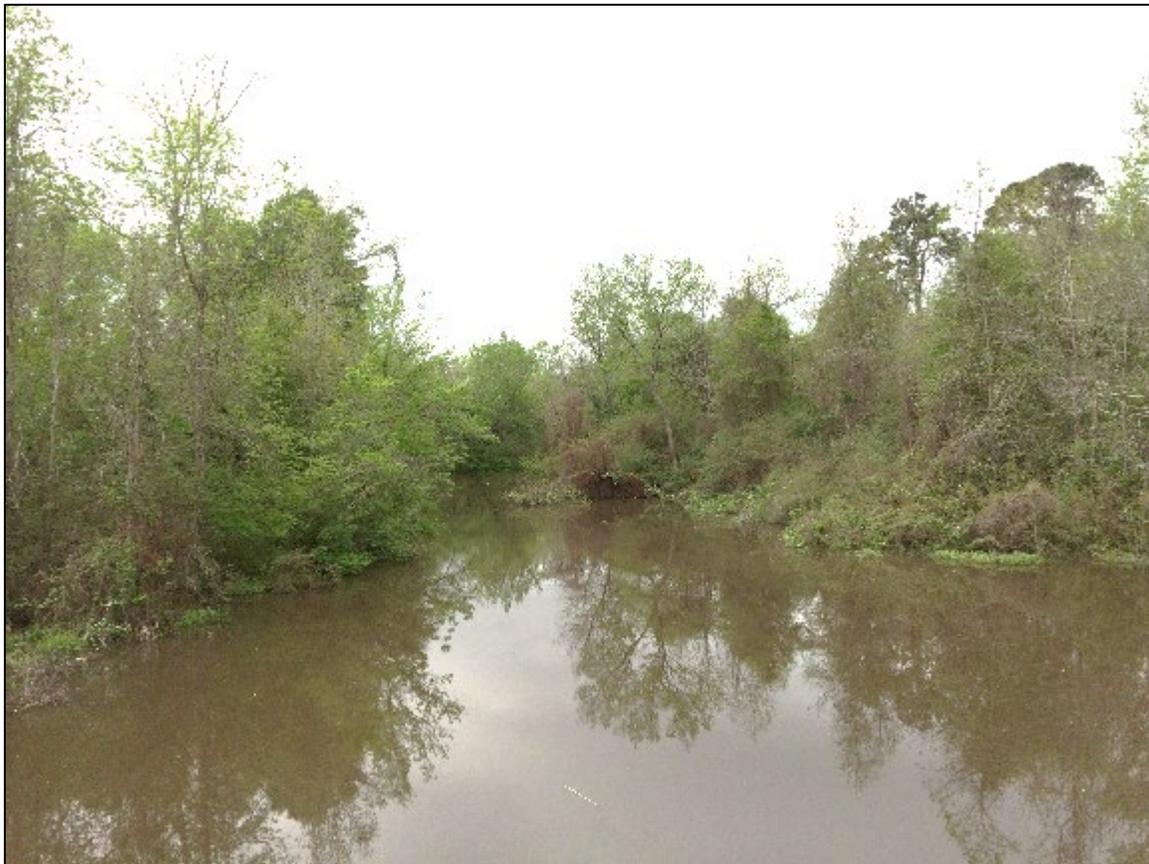


Technical Support Document for Total Maximum Daily Loads for Dissolved Oxygen and pH in Adams Bayou, Cow Bayou, and Associated Tributaries

Segments 0508, 0508C, 0511, 0511A, 0511B, 0511C

Assessment Units 0508_01, 0508_02, 0508_03,
0508_04, 0508C_01, 0511_02, 0511_03, 0511_04,
0511A_02, 0511B_01, 0511C_01



Adams Bayou at FM 3247

Technical Support Document for Total Maximum Daily Loads for Dissolved Oxygen and pH in Adams Bayou, Cow Bayou, and Associated Tributaries

Segments 0508, 0508C, 0511, 0511A, 0511B, 0511C

Assessment Unit 0508_01, 0508_02, 0508_03, 0508_04, 0508C_01, 0511_02, 0511_03, 0511_04, 0511A_02, 0511B_01, 0511C_01

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This report represents a major revision of a previous report. That report was co-authored by Dr. Kirk Dean and Ms. Monica Suarez of Parsons Corporation and provided to TCEQ as a draft final on October 29, 2015. The report is titled: *Technical Support Document for the Cow and Adams Bayou Total Maximum Daily Loads*. Much of the material in the present report is taken directly from the earlier report, and the basic construct of the present report is almost entirely based on the earlier report. The modeling system, which is a major theme of both reports, was developed by Parsons Corporation.

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Table of Contents

Acknowledgements	iii
Table of Contents	iv
List of Figures.....	vii
List of Tables.....	xiii
Abbreviations.....	xvi
1. Background and Introduction.....	1
1.1 Regulatory Background.....	1
1.2 Water Body Descriptions and Assessments	2
1.3 Past TMDLs.....	5
1.4 Document Summary	6
2. Summary of Modeling System Developed for Linkage Analysis	7
3. HSPF Hydrologic and Water Quality Model	9
3.1 HSPF Model Description	9
3.2 Inputs, Data Sources and Assumptions	14
3.2.1 Climate and Meteorology.....	14
3.2.2 Land Use and Land Cover	15
3.2.3 Geology, Topography, and Soils	18
3.2.4 Nonpoint Sources of Pollutants.....	18
3.2.4.1 Agricultural Sources	20
3.2.4.2 On-site Sewerage Facilities	22
3.2.4.3 Wildlife	27
3.2.4.4 Atmospheric Deposition.....	28
3.2.4.5 Forest Leaf Litter	29
3.2.4.6 Residential Area Nonpoint Sources	29
3.2.5 Permitted PS Discharge Facilities	30
3.2.6 Municipal Separate Stormwater Systems	30
3.3 HSPF Model Verification	34
4. RMA2 Hydrodynamic Model	39

4.1	RMA2 Model Description.....	39
4.2	RMA2 Inputs and Data Sources	40
4.3	RMA2 Calibration and Validation	51
5.	WASP Water Quality Model	59
5.1	WASP Model Description.....	59
5.2	WASP Input Data.....	80
5.2.1	Lower Boundary Condition.....	80
5.2.2	Carbonaceous Biochemical Oxygen Demand.....	81
5.2.3	WASP Linkage to the RMA2 Hydrodynamic Model.....	82
5.2.4	WASP Linkage to the HSPF Model and Point-Source Loads.....	82
5.3	Calibration and Validation of the WASP Models.....	84
6.	Existing Conditions and Water Quality Targets.....	95
6.1	Methodology for Calculating Pollutant Loads at AU Level	96
6.2	Water Quality Targets.....	98
6.3	Full Permitted Pollutant Loads	101
6.4	Assessment of Compliance with Water Quality Standards under Existing Conditions and Full Permitted Conditions.....	107
7.	DO and pH TMDL Allocations	110
7.1	DO Modeling Scenarios.....	110
7.1.1	No Load Scenario.....	110
7.1.2	Pristine Condition Scenario	110
7.1.3	TMDL Scenarios	113
7.2	Margin of Safety for DO TMDLs.....	117
7.3	Pollutant Load Allocation for DO	117
7.3.1	Wasteload Allocation for DO.....	118
7.3.1.1	WWTFs.....	118
7.3.1.2	Regulated Stormwater	119
7.3.2	Load Allocation	119
7.3.3	Allowance for Future Growth for DO TMDLS.....	119
7.3.4	TMDL Calculations for DO	120
7.3.5	Summary of TMDL Calculations for DO.....	124

7.4	Pollutant Load Allocations for pH	124
7.5	Consideration of Seasonal Variation for DO and pH	127
8.	References	129
Appendix A	Adams Bayou HSPF User Control Interface File	133
Appendix B	Cow Bayou HSPF User Control Interface File	168
Appendix C	Adams Bayou RMA2 Geometry and Boundary Condition Files	225
Appendix D	Cow Bayou RMA2 Geometry and Boundary Condition Files	239
Appendix E	Goodness-of-fit for the Adams Bayou RMA2 Hydrodynamic Model	254
Appendix F	Goodness-of-fit for the Cow Bayou RMA2 Hydrodynamic Model	268
Appendix G	Goodness-of-fit for the Adams Bayou WASP Model	287
Appendix H	Goodness-of-fit for the Cow Bayou WASP Model	296

List of Figures

Figure 1-1	Location of Adams and Cow Bayous in southeast Texas showing impaired AU for depressed dissolved oxygen (DO) and pH.....	3
Figure 2-1	Schematic of modeling system.....	8
Figure 3-1	Adams Bayou sub-basins in HSPF.....	11
Figure 3-2	Cow Bayou sub-basins in HSPF.....	12
Figure 3-3	2006 land use/land cover in the Adams and Cow Bayou watersheds.....	17
Figure 3-4	Septic tank density within the Adams Bayou and Cow Bayou watersheds based on 1990 federal census data.....	24
Figure 3-5	Soil suitability for septic fields in the Adams Bayou and Cow Bayou watersheds (USDA, 2016).....	26
Figure 3-6	Observed and simulated flow duration curves for Cow Bayou.....	35
Figure 3-7	Observed and simulated annual average flows for Cow Bayou.....	36
Figure 3-8	Observed and simulated average monthly flows for Cow Bayou.....	36
Figure 3-9	Observed and simulated total monthly flows for Cow Bayou.....	37
Figure 4-1	RMA2 element (channel) geometry.....	39
Figure 4-2a	Adams Bayou RMA2 model segmentation.....	41
Figure 4-2b	Adams Bayou RMA2 model segmentation.....	42
Figure 4-2c	Adams Bayou RMA2 model segmentation.....	43
Figure 4-3a	Cow Bayou RMA2 model segmentation.....	44
Figure 4-3b	Cow Bayou RMA2 model segmentation.....	45
Figure 4-3c	Cow Bayou RMA2 model segmentation.....	46
Figure 4-3d	Cow Bayou RMA2 model segmentation.....	47
Figure 4-3e	Cow Bayou RMA2 model segmentation.....	48

Figure 5-1a Adams Bayou WASP model segments.....60

Figure 5-1b Adams Bayou WASP model segments.....61

Figure 5-1c Adams Bayou WASP model segments.....62

Figure 5-2a Cow Bayou WASP model segments.....63

Figure 5-2b Cow Bayou WASP model segments.....64

Figure 5-2c Cow Bayou WASP model segments.....65

Figure 5-2d Cow Bayou WASP model segments.....66

Figure 5-2e Cow Bayou WASP model segments.....67

Figure 5.3 Carbonaceous BOD after 5, 15, and 20 days.....81

Figure 5.4 Measured rates of cBOD decay in laboratory incubations82

Figure 5-5 Longitudinal model fit of Adams Bayou daily average DO for the calibration period86

Figure 5-6 Longitudinal model fit of Adams Bayou daily average DO for the validation period86

Figure 5-7 Longitudinal model fit of Cow Bayou daily average DO for the calibration period 91

Figure 7-1 Average measured pH and cBOD₅ in Cow Bayou with distance upstream during the summer 2004 summer intensive surveys used for RMA2 and WASP validation..128

Figure E-1 Flow calibration at station AB2254

Figure E-2 Water level validation at station AB2.....254

Figure E-3 Flow validation at station AB2.....255

Figure E-4 Water level calibration at station AB3255

Figure E-5 Flow calibration at station AB3256

Figure E-6 Water level validation at station AB3.....256

Figure E-7 Flow validation at station AB3.....257

Figure E-8 Water level calibration at station AB4257

Figure E-9 Flow calibration at station AB4258

Figure E-10 Water level validation at station AB4.....258

Figure E-11 Flow validation at station AB4.....259

Figure E-12 Flow calibration at station AB5259

Figure E-13 Flow validation at station AB5.....260

Figure E-14 Flow calibration at station AB6260

Figure E-15 Water level validation at station AB6.....261

Figure E-16 Flow validation at station AB6.....261

Figure E-17 Flow calibration at station AB7262

Figure E-18 Flow validation at station AB7.....262

Figure E-19 Water level calibration at station AB8263

Figure E-20 Flow calibration at station AB8263

Figure E-21 Water level validation at station AB8.....264

Figure E-22 Flow validation at station AB8.....264

Figure E-23 Water level calibration at station GG (Gum Gully).....265

Figure E-24 Flow calibration at station GG (Gum Gully).....265

Figure E-25 Flow validation at station GG (Gum Gully).....266

Figure E-26 Flow calibration at station HG (Hudson Gully)266

Figure E-27 Flow validation at station HG (Hudson Gully)267

Figure F-1 Flow calibration at Station CB0.5268

Figure F-2 Water level validation at Station CB0.5.....269

Figure F-3 Flow validation at Station CB0.5.....269

Figure F-4 Water level calibration at Station CB1270

Figure F-5 Flow calibration at station CB1.....270

Figure F-6 Water level Validation at station CB1271

Figure F-7 Flow validation at station CB1271

Figure F-8 Water level calibration at station CB2.....272

Figure F-9 Flow calibration at station CB2.....272

Figure F-10 Water level validation at station CB2273

Figure F-11 Flow validation at station CB2273

Figure F-12 Flow calibration at station CB2.5.....274

Figure F-13 Flow validation at station CB2.5.....274

Figure F-14 Water level calibration at station CB3.....275

Figure F-15 Flow calibration at station CB3.....275

Figure F-16 Water level validation at station CB3276

Figure F-17 Flow validation at station CB3276

Figure F-18 Water level calibration at station CB3.5.....277

Figure F-19 Flow calibration at station CB3.5.....277

Figure F-20 Flow validation at station CB3.5.....278

Figure F-21 Water level calibration at station CB4.....278

Figure F-22 Flow calibration at station CB4.....279

Figure F-23 Water level validation at station CB4279

Figure F-24 Flow validation at station CB4280

Figure F-25 Water level calibration at station CB5.....280

Figure F-26 Flow calibration at station CB5.....281

Figure F-27 Water level validation at station CB5281

Figure F-28 Flow validation at station CB5282

Figure F-29 Water level calibration at station CNB (Coon Bayou)282

Figure F-30 Flow calibration at station CNB (Coon Bayou)283

Figure F-31 Water level validation at station CNB (Coon Bayou)283

Figure F-32 Flow validation at station CNB (Coon Bayou).....284

Figure F-33 Flow calibration at station TG2 (Terry Gully)285

Figure F-34 Water level validation at station TG2 (Terry Gully).....285

Figure F-35 Flow validation at station TG (Terry Gully).....286

Figure G-1. Calibration of salinity in the Adams Bayou WASP model.....287

Figure G-2. Validation of salinity in the Adams Bayou WASP model.....287

Figure G-3 Long-term validation of salinity calibration at Adams Bayou station AB2.....288

Figure G-4 Calibration of TSS in the Adams Bayou WASP model288

Figure G-5 Validation of TSS in the Adams Bayou WASP model.....289

Figure G-6 Calibration of ultimate cBOD in the Adams Bayou WASP model289

Figure G-7 Validation of ultimate cBOD in the Adams Bayou WASP model.....290

Figure G-8 Calibration of OrgN in the Adams Bayou WASP model.....290

Figure G-9 Validation of OrgN in the Adams Bayou WASP model.....291

Figure G-10 Calibration of NH₃N in the Adams Bayou WASP model291

Figure G-11 Validation of NH₃N in the Adams Bayou WASP model292

Figure G-12 Calibration of NO₃N in the Adams Bayou WASP model.....292

Figure G-13 Validation of NO₃N in the Adams Bayou WASP model293

Figure G-14 Calibration of PO₄P in the Adams Bayou WASP model.....293

Figure G-15 Validation of PO₄P in the Adams Bayou WASP model294

Figure G-16 Calibration of Chlorophyll-a in the Adams Bayou WASP model294

Figure G-17 Validation of Chlorophyll-a in the Adams Bayou WASP model.....295

Figure H-1 Calibration of salinity in the Cow Bayou WASP model.....296

Figure H-2	Validation of salinity in the Cow Bayou WASP model.....	296
Figure H-3	Long-term validation of salinity calibration at Cow Bayou station CB1.....	297
Figure H-4	Calibration of salinity in the Cow Bayou WASP model.....	297
Figure H-5	Validation of TSS in the Cow Bayou WASP model.....	298
Figure H-6	Calibration of ultimate cBOD in the Cow Bayou WASP model	298
Figure H-7	Validation of ultimate cBOD in the Cow Bayou WASP model.....	299
Figure H-8	Calibration of OrgN in the Cow Bayou WASP model.....	299
Figure H-9	Validation of OrgN in the Cow Bayou WASP model.....	300
Figure H-10	Calibration of NH ₃ N in the Cow Bayou WASP model	300
Figure H-11	Validation of NH ₃ N in the Cow Bayou WASP model	301
Figure H-12	Calibration of NO ₃ N in the Cow Bayou WASP model.....	301
Figure H-13	Validation of NO ₃ N in the Cow Bayou WASP model	302
Figure H-14	Calibration of PO ₄ P in the Cow Bayou WASP model.....	302
Figure H-15	Validation of PO ₄ P in the Cow Bayou WASP model	303
Figure H-16	Calibration of Chlorophyll-a in the Cow Bayou WASP model	303
Figure H-17	Validation of Chlorophyll-a in the Cow Bayou WASP model.....	304

List of Tables

Table 3-1	HSPF model summary.....	10
Table 3-2	Meteorological inputs to the HSPF models.....	15
Table 3-3	Land use/land cover in the Adams and Cow Bayou watersheds	16
Table 3-4	Selected properties of major soil map units of Adams and Cow Bayou watersheds	19
Table 3-5	Count of farms/production operations by county and type: 2007 agricultural census	20
Table 3-6	Crops planted by county, in acres: 2007 agricultural census.....	21
Table 3-7	Domestic livestock populations by county: 2007 agricultural census	21
Table 3-8	Pollutant production rates of livestock in manure	22
Table 3-9	Assumed pollutant concentrations in malfunctioning septic tank effluent.....	27
Table 3-10	Assumed wildlife population densities for various land use categories.....	27
Table 3-11	Pollutant production rates of wildlife	28
Table 3-12	Total average atmospheric loadings of pollutants.....	28
Table 3-13	Pollutant production rates of dogs and cats	29
Table 3-14	Areas of Adams Bayou watersheds within MS4s, in acres.....	32
Table 3-15	Areas of Cow Bayou watersheds within MS4s, in acres.....	33
Table 3-16	Goodness-of-fit for HSPF Cow Bayou model hydrologic calibration.....	37
Table 3-17	Calibration and validation of HSPF model for water quality (Cow and Adams Bayous considered jointly).....	38
Table 4-1	RMA2 model summary.....	40
Table 4-2	Flow/elevation linkages for the Adams Bayou RMA2 model.....	49
Table 4-3	Flow/elevation linkages for the Cow Bayou RMA2 model.....	50

Table 4-4	Water level error statistics for the RMA2 hydrodynamic model of Adam Bayou	53
Table 4-5	Water level error statistics for the RMA2 hydrodynamic model of Cow Bayou...	53
Table 4-6	Flow error statistics for the RMA2 hydrodynamic model of Adams Bayou.....	55
Table 4-7	Flow error statistics for the RMA2 hydrodynamic model of Cow Bayou.....	56
Table 4-8	Parameters of the Adams Bayou RMA2 model.....	57
Table 4-9	Parameters of the Cow Bayou RMA2 model.....	58
Table 5-1	WASP model summary	59
Table 5-2	Physical properties of Adams Bayou WASP model segments.....	68
Table 5-3	Physical properties of Cow Bayou WASP model segments.....	72
Table 5-4	WASP state variables.....	77
Table 5-5	External inputs for the Adams Bayou WASP model.....	83
Table 5-6	External inputs to the Cow Bayou WASP model	84
Table 5-7	Model fit statistics for daily average DO in Adams Bayou	87
Table 5-8	Calibration statistics for the Adams Bayou WASP model	87
Table 5-9	Validation statistics for the Adams Bayou WASP model.....	88
Table 5-10	Key parameters of the Adams Bayou WASP model	88
Table 5-11	Model fit statistics for daily average DO (mg/L) in Cow Bayou.....	92
Table 5-12	Calibration statistics for the Cow Bayou WASP model	92
Table 5-13	Validation statistics for the Cow Bayou WASP model.....	93
Table 5-14	Key parameters of the Cow Bayou WASP model	93
Table 6-1	Comparison of the 2006 and 2016 NLCD land use and land cover in the Adams Bayou and Cow Bayou watersheds	96
Table 6-2	Percentages used to separate HSPF sub-basin-level pollutant loads into AUs.....	97
Table 6-3	DO criteria and modeling system connections for DO assessment	100

