 7.14 | 10
 | 1.00 | 3.7 | 0.0 | - | | - | - | - | _ | |
| | | | | | |

 | | |
 |
 | | | | | | | | | | |
 | | | |
 | | | | | | | | | | |
| STREET FLOW | AND INL | ET CALCUL | ATIONS | | |

 | | |
 |
 | | | | | | | | | | |
 | | | |
 | | | | | | | | | | |
| STREET FLOW
100 YEAR STOP | AND INLI | ET CALCUL | ATIONS | | |

 | | | STREE
 |
 | | | | | | | | | | |
 | | | INL |
 | RADE CA | PACITY | | | | | SUM | | CAPAC | |
| STREET FLOW
100 YEAR STOI | AND INLI | ET CALCUL | ATIONS | | | Street

 | Crown | Curb | STREE
Gutter
 | T CAPAC
 | | Crown | Ponded | |
 | | | INL | ET ON G
 | RADE CA | PACITY | | | | | SUM | 1P INLET
CURB (W | CAPAC | TTY |
| STREET FLOW
100 YEAR STOP | AND INLI | ET CALCUL | Q 100 | Q pass | Q total | Street
Width F-F

 | Crown | Curb | STREE
Gutter
Slope
 | T CAPAC
 | Yo | Crown
Height | Ponded
Width (-) | Ео | S'w
 | Sx | Se | INLI | ET ON G
 | RADE CA | PACITY | Qpass | Pass | s to Inlet | | SUM | 1P INLET
CURB (w
Length | CAPAC
vith Dep | Dirty
Diression
d (ft) |
| STREET FLOW
100 YEAR STOP
Inlet
No. | AND INLI | Drainage
Area | Q 100
(cfs) | Q pass
(cfs) | Q total
(cfs) | Street
Width F-F
(ft)

 | Crown
Type | Curb
Height
(ft) | STREE
Gutter
Slope
(%)
 | T CAPAC
a
(ft)
 | Yo
(ft) | Crown
Height
(ft) | Ponded
Width (-)
(ft) | Ео | S'w
 | Sx | Se | INLI | ET ON G
 | RADE CA | PACITY | Qpass
(cfs) | Pass | s to Inlet
| | SUM
Qtotal
(cfs) | IP INLET
CURB (w
Length
(ft) | CAPAC
vith Dep
d (ft) | CITY
Corression
d (ft)
d ≤ h + |
| Inlet
No.
No.
No.
No.
No.
No.
No.
No.
No.
No. | AND INLI
M
Inlet
Type
DITION D
G-1 | Drainage
Area
RAINAGE A
0.79 | Q 100
(cfs)
REAS
8.33 | Q pass
(cfs) | Q total
(cfs)
8.3 | Street
Width F-F
(ft)
27

 | Crown
Type
P | Curb
Height
(ft)
0.50 | STREE
Gutter
Slope
(%)
1.00%
 | a
(ft)
0.42
 | Yo
(ft)
0.49 | Crown
Height
(ft)
0.50 | Ponded
Width (-)
(ft)
11.96 | Eo | S'w
 | Sx | Se | INLI
LT
14.52 | ET ON G
 | E | PACITY
Qi
7.3 | Qpass
(cfs)
1.0 | Pass | s to Inlet
#
s B1.17 | | SUM
Qtotal
(cfs) | IP INLET
CURB (w
Length
(ft)
- | CAPAC
/ith Dep
d (ft)
- | CITY
Diression
d (ft)
d ≤ h + |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1 | Drainage
Area
RAINAGE A
0.79
0.81 | Q 100
(cfs)
REAS
8.33
7.50 | Q pass
(cfs) | Q total
(cfs)
8.3
8.5 | Street
Width F-F
(ft)
27
27

 | Crown
Type
P
P | Curb
Height
(ft)
0.50
0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
 | a
(ft)
0.42
0.42
 | Yo
(ft)
0.49
0.41 | Crown
Height
(ft)
0.50
0.50 | Ponded
Width (-)
(ft)
11.96
7.65 | Eo
0.36
0.59 | S'w
0.28
0.28
 | Sx
0.04
0.04 | Se
0.14
0.20 | INL
LT
14.52
16.69 | ET ON G
L
10
10
 | E
0.88
0.81 | PACITY
Qi
7.3
6.9 | Qpass
(cfs)
1.0
1.6 | Pass | s <u>B1.17</u>
s B6.12 | | SUM
Qtotal
(cfs)
- | IP INLET
CURB (w
Length
(ft)
- | CAPAC
/ith Dep
d (ft)
- | CITY
Dression
d (ft)
d ≤ h + |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1 | Drainage
Area
RAINAGE A
0.79
0.81 | Q 100
(cfs)
REAS
8.33
7.50
5.51 | Q pass
(cfs)
1.0 | Q total
(cfs)
8.3
8.5
5.6 | Street
Width F-F
(ft)
27
27
27
27

 | Crown
Type
P
P | Curb
Height
(ft)
0.50
0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
 | a
(ft)
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.49 | Crown
Height
(ft)
0.50
0.50 | Ponded
Width (-)
(ft)
11.96
7.65
11.21 | Eo
0.36
0.59 | S'w
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04 | Se
0.14
0.20
0.14 | INL! | ET ON G
L
10
10
10
 | RADE CA
E
0.88
0.81
1.00 | PACITY
Qi
7.3
6.9
5.6 | Qpass
(cfs)
1.0
1.6
0.0 | Pass | s to Inlet
#
s B1.17
s B6.12 | | SUM
Qtotal
(cfs)
-
- | IP INLET
CURB (w
Length
(ft)
-
- | CAPAC
/ith Dep
d (ft)
-
- | 2ITY
pression
d (ft)
d ≤ h + |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1 | Drainage
Area
PRAINAGE A
0.79
0.81
0.73
0.82
0.85 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60 | Q pass
(cfs)
1.0
0.1
0.0
0.3 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9 | Street
Width F-F
(ft)
27
27
27
27
27
40

 | Crown
Type
P
P
P
P
P | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.48
0.43 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67 | Eo
0.36
0.59
0.38
0.40
0.35 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.04
0.03 | Se
0.14
0.20
0.14
0.15
0.12 | INL
LT
14.52
16.69
9.69
10.46
15.10 | ET ON G
L
10
10
10
10
10
10
10
 | E
0.88
0.81
1.00
1.00
0.86 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0 | Pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06 | | SUM
Qtotal
(cfs)
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
- | CITY
Diression
d (ft)
d ≤ h +
-
-
-
- |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.05 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.88 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.26 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4 | Street
Width F-F
(ft)
27
27
27
27
27
40
40
40

 | Crown
Type
P
P
P
P
P
P
P | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.80%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.48
0.43
0.48
0.43
0.48 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64 | Eo
0.36
0.59
0.38
0.40
0.35
0.28 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.03
0.03
0.03 | Se
0.14
0.20
0.14
0.15
0.12
0.10 | INLI
LT
14.52
16.69
9.69
10.46
15.10
15.42 | ET ON G
L
10
10
10
10
10
10
10
10
 | E
0.88
0.81
1.00
1.00
0.86
0.85 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.3
5.0 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1 | Pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
-
s B6.06
s B6.06 | | SUM
Qtotal
(cfs)
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
- |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.05
B6.06 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.88
0.48
0.48
0.53 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3 | Street
Width F-F
(ft)
27
27
27
27
27
27
40
40
40
27
27
27

 | Сгоwn
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.80%
0.68%
0.92%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.49
0.41
0.48
0.43
0.48
0.43
0.48
0.47
0.46 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.04
0.04 | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16 | INLI
LT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
10.42
11.24 | ET ON G
L
10
10
10
10
10
10
10
10
10
10
10
10
 | E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.3
5.9
6.2 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.1 | Pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
- | | SUM
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.05
B6.06
B6.07
B6.09 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.88
0.48
0.48
0.53
0.26
0.35 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6 | Street
Width F-F
(ft)
27
27
27
27
27
27
27
40
40
40
27
27
27
27
27
27
27

 | Сгоwп
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
0.68%
0.68%
0.92%
0.56%
0.51%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.49
0.48
0.43
0.48
0.43
0.48
0.43
0.48
0.47
0.46
0.45
0.43 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.48
0.42 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.04
0.04 | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18 | INLI
LT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28 | ET ON G
L
10
10
10
10
10
10
10
10
10
10
10
10
10
 | E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.3
5.9
6.2
4.6
4.0 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.1
0.0
0.1
0.0 | Pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
- | | SUN
Qtotal
(cfs)
 | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
vith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.05
B6.06
B6.06
B6.07
B6.08
B6.09A | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.88
0.48
0.53
0.26
0.35
0.09 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1 | Street
Width F-F
(ft)
27
27
27
27
27
27
40
40
40
27
27
27
27
27
27
27
27
27
27

 | Сгоwn
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
0.68%
0.68%
0.92%
0.56%
0.51%
0.47%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.49
0.44
0.43
0.43
0.43
0.43
0.43
0.45
0.43
0.43
0.43
0.43 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50
4.65 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.48
0.52
0.85 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | 5x
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.04
0.04 | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27 | INLI
INLI
LT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28
3.23 | ET ON G
L
10
10
10
10
10
10
10
10
10
10
10
10
10
 | E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.3
5.9
6.2
4.6
4.0
1.1 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.1
0.0
0.1
0.0
0.0 | Pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
- | | SUN
Qtotal
(cfs)
 | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
JLTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.03
B6.04
B6.05
B6.06
B6.05
B6.06
B6.07
B6.08
B6.09A
B6.09A
B6.09B
B6.09
B6.09
B6.09 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.88
0.48
0.53
0.26
0.35
0.09
0.12
0.21 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59 | Q pass
(cfs)
1.0
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6 | Street
Width F-F
(ft)
27
27
27
27
27
27
40
40
40
27
27
27
27
27
27
27
27
27