Table 6-4	Existing full-permitted TPDES daily average PS loads to Adams and Cow Bayous	103
Table 6-5	Summary of daily average NH ₃ N and cBOD loads under full permitted conditons to the Adams Bayou system	105
Table 6-6	Summary of daily average NH ₃ N and cBOD loads under full permitted conditon to the Cow Bayou system	106
Table 6-7	Simulated compliance with criteria under existing conditions and full permit conditions for the Adams Bayou system.....	108
Table 6-8	Simulated compliance with criteria under existing conditions and full permit conditions for the Cow Bayou system.....	109
Table 7-1	Results of No Load Scenario	111
Table 7-2	Results of Pristine Condition Scenario	112
Table 7-3	Load Reduction Progression.....	113
Table 7-4	Results of TMDL Scenarios for conditions with and without future growth for DO impaired AUs of Adams Bayou and Cow Bayou watersheds	116
Table 7-5	Wasteload allocations for regulated domestic WWTFs in the Adams Bayou and Cow Bayou watersheds	121
Table 7-6	Wasteload allocations for regulated industrial WWTFs in the Adams Bayou and Cow Bayou watersheds	122
Table 7-7	Regulated and unregulated stormwater calculations for impaired AUs of Adams Bayou, Cow Bayou and associated tributaries	123
Table 7-8	TMDL allocation summary for AUs of Adams Bayou, Cow Bayou and associated tributaries	125
Table 7-9	Final TMDL allocations for impaired AUs of Adams Bayou, Cow Bayou and associated tributaries	126

Abbreviations

°C	degrees Celsius
°F	degrees Fahrenheit
ADP	Acoustic Doppler Profiler
ANOSIM	Analysis of Similarity
ASAE	American Society of Agricultural Engineers
AU	assessment unit
BOD	biochemical oxygen demand (general term)
BOD ₅	five-day biochemical oxygen demand
cBOD	carbonaceous biochemical oxygen demand (general term)
cBOD ₅	five-day carbonaceous biochemical oxygen demand
cfs	cubic feet per second
chla	chlorophyll-a
cm ³	cubic centimeters
cms	cubic meters per second
CWA	Clean Water Act
DO	dissolved oxygen
EPA	United States Environmental Protection Agency
FG	future growth
ft	feet
g	gram
hr	hour
HSPF	Hydraulic Simulation Program – Fortran
IH	interstate highway
ILS	impervious land surface
in	inch
K _a	reaeration coefficient
kg	kilogram
K _L	oxygen transfer coefficient
L	liter
lb	pound
m	meter
MAE	mean absolute error
ME	mean error
mg	milligrams
MGD	million gallons per day
mph	miles per hour
MS4	municipal separate storm sewer system

NCDC	National Climatic Data Center
NHD	National Hydraulic Dataset
NH ₃ N	ammonia nitrogen
NLCD	National Land Cover Dataset
NOAA	National Oceanic and Atmospheric Administration
NO ₃ N	nitrate nitrogen
NPDES	National Pollutant Discharge Elimination System
NPS	non-point source
NRCS	Natural Resource Conservation Service
NSE	Nash-Sutcliffe model efficiency
OrgC	organic carbon
OrgN	organic nitrogen
OrgP	organic phosphorus
OSSF	on-site sewerage facility
PLS	pervious land surface
PO ₄ P	orthophosphate phosphorus
POTW	publicly owned treatment works
PS	point source
ppt	parts per thousand
QAPP	quality assurance project plan
r ²	coefficient of determination
RMSE	root mean square error
s	second (of time)
SH	state highway
SOD	sediment oxygen demand
SWQMIS	Surface Water Quality Monitoring Information System
TAC	Texas Administrative Code
TCEQ	Texas Commission on Environmental Quality
TIAER	Texas Institute for Applied Environmental Research
TMDL	Total Maximum Daily Load
TOC	total organic carbon
TP	total phosphorus
TPDES	Texas Pollutant Discharge Elimination System
TSS	total suspended solids
UBOD	ultimate carbonaceous biochemical oxygen demand
USDA	United States Department of Agriculture
USGS	United States Geological Survey
WASP	Water Quality Analysis Simulation Program
WWTF	wastewater treatment facility

Technical Support Document for Total Maximum Daily Loads for Dissolved Oxygen and pH in Adams Bayou, Cow Bayou, and Associated Tributaries

1. Background and Introduction

1.1 Regulatory Background

Water quality standards serve the dual purposes of establishing the water quality goals for a specific water body and providing the regulatory basis for the establishment of water-quality-based treatment controls and strategies (40 CFR 131.10). Water quality standards are established to support designated uses and are comprised of water quality criteria. The federal Clean Water Act (CWA) requires that states designate, for each water body, desirable and appropriate uses to be achieved and protected. These designated beneficial uses of water bodies include recreation in and on the water, public water supply, navigation, agricultural and industrial water supply, and protection and propagation of fish, shellfish and wildlife. States must then set water quality criteria to support the standards necessary to protect those designated uses. Criteria are expressed as constituent concentrations, levels, or narrative statements representing a quality of water that supports a particular use. When criteria are met, water quality will generally protect the designated use (40 CFR 131.3).

Water bodies, such as rivers, lakes, and estuaries, are divided by the State of Texas into Segments. Classified Segments are those defined in Appendix A of Texas Surface Water Quality Standards (30 Texas Administrative Code [TAC] §307.1-307.7), which also defines their designated uses and water quality criteria. They are assigned an identification number. For example, the classified segment named “Cow Bayou Tidal” has the identification number “0511”. Water bodies not defined in Appendix A of Texas Surface Water Quality Standards are called “unclassified” water bodies. Their reference number refers to the downstream classified segment that they flow into, with an additional letter designation. For example, Cow Bayou Above Tidal is assigned the identification number “0511A”.

The federal CWA requires all States to assess water quality and identify water bodies with impaired designated uses that do not meet, or are not expected to meet, applicable water quality standards. The list of impaired water bodies is known as the CWA §303(d) List. Texas assesses compliance with water quality standards using a geographic unit called an Assessment Unit (AU), which is defined as the smallest geographic area of use support reported in the assessment. Often there are several AUs within a large Segment. The naming convention for AUs includes the Segment number with an appended AU sequence number. For example,

classified segment 0511 is divided into four AUs, 0511_01 to 0511_04, numbered sequentially from downstream to upstream. Water quality within an AU may be assessed using data from a single representative monitoring station, or combined from several stations.

States must develop a total maximum daily load (TMDL) for each pollutant that contributes to the impairment of a designated use of a listed water body. A TMDL is an allocation of allowable point and nonpoint source pollutant loadings that will enable the water body to meet water quality standards when implemented. The Texas Commission on Environmental Quality (TCEQ) is responsible for ensuring that TMDLs are developed for impaired surface waters in Texas.

1.2 Water Body Descriptions and Assessments

Adams Bayou and Cow Bayou are sluggish streams that flow into the Sabine River (U.S. Geological Survey [USGS] Hydrologic Unit Code 12010005) just upstream of Sabine Lake in Orange County, Texas. Adams Bayou extends from its confluence with the Sabine River in a northerly direction across Orange County to near the Newton County Line (Figure 1-1). Adams Bayou previously extended to a greater extent into southern Newton County, but flow from this upper section has been redirected eastward to the Sabine River for flood control purposes. Cow Bayou extends from its confluence with the Sabine River in a northerly direction, roughly parallel to, but west of Adams Bayou, across Orange County to southern Jasper County southeast of Evadale.

The lower portions of both bayous have been channelized, straightened, and dredged for navigation, creating numerous oxbows in the former, more sinuous, channels. Both bayous are under tidal influence below and a short distance above Interstate Highway (IH)-10. The tidal portions of Adams and Cow Bayous extend approximately 8 and 20 miles, respectively, above their confluences with the Sabine River. In Texas Surface Water Quality Standards (30 TAC §§307.1 – 307.10), the term “tidal” is defined as “descriptive of coastal waters that are subject to the ebb and flow of tides. For purposes of standards applicability, tidal waters are considered to be saltwater.”

A USGS gauging station measures flow in Cow Bayou Above Tidal at the State Highway (SH) 12 bridge near Mauriceville. The period of record of this gauge is from 1952 to 1986, and again from October of 2002 to the present time. For the recent 16-year period of January 2003 through December 2018, the daily average, maximum, and minimum flow at this site were 131.7 cubic feet per second (cfs), 21,700 cfs, and 0 cfs, respectively. The above tidal reaches are considered intermittent with pools.

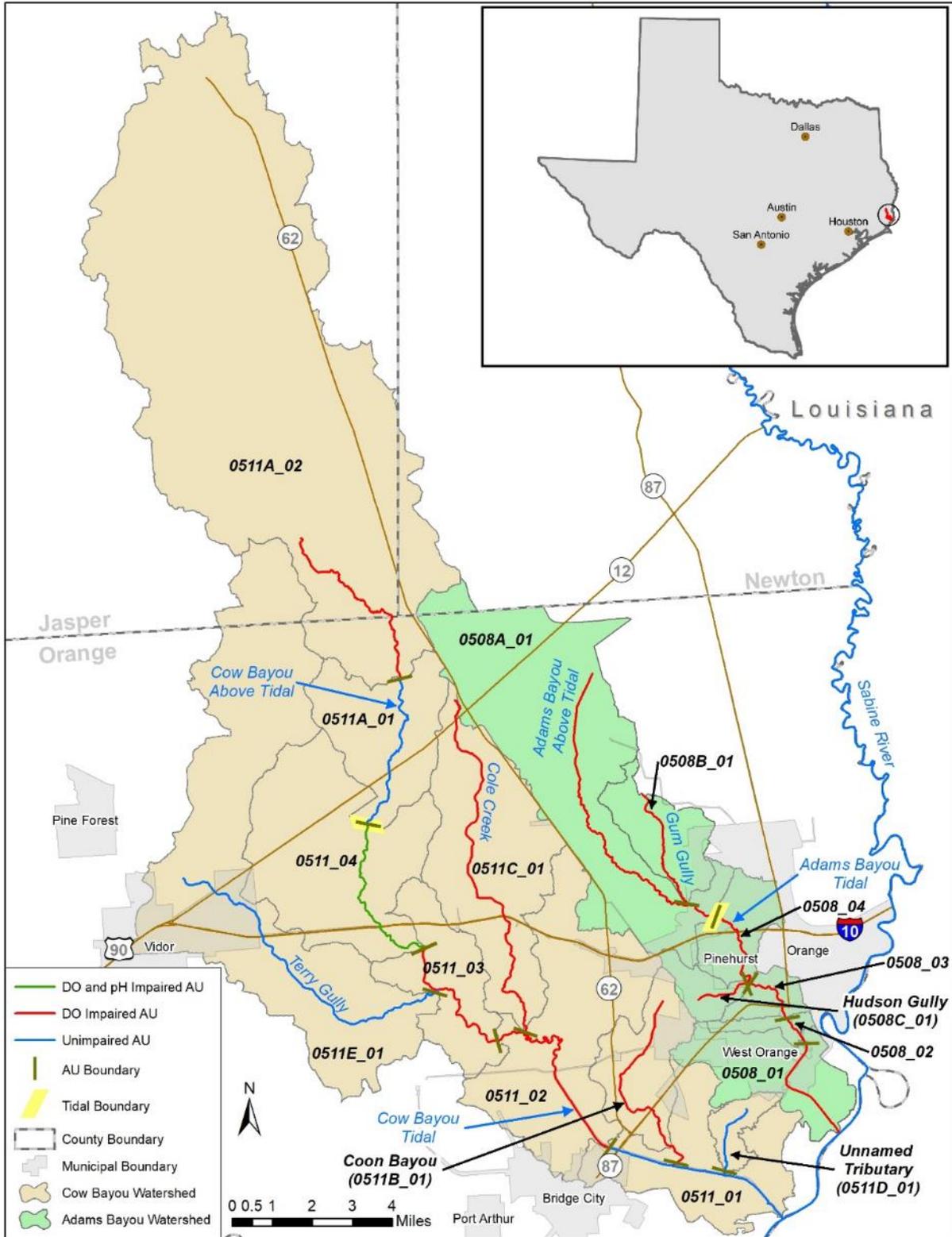


Figure 1-1 Location of Adams and Cow Bayous in southeast Texas showing impaired AU for depressed dissolved oxygen (DO) and pH

There is no flow gauging station on Adams Bayou, but field surveys indicate that under low-flow conditions there is essentially no base flow (TWC, 1986). Under these conditions, water movement occurs due to tidal ebb and flow and wastewater discharges to the bayou. The upper reaches of Adams Bayou and non-tidal tributaries are considered to be intermittent streams with pools.

The Adams Bayou watershed of 46.355 square miles (29,667 acres) is almost entirely within Orange County with a small portion of its upper watershed in Newton County. The Cow Bayou watershed comprises 198.765 square miles (127,210 acres) covering substantial portions of Orange and Jasper Counties, as well as a small corner of Newton County.

Further details of water bodies and watershed properties are described in later chapters related to model development.

Cow Bayou, Adams Bayou, and several of their tributaries have been identified by the State of Texas as not meeting water quality standards for support of aquatic life due to depressed dissolved oxygen (DO) levels. The impaired AUs for depressed DO include:

AU	Description
0508_01	Adams Bayou Tidal (lower 3 miles of segment)
0508_02	Adams Bayou Tidal (2 mile reach near Western Avenue)
0508_03	Adams Bayou Tidal (1 mile reach near Green Avenue)
0508_04	Adams Bayou Tidal (Upper 2 miles of tidal segment)
0508A_01 *	Adams Bayou Above Tidal (entire bayou above tidal; 8.8 miles)
0508B_01 *	Gum Gully (entire creek; 3.4 miles)
0508C_01	Hudson Gully (entire creek; 1.5 miles)
0511_02	Cow Bayou Tidal (6 mile reach near FM 105)
0511_03	Cow Bayou Tidal (5 mile reach near FM 1442 [north crossing])
0511_04	Cow Bayou Tidal (upper 4 miles of tidal segment)
0511A_02	Cow Bayou Above Tidal (upper 5.3 miles of above tidal reach)
0511B_01	Coon Bayou (entire tidal reach; 5.2 miles)
0511C_01	Cole Creek (entire tidal reach; 10.6 miles)

* An aquatic life use attainability analysis is to be conducted for AUs 0508A_01 and 0508B_01. If the finding of this analysis indicates either or both AUs require a TMDL, then the impairment will be addressed by TCEQ through Texas' Water Quality Management Plan update process.

These impaired water bodies include all of the AUs that were assessed in the Adams Bayou system. In the Cow Bayou system, AU 0511_01 (lower 5 miles of Cow Bayou Tidal) met water quality standards, and, while there was concern over depressed DO in Terry Gully (AU 0511E_01), this water body is not listed as impaired for depressed DO. Other AUs, such as

0511A_01 and 0511D_01, were not assessed due to lack of data and are therefore considered unimpaired. The history of the appearances of these water bodies on the State of Texas' Clean Water Act Section 303(d) list begins in 1992 with Adams Bayou Tidal (AUs 0508_01, 0508_02, 0508_03, and 0508_04). In 1994, TCEQ added Cow Bayou Tidal (AUs 0511_02, 0511_03, and 0511_04) to the Texas 303(d) List. Then in 2000, TCEQ added Adams Bayou Above Tidal (AU 0508A_01), Gum Gully (AU 0508B_01), Cow Bayou Above Tidal (AU 0511A_02), Coon Bayou (AU 0511B_01), and Cole Creek (AU 0511C_01) to the State of Texas 303(d) List. Hudson Gully (AU0508C_01) first appeared on the 2002 Texas 303(d) list.

This document will also consider impairments in 1 water body (segment) and 1 AU for low pH. The water body and its identifying AU number is shown below:

AU	Description
0511_04	Cow Bayou Tidal (upper 4 miles of tidal segment)

The pH-impaired AU 0511_04 was added to the Texas 303(d) List in 2000. In the 2006 Texas Water Quality Inventory, AU 0511_03 was listed as a "concern" for pH. Because AU 0511_03 was listed at the concern level and not as impaired, TCEQ made the decision to proceed with TMDL development only for Cow Bayou Tidal AU 0511_04.

1.3 Past TMDLs

From 2003 to 2007, Adams Bayou and Cow Bayou were the subject of a TMDL project of TCEQ. The project included development of water quality models to link point and nonpoint sources of pollution to instream conditions (Parsons, 2006a, 2006b); and data collection to quantify pollutant sources and instream processes, and to provide data for model calibration and validation (Parsons, 2003a, 2003b).

Based on this work, TCEQ adopted TMDLs for DO and pH in Adams Bayou, Cow Bayou, and their tributaries on June 13, 2007, and the United States Environmental Protection Agency (EPA) approved these TMDLs on August 28, 2007. The adopted and approved TMDL document also included TMDLs for indicator bacteria impairments in a number of the segments within the watersheds of Adams Bayou and Cow Bayou.

Since the models were developed, there have been a number of changes in the watershed, including new and eliminated permitted discharges, and expansions in the availability of centralized wastewater collection and treatment. Additional changes in wastewater discharge permit limits have been proposed. TCEQ adopted an approach of subdividing segments into AUs for TMDLs that was not entirely consistent with the existing model segmentation. The TMDL was also determined by model scenarios involving reductions from existing loading, rather than from a fully permitted scenario. This existing-loading approach is not consistent with current practice. Thus, an update of the models and TMDLs was needed.

Due to the complexity of the modeling system, and because these models are not the typical tools used by TCEQ in evaluating water quality permits, TCEQ requested assistance from a Texas Institute of Applied Environmental Research (TIAER)/Parsons team in providing an updated and fully documented modeling system. The modeling system is intended to provide TCEQ with a tool to use in water quality permitting, specifically, to set permit limits for DO and oxygen-demanding substances consistent with the TMDLs for Adams Bayou and Cow Bayou, and their tributaries.

1.4 Document Summary

This document first summarizes the comprehensive modeling system developed to link instream DO to point-source (PS) and nonpoint-source (NPS) loads of oxygen demanding substances in the Adams and Cow Bayou systems, then describes various loading scenarios and their impact on instream dissolved oxygen, and finally describes development of updated TMDLs for oxygen-demanding substances in the impaired water bodies.

The document also provides an explanation of the environmental linkage of low pH in the upper reaches of Cow Bayou Tidal to the depressed DO that occurs in the water body. Further, this linkage is used to update the TMDL for low pH in the single pH-impaired AU of Cow Bayou Tidal.

2. Summary of Modeling System Developed for Linkage Analysis

The modeling system used in the TMDL revisions was developed under a quality assurance project plan (QAPP) for modeling titled “Technical Support for Revision and Documentation of Watershed and In-Stream Water Quality Models Used to Establish Total Maximum Daily Loads (TMDLs) for Dissolved Oxygen in Adams and Cow Bayous and Associated Tributaries.” The QAPP was approved by TCEQ on May 6, 2013 and re-issued on May 5, 2014, revised on February 3, 2015, and amended with minor revisions to staff responsibilities, on June 17, 2015. The QAPP was re-issued as Revision # 3 on February 4, 2016, and thereafter annual renewals occurred on January 18, 2017, January 18, 2018, January 9, 2019, and January 7, 2020. With Revision #3, pH and bacteria investigations were incorporated into the QAPP and the title changed to “Technical Support for Revision and Documentation of Watershed and In-Stream Water Quality Models Used to Establish Total Maximum Daily Loads (TMDLs) for Dissolved Oxygen, pH and Bacteria in Adams and Cow Bayous and Associated Tributaries.”