 | Сгоwп
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
0.68%
0.92%
0.56%
0.51%
0.51%
0.47%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50
4.65
4.66 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.48
0.52
0.85
0.85 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.04
0.04 | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27 | INLI
LT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28
3.23
4.53 | ET ON G
L
10
10
10
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.3
5.9
6.2
4.6
4.0
1.1
1.5 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.1
0.0
0.1
0.0
0.0 | Pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
- | | SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.03
B6.04
B6.05
B6.06
B6.05
B6.06
B6.07
B6.08
B6.09A
B6.09A
B6.09B
B6.09B
B6.09
B6.09
B6.10A | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.53
0.26
0.35
0.09
0.12
0.21
0.70 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3 | Street
Width F-F
(ft)
27
27
27
27
27
27
40
40
40
27
27
27
27
27
27
27
27
27
27
27
27
27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
0.64%
0.68%
0.68%
0.92%
0.56%
0.51%
0.51%
0.47%
0.91%
-
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50
4.65
4.65
4.66
-
12.23 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.48
0.52
0.85
0.85
-
0.35 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.03 | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13 | INLI
INLI
ILT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28
3.23
4.53
-
9.24 | ET ON G
L
10
10
10
10
10
10
10
10
10
10
10
10
10
 | E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.1
0.0
0.1
0.0
0.0 | Pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | | SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW
100 YEAR STOP
100 YEAR STOP
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.03
B6.04
B6.05
B6.06
B6.05
B6.06
B6.07
B6.08
B6.09A
B6.09A
B6.09B
B6.09B
B6.09
B6.10A
B6.10B
B6.10B
B6.10 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.53
0.26
0.35
0.09
0.12
0.21
0.70
0.74
1.44 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0 | Street
Width F-F
(ft)
27
27
27
27
27
27
27
27
27
27
27
27
27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
0.64%
0.68%
0.68%
0.92%
0.56%
0.51%
0.51%
0.51%
0.47%
0.91%
-
0.40%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50
4.65
4.65
4.66
-
12.23
10.03 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
-
0.35
0.43 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.04
0.04 | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16 | INLI
INLI
LT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28
3.23
4.53
-
9.24
11.76 | ET ON G
L
10
10
10
10
10
10
10
10
10
10
10
10
10
 | E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.1
0.0
0.1
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | | SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW
100 YEAR STOP
100 YEAR STOP
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.02
B6.03
B6.04
B6.05
B6.06
B6.05
B6.06
B6.07
B6.08
B6.09
B6.09
B6.09
B6.09
B6.10
B6.10
B6.10
B6.11 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.53
0.26
0.35
0.09
0.12
0.21
0.70
0.74
1.44
0.49 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-2.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7 | Street
Width F-F
(ft)
27
27
27
27
27
27
40
40
40
27
27
27
27
27
27
27
27
27
27
27
27
27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
0.64%
0.68%
0.68%
0.92%
0.56%
0.51%
0.51%
0.51%
0.51%
0.47%
0.91%
-
0.40%
0.90%
-
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50
4.65
4.65
4.66
-
12.23
10.03
-
8.44 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
-
0.35
0.43
-
0.53 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.04
0.04 | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
-
0.18 | INLI
INLI
ILT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28
3.23
4.53
-
9.24
11.76
-
10.53 | ET ON G
L
10
10
10
10
10
10
10
10
10
10
10
10
10
 | E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
1.0 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.1
0.0
0.1
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | | SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW
100 YEAR STOP
100 YEAR STOP
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.03
B6.04
B6.05
B6.06
B6.05
B6.06
B6.07
B6.08
B6.09
B6.09
B6.09
B6.09
B6.10
B6.10
B6.10
B6.11
B6.12
B6.13 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.53
0.26
0.35
0.26
0.35
0.09
0.12
0.21
0.70
0.74
1.44
0.49
0.80
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.52 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-2.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5 | Street
Width F-F
(ft)
27
27
27
27
27
27
27
27
27
27
27
27
27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.64%
0.92%
0.68%
0.92%
0.56%
0.92%
0.56%
0.51%
0.51%
0.51%
0.47%
0.91%
-
0.40%
0.90%
-
1.07%
2.70%
2.50%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.49
0.41
0.49
0.43
0.48
0.43
0.48
0.43
0.48
0.43
0.43
0.48
0.43
0.43
0.43
0.45
0.43
0.29
0.29
0.29
0.29
0.29
0.29
0.29
0.29 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50
4.65
4.65
4.66
-
12.23
10.03
-
8.44
8.10
6.02 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.52
0.85
0.85
0.35
0.35
0.43
-
0.53
0.55
0.80 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.04
0.03
0.03
0.03 | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
-
0.18
0.18
0.19
0.26 | INLI
INLI
LT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28
3.23
4.53
-
9.24
11.76
-
10.53
16.01
10.06 | ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
1.0 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.3
6.7
-
5.6
7.0
4.5 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
0.1
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | | SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.05
B6.06
B6.05
B6.06
B6.07
B6.08
B6.09
B6.09
B6.09
B6.09
B6.10A
B6.10B
B6.10
B6.11
B6.12
B6.13 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.53
0.26
0.35
0.26
0.35
0.09
0.12
0.21
0.70
0.74
1.44
0.49
0.80
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.52 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-2.5
-2.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5 | Street
Width F-F
(ft)
27
27
27
27
27
27
40
40
40
27
27
27
27
27
27
27
27
27
27
27
27
27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.64%
0.68%
0.92%
0.56%
0.51%
0.51%
0.51%
0.51%
0.51%
0.92%
0.56%
0.92%
0.56%
0.92%
0.51%
0.92%
0.51%
0.92%
0.50%
0.91%
-
1.07%
2.70%
2.50%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.41
0.49
0.43
0.48
0.43
0.48
0.43
0.48
0.43
0.48
0.43
0.43
0.43
0.43
0.45
0.43
0.29
0.29
0.29
-
0.50
0.29
0.29
-
0.50
0.43
0.43
0.42
0.43
0.42
0.35 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50
4.65
4.65
4.65
4.66
-
12.23
10.03
-
8.44
8.10
6.02 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
-
0.35
0.35
0.43
-
0.53
0.55
0.80 | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
 | Sx
0.04
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
-
0.18
0.19
0.26 | INLI
INLI
LT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28
3.23
4.53
-
9.24
11.76
-
10.53
16.01
10.06 | ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
1.0 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.3
6.7
-
5.6
7.0
4.5 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.1
0.0
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | | SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
ULTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.05
B6.06
B6.05
B6.06
B6.07
B6.08
B6.09
B6.09
B6.09
B6.09
B6.10A
B6.10B
B6.10
B6.10
B6.11
B6.12
B6.13
B7.05
B7.06 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.53
0.26
0.35
0.09
0.12
0.21
0.70
0.74
1.44
0.49
0.70
0.74
1.44
0.49
0.80
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.52
6.79
4.52 | Q pass
(cfs)
1.0
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-2.5
-2.5
-1.4
1.6 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9 | Street Width F-F (ft) 27 27 27 27 40 40 27 27 27 27 27 27 27 27 27 27 27 27 27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.56%
0.51%
0.51%
0.51%
0.51%
0.51%
0.51%
0.92%
0.56%
0.51%
0.92%
0.56%
0.92%
0.56%
0.92%
0.50%
0.51%
0.91%
2.70%
2.50%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded
Width (-)
(ft)
11.96
7.65
11.21
10.66
12.67
15.64
10.24
9.53
9.12
8.50
4.65
4.65
4.66
-
12.23
10.03
-
8.44
8.10
6.02
9.80
5.70 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
-
0.35
0.43
-
0.53
0.55
0.80
- |
S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0 | Sx
0.04
0.04
0.04
0.04
0.04
0.03
0.03
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
-
0.18
0.18
0.19
0.26
- | INLI
INLI
ILT
14.52
16.69
9.69
10.46
15.10
15.42
10.42
10.42
11.24
8.30
7.28
3.23
4.53
-
9.24
11.76
-
10.53
16.01
10.06
-
10.53
16.01
10.06 | ET ON Gi
ET ON Gi
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
1.00
0.83
1.00
0.83
1.00
0.83
1.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
0.1
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | | SUN
Qtotal
(cfs)
 | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
JLTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.03
B6.04
B6.05
B6.06
B6.07
B6.08
B6.09
B6.09
B6.09
B6.09
B6.10A
B6.10B
B6.10B
B6.10
B6.10
B6.11
B6.12
B6.13
B7.05
B7.06
B7.07 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.53
0.26
0.35
0.26
0.35
0.09
0.12
0.21
0.70
0.74
1.44
0.49
0.70
0.74
1.44
0.49
0.80
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.52 | Q pass
(cfs)
1.0
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5
-
2.5 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6 | Street Width F-F (ft) 27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
-
1.07%
2.70%
2.50%
1.90%
2.40%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
-
0.35
0.35
0.43
-
0.53
0.55
0.80
- |
S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0 | Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.03
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
-
0.18
0.19
0.26
- | INLI
INLI
ILT
I4.52
I6.69
9.69
10.46
15.10
15.42
10.42
11.24
8.30
7.28
3.23
4.53
-
9.24
11.76
-
10.53
16.01
10.06
-
16.80
9.06
9.54 | ET ON Gi
ET ON Gi
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | | SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
JLTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.03
B6.04
B6.05
B6.06
B6.07
B6.08
B6.09
B6.09
B6.09
B6.09
B6.10A
B6.09
B6.10A
B6.10B
B6.10B
B6.10
B6.11
B6.12
B6.11
B6.12
B6.13
B7.05
B7.06
B7.06
B7.07
B7.08
B7.09 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.20
0.74
1.44
0.49
0.70
0.74
1.44
0.49
0.80
0.38
0.38
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.52
9.43
3.02
4.89 | Q pass
(cfs)
1.0
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9 | Street Width F-F (ft) 27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.56%
0.51%
0.47%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.92%
0.56%
0.92%
0.56%
0.51%
0.40%
0.90%
-
1.07%
2.70%
2.50%
1.90%
2.40%
1.60%
2.90%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
0.85
0.35
0.43
-
0.53
0.55
0.80
-
0.55
0.80
- |
S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0 | Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.03
0.03
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.27
-
0.13
0.16
0.16
0.16
0.19
0.26 | INLI
INLI
ILT
ILT
ILT
IL52
IC69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.06
9.06
9.054
I6.38
I0.55 | ET ON Gi
ET ON Gi
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | | SUN
SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet
No.
JLTIMATE CON
B1.16
B1.17
B6.01
B6.02
B6.03
B6.04
B6.03
B6.04
B6.05
B6.06
B6.07
B6.08
B6.09
B6.09
B6.09
B6.09
B6.10A
B6.09
B6.10A
B6.10B
B6.10B
B6.10B
B6.10B
B6.10B
B6.11
B6.12
B6.13
B6.13
B7.05
B7.06
B7.07
B7.08
B7.09
B7.10 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.71
0.71
0.72
0.21
0.70
0.74
1.44
0.49
0.80
0.38
0.35
0.35
0.35
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.895 | Q pass
(cfs)
1.0
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-2.5
-2.5
-1.4
1.6
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2.5
-2. | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
9.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7 | Street Width F-F (ft) 27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb
Height
(ft)
0.50
0.50
0.50
0.50
0.50
0.50
0.50
0.5 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.92%
0.56%
0.51%
0.40%
0.92%
0.56%
0.51%
0.40%
0.90%
-
1.07%
2.50%
2.50%
2.35%
1.00%
 | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42
 | Yo
(ft)
0.49
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.52
0.85
0.85
0.85
0.35
0.43
-
0.35
0.43
0.55
0.85
0.43
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.85
0.43
-
0.55
0.43
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.45
0.55
0.43
0.55
0.55
0.80
-
0.55
0.80
-
0.55
0.85
0.55
0.85
0.55
0.43
0.55
0.55
0.80
-
0.55
0.85
0.55
0.80
-
0.55
0.85
0.55
0.80
-
0.55
0.85
0.85
0.55
0.80
-
0.55
0.85
0.85
0.55
0.85
0.55
0.85
0.85
0.55
0.85
0.55
0.85
0.85
0.55
0.85
0.85
0.55
0.85
0.55
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.55
0.80
0.55
0.55
0.69
0.55
0.32
0.55
0.32 |
S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0 | Sx
0.04
0.04
0.04
0.04
0.04
0.03
0.03
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.19
0.26
-
0.16
0.27
0.23
0.19
0.24
0.13 | INLI
INLI
ILT
ILT
ILT
IL52
IC.69
9.69
IO.46
I5.10
I5.42
IO.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
IC.01
I0.53
IC.01
I0.06
9.54
IC.80
9.06
9.54
IC.80
9.54
IC.80
9.55
IC.57 | ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.82
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.84
1.00
0.85
1.00
0.00
1.00
0.00
1.00
0.00
1.00
0.00
1.00
0.00
1.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | 7.12 | SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET
CURB (w
Length
(ft)
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW
100 YEAR STOP
100 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.74
1.44
0.49
0.80
0.38
0.38
0.38
0.35
0.38
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93 | Q pass
(cfs)
1.0
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-
2.5
-
-2.5
-
-
2.5
-
-
2.5
-
-
2.5
-
-
2.5
-
-
2.5
-
-
2.5
-
-
2.5
-
-
2.5
-
-
-
2.5
-
-
-
2.5
-
-
-
2.5
-
-
-
2.5
-
-
-
2.5
-
-
-
-
2.5
-
-
-
-
2.5
-
-
-
-
2.5
-
-
-
-
2.5
-
-
-
-
2.5
-
-
-
-
-
2.5
-
-
-
-
-
2.5
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7 | Street Width F-F (ft) 27

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Height (ft) 0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.92%
0.56%
0.51%
0.40%
2.50%
1.07%
2.50%
1.00%
2.35%
1.01%
0.60% | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42

 | Yo
(ft)
0.49
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.35
0.43
0.55
0.85
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.55
0.80
0.55
0.80
0.55
0.80
0.44
0.55
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.31
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0. | S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0 |
Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.13
0.16
-
0.18
0.27
0.27
-
0.27
-
0.27
-
0.13
0.16
0.16
0.16
0.19
0.26
-
0.23
0.19
0.24
0.12
0.12 | INLI
INLI
ILT
ILT
IL52
I6.69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
10.53
I6.01
I0.53
I6.01
I0.06
9.54
I6.80
9.06
9.54
I6.38
I0.55
I5.57
I2.01
I1.98 | L
10
10
10
10
10
10
10
10
10
10 | RADE CA
 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0 | Pass pass pass pass pass pass pass pass | s to Inlet
s B1.17 s B6.12 | 7.12 6.08 6.08 | SUN
SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td> | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW
100 YEAR STOP
100 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.71
1.44
0.49
0.80
0.38
0.38
0.38
0.88
0.38
0.38
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93 | Q pass
(cfs)
1.0
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-
-2.5
-
-
-2.5
-
-
-
-
-
-
-
-
-
-
-
-
- | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7 | Street Width F-F (ft) 27 </td <td>Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р</td> <td>Curb Height (ft) 0.50</td> <td>STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.92%
0.56%
0.51%
0.40%
0.90%
-
1.07%
2.70%
2.50%
1.90%
2.35%
1.90%
2.35%
1.01%
0.60%</td> <td>a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42</td> <td>Yo
(ft)
0.49
0.49
0.49
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43</td> <td>Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5</td> <td>Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44</td>
<td>Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
0.85
0.35
0.43
-
0.35
0.43
-
0.35
0.43
-
0.53
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.85
0.85
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.85
0.85
0.85
0.80
-
0.55
0.80
-
0.55
0.83
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0</td> <td>S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0</td> <td>Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.</td> <td>Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.19
0.26
-
0.16
0.26
-
0.16
0.27
0.23
0.19
0.24
0.12
0.12</td> <td>INLI
INLI
ILT
ILT
ILT
IL52
I6.69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.06
9.54
I1.76
-
I0.53
I6.01
I0.06
9.54
I1.38
I0.55
I5.57
I2.01
I1.98</td> <td>ET ON G
ET ON
G
L
10
10
10
10
10
10
10
10
10
10</td> <td>RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.82
1.00
0.84
0.96
0.96</td> <td>PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5</td> <td>Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0</td> <td>Pass pass pass pass pass pass pass pass</td> <td>s to Inlet
s B1.17 s B6.12</td> <td>7.12 6.08 6.08</td> <td>SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td></td> | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Height (ft) 0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.92%
0.56%
0.51%
0.40%
0.90%
-
1.07%
2.70%
2.50%
1.90%
2.35%
1.90%
2.35%
1.01%
0.60% | a
(ft)
0.42
0.42
0.42
0.42
0.42
0.42
0.42
0.42

 | Yo
(ft)
0.49
0.49
0.49
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
0.85
0.35
0.43
-
0.35
0.43
-
0.35
0.43
-
0.53
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.43
-
0.55
0.85
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.85
0.85
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.85
0.85
0.85
0.80
-
0.55
0.80
-
0.55
0.83
0.55
0.80
-
0.55
0.80
-
0.55
0.80
-
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0 |
S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0 | Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.19
0.26
-
0.16
0.26
-
0.16
0.27
0.23
0.19
0.24
0.12
0.12 | INLI
INLI
ILT
ILT
ILT
IL52
I6.69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.06
9.54
I1.76
-
I0.53
I6.01
I0.06
9.54
I1.38
I0.55
I5.57
I2.01
I1.98 | ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.82
1.00
0.84
0.96
0.96 | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0 | Pass pass pass pass pass pass pass pass | s to Inlet
s B1.17 s B6.12 | 7.12 6.08 6.08 | SUN
Qtotal
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td> | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW 100 YEAR STOP 100 YEAR STOP 100 YEAR STOP Inlet No. JLTIMATE CON B1.16 B1.17 B6.01 B6.02 B6.03 B6.04 B6.05 B6.06 B6.07 B6.08 B6.09B B6.09B B6.10A B6.10B B6.10 B6.11 B6.12 B6.13 B7.05 B7.06 B7.07 B7.08 B7.09 B7.10 B7.11 B7.12 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.74
1.44
0.49
0.80
0.38
0.38
0.38
0.35
0.38
0.38
0.38
0.38
0.38
0.38
0.38
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93
4.88 | Q pass
(cfs)
1.0
0.1
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-
-2.5
-
-
-2.5
-
-
-
-
-
-
-
-
-
-
-
-
- | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7
6.7
6.7 | Street Width F-F (ft) 27 <tr tr=""> 27 27</tr>

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Height (ft) 0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.50%
0.64%
1.20%
0.64%
0.68%
0.92%
0.56%
0.51%
0.47%
0.92%
0.56%
0.51%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
2.50%
1.07%
2.50%
1.07%
2.50%
2.35%
1.00%
2.35%
1.01%
0.60%
 | a (ft) 0.42 0
 | Yo
(ft)
0.49
0.49
0.41
0.49
0.43
0.43
0.43
0.43
0.43
0.43
0.43
0.43 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 - 16.41 16.35 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.85
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.27
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.27
0.27
0.27
0.27
0.27 |
S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0 | Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
0.17
0.27
0.27
-
0.13
0.16
0.27
0.27
-
0.27
0.27
-
0.13
0.16
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12 | INLI
INLI
ILT
ILT
ILT
ILT
IL52
IC69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.06
9.54
I1.76
I0.53
I6.01
I0.06
9.54
I1.76
I0.55
I5.57
I2.01
I1.98
I14.24
I3.11 | ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA
E
0.88
0.81
1.00
1.00
1.00
0.86
0.85
1.00
0.98
1.00
1.00
1.00
1.00
1.00
1.00
1.00
1.00
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.83
1.00
0.84
0.96
0.96
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.98
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.99
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90
0.90 | PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.3
6.4
6.4
7.3
6.4
6.4 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | 7.12 6.08 6.08 | SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td> | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| | | | | | |