The separate Adams Bayou and Cow Bayou modeling systems consists of the same fundamental components tailored to the features of each water body and watershed:

- An Hydrologic Simulation Program - Fortran (HSPF) hydrologic and water quality model of the watershed and above tidal reaches,
- an RMA2 hydrodynamic model for the tidal reaches,
- a Water Quality Analysis Simulation Program (WASP) water quality model for the tidal reaches,
- accessory programs to link the models,
- a user interface to edit model inputs and review model outputs

Figure 2-1 illustrates the basic structure of the modeling system. The HSPF model serves as the hydrologic and water quality model for the above tidal reaches of Adams Bayou, Cow Bayou, and their tributaries. HSPF does not have the capacity to simulate tidal flows and water quality. HSPF sub-basins and reaches are split near the upper tidal boundary of each stream and major tributary, and the RMA2 and WASP models extend to just above this tidal boundary. At this tidal boundary, the HSPF-simulated instream flows serve as boundary flow conditions for the RMA2 hydrodynamic model. Similarly, the HSPF-simulated loads of water quality constituents serve as boundary input loads to the WASP water quality model. The HSPF watershed model also simulates runoff flows and water quality constituents to portions of the watershed that run off directly to the tidal reaches of Adams Bayou and Cow Bayou and their tributaries. The model

linkages of HSPF output involve straightforward spatial and temporal aggregations, unit conversions, and data format modifications. The RMA2 linkage to WASP includes these, as well as conversions from water velocity to flow based on cross-sectional area. The linkages were created using utility programs.

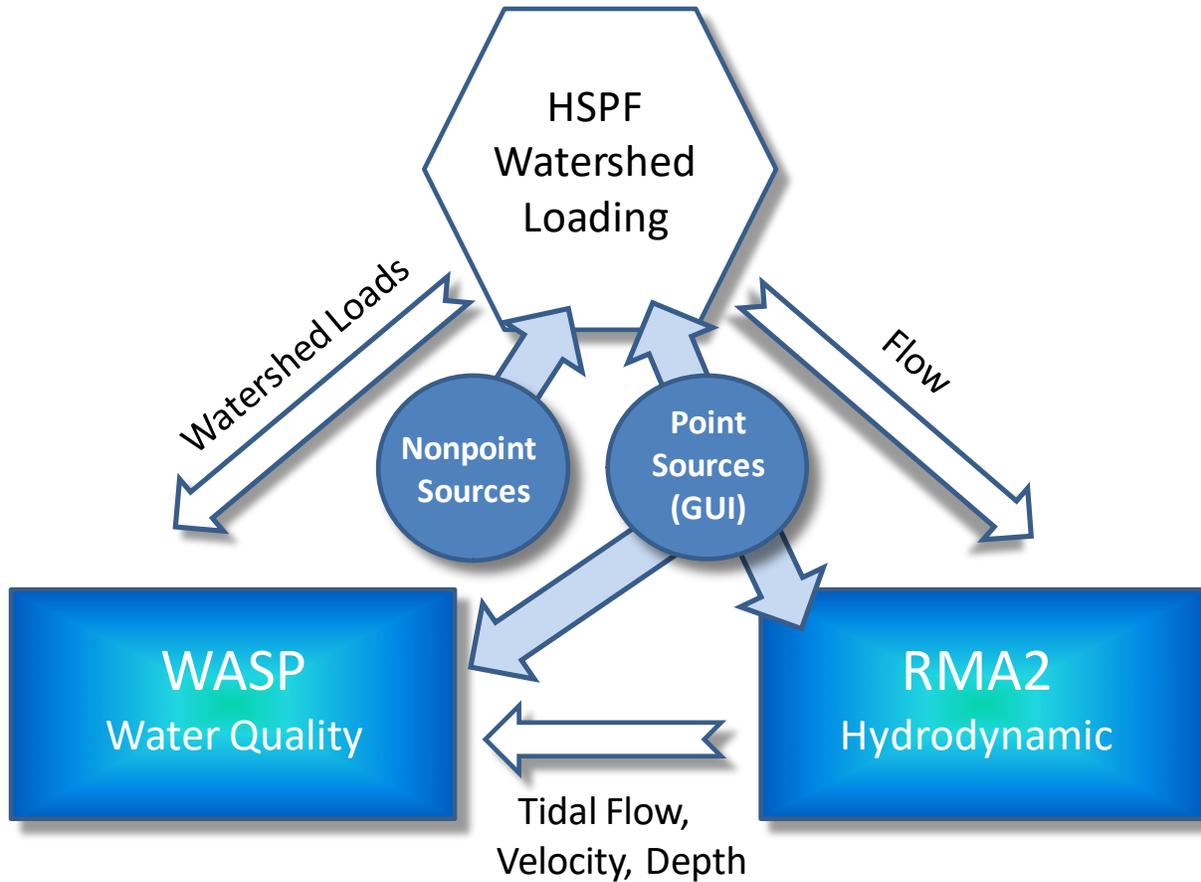


Figure 2-1 Schematic of modeling system

3. HSPF Hydrologic and Water Quality Model

The HSPF models of the Adams Bayou and Cow Bayou watersheds were developed to be run under HSPF version 12.0, either as the stand-alone executable program or using WinHSPF version 2.3 or WinHSPFLt, which are components of the EPA’s BASINS modeling software. The models utilize algorithms developed for version 12.0 for high water table, low topography conditions, and will not run under older versions of HSPF.

3.1 HSPF Model Description

In HSPF, the watersheds were first divided spatially into sub-basins based on topography; a 10-m resolution digital elevation model was used for this purpose. Key model characteristics are summarized in Table 3-1. There are 12 sub-basins in the Adams Bayou watershed model (Figure 3-1)¹, and 18 sub-basins in the larger Cow Bayou watershed model (Figure 3-2). Next, the watersheds were further sub-divided into a series of land segments, either pervious land surface (PLS) or impervious land surface (ILS), based on land cover. Pervious land surfaces allow water to pass through to the sub-surface, while ILS’s such as concrete or asphalt do not. Land within a PLS or ILS is considered to have similar characteristics, though not necessarily nearby or connected. In each model, there are 17 PLS and 4 ILS. Most of the PLS and ILS correspond to land cover categories from the 2006 National Land Cover Dataset (NLCD). However, one PLS (PERLND 117) is reserved for future use, and another (PERLND 116) is a sub-set of the pervious low-density residential land use that is attributed to malfunctioning on-site sewerage facilities (OSSFs). The four “developed” land cover categories were divided into PLS and ILS based on the assumption that impervious surfaces comprised 11 percent of the open developed land, 31 percent of the low-density developed land, 62 percent of the medium-density developed land, and 88 percent of the high-density developed lands. These percentages were calculated in a geographic information system by intersecting the 2006 NLCD impervious land cover dataset

¹ The northern portion of the Adams Bayou watershed, as included in HSPF Subbasin 2, was refined from its definition in Dean et al. (2015). A 2015 report by the consulting firm of Carroll and Blackman, Inc. contained information on a flood planning study performed for the Orange County Drainage District and the Texas Water Development Board (Carroll & Blackman, 2015). The report provided information from topographic data supplemented with actual physical survey data resulting in a significantly different delineation of this portion of the watershed from that used in the initial HSPF model of Adams Bayou watershed (Parsons, 2006a). The refined Adams Bayou delineation from Carroll & Blackman (2015) was subsequently agreed to by TCEQ and Sabine River Authority. The source of the differences in watershed boundaries is a flood diversion canal, which diverts water eastward directly to the Sabine River. The actual drainage of the Adams Bayou watershed that is intercepted by the diversion canal was difficult to accurately determine absent actual physical survey data obtained for the flood planning study.

with the land cover classes from the land cover dataset. All other land use categories were assumed to be 100 percent pervious.

Table 3-1 HSPF model summary

Version/Date	WinHSPF Version 2.3 Build 30 (5/13/2008 12:22 PM)
Model Period	1/1/2001 – 12/31/2012 (2001 is spin-up period)
Time Step	1 hour
Sub-basins	18 (Cow Bayou); 12 (Adams Bayou)
Pervious Land Categories	17: corresponding to 2006 NLCD land cover categories, plus a “failing OSSF” PERLND (116) carved from low-density residential and a currently unused category (117) to facilitate BMP evaluation or future land use changes
Impervious Land Categories	4; corresponding to fractions of 2006 NLCD “developed” land cover categories
Reaches	18 (Cow Bayou); 12 (Adams Bayou)
Active Modules and Sections	PERLND: PWATER, ATEMP, SEDMNT, PSTEMP, PWTGAS, PQUAL IMPLND: IWATER, ATEMP, SOLIDS, IWTGAS, IQUAL RCHRES: HYDR, ADCALC, HTRCH, SEDTRN, OXRX, NUTRX, PLANK
Sub-basin Constituents	runoff; temperature; TSS; NH ₃ N; NO ₃ N; PO ₄ P; cBOD
Reach Constituents	flow; temperature; DO, TSS (as sand, silt, & clay); NH ₃ N; NO ₃ N; PO ₄ P; cBOD; OrgN, OrgP, and OrgC; chla; detritus
Meteorology Inputs	precipitation, air temperature, dew point temperature, wind speed, potential evapotranspiration, pan evaporation, cloud cover, solar radiation
Point Source Discharge Placeholders	18 (Cow Bayou); 12 (Adams Bayou): There is 1 PS discharge input placeholder to each sub-basin. However, most of these are inactive, with no flow or loads, and inserted as placeholders for future modifications or scenario runs. All PS discharges to a given reach are summed.

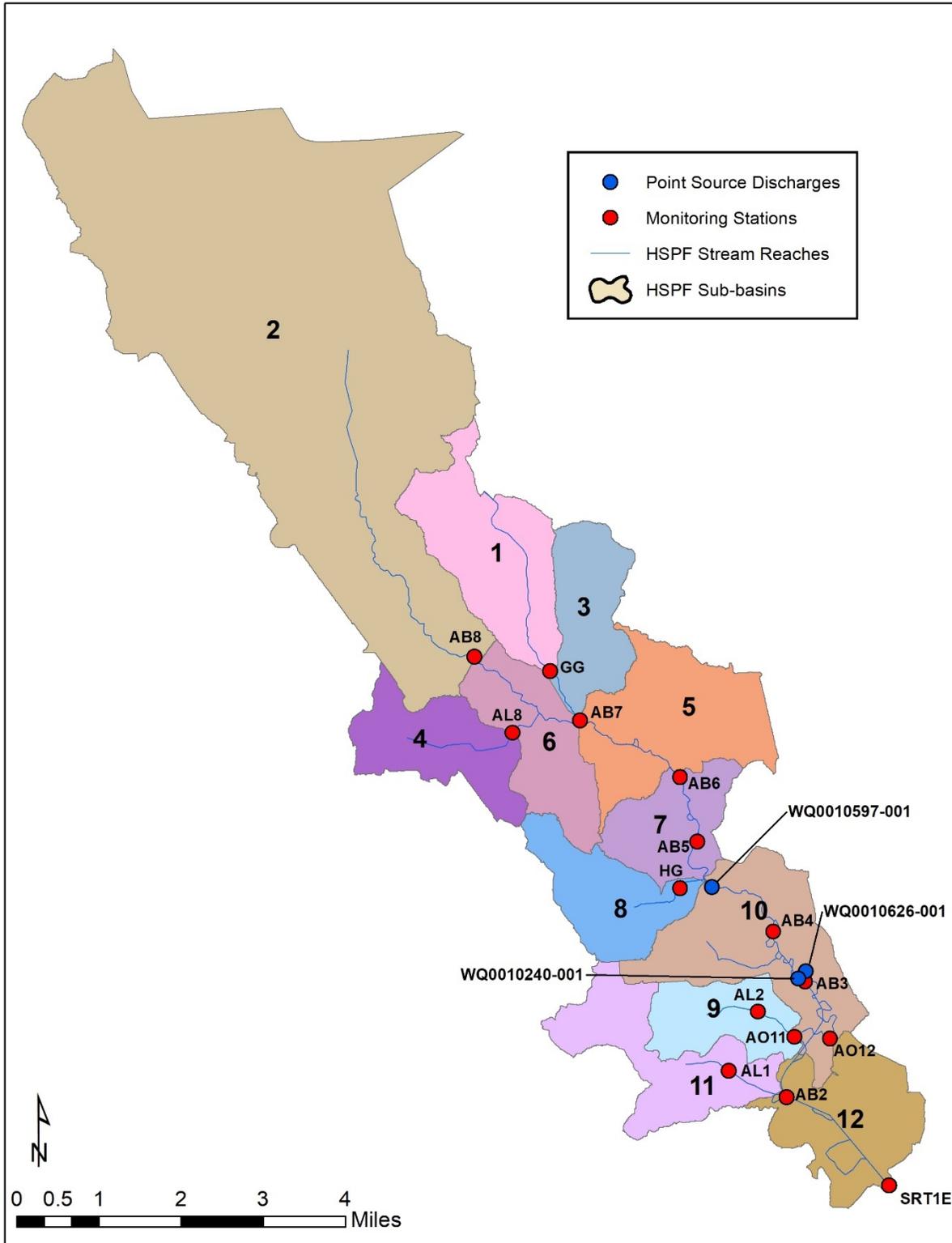


Figure 3-1 Adams Bayou sub-basins in HSPF

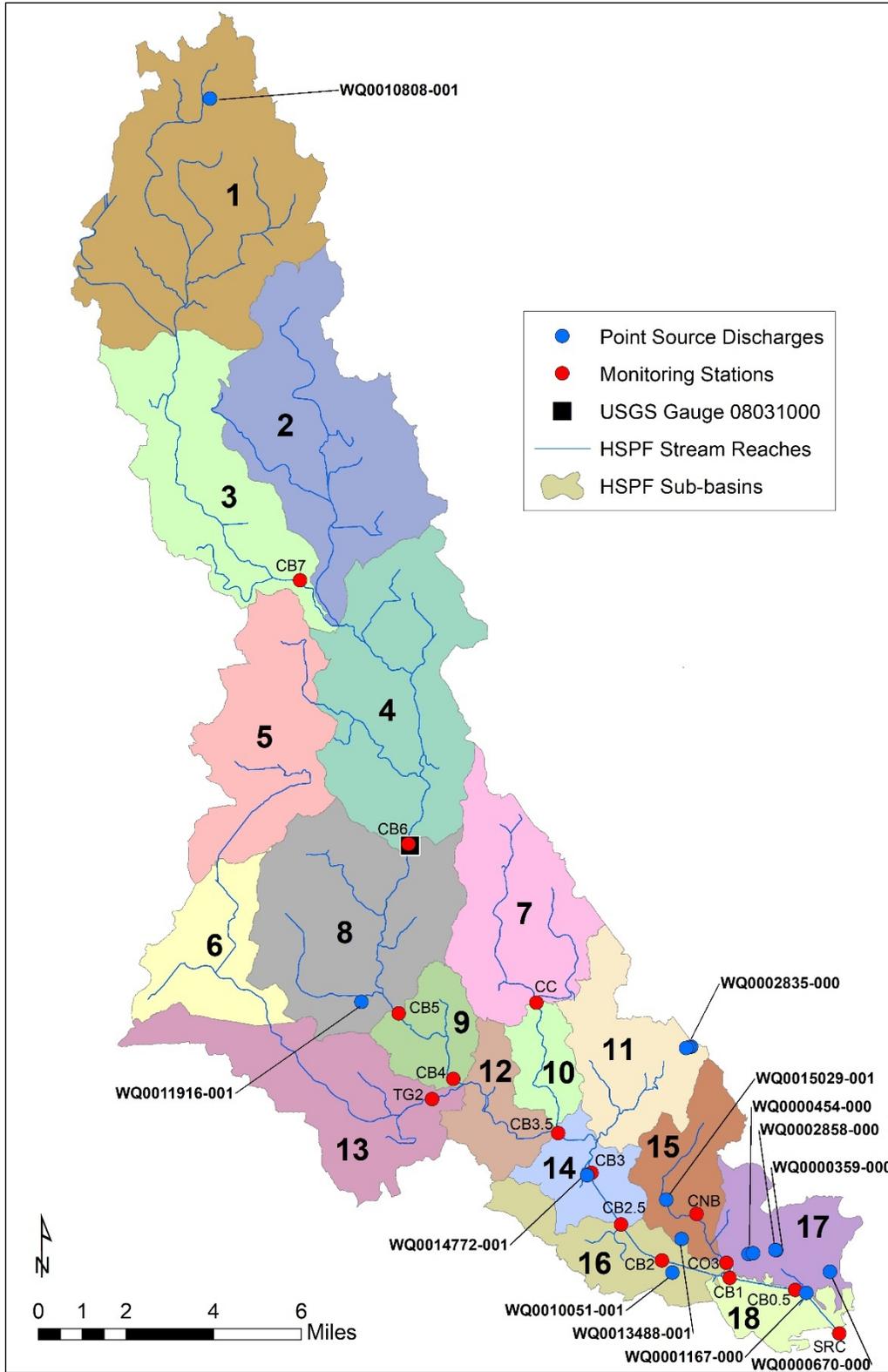


Figure 3-2 Cow Bayou sub-basins in HSPF

In HSPF, the PERLND module simulates water quantity and quality for each PLS, and the IMPLND module simulates water quantity and quality for each ILS. Runoff from each PLS and ILS is routed to a reach or reservoir in the RCHRES module. The RCHRES module simulates unidirectional flow and water quality in an open or closed channel as a stream or mixed reservoir. Upstream reaches are also routed to downstream reaches.

The model is based on English units. The active modules for pervious land use categories include:

- ATEMP (air temperature elevation difference),
- PWATER (water budget pervious),
- SEDMNT (production and removal of sediment),
- PSTEMP (soil temperature),
- PWTGAS (water temperature and dissolved gas concentrations), and
- PQUAL (quality constituents using simple relationships).

The active modules for impervious land use categories included:

- ATMP (air temperature elevation difference),
- IWATER (water budget impervious),
- SOLIDS (accumulation and removal of solids),
- IWTGAS (water temperature and dissolved gas concentrations), and
- IQUAL (washoff of quality constituents using simple relationships).

The active modules for the RCHRES (stream) sections include:

- HYDR (hydraulic behavior),
- ADCALC (advection of fully entrained constituents),
- HTRCH (heat exchange and water temperature)
- SEDTRN (behavior of inorganic sediment)
- OXRX (primary carbonaceous biochemical oxygen demand [cBOD] and DO balances)
- NUTRX (primary inorganic nitrogen and phosphorus balances)
- PLANK (plankton populations and associated reactions)

Key water quality constituents simulated in the model include DO, cBOD, nitrate nitrogen (NO₃N), ammonia nitrogen (NH₃N), organic nitrogen (OrgN), orthophosphate phosphorus (PO₄P), and total suspended solids (TSS). Chlorophyll-*a* (chl_a), detritus (non-living particulate organic matter), organic phosphorus (OrgP), and organic carbon (OrgC) were also simulated,

but were not calibrated because of a lack of data. The cBOD parameter simulated in HSPF was the commonly measured 5-day cBOD(cBOD₅).