 | | |
 |
 | | | | | | | | | | |
 | | | |
 | | | | | | | | | | |
| STREET FLOW 100 YEAR STOP 100 YEAR STOP 100 YEAR STOP No. JLTIMATE CON B1.16 B1.17 B6.01 B6.02 B6.03 B6.04 B6.05 B6.06 B6.07 B6.08 B6.09A B6.09B B6.10A B6.10A B6.10 B6.10 B6.10 B6.10 B6.10 B6.11 B6.12 B6.13 B7.05 B7.06 B7.07 B7.08 B7.09 B7.10 B7.11 B7.12 B9.01 B9.02 B9.03 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.74
1.44
0.49
0.80
0.38
0.38
0.38
0.38
0.38
0.38
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93
4.88 | Q pass
(cfs)
1.0
0.1
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-
-2.5
-
-
-2.5
-
-
-
-
-
-
-
-
-
-
-
-
- | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7
6.7
6.7 | Street Width F-F (ft) 27 27 </td <td>Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р</td> <td>Curb Height (ft) 0.50
0.50 0.50</td> <td>STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.50%
0.64%
1.20%
0.64%
0.80%
0.92%
0.56%
0.51%
0.31%
0.56%
0.51%
0.51%
0.51%
0.51%
0.51%
0.51%
0.51%
0.47%
0.91%
0.50%
2.50%
1.07%
2.50%
1.07%
2.50%
1.90%
2.35%
1.01%
0.60%
0.60%
0.60%</td> <td>a (ft) 0.42 0</td> <td>Yo (ft) 0.49 0.49 0.41 0.49 0.43 0.43 0.43 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.29 - 0.50 0.43 0.43 0.29 - 0.50 0.43 0.50 0.43 0.45 0.45 0.45 0.45 0.45</td> <td>Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5</td> <td>Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 - 16.41 16.35 13.41</td> <td>Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.85
0.43
0.55
0.43
0.55
0.80
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0</td> <td>S'w</td> <td>Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.</td> <td>Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.19
0.26
-
0.16
0.27
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12</td> <td>INLI
INLI
ILT
ILT
ILT
IL52
I6.69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
10.53
I6.01
I0.53
I6.01
I0.06
9.54
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.53
I6.01
I0.55
I5.57
I2.01
I1.98
I14.24
I3.11
I2.66</td> <td>ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10</td> <td>RADE CA</td> <td>PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
5.5
5.2
6.4</td> <td>Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0</td> <td>Pass
pass
pass
pass
pass
pass
pass
pass</td> <td>s to Inlet
#
s B1.17
s B6.12
-
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>7.12
6.08 6.08 9.04</td> <td>SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>IP INLET CURB (w Length (ft) - - - - - - - - - - - - - - - - 10 - 10 - 110 - - 10 -</td> <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td> | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Height (ft) 0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.50%
0.64%
1.20%
0.64%
0.80%
0.92%
0.56%
0.51%
0.31%
0.56%
0.51%
0.51%
0.51%
0.51%
0.51%
0.51%
0.51%
0.47%
0.91%
0.50%
2.50%
1.07%
2.50%
1.07%
2.50%
1.90%
2.35%
1.01%
0.60%
0.60%
0.60%
 | a (ft) 0.42 0
 | Yo (ft) 0.49 0.49 0.41 0.49 0.43 0.43 0.43 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.29 - 0.50 0.43 0.43 0.29 - 0.50 0.43 0.50 0.43 0.45 0.45 0.45 0.45 0.45 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 - 16.41 16.35 13.41 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.85
0.43
0.55
0.43
0.55
0.80
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0 | S'w
 | Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.19
0.26
-
0.16
0.27
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12 | INLI
INLI
ILT
ILT
ILT
IL52
I6.69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
10.53
I6.01
I0.53
I6.01
I0.06
9.54
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.53
I6.01
I0.55
I5.57
I2.01
I1.98
I14.24
I3.11
I2.66 | ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10
 | RADE CA | PACITY
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
-
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
5.5
5.2
6.4 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | 7.12 6.08 6.08 9.04 | SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET CURB (w Length (ft) - - - - - - - - - - - - - - - - 10 - 10 - 110 - - 10 - | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW 100 YEAR STOP 100 YEAR STOP 100 YEAR STOP No. JLTIMATE CON B1.16 B1.17 B6.01 B6.02 B6.03 B6.04 B6.05 B6.06 B6.07 B6.08 B6.09A B6.09B B6.10A B6.10A B6.10A B6.10A B6.10A B6.10A B6.10A B6.10 B6.10 B6.11 B6.12 B6.13 B7.05 B7.06 B7.07 B7.08 B7.09 B7.10 B7.11 B7.12 B9.01 B9.02 B9.03 B9.04 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCULA
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.71
0.70
0.74
1.44
0.49
0.80
0.38
0.38
0.88
0.35
0.80
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.22
0.35
0.22
0.35
0.22
0.35
0.22
0.35
0.22
0.35
0.22
0.35
0.35
0.35
0.35
0.38
0.38
0.38
0.38
0.38
0.38
0.38
0.38 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88 | Q pass
(cfs)
1.0
0.1
0.1
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-
-2.5
-
-
-2.5
-
-
-
-
-
-
-
-
-
-
-
-
- | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7
6.7
6.7
6.7
6.7 | Street Width F-F (ft) 27 </td <td>Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р</td> <td>Curb Curb Height (ft) 0.50
0.50 0.50</td> <td>STREE
Gutter
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.64%
0.92%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.40%
0.92%
1.07%
2.50%
1.07%
2.50%
1.00%
2.35%
1.01%
0.60%
0.60%
0.60%
0.60%</td> <td>a (ft) 0.42 <td>Yo (ft) 0.49 0.41 0.49 0.41 0.43 0.43 0.43 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.29 - 0.50 0.43 0.29 - 0.50 0.43 0.42 0.50 0.45 0.45 0.45 0.45 0.45 0.45</td><td>Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5</td><td>Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 9.80 5.70 6.76 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 16.41 16.35 13.41 9.36
9.47</td><td>Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.43
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.28
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.44
0.52
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.</td><td>S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0</td><td>Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.</td><td>Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.23
0.19
0.26
-
0.16
0.27
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.13
0.12
0.14
0.14
0.15
0.15
0.15
0.12
0.15
0.12
0.12
0.12
0.13
0.12
0.13
0.14
0.14
0.15
0.15
0.12
0.15
0.12
0.15
0.12
0.15
0.12
0.15
0.12
0.14
0.15
0.12
0.15
0.12
0.12
0.12
0.13
0.12
0.13
0.12
0.14
0.14
0.27
0.27
-

0.27
0.27
0.27
0.27
0.21
0.13
0.16
0.12
0.110
0.15
0.12
0.13
0.12
0.13
0.16
0.12
0.110
0.15
0.12
0.110
0.15
0.12
0.110
0.12
0.12
0.12
0.110
0.15
0.12
0.12
0.12
0.110
0.15
0.12
0.12
0.110
0.15
0.12
0.110
0.12
0.12
0.110
0.12
0.12
0.</td><td>INLI
INLI
ILT
ILT
ILT
IL52
I6.69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.63
I6.80
9.06
9.54
I1.76
-
I0.53
I6.01
I0.55
I5.57
I2.01
I1.98
I14.24
I3.11
I2.66
8.87
9.16</td><td>ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10</td><td>E E 0.88 0.81 1.00 1.00 1.00 0.86 0.85 1.00 1.00 1.00 0.88 0.81 0.86 0.85 1.00 1.00 1.00 1.00 1.00 0.88 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.83 1.00 0.83 1.00 0.82 1.00 0.84 0.96 0.96 0.92 0.94 1.00 1.00</td><td>PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4</td><td>Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0</td><td>Pass
pass
pass
pass
pass
pass
pass
pass</td><td>s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>7.12 6.08 6.08 9.04</td><td>SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td></td></td> | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Curb Height (ft) 0.50 | STREE
Gutter
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.64%
0.92%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.40%
0.92%
1.07%
2.50%
1.07%
2.50%
1.00%
2.35%
1.01%
0.60%
0.60%
0.60%
0.60% | a (ft) 0.42 <td>Yo (ft) 0.49 0.41 0.49 0.41 0.43 0.43 0.43 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.29 - 0.50 0.43 0.29 - 0.50 0.43 0.42 0.50 0.45 0.45 0.45 0.45 0.45 0.45</td> <td>Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5</td> <td>Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 9.80 5.70 6.76 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 16.41 16.35 13.41 9.36 9.47</td>
<td>Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.43
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.28
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.44
0.52
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.</td> <td>S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0</td> <td>Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.</td>
<td>Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.23
0.19
0.26
-
0.16
0.27
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.13
0.12
0.14
0.14
0.15
0.15
0.15
0.12
0.15
0.12
0.12
0.12
0.13
0.12
0.13
0.14
0.14
0.15
0.15
0.12
0.15
0.12
0.15
0.12
0.15
0.12
0.15
0.12
0.14
0.15
0.12
0.15
0.12
0.12
0.12
0.13
0.12
0.13
0.12
0.14
0.14
0.27
0.27
-
0.27
0.27
0.27
0.27
0.21
0.13
0.16
0.12
0.110
0.15
0.12
0.13
0.12
0.13
0.16
0.12
0.110
0.15
0.12
0.110
0.15
0.12
0.110
0.12
0.12
0.12
0.110
0.15
0.12
0.12
0.12
0.110
0.15
0.12
0.12
0.110
0.15
0.12
0.110
0.12
0.12
0.110
0.12
0.12
0.</td> <td>INLI
INLI
ILT
ILT
ILT
IL52
I6.69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.63
I6.80
9.06
9.54
I1.76
-
I0.53
I6.01
I0.55
I5.57
I2.01
I1.98
I14.24
I3.11
I2.66
8.87
9.16</td> <td>ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10</td> <td>E E 0.88 0.81 1.00 1.00 1.00 0.86 0.85 1.00 1.00 1.00 0.88 0.81 0.86 0.85 1.00 1.00 1.00 1.00 1.00 0.88 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.83 1.00 0.83 1.00 0.82 1.00 0.84 0.96 0.96 0.92 0.94 1.00 1.00</td> <td>PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4</td> <td>Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0</td> <td>Pass
pass
pass
pass
pass
pass
pass
pass</td> <td>s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>7.12 6.08 6.08 9.04</td> <td>SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td></td> | Yo (ft) 0.49 0.41 0.49 0.41 0.43 0.43 0.43 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.29 - 0.50 0.43 0.29 - 0.50 0.43 0.42 0.50 0.45 0.45 0.45 0.45 0.45 0.45 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 9.80 5.70 6.76 8.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 16.41 16.35 13.41 9.36 9.47 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.43
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.28
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.44
0.52
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0. |
S'w
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0.28
0 | Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.23
0.19
0.26
-
0.16
0.27
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.13
0.12
0.14
0.14
0.15
0.15
0.15
0.12
0.15
0.12
0.12
0.12
0.13
0.12
0.13
0.14
0.14
0.15
0.15
0.12
0.15
0.12
0.15
0.12
0.15
0.12
0.15
0.12
0.14
0.15
0.12
0.15
0.12
0.12
0.12
0.13
0.12
0.13
0.12
0.14
0.14
0.27
0.27
-
0.27
0.27
0.27
0.27
0.21
0.13
0.16
0.12
0.110
0.15
0.12
0.13
0.12
0.13
0.16
0.12
0.110
0.15
0.12
0.110
0.15
0.12
0.110
0.12
0.12
0.12
0.110
0.15
0.12
0.12
0.12
0.110
0.15
0.12
0.12
0.110
0.15
0.12
0.110
0.12
0.12
0.110
0.12
0.12
0. | INLI
INLI
ILT
ILT
ILT
IL52
I6.69
9.69
I0.46
I5.10
I5.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.63
I6.80
9.06
9.54
I1.76
-
I0.53
I6.01
I0.55
I5.57
I2.01
I1.98
I14.24
I3.11
I2.66
8.87
9.16 | ET ON G
ET ON G
L
10
10
10
10
10
10
10
10
10
10
 | E E 0.88 0.81 1.00 1.00 1.00 0.86 0.85 1.00 1.00 1.00 0.88 0.81 0.86 0.85 1.00 1.00 1.00 1.00 1.00 0.88 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.83 1.00 0.83 1.00 0.82 1.00 0.84 0.96 0.96 0.92 0.94 1.00 1.00 | PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
1.1
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
#
s B1.17
s B6.12
-
-
s B6.06
s B6.06
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
-
- | 7.12 6.08 6.08 9.04 | SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td> | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | 2ITY
pression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| Inlet No. JLTIMATE CON B1.16 B1.17 B6.01 B6.02 B6.03 B6.04 B6.05 B6.06 B6.07 B6.08 B6.09A B6.09B B6.10A B6.10B B6.10 B7.05 B7.06 B7.07 B7.08 B7.09 B7.10 B7.11 B7.12 B9.01 B9.02 B9.03 B9.04 B9.05 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCULA
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.74
1.44
0.49
0.80
0.38
0.80
0.38
0.88
0.35
0.80
0.35
0.48
0.80
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.52
0.80
0.70
0.71
0.70
0.71
0.70
0.71
0.70
0.74 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.58
2.64 | Q pass
(cfs)
1.0
0.1
0.1
0.1
0.1
0.3
0.4
0.6
2.1
1.5
0.5
-
-
-
-
-
-
-
-
-
-
-
-
- | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7
6.7
6.7
6.7
7.1
5.0
5.2 | Street Width F-F (ft) 27 </td <td>Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р</td> <td>Curb Height (ft) 0.50
0.50 0.50</td> <td>STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.40%
0.92%
1.00%
2.50%
1.07%
2.50%
1.00%
2.35%
1.01%
0.60%
0.60%
0.60%
0.60%</td> <td>a (ft) 0.42 0</td> <td>Yo (ft) 0.49 0.41 0.49 0.41 0.43 0.43 0.43 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.29 - 0.50 0.43 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35</td> <td>Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5</td> <td>Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 16.41 16.35 13.41 9.36 9.47</td> <td>Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.47
0.32
0.44
0.52
0.32
0.32
0.32
0.44
0.52
0.32
0.32
0.32
0.44
0.52
0.35
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.44
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.32
0.44
0.55
0.32
0.55
0.32
0.44
0.55
0.55
0.32
0.55
0.32
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.</td> <td>S'w</td> <td>Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.</td> <td>Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12</td> <td>INLI
INLI
INLI
INLI
INLI
INLI
INLI
INLI</td> <td>T ON G
T ON G</td> <td>E E 0.88 0.81 1.00 1.00 0.86 0.85 1.00 0.98 1.00 0.86 0.83 1.00 1.00 1.00 1.00 0.98 1.00 1.00 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.80 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.80 1.00 0.82 1.00 0.84 0.96 0.92 0.94 1.00 0.94 1.00 0.94</td> <td>PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
5.5
5.2
6.7
5.2
6.7
5.0
5.2</td> <td>Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
0.0
0.0
0.0
0.0</td> <td>Pass
pass
pass
pass
pass
pass
pass
pass</td> <td>s to Inlet
s B1.17 s B6.12</td> <td>7.12 6.08 6.08 9.04</td>
<td>SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td></td> | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Height (ft) 0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.68%
0.92%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.40%
0.92%
1.00%
2.50%
1.07%
2.50%
1.00%
2.35%
1.01%
0.60%
0.60%
0.60%
0.60% | a (ft) 0.42 0