The new high water table, low-gradient algorithms incorporated into version 12 of HSPF were applied to herbaceous wetlands in the Adams Bayou and Cow Bayou models. These algorithms were developed for wetland environments. Wetlands appear to exert a controlling influence on the hydrology of Cow Bayou. In essence, the wetlands act like a sponge, absorbing rainfall with little or no runoff until the sponge is saturated. For this reason, there is often very little flow in Cow Bayou in the summer, when evaporation and evapotranspiration by plants speeds the drying of the wetlands. To represent the pervious soil environment, the new HSPF algorithms keep track of the groundwater levels (top of saturated zone) and the interaction between the saturated and unsaturated zone. Also, surface flow in herbaceous wetlands is simulated as a power function of the water storage on the land surface, rather than the traditional approach based on the length, slope, and roughness of the overland flow plane.

3.2 Inputs, Data Sources and Assumptions

Each model has specific data requirements compiled from various data sources. In some cases, it was necessary to establish certain assumptions when data were lacking or to clarify data interpretation. As a watershed loading model, data inputs for HSPF include information that influences the transport of stormwater runoff and groundwater filtration to each receiving stream. The data inputs used for this HSPF model include: meteorology, land use/land cover, landscape physiography, numerous categories of NPS pollution including atmospheric deposition, PS discharges, flow, and meteorology.

3.2.1 Climate and Meteorology

Adams Bayou and Cow Bayou experience a subtropical humid climate. The average temperature varies from 50 degrees Fahrenheit in January to 83 degrees in August. Rain is abundant in this corner of Texas, with an average annual rainfall of almost 60 inches. The frequency of significant rainfall (one half inch or more in a 24-hour period) has averaged approximately 3.2 days per month, or roughly 1 in 10 days, over the last 30 years. Seasonal variations in precipitation frequency and magnitude are not great. June, July and September have the most frequent rainfall, and February, March, and April have the least frequent.

Meteorological inputs required by the HSPF model are described in Table 3-2. Most data were available on an hourly basis. Pan evaporation and potential evapotranspiration were measured daily, and disaggregated to hourly using the time series utility program WDMutil. Also, during the validation period of the Adams Bayou model, daily rainfall totals measured in the watershed differed significantly from those at Southeast Texas Regional Airport and also decreased in a southeast to northwest direction across the watershed (PRISM, 2017). The daily rainfall totals for the centroid of the Adams Bayou watershed were used for the May – June 2004 precipitation

input to HSPF. These daily rainfall total were estimated using the Oregon State University PRISM Climate Group (PRISM, 2017), which was disaggregated into hourly data.

Table 3-2 Meteorological inputs to the HSPF models

Data Type	Frequency	Cow Bayou Dataset Number	Adams Bayou Dataset Number	Source
Precipitation	Hourly	35	27	Southeast Texas Regional Airport (Port Arthur), except for Adams Bayou calibration and validation period (May-June 2004) used daily data from NRCS High Resolution Climatic Data
Precipitation	Hourly (disaggregated from daily)	NA	27	PRISM Climate Data (May – June 2004)
Air Temperature	Hourly	36	28	Southeast Texas Regional Airport (Port Arthur)
Dew Point Temperature	Hourly	39	29	Southeast Texas Regional Airport (Port Arthur)
Cloud Cover	Hourly	41	30	Southeast Texas Regional Airport (Port Arthur)
Potential Evapotranspiration	Hourly (disaggregated from daily)	42	31	Texas A&M University Research Center (Beaumont)
Pan Evaporation	Hourly (disaggregated from daily)	43	34	Texas A&M University Research Center (Beaumont)
Wind Speed	Hourly	38	25	TCEQ Continuous Air Monitoring Station (West Orange)
Solar Radiation	Hourly	40	26	TCEQ Continuous Air Monitoring Station (West Orange)

3.2.2 Land Use and Land Cover

Land use in the Adams and Cow Bayou watersheds is illustrated in Figure 3-3, from the Multi-Resolution Land Cover Consortium’s 2006 NLCD. This land use classification is based on satellite imagery from approximately 2006. Overall, 32 percent of the Adams Bayou watershed and 16 percent of the Cow Bayou watershed were considered developed or built-up land (Table 3-3). Approximately 23 percent of the Cow Bayou watershed, and 9 percent of the Adams Bayou watershed, is covered by forest. Approximately 9 percent of the Cow Bayou watershed and 22 percent of the Adams Bayou watershed is used for pasture or hay production for grazing animals. Water and wetlands comprise approximately 38 percent and 27 percent, respectively, of the Cow and Adams Bayou watersheds.

The 2006 land use was selected for use in developing input to HSPF because these data characterize conditions for roughly the temporal midpoint of the 2002 through 2012 time period used for hydrologic model verification. Further, the 2006 land use represents conditions near the 2004 time period of the intensive surveys for collection of water quality data in the watersheds of Adams Bayou and Cow Bayou used for verification of the water quality model components of HSPF and WASP.

Table 3-3 Land use/land cover in the Adams and Cow Bayou watersheds

NLCD Land Cover Category†	Adams Bayou	Cow Bayou
Open Water	1.48%	0.79%
Developed, Open Space	12.00%	8.08%
Developed, Low Intensity	15.07%	5.65%
Developed, Medium Intensity	2.92%	1.19%
Developed, High Intensity	1.74%	0.69%
Barren Land	0.03%	0.05%
Deciduous Forest	0.50%	0.08%
Evergreen Forest	4.16%	12.41%
Mixed Forest	4.60%	10.90%
Shrub/Scrub	2.75%	6.41%
Grassland/Herbaceous	4.73%	6.45%
Pasture Hay	22.16%	9.27%
Cultivated Crops	2.79%	1.24%
Woody Wetlands	20.06%	34.13%
Emergent Herbaceous Wetlands	5.02%	2.67%

†from 2006 NLCD

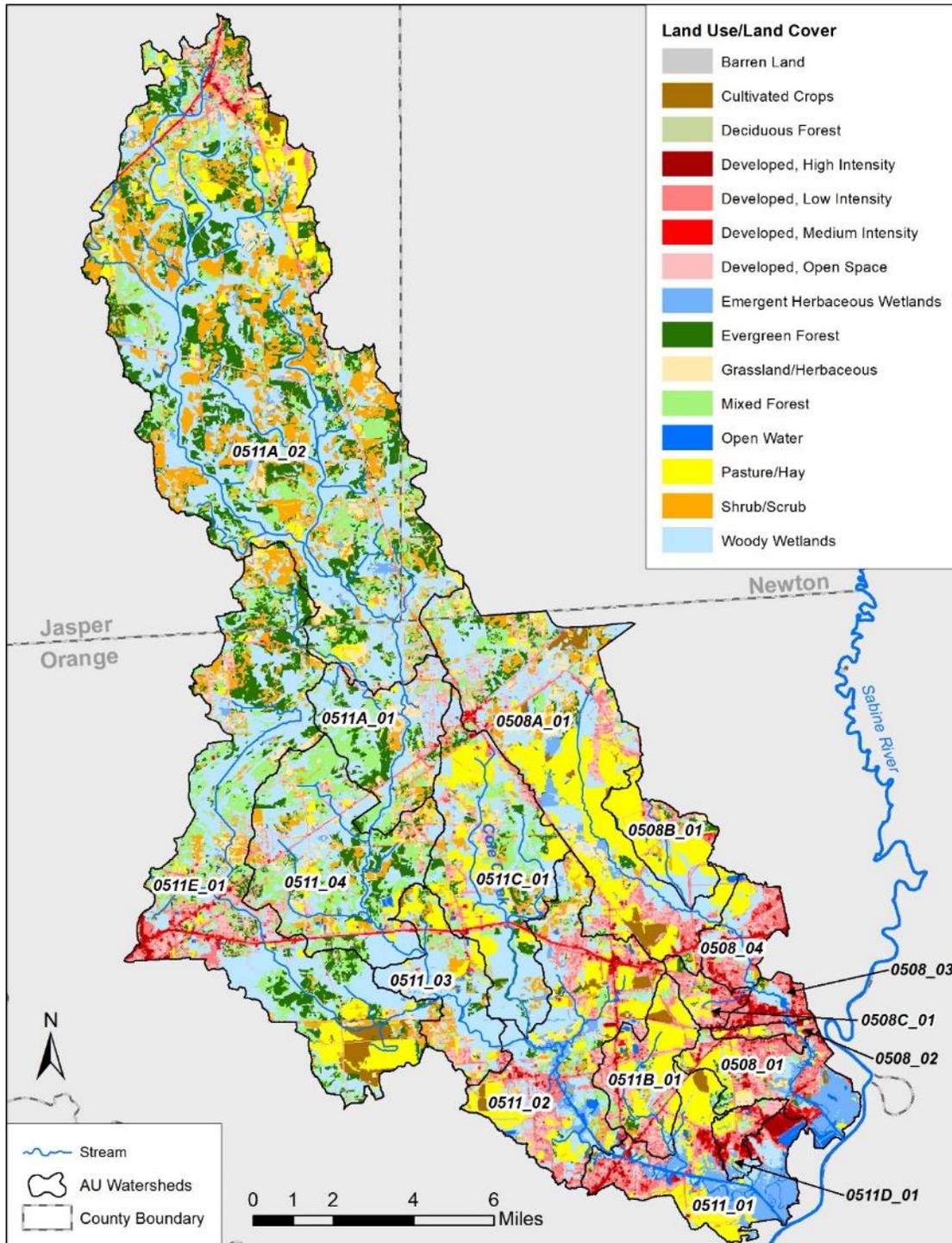


Figure 3-3 2006 land use/land cover in the Adams and Cow Bayou watersheds

3.2.3 Geology, Topography, and Soils

Adams Bayou and Cow Bayou are located in the Gulf of Mexico coastal plain. The southeastern parts of their watersheds lie in the Texas ecological region known as Gulf prairies and marshes, while the northwestern parts lie in the piney woods region. The terrain is level and low. The elevation of Adams Bayou varies from sea level at the Sabine River to 4.5 feet (ft) at its uppermost extent (TWC, 1986), with an average slope of only 6 cm/km, or 0.006 percent. The elevation of Cow Bayou varies from sea level at the Sabine River to 7 ft at its uppermost extent (TWC, 1986), and also has an average slope of 6 cm/km (TWC, 1988).

Sedimentary rocks comprise the geologic base of the watersheds of Adams Bayou and Cow Bayou. The Beaumont Clay is the surface formation over the entire watershed. It is composed of mixed sand, silt, clay and gravel. The soils are primarily fine sands, silts, and clays. Most are fine-textured, have high water holding capacity, and very slow water permeability. Soils also tend to be acidic and have high organic matter content in the surface layer. Some soils have frequent flooding and/or surface ponding of water for long durations in the cooler months of the year. Finally, many of the soils are saturated in the cooler months, with water tables at or near the surface. Together with the low and level topography, these soil properties give rise to an abundance of wetlands within the watersheds. Table 3-4 describes some of the properties of the major soil map units found in the watersheds of Adams Bayou and Cow Bayou.

3.2.4 Nonpoint Sources of Pollutants

A non-point pollutant source inventory was developed for each watershed and sub-watershed using a system of linked Microsoft Excel™ spreadsheets. This tool was adapted from the Bacterial Indicator Tool developed by the EPA (2000). The tool provides estimates of loading of cBOD₅, PO₄P, NH₃N, and NO₃N for the HSPF model based on land use, livestock and wildlife populations, waste management practices, and other watershed properties. This “Loading Tool” spreadsheet was modified to address watershed-specific conditions. In HSPF, the parameter ACQOP describes the accumulation rate for each water quality constituent on pervious and impervious land cover categories in pounds per acre per day. The ACQOP values in the HSPF model are taken from the “Summary” worksheet in the Loading Tool spreadsheet. Although not dynamically linked to the HSPF input file, the HSPF model can be manually modified if the loading assumptions in the spreadsheet are modified.

Table 3-4 Selected properties of major soil map units of Adams and Cow Bayou watersheds

(Information provided for soil map units comprising >2 percent of either Adams Bayou watershed or Cow Bayou watershed)

Map Unit Name	Area %		Runoff	Flooding	Surface Ponding	High Water Table		Hydraulic Permeability
	Adams	Cow	Potential	Frequency	Frequency	Depth (ft)	months	Percolation
Anahuac-Aris complex	2.5%	0.6%	medium	none	none	4-6	Nov-Apr	very slow
Bleakwood loam	0.0%	2.3%	negligible	frequent	none	0-1.5	Nov-May	moderate
Camptown silt loam	2.9%	0.9%	negligible	none	frequent	0	Dec-Aug	very slow
Craigen loamy fine sand	0.0%	2.9%	very low	none	none	3-5	Jan-Apr	moderate
Evadale silt loam	0.0%	6.7%	very high	none	none	0-1.5	Dec-Apr	very slow
Evadale-Gist complex	0.0%	20%	very high	none	none	0-1.5	Dec-Apr	very slow
Evadale-Vidrine complex	2.6%	3.4%	high	none	none	0-1.5	Dec-Apr	very slow
Fausse clay	2.1%	0.0%	negligible	frequent	frequent	0-1.5	all year	very slow
Labelle silt loam	10.2%	2.0%	high	none	none	0.5-1.5	Jan-Mar	very slow
Labelle-Levac complex	4.4%	1.0%	high	none	none	0.5-1.5	Jan-Mar	very slow
Leerco muck	3.7%	0.0%	negligible	frequent	frequent	0	all year	very slow
Malbis-Kirbyville association	0.0%	4.6%	medium	none	none	2.5-4.0	Dec-Mar	slow
Orcadia silt loam	1.9%	2.6%	very high	none	none	0.8-1.5	Jan-Mar	very slow
Orcadia-Anahuac complex	17.3%	5.9%	high	none	none	0.8-1.5	Jan-Mar	very slow
Orcadia-Aris complex	6.6%	6.7%	medium	none	none	0.8-1.5	Jan-Mar	very slow
Orcadia-urban land complex	18.4%	3.4%	very high	none	none	0.8-1.5	Jan-Mar	very slow
Texla silt loam	15.1%	3.2%	high	none	none	0.5-1.5	Jan-Mar	very slow
Texla-Evadale complex	1.5%	14%	high	none	none	0.5-1.5	Jan-Mar	very slow
Texla-Gist complex	6.8%	3.6%	high	none	none	0.5-1.5	Jan-Mar	very slow

3.2.4.1 Agricultural Sources

The major agricultural activities within the watersheds include beef cattle ranching and hay production. The 2007 U.S. Department of Agriculture (USDA) census of agriculture provides a more detailed inventory of agricultural activities at the county level (Tables 3-5 through 3-7). In addition to hay and other forage, the other major crop in Orange County is rice, but this is primarily outside the watersheds of Adams Bayou and Cow Bayou. Cattle are the most abundant livestock by a large margin. Other abundant livestock include chickens, sheep, goats and horses.

The 2007 USDA census of agriculture was selected for use in developing input to HSPF because these data characterize conditions for roughly the temporal midpoint of the 2002 through 2012 time period used for hydrologic model verification. The 2007 USDA agricultural census also represents conditions near the 2004 time period of the intensive surveys for collection of water quality data in the watersheds of Adams Bayou and Cow Bayou used for verification of the water quality model components of HSPF and WASP.

Table 3-5 Count of farms/production operations by county and type: 2007 agricultural census

Type	Orange	Jasper	Newton
Farms	675	920	403
Acres harvested	5,046	11,399	4050
Irrigated farms	35	32	10
Oilseed and grain farming	-	-	-
Vegetable and melon farming	15	31	9
Fruit and tree nut farming	18	32	12
Greenhouse, nursery, and floriculture production	12	30	6
Sugarcane farming, hay farming, and all other crop farming	76	181	57
Beef cattle ranching and farming	349	435	210
Cattle feedlots	6	6	4
Dairy cattle and milk production	6	3	1
Hog and pig farming	5	2	26
Poultry and egg production	19	30	15
Sheep and goat farming	38	29	14
Animal aquaculture and other animal production	131	141	49

Table 3-6 Crops planted by county, in acres: 2007 agricultural census

Crop	Orange	Jasper	Newton
Rice	D	-	-
Forage - hay and hay land, grass silage, and greenchop	4,442	9,764	3,894
Vegetables	50	170	15
Orchards	59	422	22
Corn for grain	-	23	D
Wheat for grain	-	-	-
Soybeans	D	-	-
Potatoes	2	4	1
Sugarcane	-	-	-

D - Withheld to avoid disclosing data from individual farms
 - represents zero

Table 3-7 Domestic livestock populations by county: 2007 agricultural census

Type	Orange	Jasper	Newton
Cattle and calves*	8,528	13,657	5,354
Hogs/pigs	176	100	65
Horses/ponies	1,427	1,826	714
Sheep/lamb	150	201	54
Goats	838	853	713
Mules/burros/donkeys	201	168	62
Rabbits	112	66	33
Deer	342	504	114
Chickens/layers and pullets	1,707	2,444	1,839
Chickens/broilers	460	153	40
Turkeys	D	10	D
Pheasants	D	D	D
Pigeons and squab	D	D	D
Quail	D	-	-
Ducks	688	265	142
Geese	80	58	27
Other poultry	D	229	99

* all were beef cattle except a few dairy cows in Orange County
 D -Withheld to avoid disclosing data from individual farms
 - represents zero

Livestock fecal waste may serve as a major nonpoint source pollutant, either by runoff of manure directly deposited by grazing animals on pasture, rangeland, or in water, or by application of

manure from confined animals to fields as fertilizer. Manure production by livestock was estimated based on the animal population estimate from the 2007 USDA Census of Agriculture multiplied by the American Society of Agricultural Engineers (ASAE) estimated average daily manure production (ASAE, 1998). Ammonia nitrogen and phosphorus production estimates were also derived from published ASAE estimates. Table 3-8 provides a summary of the estimated pollutant productions rates from the manure of various livestock.

Manure from cattle, horses, sheep, and goats was assumed to be directly deposited to pastureland. Because there are few if any dairy cattle in the watersheds, and other cattle are not confined, it was assumed that no cattle manure was collected and spread on cropland as fertilizer. However, manure from swine and poultry within the watershed was assumed to be collected and applied to cropland as fertilizer.

Table 3-8 Pollutant production rates of livestock in manure

Animal	BOD [†] Production (lb/animal/day)	NH ₃ N Production (lb/animal/day)	PO ₄ P Production (lb/animal/day)	Solids Production (lb/animal/day)
Beef cow	1.28	0.069	0.074	6.8
Hog	0.42	0.039	0.024	1.5
Sheep	0.07	0.005	0.005	0.66
Horse	1.70	0.079	0.071	15
Goat	0.07 [#]	0.005 [#]	0.005 [#]	0.66 [#]
Chicken	0.02	0.001	0.001	0.06
Turkey	0.03	0.001	0.004	0.18

All values from ASAE (1998) or Shaffer et al (2005) except where otherwise noted.

[†] 5-day biochemical oxygen demand without nitrogen inhibition

[#] best professional judgment – no data exist

3.2.4.2 On-site Sewerage Facilities

OSSFs, such as septic tanks, can serve as nonpoint sources of pollutants. Malfunctioning septic tanks are those that have been improperly engineered or installed, poorly maintained, or where soils do not permit the sanitary absorption of septic effluent. In rural and some suburban areas of Adams Bayou and Cow Bayou, conventional septic tanks serve as the primary mechanism for sewage disposal. The most recent available data on the abundance of septic tanks in the watersheds comes from the 1990 decennial federal census. In the long questionnaire given to roughly 1 in 6 households, respondents were asked to identify the sewage disposal method of their housing unit as either “public sewer”, “septic tank or cesspool”, or “other means”. In the Adams Bayou watershed, 6,754 housing units (88 percent) were connected to a public sewer, 888 units (12 percent) used septic tanks or cesspools for sewage disposal, and 20 units reported an “other” sewage disposal method. In the Cow Bayou watershed, 2,205 housing units (28 percent) were connected to a public sewer, 5,582 units (71 percent) used septic tanks or cesspools, and 108 units (1 percent) reported an “other” sewage disposal method.