 | Yo (ft) 0.49 0.41 0.49 0.41 0.43 0.43 0.43 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.45 0.43 0.29 - 0.50 0.43 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 16.41 16.35 13.41 9.36 9.47 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.47
0.32
0.44
0.52
0.32
0.32
0.32
0.44
0.52
0.32
0.32
0.32
0.44
0.52
0.35
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.43
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.44
0.55
0.32
0.32
0.32
0.32
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.44
0.55
0.32
0.32
0.32
0.44
0.55
0.32
0.55
0.32
0.44
0.55
0.55
0.32
0.55
0.32
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0.55
0. | S'w |
Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12 | INLI
INLI
INLI
INLI
INLI
INLI
INLI
INLI | T ON G
T ON G | E E 0.88 0.81 1.00 1.00 0.86 0.85 1.00 0.98 1.00 0.86 0.83 1.00 1.00 1.00 1.00 0.98 1.00 1.00 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.80 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.80 1.00 0.82 1.00 0.84 0.96 0.92 0.94 1.00 0.94 1.00 0.94 |
PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
5.5
5.2
6.7
5.2
6.7
5.0
5.2 | Qpass
(cfs)
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
0.0
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
s B1.17 s B6.12 | 7.12 6.08 6.08 9.04 | SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET CURB (w Length (ft) - <td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td> <td>CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td> | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW
100 YEAR STOP
100 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.71
0.70
0.80
0.38
0.80
0.35
0.80
0.35
0.48
0.80
0.35
0.48
0.80
0.35
0.48
0.80
0.35
0.48
0.80
0.52
0.80
0.70
0.71
0.70
0.71
0.70
0.71
0.70
0.71
0.70
0.84
0.59
0.22 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.58
2.64
9.86
9.76 | Q pass
(cfs)
1.0
0.1
0.1
0.1
0.1
0.3
0.4
0.6
2.1
1.5
0.5
-2.5
-1.5
0.5
-2.5
-1.0
2.8
-2.5
-1.0
2.8
-1.4
0.4
-2.5
-1.0
2.8
-1.4
0.4
-2.5
-1.0
2.8 | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7
6.7
6.7
6.7
6.7
7.1
5.0
5.2 | Street Width F-F (ft) 27 <tr tr=""> 27 27</tr>

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Height (ft) 0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.64%
0.92%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.92%
0.56%
0.51%
0.40%
0.50%
2.50%
2.50%
2.50%
1.00%
2.50%
1.00%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60% | a (ft) 0.42 0

 | Yo (ft) 0.49 0.41 0.49 0.41 0.49 0.41 0.43 0.43 0.43 0.43 0.45 0.46 0.43 0.42 0.50 0.43 0.42 0.50 0.43 0.42 0.50 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.46 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 13.44 8.10 6.02 - 12.23 10.03 - 13.44 8.10 6.02 - 14.65 13.33 13.50 13.44 - 16.41 16.35 13.41 9.36 9.47 - 18.89 13.50 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.43
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.85
0.43
0.55
0.80
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.32
0.31
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.33
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.33
0.32
0.32
0.33
0.32
0.32
0.33
0.32
0.33
0.32
0.33
0.32
0.33
0.32
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0.33
0. | S'w |
Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.23
0.19
0.26
-
0.16
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12 | INLI
INLI
INLI
INLI
INLI
INLI
INLI
INT
INT
INT
INT
INT
INT
INT
INT
INT
IN | Image: Construct of the second sec | E E 0.88 0.81 1.00 1.00 0.86 0.85 1.00 0.98 1.00 0.88 0.83 1.00 1.00 1.00 0.88 1.00 1.00 1.00 1.00 0.88 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.83 1.00 0.80 1.00 0.80 1.00 0.80 1.00 0.82 1.00 0.82 1.00 0.84 0.96 0.92 0.94 1.00 0.65 0.96
 | PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.3
6.4
6.4
9.5 | Qpass
(cfs)
1.0
1.0
1.6
0.0
0.0
1.0
1.1
0.0
0.0
0.0
0.0
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
s B1.17 s B6.12 | 7. 12 6.08 6.08 9.04 | SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET CURB (w Length (ft) - - - - - - - - - - - - - - - 10 - 10 - 110 - 12 - | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| | | | | | |

 | | |
 |
 | | | | | | | | | | |
 | | | |
 | | | | | | | | | | |
| STREET FLOW
100 YEAR STOP
100 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.74
1.44
0.49
0.80
0.70
0.74
1.44
0.49
0.80
0.38
0.38
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.52
0.35
0.48
0.52
0.48
0.52
0.48
0.52
0.48
0.52
0.48
0.52
0.48
0.52
0.48
0.52
0.48
0.52
0.52
0.48
0.52
0.52
0.52
0.52
0.52
0.52
0.48
0.52
0.52
0.52
0.52
0.52
0.52
0.52
0.52 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.58
2.64
9.86
9.76
2.93 | Q pass
(cfs)
1.0
0.1
0.1
0.1
0.1
0.3
0.4
0.6
2.1
1.5
0.5
-
-
-
-
-
-
-
-
-
-
-
-
- | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7
6.7
6.7
6.7
6.7
6.7
6.7
6.7
6 | Street Width F-F (ft) 27 27 27 <t< td=""><td>Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р</td><td>Curb Curb Curb Curb</td><td>STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.64%
0.68%
0.92%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.92%
1.20%
2.50%
2.50%
2.50%
1.07%
2.50%
1.07%
2.50%
1.00%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%</td><td>a (ft) 0.42 0</td><td>Yo (ft) 0.49 0.41 0.49 0.41 0.43 0.43 0.43 0.43 0.43 0.43 0.45 0.46 0.43 0.42 0.50 0.43 0.29 - 0.50 0.43 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.36 0.50 0.50 0.50 0.45 0.45 0.45 0.45 0.45 0.46 0.45 0.46</td><td>Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5</td><td>Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 13.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 - 16.41 16.35 13.41 9.36 9.47 - 18.89 13.50 13.48</td><td>Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.80
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.31
0.32
0.32
0.31
0.32
0.47
0.32
0.32
0.31
0.32
0.31
0.32
0.31
0.32
0.31
0.32</td><td>S'w 0.28
<</td><td>Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.</td><td>Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
0.17
0.27
-
0.23
0.19
0.26
-
0.16
0.27
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12</td><td>INLI
INLI
INLI
INLI
INLI
INLI
INLI
INT
INT
INT
INT
INT
INT
INT
INT
INT
IN</td><td>T ON G
T ON G</td><td>E E 0.88 0.81 1.00 1.00 0.86 0.85 1.00 0.98 1.00 1.00 0.88 0.81 0.86 0.85 1.00 0.98 1.00 1.00 1.00 0.88 0.80 1.00 0.83 1.00 0.83 1.00 0.83 1.00 0.83 1.00 0.80 1.00 0.81 0.82 1.00 0.84 0.96 0.96 0.96 0.92 0.94 1.00 0.65 0.96 0.96 0.96 0.96 0.96 0.96 0.96</td><td>PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.0
4.5
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.5
7.3
6.7
7.3
6.7
7.3
6.7
7.5
7.3
6.7
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7</td><td>Qpass
(cfs)
1.0
1.0
1.0
0.0
0.0
0.0
1.0
1.1
0.0
0.0</td><td>Pass
pass
pass
pass
pass
pass
pass
pass</td><td>s to Inlet
s B1.17 s B6.12</td><td>7. 12
6.08
6.08
9.04</td><td>SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>IP INLET CURB (w Length (ft) - - - - - - - - - - - - - - - 10 - 10 - 110 - 12 -</td><td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td></t<> | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Curb Curb | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.64%
1.20%
0.64%
1.20%
0.64%
0.68%
0.92%
0.68%
0.92%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.91%
0.56%
0.51%
0.47%
0.92%
1.20%
2.50%
2.50%
2.50%
1.07%
2.50%
1.07%
2.50%
1.00%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
0.60%
 | a (ft) 0.42 0
 | Yo (ft) 0.49 0.41 0.49 0.41 0.43 0.43 0.43 0.43 0.43 0.43 0.45 0.46 0.43 0.42 0.50 0.43 0.29 - 0.50 0.43 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.35 0.42 0.36 0.50 0.50 0.50 0.45 0.45 0.45 0.45 0.45 0.46 0.45 0.46 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 13.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 - 16.41 16.35 13.41 9.36 9.47 - 18.89 13.50 13.48 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.80
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.31
0.32
0.32
0.31
0.32
0.47
0.32
0.32
0.31
0.32
0.31
0.32
0.31
0.32
0.31
0.32 | S'w 0.28
 0.28 0.28 < | Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
-
0.18
0.27
0.27
-
0.13
0.16
0.17
0.27
-
0.23
0.19
0.26
-
0.16
0.27
0.23
0.19
0.26
-
0.12
0.12
0.12
0.12
0.12
0.12
0.12
0.12 | INLI
INLI
INLI
INLI
INLI
INLI
INLI
INT
INT
INT
INT
INT
INT
INT
INT
INT
IN | T ON G
T ON G | E E 0.88 0.81 1.00 1.00 0.86 0.85 1.00 0.98 1.00 1.00 0.88 0.81 0.86 0.85 1.00 0.98 1.00 1.00 1.00 0.88 0.80 1.00 0.83 1.00 0.83 1.00 0.83 1.00 0.83 1.00 0.80
1.00 0.81 0.82 1.00 0.84 0.96 0.96 0.96 0.92 0.94 1.00 0.65 0.96 0.96 0.96 0.96 0.96 0.96 0.96 | PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.0
4.5
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.5
7.3
6.7
7.3
6.7
7.3
6.7
7.5
7.3
6.7
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7 | Qpass
(cfs)
1.0
1.0
1.0
0.0
0.0
0.0
1.0
1.1
0.0
0.0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
s B1.17 s B6.12 | 7. 12
6.08
6.08
9.04 | SUN
(cfs)
-
-
-
-
-
-
-
-
-
-
-
-
- | IP INLET CURB (w Length (ft) - - - - - - - - - - - - - - - 10 - 10 - 110 - 12 - | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| STREET FLOW
100 YEAR STOP
100 | AND INLI
M
Inlet
Type
DITION D
G-1
G-1
G-1
G-1
G-1
G-1
G-1
G-1 | ET CALCUL
Drainage
Area
RAINAGE A
0.79
0.81
0.73
0.82
0.85
0.85
0.88
0.48
0.48
0.53
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.26
0.35
0.21
0.70
0.71
0.70
0.74
1.44
0.49
0.80
0.38
0.38
0.86
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.35
0.48
0.52
0.52
0.52
0.52
0.57 | ATIONS
Q 100
(cfs)
REAS
8.33
7.50
5.51
6.02
6.60
7.02
5.36
4.20
3.16
3.43
1.08
1.51
2.59
7.84
6.68
12.99
4.22
6.79
4.22
6.79
4.22
6.79
4.52
9.43
3.02
4.60
5.39
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.88
8.95
7.76
3.93
4.58
2.64
9.86
9.76
2.93 | Q pass
(cfs)
1.0
0.1
0.1
0.1
0.0
0.3
0.4
0.6
2.1
1.5
0.5
-
-
-
2.5
-
-
-
-
-
2.5
-
-
-
-
-
-
-
-
-
-
-
-
- | Q total
(cfs)
8.3
8.5
5.6
6.0
6.9
7.4
6.0
6.3
4.6
4.0
1.1
1.5
2.6
5.3
6.7
12.0
5.7
8.4
4.5
5.3
6.7
12.0
5.7
8.4
4.5
9.4
3.9
4.6
8.5
4.9
8.7
6.7
6.7
6.7
6.7
6.7
6.7
6.7
6.7
6.7
6 | Street Width F-F (ft) 27 <tr tr=""> 48 27</tr>