The 1990 federal census information was used to develop a map showing the density of the pre-1991 households with conventional septic systems, which represent those OSSFs with the highest likelihood of failure (Figure 3-4). The 1990 federal census information was used at the census-block level with the associated census responses to OSSF presence or absence in developing this figure.

In the 2000 and 2010 federal censuses, the questionnaire did not include a question on sewage disposal. Since 1991, when Orange County adopted its OSSF program, it has been a requirement that a soil survey must be performed before installation of an OSSF. Given that almost all soils in the watersheds are unsuitable for conventional septic systems, in most cases an aerobic OSSF must be installed. Thus, since 1991 new housing in areas not served by public sewers has generally required aerobic OSSF systems, and the number of housing units utilizing conventional septic systems has likely not increased.

The Orangefield Water Supply Corporation was established in 1995 and in recent years began to provide sanitary sewer service to portions of the Cow Bayou watershed. By 2013, their 0.75 million gallons per day (MGD) wastewater treatment facility (WWTF) was treating wastewater from 1,000 connections in the Cow Bayou watershed that previously used OSSFs (Morton, 2013). These 1,000 connections were removed from the 1990 inventory of OSSFs in each Cow Bayou sub-basin based on the portion of each Cow Bayou sub-basin within the Orangefield Water Supply Corporation service area.

Conventional septic tank systems rely on absorption fields to disperse liquid components of sewage into the soil, after solids have settled into the tank. Several factors affect the suitability of soils for septic tank absorption fields (NRCS, 2004). These factors include:

1) frequency and duration of flooding

Flooding here indicates the temporary inundation of an area caused by overflowing streams, tides, or runoff from adjacent slopes. Flooding may allow the widespread contamination of surface waters with septic tank effluent.

2) frequency and duration of ponding

Ponding is standing water in a closed depression. Ponding may allow the localized contamination of surface waters with septic tank effluent.

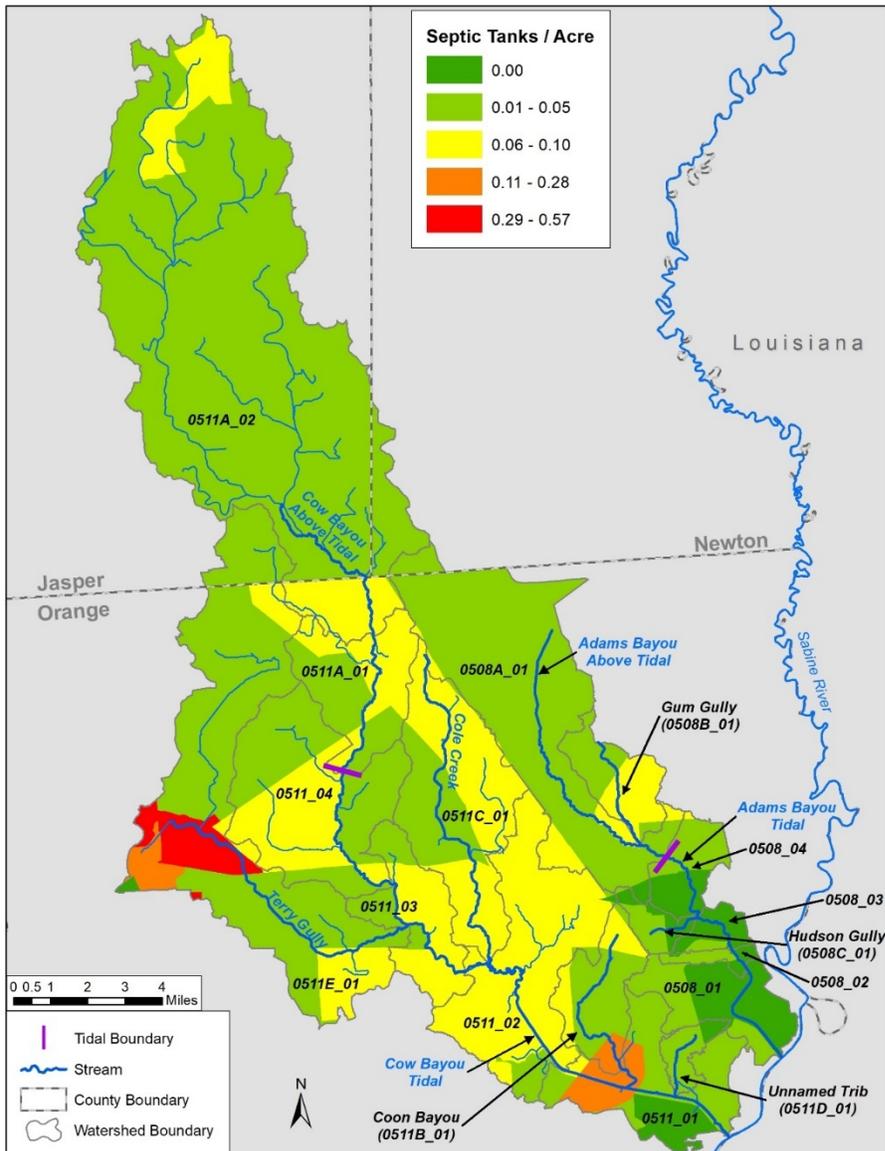


Figure 3-4 Septic tank density within the Adams Bayou and Cow Bayou watersheds based on 1990 federal census data

3) frequency and duration of flooding

Flooding here indicates the temporary inundation of an area caused by overflowing streams, tides, or runoff from adjacent slopes. Flooding may allow the widespread contamination of surface waters with septic tank effluent.

4) frequency and duration of ponding

Ponding is standing water in a closed depression. Ponding may allow the localized contamination of surface waters with septic tank effluent.

5) soil water permeability

Limited soil water permeability limits the rate at which the septic field can absorb and transmit septic effluent. The soil hydrologic group indicates the soil water permeability.

6) depth to the saturated zone

The saturated zone refers to the depth from the land surface down to where the soil is saturated with ground water. Shallow saturated zones may lead to contamination of ground water. Most of the soils in the Adams and Cow Bayou tend to be saturated near the surface at least part of the year, which makes them inappropriate for septic fields.

7) tendency for subsidence

Soil subsidence may cause leaks or other malfunctions in the septic tank. Subsidence is not a major problem for many of the soils in these watersheds

Based on one or more of these factors, almost all of the soils in the Adams Bayou and Cow Bayou watersheds are very limited in their utility for septic tank absorption fields (Figure 3-5), according to the Soil Survey Geographic Database developed by the NRCS of the USDA (NRCS, 2016). Extensive site engineering may minimize the effects of some of these factors. A survey of septic tank failure in Texas (Reed Stowe and Yanke, 2001) estimated that the overall chronic malfunction rate of OSSF systems in east Texas was 19 percent, more than any other region in the state. The estimated chronic malfunction rate rose to 54 percent for systems installed in the fine-textured, clayey soils common in the Adams Bayou and Cow Bayou watersheds. In this region, the factor reported to have the highest impact on malfunction was unsuitable soils, followed by the high water table, then system age. Project stakeholders with knowledge of the watersheds, including septic system inspectors, believe that the actual rate of malfunction of conventional septic systems in these watersheds is close to 100 percent. They cited observations that almost all conventional systems had the cap removed from the septic field drain line, essentially conveying the septage directly from the tank to the ditch. In accordance with these estimates, it was assumed in the HSPF model that 95 percent of the conventional septic systems in these watersheds are malfunctioning.

Properly functioning conventional septic tank systems and aerobic systems were assumed to produce no pollutant loads to the bayous, while loads from malfunctioning septic tank systems were included in the HSPF model as loads to land and to the bayous. Flows from septic systems were estimated based on an average of 2.5 persons per household and 70 gallons of wastewater produced per person per day (Horsely and Whitten, 1996). Pollutant concentrations in septic tank effluent (Table 3-9) were estimated based on data provided by Metcalf and Eddy (1991) for medium strength waste.

In the HSPF model, data set numbers 8111 to 8115 represent the loads of cBOD, solids, water (flow), NH₃N, and PO₄P from a single failing OSSF. Ninety percent of the pollutant load from failing

OSSFs is applied to pervious land use category 116, present in the HSPF model at an amount of 0.1 acre per failing OSSF. The other 10 percent of the pollutant load from failing OSSFs is a direct load to surface water reaches.

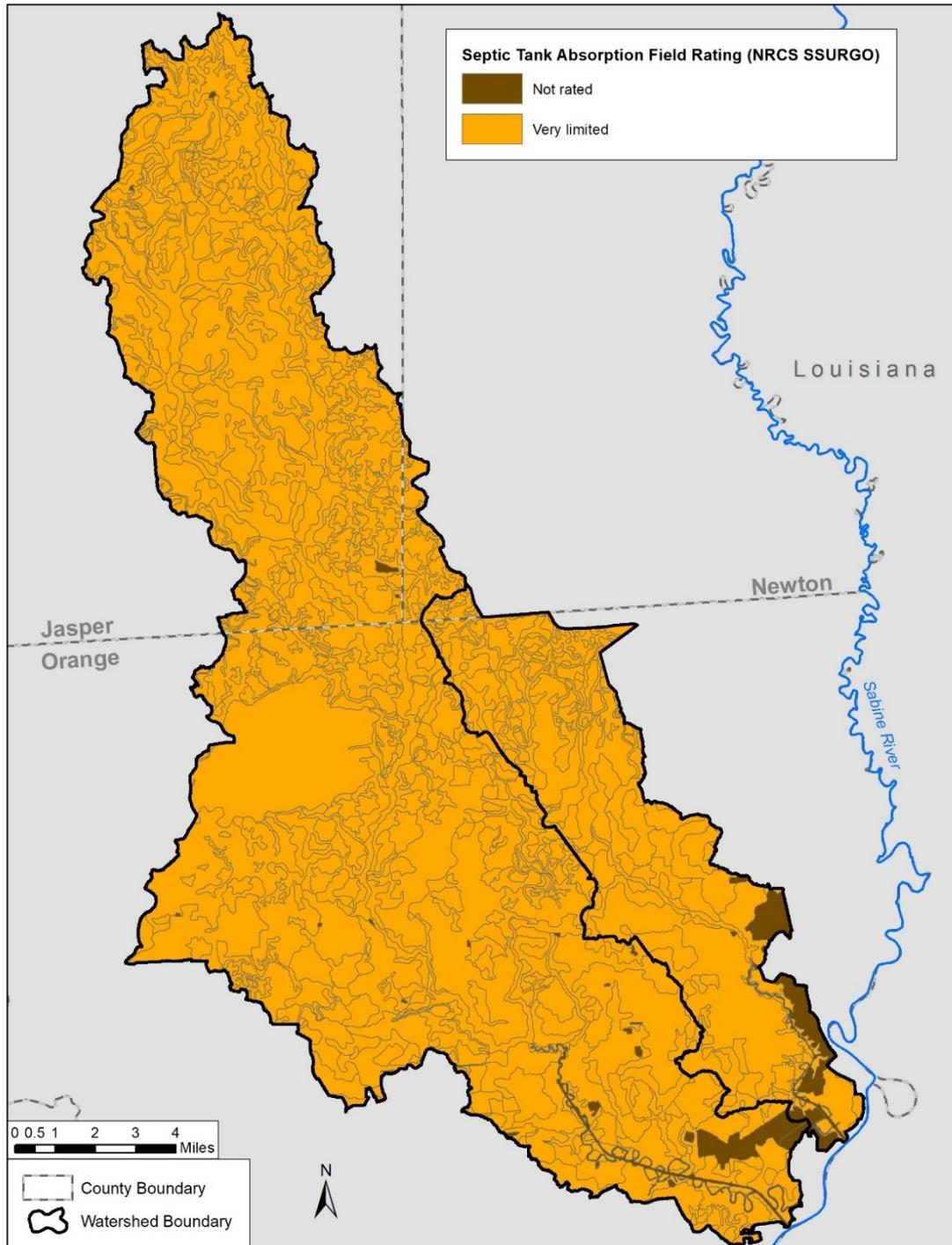


Figure 3-5 Soil suitability for septic fields in the Adams Bayou and Cow Bayou watersheds (USDA, 2016)

Table 3-9 Assumed pollutant concentrations in malfunctioning septic tank effluent

Parameter	Concentration
cBOD ₅	190 mg/L
TSS	210 mg/L
NH ₃ N	25 mg/L as N
PO ₄ P	5 mg/L as P

3.2.4.3 Wildlife

Very few data exist on the population size of wildlife species in the watersheds. The whitetail deer population in Jasper County has hovered around 50 per 1,000 acres, in Newton County, the deer population has stayed closer to 30 per 1,000 acres, according to information obtained from the Texas Parks and Wildlife Department website and reported in the initial HSPF modeling report (Parsons, 2006a). No deer population estimates were found for Orange County, which has a greater urban influence, and less forest. As with land use and agricultural census data, the wildlife data used were those thought to reflect conditions existing during model verification.

Wildlife were assumed to contribute pollutants to all land use categories and subwatersheds. The assumed populations of wildlife are shown in Table 3-10. Pollutant production rates of wildlife (Table 3-11) were estimated based on Schueler (2001) and other references in the Bacterial Indicator Tool (EPA, 2000). In cases where pollutant production rates from wildlife species were not available, they were estimated by multiplying the manure production rate estimate for the animal by the average pollutant concentration in manure for other animal species. While the levels of uncertainty in the wildlife populations and pollutant production rates are very large, sensitivity analyses showed that varying these numbers had little effect on the model outcome as wildlife were a relatively minor source.

Table 3-10 Assumed wildlife population densities for various land use categories

Species	Population Density (animals/ square mile)					
	Cropland	Wetlands	Pasture	Forest	Grassland	Residential
Deer	20	50	20	50	10	40
Waterfowl	10	128	10	0	0	0
Other birds	100	1,500	1,000	1,500	1,500	1,500
Opossum	20	100	50	100	20	50
Raccoon	4	100	4	100	20	50
Rodents	2,000	2,000	2,000	2,000	2,000	2,000

Table 3-11 Pollutant production rates of wildlife

Animal	cBOD ₅ Production (lb/animal/day)	NH ₃ N Production (lb/animal/day)	PO ₄ P Production (lb/animal/day)
Deer	0.050	3.3E-3	3.2E-3
Waterfowl	0.011	7.4E-4	7.1E-4
Other birds	0.0006	3.7E-5	3.5E-5
Opossum	0.028	1.8E-3	1.8E-3
Raccoon	0.10	6.5E-3	6.3E-3
Rodents	0.0027	1.8E-4	1.7E-4

3.2.4.4 Atmospheric Deposition

Atmospheric deposition was assumed to contribute NH₃N and NO₃N to all land uses via wet (precipitation) and dry (particle) deposition. Annual wet and dry deposition rates of ammonia and nitrate nitrogen for the project watersheds were estimated from isopleth maps prepared by the National Atmospheric Deposition Program (NADP, 2005). and summarized in Table 3-12.

Table 3-12 Total average atmospheric loadings of pollutants

Year	NO ₃ N (lb/acre/yr)	NH ₃ N (lb/acre/yr)
2001	2.58	2.08
2002	2.80	2.57
2003	2.32	2.64
2004	2.32	2.29
2005	2.14	2.22
2006	2.22	2.50
2007	2.24	2.29
2008	1.87	2.01
2009	1.55	2.08
2010	1.29	1.32
2011	1.39	1.87
2012	2.06	2.17

3.2.4.5 Forest Leaf Litter

Forest leaf litter deposition can be a nonpoint source of nitrogen, phosphorus, and cBOD to waters. An estimated 30 pounds of nitrogen and 2 pounds of phosphorus are deposited in leaf litter per acre of forest per year, based on the measurements of Finzi et al. (2001) for a mature loblolly pine/hardwood forest, similar to the dominant type in the Adams and Cow Bayou watersheds. The nitrogen was assumed to be NH₃N, phosphorus assumed to be PO₄P, and a cBOD₅/nitrogen ratio of 5.0 was used to estimate the cBOD₅ content. Evergreen forests were assumed to deposit leaf litter evenly throughout the year, while litter fall from deciduous forests was assumed to occur primarily in October and November, and mixed forests leaf litter combined the aspects of evergreen and deciduous forests.

3.2.4.6 Residential Area Nonpoint Sources

Potential nutrient pollutant sources in residential areas that were considered in the model include malfunctioning septic systems, dog and cat fecal waste, wildlife fecal waste, and lawn fertilizer. Malfunctioning septic systems were described previously and incorporated in the model independently. The populations of dogs and cats were estimated based on the number of households in each subwatershed, along with the national average numbers of 0.58 dogs and 0.66 cats per household, from the American Veterinary Medicine Association (AVMA, 2002). As with land use and agricultural census data and wildlife population data, the household pet population data used were thought to reflect conditions existing during model verification period. Estimates of pollutant loadings to residential land in pet fecal waste are summarized in Table 3-13. It was assumed that 100 percent of dog feces and 50 percent of cat feces was applied outdoors. Of the outdoor applied dog feces, 20 percent was assumed to be collected and removed to a landfill.

Table 3-13 Pollutant production rates of dogs and cats

Animal	BOD₅ Production (lb/animal/day)	NH₃N Production (lb/animal/day)	PO₄P Production (lb/animal/day)
Dog	0.10	6.5E-3	6.3E-3
Cat	0.028	1.8E-3	1.8E-3

To estimate the amount of commercial fertilizer applied to lawns, it was assumed that:

- 50 percent of the residential land was covered by turf grasses,
- nitrogen was applied to turf at the rate of 4 lbs of NH₃N per 1,000 square feet (ft²) per year, and
- phosphorus was applied at a rate of 2 lbs of PO₄P per 1,000 ft² per year.

These assumptions are in line with the low end of Texas Agricultural Extension recommendations for St. Augustine and Bermuda grass lawns in eastern Texas. It was assumed that 49 percent of the applied nutrients were collected and removed to the landfill each year as grass clippings and other yard waste (Baker et al., 2001).

3.2.5 Permitted PS Discharge Facilities

There are only two active Texas Pollution Discharge Elimination System (TPDES) permitted facilities discharging into the above tidal reaches of Cow Bayou, and none in the above tidal reaches of Adams Bayou. These facilities are

- TPDES WQ0010808-001 – Jasper County Water Control and Improvement District 1
- TPDES WQ0002835-000 – Miller Waste Mills, Inc. (three outfalls)

These facilities occur in sub-basins 1 and 11, respectively, of the Cow Bayou HSPF model. Point source flows and loadings of cBOD, NH₃N, and DO in discharges from these facilities were set in the model at their actual self-reported discharges for calibration runs, and at the discharge limits in their TPDES permits for non-calibration scenarios. All of the other existing PS discharges are to tidal reaches of the bayous and, as such, they are incorporated into the RMA2 hydrodynamic and WASP water quality models rather than the HSPF model. However, a placeholder for future point sources to above tidal reaches has been included in each sub-basin in the HSPF model.

3.2.6 Municipal Separate Stormwater Systems

In 1990, EPA developed Phase I of the National Pollutant Discharge Elimination System (NPDES) Stormwater Program for Municipal Separate Storm Sewer Systems (MS4s). A MS4 is defined in 40 CFR 122.26(b)(8) as “a conveyance or system of conveyances (including roads with drainage systems, municipal streets, catch basins, curbs, gutters, ditches, man-made channels, or storm drains):

- (i) Owned or operated by a State, city, town, borough, county, parish, district, association, or other public body (created by or pursuant to State law)...including special districts under State law such as a sewer district, flood control district or drainage district, or similar entity, or an Indian tribe or an authorized Indian tribal organization, or a designated and approved management agency under section 208 of the Clean Water Act that discharges into waters of the United States.
- (ii) Designed or used for collecting or conveying stormwater;
- (iii) Which is not a combined sewer; and
- (iv) Which is not part of a Publicly Owned Treatment Works (POTW) as defined at 40 CFR 122.2.

The NPDES Stormwater program was designed to prevent harmful pollutants in MS4s from being washed by stormwater runoff into local water bodies (EPA, 2005). Phase I of the program

required operators of medium and large MS4s (those generally serving populations of 100,000 or greater) to implement a stormwater management program as a means to control polluted discharges. Approved stormwater management programs for medium and large MS4s are required to address a variety of water quality-related issues, including roadway runoff management, municipal-owned operations, and hazardous waste treatment. There are no Phase I MS4s in the watersheds of Adams Bayou or Cow Bayou.

In 1999, Phase II began requiring certain small regulated MS4s located in “urbanized areas” to comply with the NPDES stormwater program. Small MS4s are defined as any MS4 that is not a medium or large MS4 covered by Phase I of the NPDES Stormwater Program. The boundaries of “urbanized areas” are defined by the U.S Bureau of the Census, and generally involve a population density of at least 1,000 people per square mile and a total population of at least 10,000 people. Phase II requires operators of regulated small MS4s to obtain NPDES permits and develop a stormwater management program. The programs are designed to reduce discharges of pollutants to the “maximum extent practicable,” to protect water quality, and to satisfy appropriate water quality requirements of the CWA. Phase II MS4 stormwater programs must address the following six minimum control measures:

- Public Education, Outreach, and Involvement
- Illicit Discharge Detection and Elimination
- Construction Site Runoff Control
- Post- Construction Stormwater Management in New Development and Redevelopment
- Pollution Prevention and Good Housekeeping for Municipal Operators
- Industrial stormwater Sources

Discharges of stormwater from a Phase II MS4 areas are required to be covered under TPDES general permit TXR040000. There are five Phase II MS4 authorizations within the Adams Bayou watershed and two within the Cow Bayou watershed. The area within each HSPF model sub-basin that is within each MS4 is listed in Table 3-14 (Adams Bayou) and Table 3-15 (Cow Bayou). Most of these MS4s are discrete cities, but the Orange County Drainage District and Orange County jointly address those portions of the urbanized areas that do not fall within city limits.

For the purpose of TMDL load allocations, MS4s are treated as point sources of pollutants even though they originate from diffuse locations.

Table 3-14 Areas of Adams Bayou watersheds within MS4s, in acres

Sub-basin	Total Sub-basin Area	Urbanized Area	City of Orange (TXR040430)	City of Pinehurst (TXR040428)	City of West Orange (TXR040431)	Orange County (TXR040030)	Orange County Drainage District (TXR040029)
1	1,864	18	6				12
2	13,584	0					
3	1,144	53	49				4
4	1,268	86	77				9
5	2,019	962	861	101			
6	1,311	476	397	53			26
7	1,051	1,068	369	699			
8	1,180	1,170	1046	100			24
9	932	730			717		13
10	2,217	2,217	1229	255	733		
11	1,490	1,012	243		524		245
12	1,601	505	224		49		232

Table 3-15 Areas of Cow Bayou watersheds within MS4s, in acres

Sub-basin	Total Sub-basin Area	Urbanized Area	City of Orange (TXR040430)	City of Vidor (TXR040028)	City of West Orange (TXR040431)	City of Bridge City (TXR040429)	Orange County (TXR040030)	Orange County Drainage District (TXR040029)
1	17,801	0						
2	13,389	0						
3	10,036	0						
4	12,487	0						
5	8,600	0						
6	5,063	2,859		1,702				1,157
7	8,288	0						
8	11,740	631		150				481
9	2,913	0						
10	2,160	3	3					
11	5,641	533	334					199
12	2,993	0						
13	8,609	1,239		1,184				55
14	3,013	6						6
15	4,074	1,118	243		4			871
16	4,011	1,524				856		669
17	4,049	1,537	7		59			1,471
18	2,302	52				6		46

3.3 HSPF Model Verification

Model calibration and validation, which collectively are referred to as verification, are defined as follows:

- Calibration—The first stage testing and tuning of a model to a set of observational data, such that the tuning results in a consistent and rational set of theoretically defensible input parameters.
- Validation—Subsequent testing of a calibrated model to additional observational data to further examine model validity and preferably under different external conditions from those used during calibration (Thomann and Mueller, 1987).

The HSPF models were hydrologically calibrated to measured daily flows from USGS gauge 08031000 on Cow Bayou near Mauriceville (Figure 3-2). This is the only flow gauge within either watershed. The flow calibration period was from October 1, 2002 through December 31, 2012. Model calibration statistics such as the coefficient of determination (r^2), mean error (ME), mean absolute error (MAE), root-mean-square error (RMSE), and Nash-Sutcliffe modeling efficiency (NSE) (Nash and Sutcliffe, 1970), were used as quantitative measures of model fit to supplement the visual evaluation of fit. The formulas for model fit statistics are provided below, where y_i is the measured value, \hat{y}_i is the model predicted value, an overscore indicates a mean value, and n is the number of measurements.

Coefficient of Determination

$$r^2 = \left\{ \frac{\sum_{i=1}^n (y_i - \bar{y})(\hat{y}_i - \bar{\hat{y}})}{\left[\sum_{i=1}^n (y_i - \bar{y})^2 \right]^{0.5} * \left[\sum_{i=1}^n (\hat{y}_i - \bar{\hat{y}})^2 \right]^{0.5}} \right\}^2$$

Root Mean Square Error

$$RMSE = \left\{ \left[\sum (y_i - \hat{y}_i)^2 \right] / n \right\}^{0.5}$$

Nash-Sutcliffe Efficiency

$$NSE = 1 - \frac{\sum_{i=1}^n (y_i - \hat{y}_i)^2}{\sum_{i=1}^n (y_i - \bar{y})^2}$$

Mean Error

$$ME = \left(\sum_{i=1}^n (y_i - \hat{y}_i) \right) / n$$

Mean Absolute Error

$$MAE = \left(\sum_{i=1}^n |y_i - \hat{y}_i| \right) / n$$

The primary calibration targets were the flow duration curve (percentiles of the flow distribution), annual, seasonal, and monthly flows. The calibration fits are illustrated in Figures 3-6 to 3-9. The primary model calibration goal was a NSE and r^2 value for simulated and observed daily flow of greater than 0.4. Also, simulated and observed total and seasonal (monthly) flows were to agree within 20 percent. All calibration targets were met. Hydrologic goodness-of-fit is summarized in Table 3-16.

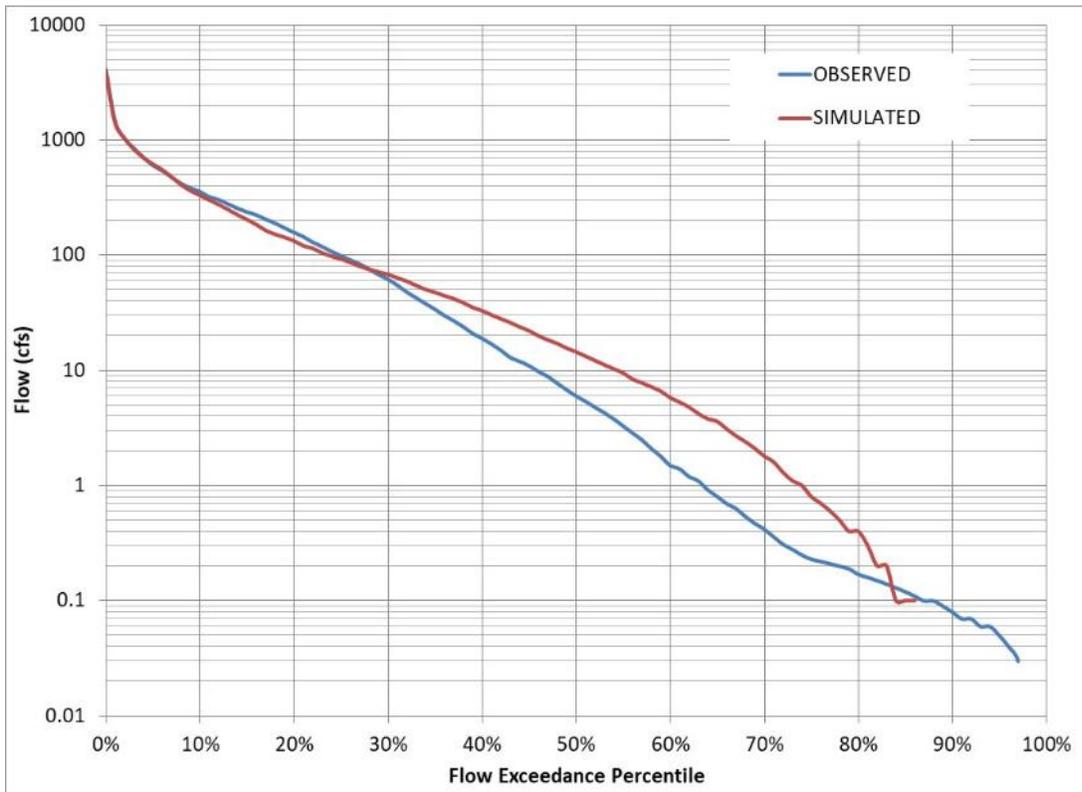


Figure 3-6 Observed and simulated flow duration curves for Cow Bayou

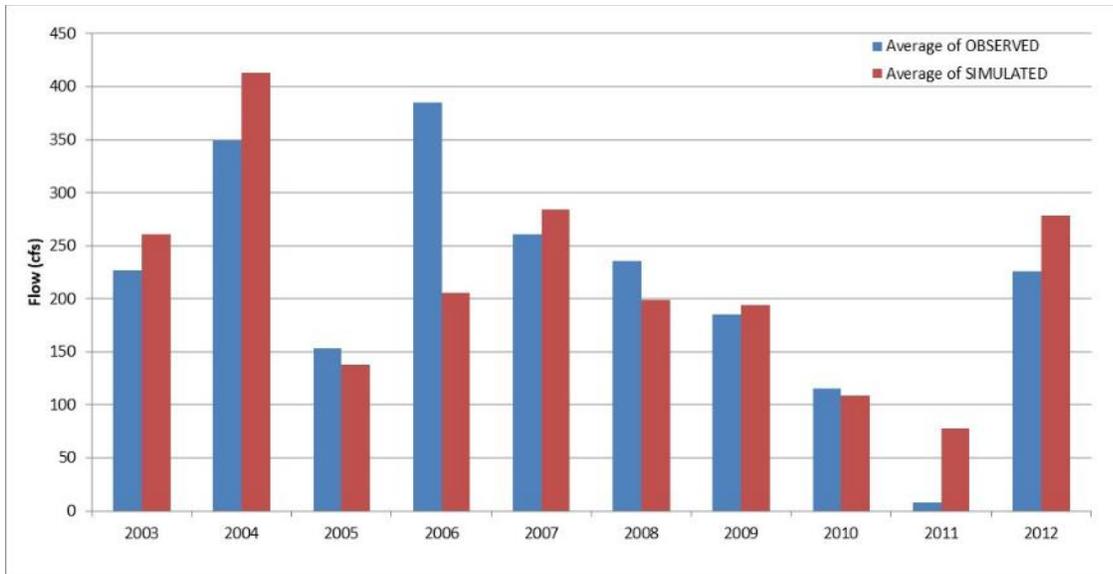


Figure 3-7 Observed and simulated annual average flows for Cow Bayou

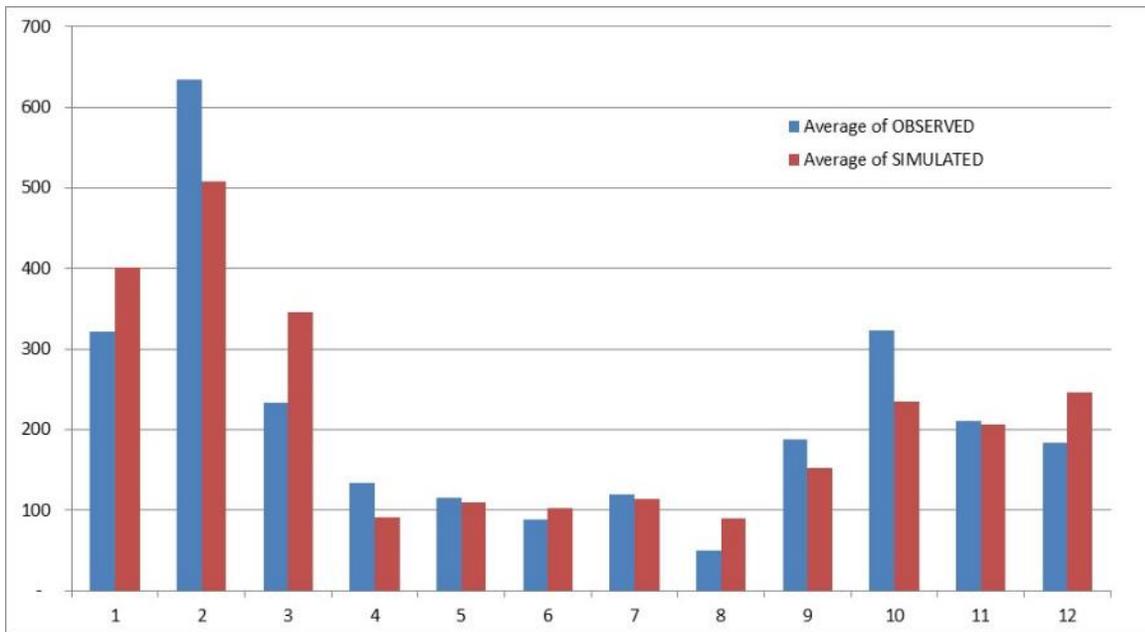


Figure 3-8 Observed and simulated average monthly flows for Cow Bayou

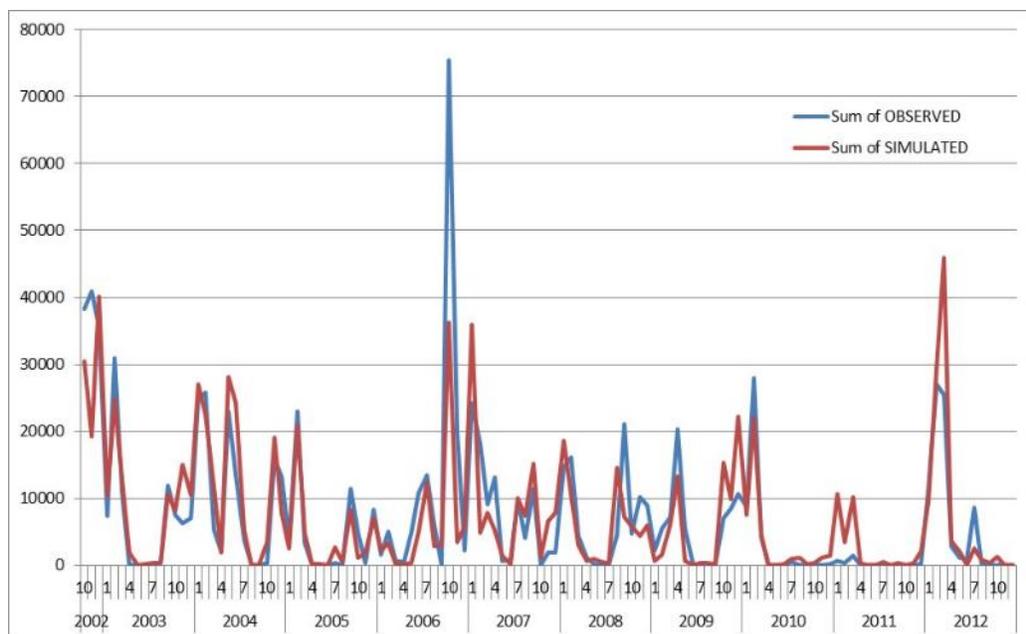


Figure 3-9 Observed and simulated total monthly flows for Cow Bayou

Table 3-16 Goodness-of-fit for HSPF Cow Bayou model hydrologic calibration

Period	Quantity	Percent Difference	Statistic			
			MAE (cfs)	RMSE (cfs)	NSE	r ²
Daily	Flow		4.71	7.51	0.405	0.529
Monthly	Flow		1.27	1.34	0.807	0.808
Annual	Flow		1.48	2.13	0.559	0.579
Winter	Total Flow	+5.72%				
Spring	Total Flow	-10.34%				
Summer	Total Flow	-0.27%				
Autumn	Total Flow	-4.05%				
Full Period	Total Flow	-2.40%				

Water quality calibration of the HSPF model was performed by comparing model-predicted water quality to water quality data collected during stormwater runoff events. There were three monitoring stations in the Adams Bayou subwatersheds and three in the Cow Bayou subwatersheds. The data that served for calibration were collected on January 8 - 10 and June 16 - 17, 2004. The data used for validation were collected January 11 - 23 and November 2 - 4, 2004.

The calibration was limited by a dearth of runoff events and scarcity of water quality monitoring stations on non-tidal reaches. Model parameters were adjusted within physically realistic ranges used in prior modeling studies to ensure that the average model concentrations were similar to

the average of measured concentrations, and that the range of model concentrations encompassed the measured concentrations. A quantitative calibration target was that average predicted concentrations of TSS, cBOD₅, NH₃N, NO₃N, PO₄P, and DO fall within a range calculated as the mean of the observed concentrations plus or minus two standard deviations. These calibration and validation goals were met (Table 3-17).

Concentration time series comparisons indicate that the model captures the typical levels of water quality constituents, but does not precisely match every storm event at every station. Given the uncertainties in the rainfall data and other model input data, the HSPF model is not designed to reliably simulate pollutant concentration time series for individual storm events, but rather to simulate pollutant loadings over a longer period of time. Thus, the model was deemed to meet project objectives.

Table 3-17 Calibration and validation of HSPF model for water quality (Cow and Adams Bayous considered jointly)

Parameter	Event	Measured					Simulated			
		N	Min	Max	Mean	SD	Min	Max	Mean	Meets?
TSS	Cal	17	11	85	31	21	0.4	162	40	Yes
TSS	Ver	20	10	154	39	41	0.1	230	47	Yes
cBOD	Cal	17	<2	6	3.8	1.3	1.8	16	4.6	Yes
cBOD	Ver	20	<2	4	3.0	0.7	2.3	9	3.6	Yes
NH ₃ N	Cal	17	.02	0.41	0.18	0.09	0.06	0.99	0.26	Yes
NH ₃ N	Ver	20	.04	0.46	0.14	0.10	0.09	0.70	0.23	Yes
NO ₃ N	Cal	17	.04	0.23	0.09	.06	0	0.45	0.10	Yes
NO ₃ N	Ver	20	.04	0.21	0.08	.06	0	0.27	0.10	Yes
OrgN	Cal	17	0.41	1.49	0.90	0.23	0.34	1.94	0.72	Yes
OrgN	Ver	20	0.38	1.73	0.94	0.31	0.34	1.06	0.57	Yes
PO ₄ P	Cal	17	0.04	0.56	0.15	0.15	0.01	0.88	0.16	Yes
PO ₄ P	Ver	20	.04	0.53	0.16	0.13	0.01	0.41	0.09	Yes
DO	Cal	17	3.7	9.6	7.1	2.0	4.5	10.9	7.1	Yes
DO	Ver	20	4.4	9.4	6.4	1.3	4.8	9.8	6.6	Yes

The User Control Input files (UCI) for the HSPF models, listing all calibrated and non-calibrated parameters, are provided in their entirety in Appendix A (Adams Bayou) and Appendix B (Cow Bayou).

4. RMA2 Hydrodynamic Model

RMA2 is a two-dimensional, vertically averaged, finite element hydrodynamic model supported by the U.S. Army Corps of Engineers. It computes water surface elevations and horizontal velocities for subcritical, free-surface two-dimensional flows. The RMA2 model is comprised of elements and nodes. Elements represent a finite stretch of the channel of a bayou, and hold water. Each element is composed of three or more nodes. Nodes are the points where water surface elevation and velocity calculations are performed, and all linkages between elements occur at nodes. The elements have a trapezoidal shape with characteristic channel bottom width and side slope, which may vary by element to reflect the local shape of the channel (Figure 4-1). Elements may also have off-channel water storage, which is useful for simulating inundated areas such as wetlands, or oxbow channels and reservoirs linked to the main channel. The depth-dependent geometry of the off-channel storage may also be varied to reflect the actual geometry.