 | Сгоwм
Туре
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р
Р | Curb Height (ft) 0.50 | STREE
Gutter
Slope
(%)
1.00%
3.40%
0.50%
0.50%
0.64%
1.20%
0.64%
0.68%
0.92%
0.68%
0.92%
0.56%
0.51%
0.56%
0.51%
0.51%
0.56%
0.51%
0.51%
0.50%
2.50%
2.70%
2.70%
2.50%
1.07%
2.50%
1.07%
2.50%
0.40%
0.90%
0.40%
0.90%
0.40%
0.90%
0.50%
0.40%
0.90%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.50%
0.5 | a (ft) 0.42 0

 | Yo (ft) 0.49 0.49 0.41 0.49 0.43 0.43 0.43 0.43 0.43 0.43 0.45 0.46 0.43 0.42 0.50 0.43 0.43 0.29 - 0.50 0.43 0.45 0.45 0.45 0.45 0.42 0.35 - 0.45 0.42 0.35 0.42 0.350 0.50 0.50 0.50 0.45 0.45 0.45 0.45 0.45 0.46 0.47 0.48 0.40 | Crown Height (ft) 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5 | Ponded Width (-) (ft) 11.96 7.65 11.21 10.66 12.67 15.64 10.24 9.53 9.12 8.50 4.65 4.65 4.66 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 12.23 10.03 - 13.44 8.10 6.02 9.80 5.70 6.76 8.01 6.34 13.33 13.50 13.44 - 16.41 16.35 13.41 9.36 9.47 - 18.89 13.50 13.48 - 11.73 | Eo
0.36
0.59
0.38
0.40
0.35
0.28
0.42
0.42
0.46
0.42
0.46
0.42
0.46
0.42
0.45
0.52
0.85
0.85
0.85
0.85
0.85
0.85
0.43
0.55
0.85
0.43
0.55
0.80
0.43
0.55
0.80
0.43
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.80
0.55
0.32
0.31
0.32
0.32
0.31
0.32
0.31
0.32
0.32
0.31
0.32
0.31
0.32
0.31
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.33
0.34
0.32
0.32
0.32
0.32
0.33
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.32
0.33
0.32
0.33
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0.34
0. | S'w 0.28 < |
Sx
0.04
0.04
0.04
0.04
0.04
0.04
0.03
0.03
0.03
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0.04
0. | Se
0.14
0.20
0.14
0.15
0.12
0.10
0.15
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
0.17
0.18
0.27
0.27
-
0.13
0.16
0.27
0.27
-
0.27
0.27
-
0.13
0.16
0.27
0.27
0.27
0.27
0.27
0.27
0.27
0.27 | INLI
INLI
INLI
ILT
ILT
ILT
IL52
IC69
9.69
I0.46
I5.10
I5.42
I0.42
I0.42
I1.24
8.30
7.28
3.23
4.53
-
9.24
I1.76
-
I0.53
I6.01
I0.53
I6.01
I0.53
I6.01
I0.53
I6.01
I0.53
I6.01
I0.53
I6.01
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.53
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.53
I5.57
I2.01
I1.98
I0.53
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.55
I5.57
I2.01
I1.98
I0.53
I5.57
I2.01
I1.98
I0.53
I5.57
I2.01
I1.98
I0.53
I5.57
I2.01
I1.98
I0.53
I5.57
I2.01
I1.98
I0.53
I5.57
I2.01
I1.98
I0.53
I5.57
I1.01
I1.98
I0.53
I1.78
I0.53
I1.78
I0.53
I1.78
I0.55
I1.78
I0.53
I1.78
I0.53
I1.78
I0.53
I1.78
I0.53
I1.78
I0.53
I1.78
I0.53
I1.78
I0.54
I1.78
I0.54
I1.78
I0.54
I1.78
I0.54
I1.78
I0.54
I1.78
I0.54
I1.78
I0.54
I1.78
I0.54
I1.78
I0.54
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I1.78
I | T ON G
T ON G | E E 0.88 0.81 1.00 1.00 0.86 0.85 1.00 0.98 1.00 1.00 0.88 0.81 0.86 0.85 1.00 1.00 1.00 1.00 1.00 0.88 0.80 1.00 0.80 1.00 0.83 1.00 0.80 1.00 0.83 1.00 0.80 1.00 0.81 0.82 1.00 0.82 1.00 0.84 0.96 0.92 0.94 0.95 0.95 0.96 0.996 0.996 0.996 0.996 0.996 0.996 <t< td=""><td>PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.0
4.5
7.0
4.5
7.0
4.5
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.5
7.0
6.2
4.6
7.0
4.5
7.0
7.5
6.2
7.0
6.2
7.0
7.0
4.5
7.0
7.0
4.5
7.0
7.3
6.4
7.0
7.3
6.4
7.0
7.3
6.4
7.0
7.3
6.4
7.0
7.3
6.4
7.0
7.3
6.4
7.0
4.5
7.0
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5</td><td>Qpass
(cfs)
1.0
1.0
1.0
1.0
0.0
0.0
0.0
1.0
0.0
0</td><td>Pass
pass
pass
pass
pass
pass
pass
pass</td><td>s to Inlet
s B1.17 s B6.12</td><td></td><td>SUN
(cfs) (
- (
- (
- (
- (
- (
- (
- (
-</td><td>IP INLET CURB (w Length (ft) -</td><td>CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
-</td><td>CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
-</td></t<> |
PACITY
Qi
Qi
7.3
6.9
5.6
6.0
5.9
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.2
4.6
4.0
1.1
1.5
-
5.3
6.7
5.6
7.0
4.5
7.6
3.9
4.6
7.0
4.5
7.0
4.5
7.0
4.5
7.0
4.5
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
6.4
7.3
6.4
7.3
6.4
7.3
6.4
7.3
6.5
7.0
6.2
4.6
7.0
4.5
7.0
7.5
6.2
7.0
6.2
7.0
7.0
4.5
7.0
7.0
4.5
7.0
7.3
6.4
7.0
7.3
6.4
7.0
7.3
6.4
7.0
7.3
6.4
7.0
7.3
6.4
7.0
7.3
6.4
7.0
4.5
7.0
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5
7.5 | Qpass
(cfs)
1.0
1.0
1.0
1.0
0.0
0.0
0.0
1.0
0.0
0 | Pass
pass
pass
pass
pass
pass
pass
pass | s to Inlet
s B1.17 s B6.12 | | SUN
(cfs) (
- (
- (
- (
- (
- (
- (
- (
- | IP INLET CURB (w Length (ft) - | CAPAC
/ith Dep
d (ft)
-
-
-
-
-
-
-
-
-
-
-
-
- | CITY
Dression
d (ft)
d ≤ h +
-
-
-
-
-
-
-
-
-
-
-
-
- |
| | | | | | |

 | | |
 |
 | | | | | | | | | | |
 | | | |
 | | | | | | | | | | |



Event						
Hydraulic	Hydraulic					
Grade Line (In) (ft)	Grade Line (Out) (ft)					
820.76	820.73					
821.38	821.25					
821.75	821.2					
822.35	822.27					
823.01	822.65					
825.33	823.01					
825.83	825.14					
826.02	825.94					

LVCIIC				
Hydraulic	Hydraulic			
Grade Line (In) (ft)	Grade Line (Out) (ft)			
823.39	822.97			
823.89	823.59			
824.04	823.89			
824.41	824.29			
824.85	824.67			
825.46	824.95			
825.96	825.25			
826.15	826.09			

RING	CHORD	LENGTH
Έ	347.13 '	359.40'



NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH
- CALCULATION UNLESS SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON
- THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR
- TO UTILITY INSTALLATION.
- 6. EXPOSED CONCRETE THAT IS VISIBLE IS REQUIRED TO BE MADE OF STONE OR CLAD IN STONE INCLUDING BUT NOT LIMITED TO LEDGESTONE, FIELDSTONE, CAST STONE, OR OTHER DECORATIVE MATERIALS SUCH AS STAMPED AND TINTED CONCRETE THAT RESEMBLES STONE OR BRICK. THE CONCRETE TRICKLE CHANNEL IS NOT SUBJECT TO THIS REQUIREMENT.