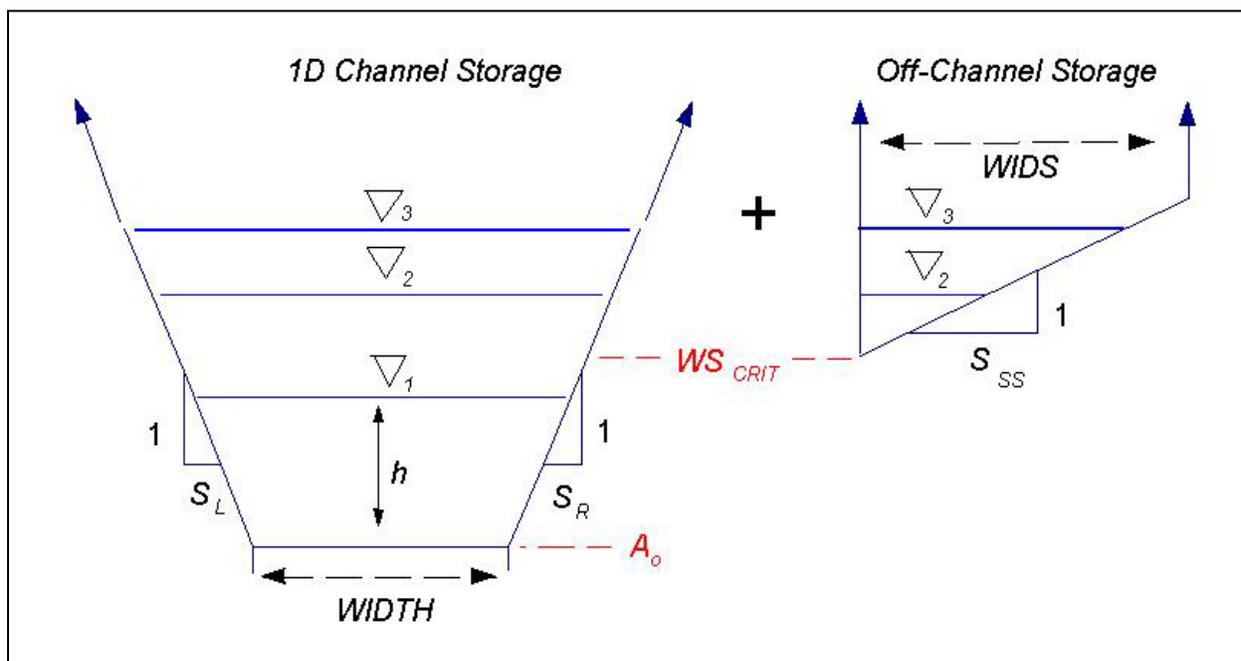


Figure 4-1 RMA2 element (channel) geometry

4.1 RMA2 Model Description

Separate hydrodynamic models were developed for the Adams Bayou and Cow Bayou systems. Both models extend from the Sabine River (the downstream boundary) to near the upstream limits of tidal influence of each bayou and their tributaries. Oxbow channels were also included in the model, either explicitly modeled as discrete elements or included as off-channel water storage attached to the main channel. Figures 4-2 (a-c) and 4-3 (a-e) illustrate the RMA2 model segmentation of Adams Bayou and Cow Bayou, respectively. Adams Bayou and Cow Bayou were

simulated with 1-dimensional model elements for simplicity. Table 4-1 includes a summary of RMA2 model segmentation and key parameters.

Table 4-1 RMA2 model summary

Item	Description
Version/Date	RMA2 version 4.5 (5/16/2013 3:08 PM)
Model Period	1/1/2002 – 12/31/2012
Time Step	half-hour
Number of Nodes	153 (Adams Bayou); 159 (Cow Bayou)
Number of Elements	76 (Adams Bayou); 80 (Cow Bayou)
Units	Metric
Friction	Calibrated using Manning's n (values from 0.03 to 0.11 depending on channel properties and water depth)

The key RMA2 model input files include a geometry file and a run control file that lists boundary condition time series. These model files are provided in Appendix C (Adams Bayou) and Appendix D (Cow Bayou).

4.2 RMA2 Inputs and Data Sources

The bottom elevations of the bayous were estimated from measurements made during the field intensive surveys.

Tidal water surface oscillations in the Sabine River drive tidal water movements through the Adams Bayou and Cow Bayou systems. Tide height data from a continuous gauge at the Rainbow Bridge (where SH 87 crosses the Neches River just upstream from Sabine Lake) were used as the Sabine River downstream boundary water surface elevation condition in the models. Water elevations measured with tide gauges deployed near the mouth of Adams and Cow Bayou during the field intensive surveys were not significantly different from those recorded at the Rainbow Bridge gauge. The average daily tidal range at the Rainbow Bridge is 0.284 m (0.93 ft).

Upstream inflows to the model from above tidal reaches were predicted by the calibrated HSPF watershed models and entered as boundary inflows to a number of tributaries. The locations of HSPF inputs are shown in Tables 4-2 and 4-3, which list the linkages of the RMA2 models systems for Adams and Cow Bayous, respectively. Point source discharge inflows were included in the RMA2 model as boundary inflows in the locations identified in Figures 4-2 and 4-3.