LEGEND

W WATER LINE WW WASTEWATER LINE & MH SD STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DUBLE WATER SERVICE DOUBLE WATER SERVICE DUBLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WATER LINE EXISTING STORM DRAIN LINE EXISTING STORM DRAIN LINE PROPOSED CONTOUR LINE PROPOSED CONTOUR LINE	
$\frac{\#01}{\substack{Q_{25}:Q25\\Q_{100}:Q100}}$ INLET # / CAPTURE Q= 25/100 YEAR PROFILE SCALES: 1" = 40' HORIZONTAL	
1" = 4' VERTICAL PROFILE LEGEND:	
	(
SUBGRADE PROPOSED STORM DRAIN 25-YR HGL 25-YR HGL 25yr HGL 100-YR HGL 100yr HGL	
CITY OF LEANDER APPROVAL	

anin . \mathbf{X} DUSTIN J. GOSS 91805 · CENSE? ENG 1111112 04/11/2025 an loss SS ΖČ PAPE-DAV ENGINEE 5 TRACT, PHASE 2 MODIFIED CITY OF LEANDER, TEXAS E 6 STORM DRAIN SD-B6.01 PHASE ≻ 2 JOB No. -----NO. 50816-26 APRIL 2025 RBB IGNER ECKED_TCK_DRAWNDY/S SHEET <u>64 of 83</u>



			25 yr Sto	rm Event		
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic	ATE
R6.02	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)	
6.03-A	13.11	10.49	1.09	823.71	822.78	
86.03-B	6.48	3.67	2.13	824.52	824.49	
86.03-C	6.5	3.68	2.04	824.64	824.59	
B6.04 B6.05	6.71	3.79	2.13	824.59	824.49	
B6.06	4.48	5.19	0.73	821.36	821.20	z
B6.07	2.55	4.3	1.26	820.02	820.01	SIO
B6.08	3.89	4.75	1.2	819.83	819.82	
B6.09	2.1	6.56	2.01	819.59	819.59	
			100 yr Sto	orm Event		0 Z
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic	
00.00	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)	
B6.02	8.19	9.85	2.65	825.03	824.95	
6.03-B	8.6	4.87	4.24	826.65	826.59	
86.03-C	8.62	4.88	4.23	826.86	826.77	*
B6.04	8.89	5.03	4.24	826.77	826.59	P
B6.05	5.94	3.36	2.74	824.35	824.29	
B6.07	3.39	1.92	3.17	821.96	821.93	• 4
B6.08	5.16	2.92	3.02	821.68	821.65	5
B6.09	2.78	0.89	3.54	821.12	821.12	
			NOTE	<u>:S:</u>		
			2. ALL R 3. THE H EVENT CALCU 4. EXISTII THIS F INTERV FIELD 5. ALL FI TO UT 6. EXPOS BE MA BUT N STONE STONE STONE NOT S	CP IS CLASS III UNLESS YDRAULIC GRADE LINE (H IS DEFINED BY THE NOF LATION UNLESS SHOWN (NG CONTOUR INFORMATIO PLAN SHEET ARE SHOWN /ALS THEY ARE COMPUT SURVEY DATA. LL AREAS SHALL BE COM ILITY INSTALLATION. ED CONCRETE THAT IS V DE OF STONE OR CLAD OT LIMITED TO LEDGESTO , OR OTHER DECORATIVE PED AND TINTED CONCRET OR BRICK. THE CONCRET UBJECT TO THIS REQUIRE CEND	OTHERWISE NOTED. AGL) OF THE 25 YEAR AMAL DEPTH OTHERWISE. N SHOWN HERE ON A AT ONE (1) FOOT TER GENERATED USING MPACTED TO 95% PRIOR ISIBLE IS REQUIRED TO IN STONE INCLUDING IN STONE INCLUDING I	I PAPE-DAWS
				WW WASTEWA SD STORM D CURB INL SINGLE W DOUBLE W DOUBLE W DOUBLE W GATE VAL FIRE HYD EXISTING EXISTING EXISTING EXISTING FIRE HYD EXISTING EXISTING EXISTING FIRE HYD EXISTING EXISTING EXISTING COPOSE #01 0 100:0100 DFILE SCALES: 40' HORIZONTAL 4' VERTICAL DFILE LEGEND: AL GROUND ED GRADE CONTAL	TER LINE & MH RAIN LINE & MH ET ATER SERVICE WATER SERVICE WW SERVICE LVE RANT GATE VALVE FIRE HYDRANT WATER LINE WASTEWATER LINE STORM DRAIN LINE CONTOUR LINE D CONTOUR LINE D CONTOUR LINE (CAPTURE 00 YEAR	ACT. PHASE 2 MODIFIED CZP



SHEET <u>65 of 83</u>

CITY OF LEANDER APPROVAL







			25 yr Sto	rm Event	
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
Label	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
B1.16	6.71	24.54	1.58	835.09	830.24
B1.17	5.66	18.58	0.98	826.05	824.22
B6.10	12.17	6.89	1.32	819.58	819.33
B6.11	4.14	13.16	1.23	819.51	818.67
B6.12	6.04	17.6	1.36	820.16	818.41
B6.13	3.68	12.54	1.25	820.16	818.1
			100 yr Sto	rm Event	
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
Label	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
B1.16	8.91	26.64	1.86	835.24	830.52
B1.17	7.5	20.16	1.45	826.19	824.68
B6.10	16.15	9.14	2.44	820.73	820.45
B6.11	5.49	14.28	2.31	819.63	819.75
B6.12	8.01	19.08	2.18	820.31	819.23
B6.13	4.88	13.61	1.93	820.27	818.79

NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND PRESERVE ANY AND ALL UNDERGROUND UTILITIES.
- 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH
- CALCULATION UNLESS SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON
- THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING FIELD SURVEY DATA.
- 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.
- 6. EXPOSED CONCRETE THAT IS VISIBLE IS REQUIRED TO BE MADE OF STONE OR CLAD IN STONE INCLUDING BUT NOT LIMITED TO LEDGESTONE, FIELDSTONE, CAST STONE, OR OTHER DECORATIVE MATERIALS SUCH AS STAMPED AND TINTED CONCRETE THAT RESEMBLES STONE OR BRICK. THE CONCRETE TRICKLE CHANNEL IS NOT SUBJECT TO THIS REQUIREMENT.

I FGFND

W	WATER LINE
— o — WW —	WASTEWATER LINE & MH
O SD	STORM DRAIN LINE & MH
	CURB INLET
0	SINGLE WATER SERVICE
 \	DOUBLE WATER SERVICE
	SINGLE WW SERVICE
R 1	DOUBLE WW SERVICE GATE VALVE
$\tilde{\otimes}$	FIRE HYDRANT
	EXISTING GATE VALVE
$-\infty + j$	EXISTING FIRE HYDRANT
	EXISTING WATER LINE
	EXISTING WASTEWATER LINE
	EXISTING STORM DRAIN LINE
- — — 786— — —	EXISTING CONTOUR LINE
	THE CONTOUR LINE
# 01	INLET # / CAPTURE
Q ₂₅ : Q25	Q= 25/100 YEAR
<mark>և ₁₀₀։ Q100</mark>	
NUTILE SUP	
= 40' HORIZO	NTAL
= 4' VERTICA	
YROFILE LEC	iEND:
AIURAL GROUND	
MOULD ORADE	
JBGRADE	
VUPUSED STORM DI	
	6
	V
ס– זא HGL 2	5yr HGL
0-YR HGL	
100yr HGL	100yr HGL

SATE OF TAIL. \mathbf{X} DUSTIN J. GOSS PROFE 91805 CENSE SIONAL ENGLISH an loss -LAS .8711 D A L .454. 0 PAPE-DAWS 500 — ო BG - 3 zz CZP PHASE 6 STORM DRAIN LATERALS B6.10-B6.13 & B1.16-B1.17 TRACT, PHASE 2 MODIFIED CITY OF LEANDER, TEXAS SD-B6.01 LIVELY CITY JOB No. _____ 50816-26 JOB NO. DATE APRIL 2025 DESIGNER RBB CHECKED TCK DRAWN DY/S CITY OF LEANDER APPROVAI SHEET 66 of 83

Hydraulic	Hydraulic
de Line (In) (ft)	Grade Line (Out) (ft)
835.09	830.24
826.05	824.22
819.58	819.33
819.51	818.67
820.16	818.41
820.16	818.1





Label B7.05 B7.06 B7.07 B7.08 B7.09 B7.10 B7.11

Label ____ B7.05 B7.06 B7.07 B7.08 B7.10

			25 yr Stor	rm Event	
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
Label	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
B7.05	7.17	9.72	2.01	829.54	829.45
B7.06	3.01	1.7	2.21	829.87	829.86
B7.07	4.08	11.11	1.06	825.35	824.82
B7.08	4.53	8.16	1.16	823.7	823.41
B7.09	3.92	7.49	0.59	821.68	821.31
B7.10	6.77	6.46	0.88	821.72	821.32
B7.11	4.62	6.89	1.11	820.9	820.99
B7.12	3.37	5.41	1.05	820.77	820.86
			100 yr Sto	rm Event	
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
Label	(efe)	16+10)	(Out) (6+)	Grade Line (In) (ft)	Grada Line (Out) (ft)

	(CIS)	(itys)	(Out) (it)	Grade Line (in) (it)	Grade Line (Out) (it)
B7.05	9.51	5.38	2.73	830.37	830.17
B7.06	3.99	2.26	3.22	830.89	830.87
B7.07	5.41	12.04	1.62	825.47	825.38
B7.08	6	3.4	2.37	824.69	824.61
B7.09	5.2	2.94	3.01	823.76	823.74
B7.10	8.98	5.08	3.18	823.8	823.62
B7.11	6.13	3.47	3.45	823.37	823.33
B7.12	4.47	2.53	3.35	823.21	823.17

NOTES:

- 1. THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY AND HAVE NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WORK, AND AGREES TO BE FULLY RESPONSIBLE FOR ANY AND ALL DAMAGES WHICH MIGHT BE ASSOCIATED BY THE CONTRACTOR'S FAILURE TO EXACTLY LOCATE AND
- PRESERVE ANY AND ALL UNDERGROUND UTILITIES. 2. ALL RCP IS CLASS III UNLESS OTHERWISE NOTED. 3. THE HYDRAULIC GRADE LINE (HGL) OF THE 25 YEAR EVENT IS DEFINED BY THE NORMAL DEPTH
- CALCULATION UNLESS SHOWN OTHERWISE. 4. EXISTING CONTOUR INFORMATION SHOWN HERE ON THIS PLAN SHEET ARE SHOWN AT ONE (1) FOOT INTERVALS THEY ARE COMPUTER GENERATED USING
- FIELD SURVEY DATA. 5. ALL FILL AREAS SHALL BE COMPACTED TO 95% PRIOR TO UTILITY INSTALLATION.
- 6. EXPOSED CONCRETE THAT IS VISIBLE IS REQUIRED TO BE MADE OF STONE OR CLAD IN STONE INCLUDING BUT NOT LIMITED TO LEDGESTONE, FIELDSTONE, CAST STONE, OR OTHER DECORATIVE MATERIALS SUCH AS STAMPED AND TINTED CONCRETE THAT RESEMBLES STONE OR BRICK. THE CONCRETE TRICKLE CHANNEL IS NOT SUBJECT TO THIS REQUIREMENT.

LEGEND

	W
-0	— ww —
-0	SD
0	
\	
\rightarrow	
	×
	$-\infty + + -$
	— — w 1,2
	— — WW —
	— — SD — —
	·786— — —
	786

WATER LINE WASTEWATER LINE & MH STORM DRAIN LINE & MH CURB INLET SINGLE WATER SERVICE DOUBLE WATER SERVICE SINGLE WW SERVICE DOUBLE WW SERVICE GATE VALVE FIRE HYDRANT EXISTING GATE VALVE EXISTING FIRE HYDRANT EXISTING WATER LINE EXISTING WASTEWATER LINE EXISTING STORM DRAIN LINE EXISTING CONTOUR LINE PROPOSED CONTOUR LINE



PROFILE SCALES: 1" = 40' HORIZONTAL 1" = 4' VERTICAL PROFILE LEGEND: NATURAL GROUND FINISHED GRADE SUBGRADE PROPOSED STORM DRAIN 25-YR HGL 100-YR HGL 100yr HGL	LIVELY TRACT, PHASE 2 MOI CITY OF LEANDER, TEX/	PHASE 6 STORM DRAIN SD-B7.01 LATERALS B7.05-I
	CITY JOB No JOB NO DATE AP	 50816-26 RII 2025
	DESIGNER CHECKED TCK	RBB DRAWN DY/SL
CITY OF LEANDER APPROVAL	SHEET 67	of 83







			25 yr Stor	rm Event	
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
Label	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
B10-A	15.6	6.84	2.16	827.93	827.93
B10-B	13.59	9.97	1.45	828.43	828.07
B10-C	9.71	9.11	1.79	828.89	828.89
B10-D	9.74	9.12	1.71	829.02	828.89
B10-E	9.81	9.13	1.35	830.45	829.25
B10-F	9.82	9.14	0.89	830.68	830.22
B10-G	9.83	10.19	1.28	831.02	830.84
B10.03	4.13	7.6	1.29	828.82	828.89
B10.04	2.21	5.08	0.95	828.03	828.07
			100 yr Sto	rm Event	
	-1		100 yr Sto	rm Event	
Label	Flow	Velocity	Depth	Hydraulic	Hydraulic
	(cfs)	(ft/s)	(Out) (ft)	Grade Line (In) (ft)	Grade Line (Out) (ft)
B10-A	20.7	4.22	2.77	828.67	828.54
B10-B	18.03	10.71	2.19	828.89	828.82
B10-C	12.89	4.1	2.17	829.28	829.27
B10-D	12.93	9.84	2.11	829.19	829.28
B10-E	13.01	9.85	1.58	830.63	829.48
B10-F	13.02	9.86	1.05	830.85	830.38
B10-G	13.03	11	1.5	831.2	831.05
B10.03	5.48	8.21	1.67	829.29	829.27
B10.04	2.93	5.51	1.69	828.83	828.82



	Elevation (ft) =	and and a state of the state o		Area (ft ²)	Lively Tract, Pha	se 2-Pond H-Batch ncremental Volume (fi	³) Cumulative N
	Length (ft) =	160.00	ਾ ਸ 810.5 ਿ ਸ 810.5	P.P. 705.36	0.016193		
			812	27,125.12	0.165008	1,973 17,156	1,9/ 19,1
	Drawdown Time		813 814 r	43,391.36 55,695.29	0.996129	35,258 ∞ 7 7 7 749,543 □	54,3 103,9
	Water Quality Volume (ft ³) =	161,181	2" 815 "" 816 "#r	58,803.52 ⁻ 61,958.81	1.349943	57,249 12 °C	<u>161,1</u> S 1 S 221.5
	Outlet Pipe Diameter (iii) =		2 = 0 817 5	65,150.47	1.495649	63,555 <u>5</u> 35,207	285,1
	Average Head (ft) =	2.63	2 1 2		[]2 		
	Coefficient = Q _{outlet} (cfs) =	0.60					
	nimum Required Drawdown Time (hr) =	48.00 h					12' WIDE N
						- J - J - K - K - K - K - K - K - K - K - K - K	
					8	7 ²⁰ 8 ²⁷	
	H V CL C CL H IV S		PA-	3:1			
		4			ine f	л 536 W	
							Stand "
				815			м <u>5</u> ра
				S P 4 S P			°a ⊄ °°° °°
				2 2 ² 2 2		5	
							ist - Po 22
						a) și	ے 1
				8° _ 2		ы Д. 	4 Å
			ລ ຢູ່ ຢູ່ ຢູ່ ເ ຈ			24 2	
			ನೆ ^{ಸ್ಟ್ರ}		5		
							- · · · · · · · · · · · · · · · · · · ·
			5000000000000000000000000000000000000				
			r : : : : : : : : : : : : : : : : : : :	N P R		render v See render v	
	з ² но V 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		<u> </u>				an vra sa vra t
							N N N
	-−⊾⊾⊔ ⊭* ≓	277 S. S. C. C.			9 7 2 2 . r	u r ^e u u	
		7				D	z fer
	Z G N G N G N						
					5. ⁵⁶ L #		
				2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			신 장전 ⁶ 또 전 긴
					יית לי ^א ר יית יית און איין איין איין איין איין איין איין		
				- 4:1 ⁸¹⁵		2 % ⁻ - 3 %	ر. بې لې
					COCCE		Vertite Contraction
					אין אין אין אין אין אין אין אין אין אין אין אין אין	S C S	р <mark>с</mark> 10 522 — 43
						고 ~ 시 - 작	
							<u>~ 1</u> ~ si
							==-] ~ M(1 ~ FL
					2 21 21 21 21 21 21 21 21 21 21 21 21 21 2		
						р с 2 _ ь х	
				5. E 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	з сё 2 в Я,	°°'' F T	
		2 Z Z X		б Г П П П П П П П			
				۲ کی دو ۱			the d
		н 2 Б 2 жал у т	2 "B & G & B & D & D & D				1-162
				신 0년 - 1 년 신왕 네 7 18			
					N S S S S S S S S S S S S S S S S S S S		2 F % 37
	1. 9. 2 8. ⁸ 1. ž.		5 % Fai 		5 6 	0. 46	ै । स्य
ע אין	ning and a second s I I I I I I I I I I I I I I I I I I I		D D (in C		49 - 2001 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2007 - 2 Fj ^o	i Cristini de Metrice Cristini P
· · · · · · · · · · · · · · · · · · ·				- 1 ST			5

2 *3*, 1a

Sa

د<u>د</u> D

& 0	U.	es 0	5	יי ק	- C	. 3	69	2 52	s; 0	Æ
<i>C</i> ² 1	0 0	9 <u>0</u>	B &	P	0	n	0	ğ D	D.	80
0_	r			9 - 2 9 - 1		о ല л	ß	ر م	5 D C	
2 °°	6 ° 1	142			90	8	2	0 0	5 - 5	9
0 	ß	4,	0	°%	0	0	9	2	00 مڑنے	
	9 <i>B</i> a	0 60	Er B	2	2		179	0	2	
, C	Bo		and the second s	B	ey	U.	ں چار	,n	- 2-	
6	\$°	5	r ²) ୩ ୪	न्त्	4 ⁰		5 6	
ь Э з	5	5 6 7	0	0	0 57	= ⁰ P	-	7	2 73	007
n na se		The second se	18 ⁷ 2	2.5000-2.0000-0.0000-0.000 2. 1			1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 21		j Z – S – S	0.
POND=81	7.50	P		100 Construction of the	12	2	। ि दी ि ग	podoo		
		14. s. s. s. s. 17	le Pr	ू ्र ्र		13. <u></u>		t o ti		81
read is sold that			-100 YR	WSE=815.	91		nananta an ka atka	i photocology	l pressentering	0
annen son St	1.L					Carlos		6		81
R WSE=8	15.69			and Connerge a	NT 3.		anigran a norte da		ennessen na	
ista (istaise Mi SA)		And the second second	-wa ws	E=815.00	L. C	1	B	l d	2	81
						N	- FINISH	ED GROUN	0	
er en		ः ३२ प	2	5 6	1000 2001	5.1	<u></u>			
								25 7 5 p		81
i ereitzen izza.		-					EVIC	TING CROI	IND	F.
					n An an	ligen = property periodicities ====================================		7.7		81
******				wanasaasaasa				l		
2					ina ".	<u>5</u>	12		<u>я</u>	80
hereare	j tomo pol med	Lo 2	7 33-2-384/2007	l L L L L L L L L L L L L L L L L L L L		generation and		t	hand	PIE S
2					6 2			8. 2		0
	Too S		2		\$	1 3				0
na de case l'Oly	parse en eneren f		second and and a second and as second and a	1920 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2000 - 2010 - 20		and a second sec		ана — 1200 Х 51 Д		Por
			- and the second		7			la construction de la construction la construction de la construction la construction de la construction la construction de la construction d		80
м- сельс) 3 ф		15 7		La Cânt			Lanna Garanan 1	annersenner Museumenner		ъ Я
				10 1000)d ' }					80

3+00 _ 2+00 0 POND_H_SECTION_A-A

FINISHED GROUND e aneren serer d EXISTING GROUND

POND H SECTION B-B 4+00 5+00 VE Gey

2 5 5 2

2		
5 Second	Table 3-6 Clay Liner Sp	ecific
L and the second	Property	
0	Permeability	
2.0	Plasticity Index of Clay	AST
	Liquid Limit of Clay	
80 F	Clay Particles Passing	la manage
", U	Clay Compaction	
3°į	Lange Ter Strange Cor NS	horne Com

50816-21 MARCH 2019 5 % G 8 8 19 10 K ට 2) ලස RBB ESIGNER HECKED DRAWN TK SHEET 74 of 83 **CITY OF LEANDER APPROVAL**

2 0 2

-⁻e 0 P 13

ß

5 80

ate: Feb 22, 2024, 8:28am User ID: slopez e: H:\Projects\508\16\24\301 Construction Documents\Civil\DT50816-