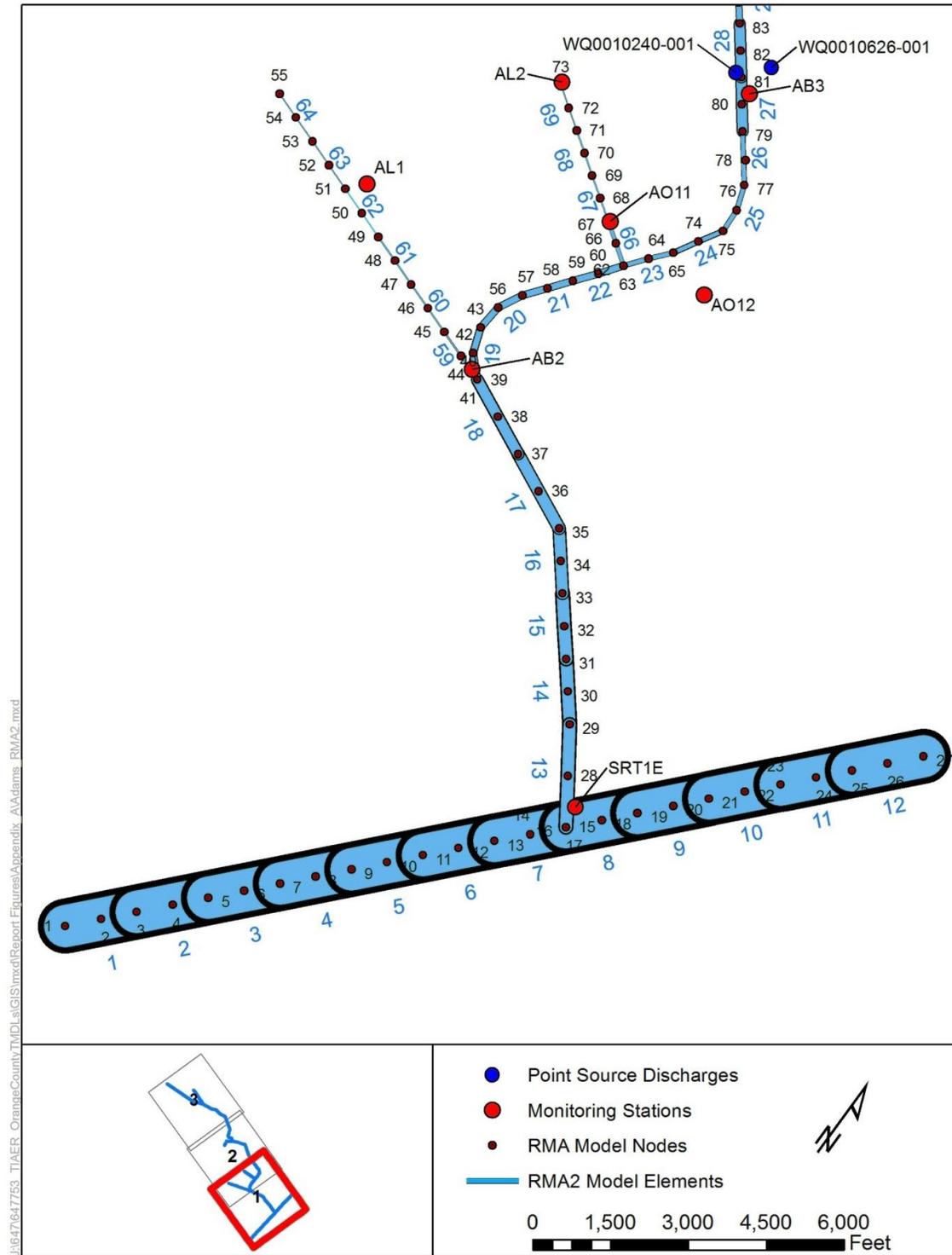


Figure 4-2a Adams Bayou RMA2 model segmentation

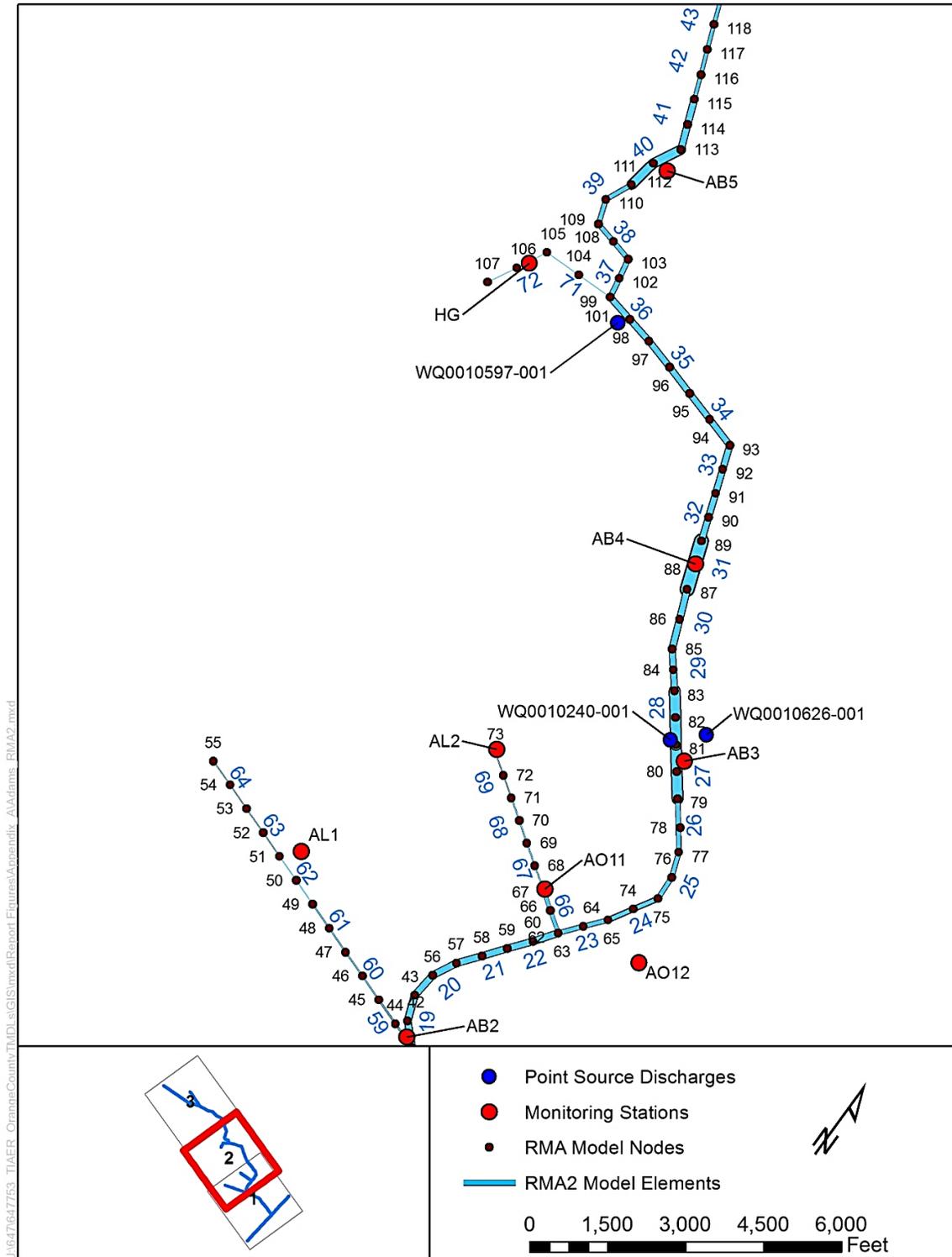


Figure 4-2b Adams Bayou RMA2 model segmentation

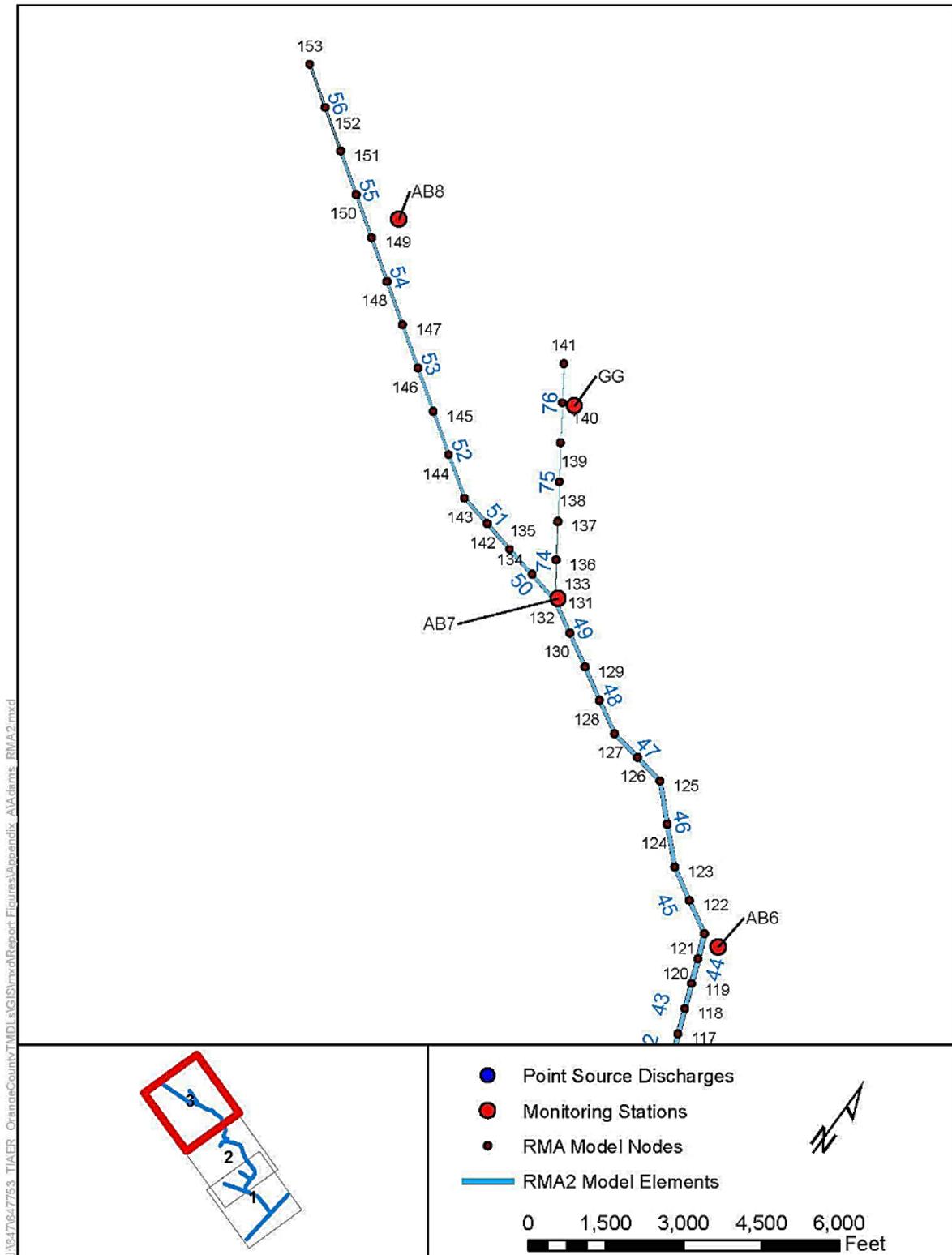


Figure 4-2c Adams Bayou RMA2 model segmentation

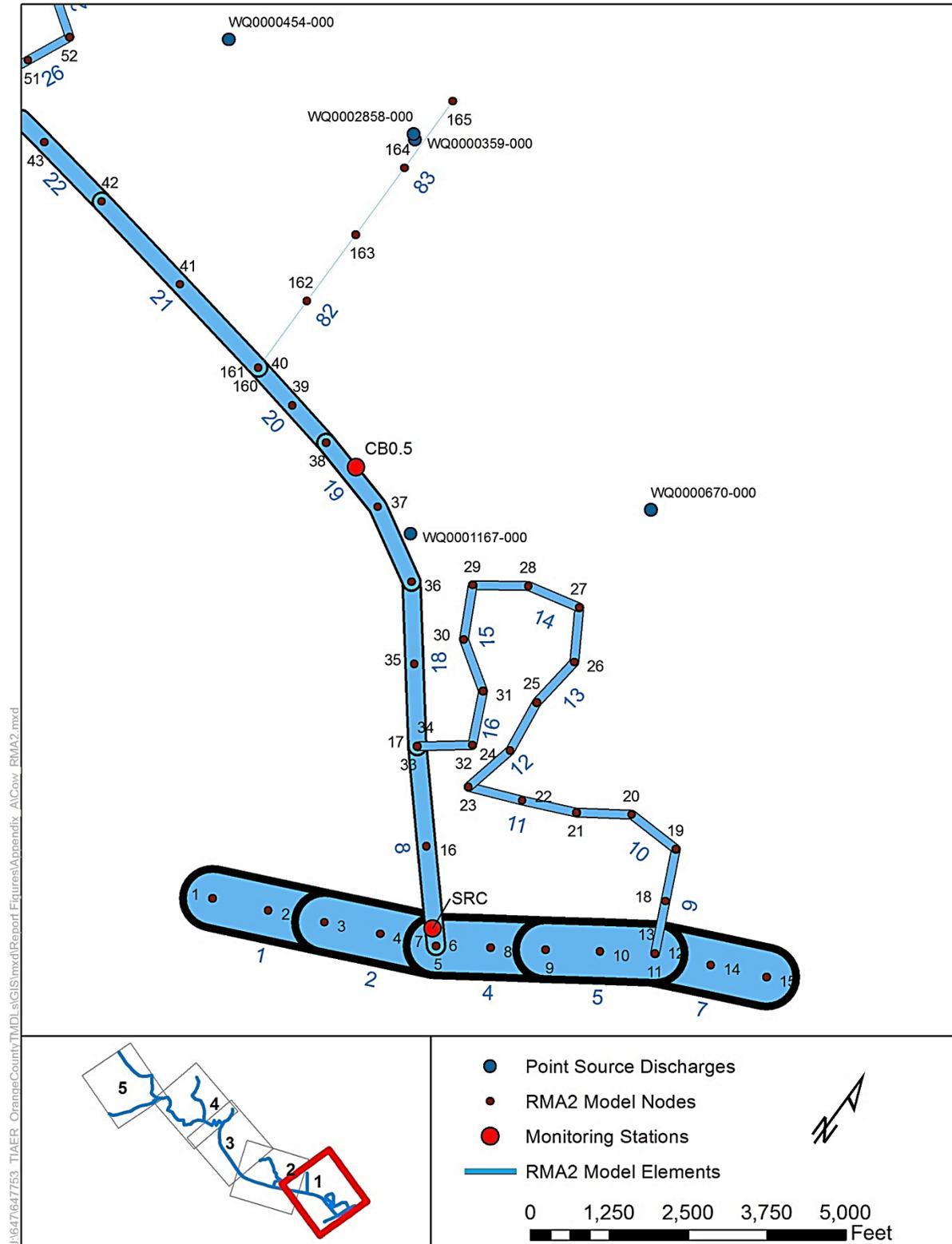


Figure 4-3a Cow Bayou RMA2 model segmentation

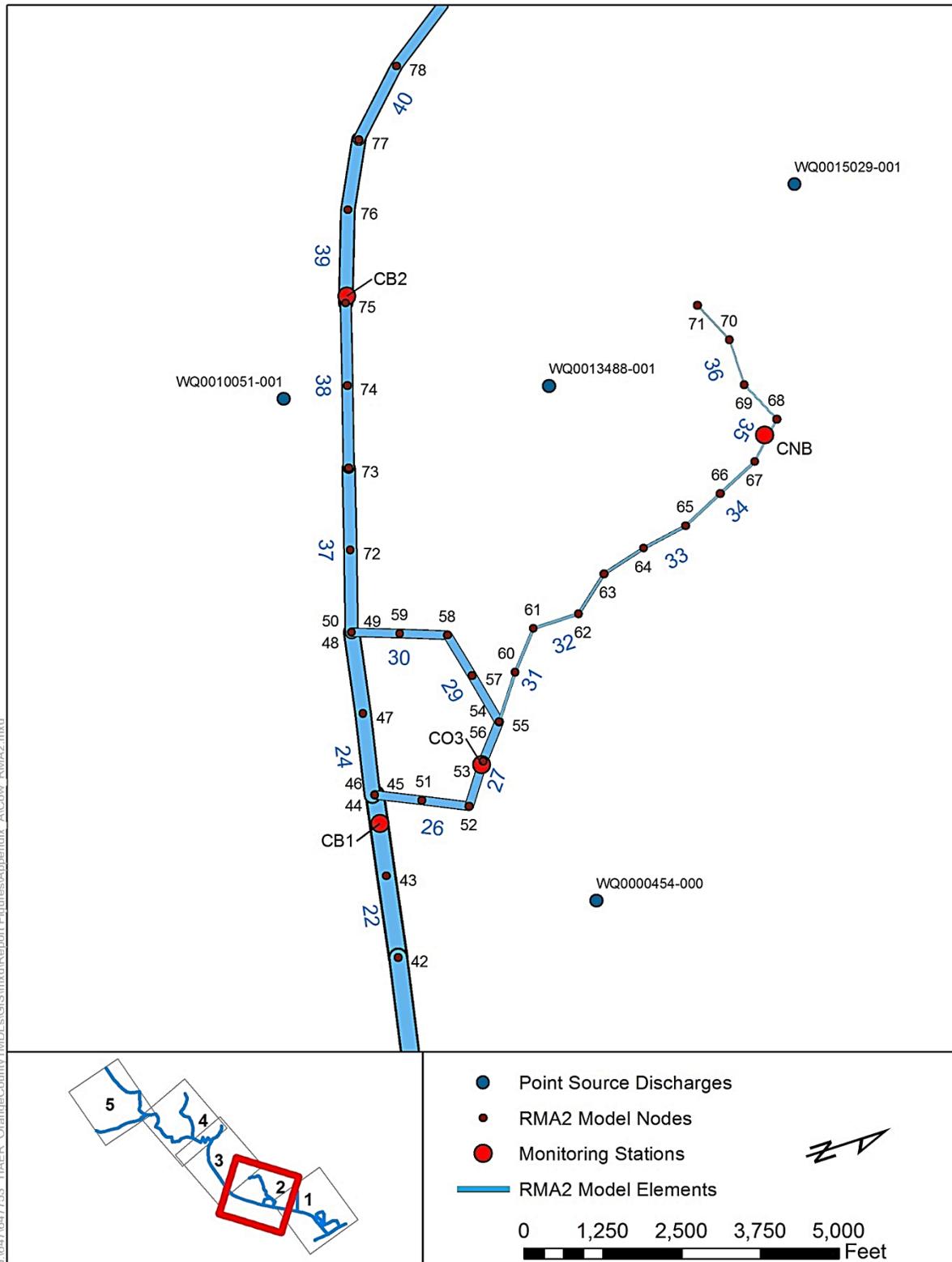


Figure 4-3b Cow Bayou RMA2 model segmentation

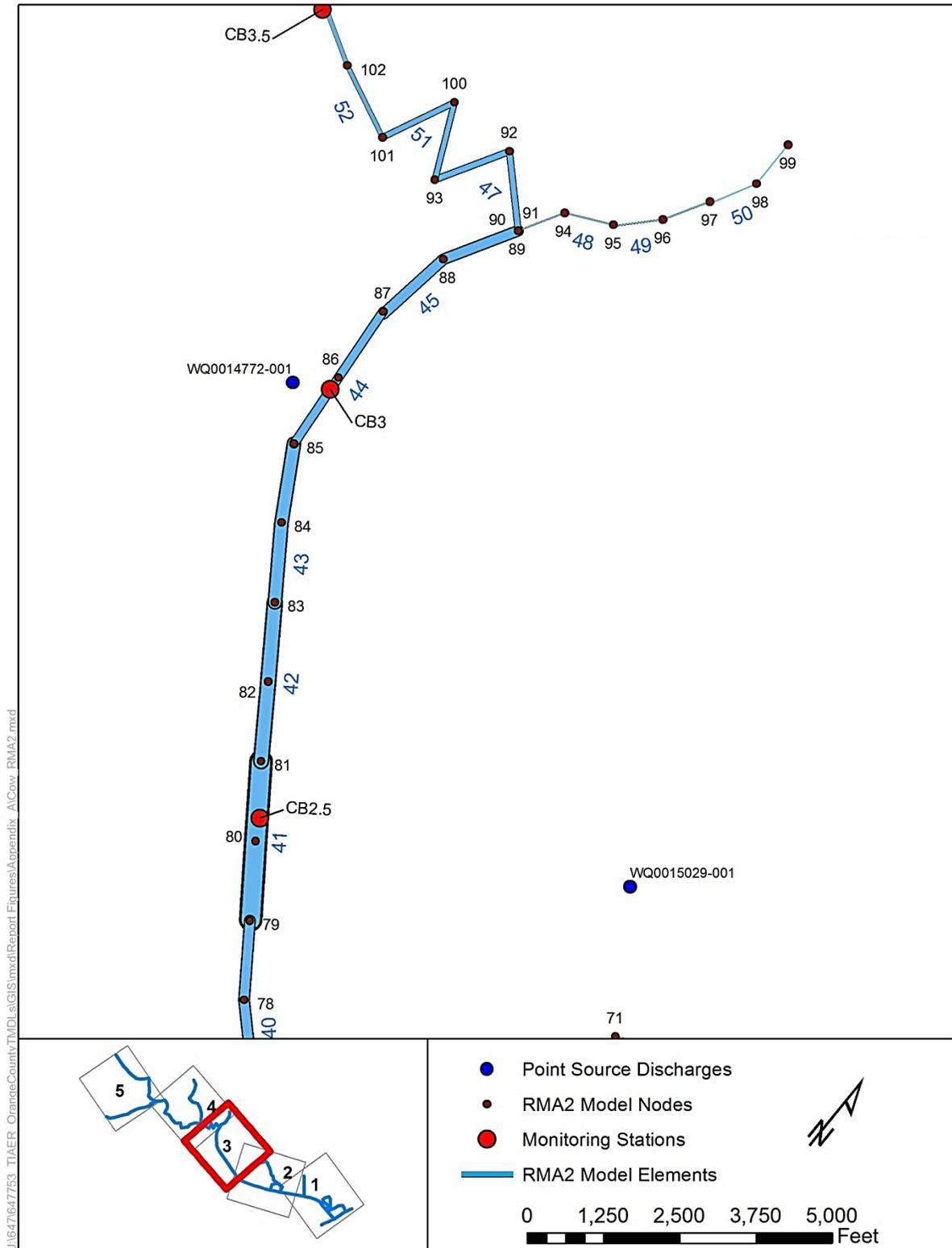


Figure 4-3c Cow Bayou RMA2 model segmentation

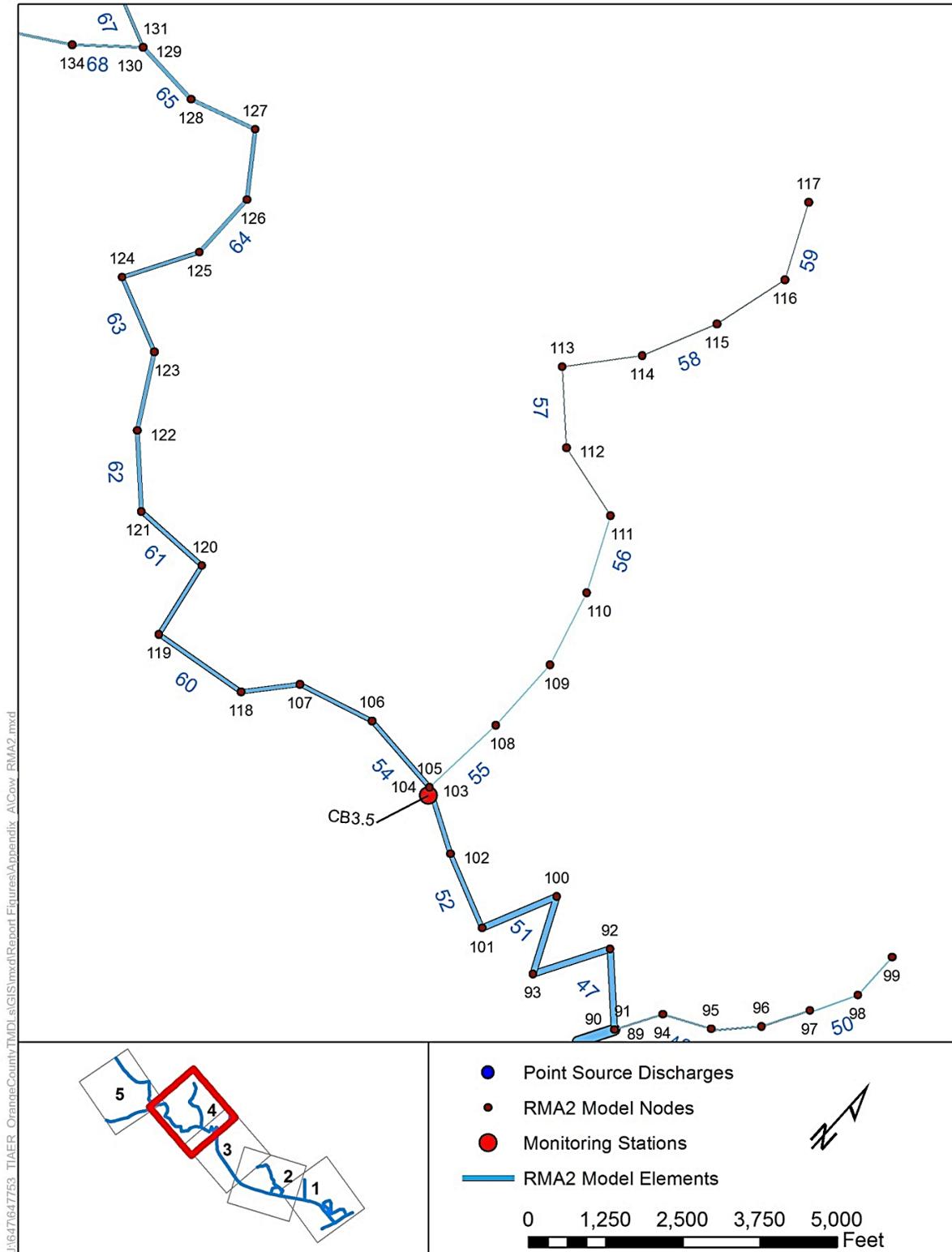


Figure 4-3d Cow Bayou RMA2 model segmentation

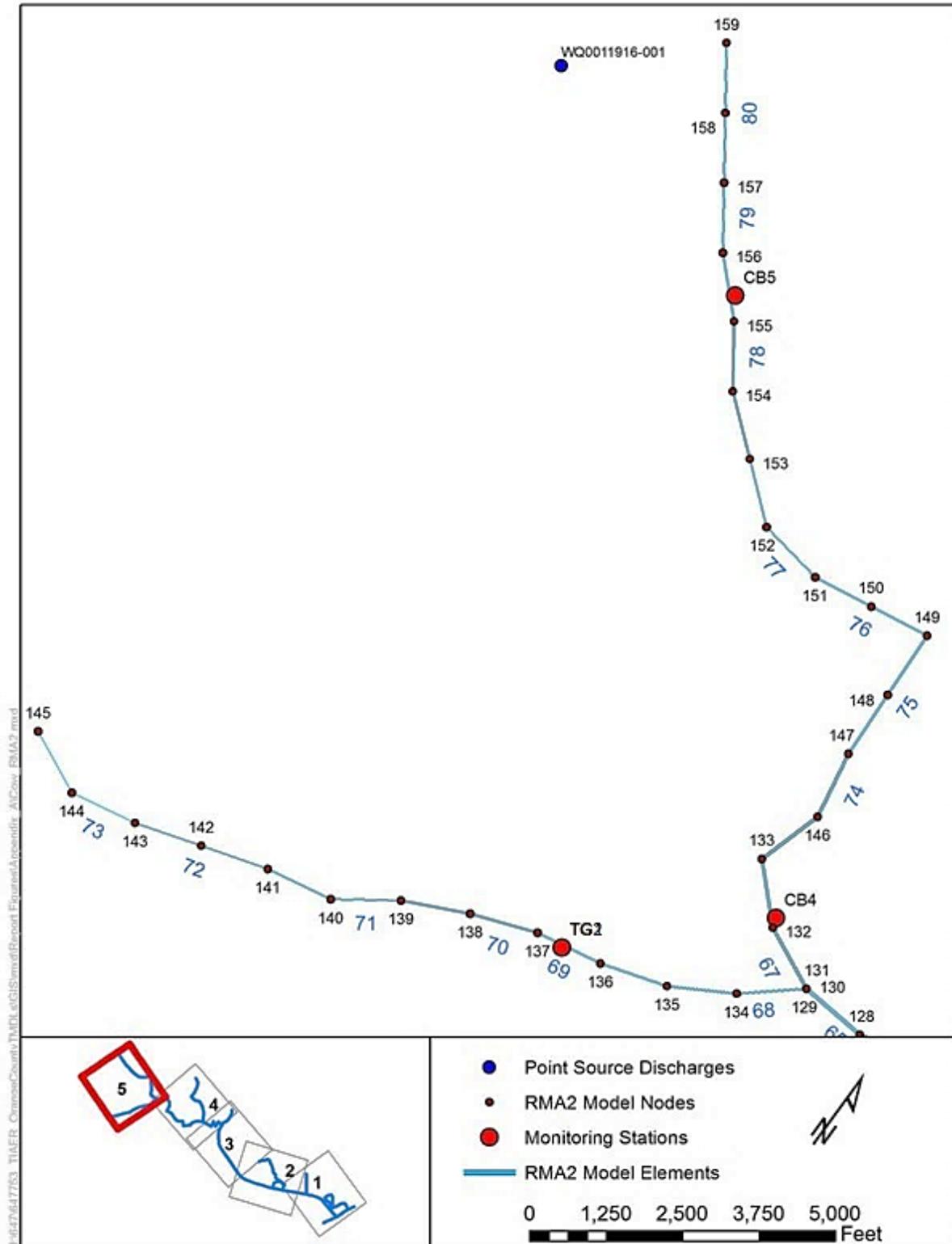


Figure 4-3e Cow Bayou RMA2 model segmentation

Table 4-2 Flow/elevation linkages for the Adams Bayou RMA2 model

Source	Type	RMA Linkage	Frequency	Fraction of Total Flow to Node/Element	Assessment Unit or Location Description
HSPF Sub-basin 1	Inflow	Node 141	Hourly	1.000	0508B_01
HSPF Sub-basin 2	Inflow	Node 153	Hourly	1.000	0508A_01
HSPF Sub-basin 3	Inflow	Element 74	Hourly	1.000	0508B_01
HSPF Sub-basin 4	Inflow	Element 51	Hourly	1.000	0508A_01
HSPF Sub-basin 5	Inflow	Element 47	Hourly	0.696	0508_04
		Element 49	Hourly	0.304	0508A_01
HSPF Sub-basin 6	Inflow	Element 50	Hourly	1.000	0508A_01
HSPF Sub-basin 7	Inflow	Element 41	Hourly	1.000	0508_04
HSPF Sub-basin 8	Inflow	Element 72	Hourly	1.000	0508C_01
HSPF Sub-basin 9	Inflow	Node 73	Hourly	1.000	0508_01
HSPF Sub-basin 10	Inflow	Element 25	Hourly	0.183	0508_01
		Element 27	Hourly	0.294	0508_02
		Element 35	Hourly	0.523	0508_03
HSPF Sub-basin 11	Inflow	Node 55	Hourly	1.000	0508_01
HSPF Sub-basin 12	Inflow	Element 15	Hourly	1.000	0508_01
USGS Gauge 08030500	Inflow	Node 27	Daily	1.000	Sabine River near Ruliff
WQ0010597-001	Inflow	Element 36	Constant	1.000	City of Pinehurst
WQ0010626-001	Inflow	Element 28	Constant	1.000	City of Orange
WQ0010240-001	Inflow	Element 28	Constant	1.000	Orange County WCID 2
Rainbow Bridge water level	boundary elevation	Node 1	30 minutes	Not Applicable	Downstream boundary

Table 4-3 Flow/elevation linkages for the Cow Bayou RMA2 model

Source	Type	RMA Linkage	Frequency	Fraction of Total Flow to Node/Element	Assessment Unit or Location Description
HSPF sub-basin 7	Inflow	Node 117	Hourly	1.000	0511C_01
HSPF sub-basin 8	Inflow	Element 78	Hourly	0.131	0511_04
		Node 159	Hourly	0.869	0511A_01
HSPF sub-basin 9	Inflow	Element 74	Hourly	0.698	0511_03
		Element 75	Hourly	0.302	0511_04
HSPF sub-basin 10	Inflow	Element 58	Hourly	1.000	0511C_01
HSPF sub-basin 11	Inflow	Node 99	Hourly	1.000	0511_02
HSPF sub-basin 12	Inflow	Element 54	Hourly	0.079	0511_02
		Element 64	Hourly	0.921	0511_03
HSPF sub-basin 13	Inflow	Node 145	Hourly	1.000	0511E_01
HSPF sub-basin 14	Inflow	Element 43	Hourly	1.000	0511_02
HSPF sub-basin 15	Inflow	Node 71	Hourly	1.000	0511B_01
HSPF sub-basin 16	Inflow	Element 40	Hourly	0.383	0511_01
		Element 45	Hourly	0.617	0511_02
HSPF sub-basin 17	Inflow	Element 22	Hourly	0.715	0511_01
		Element 82	Hourly	0.285	0511D_01
HSPF sub-basin 18	Inflow	Element 18	Hourly	1.000	0511_01
USGS gauge 08030500	Inflow	Node 15	Daily	1.000	Sabine River near Ruliff
WQ0000670-000	Inflow	Element 14	Constant	1.000	Honeywell International
WQ0001167-000	Inflow	Element 19	Constant	1.000	ARLANXEO USA, LLC
WQ0000454-000	Inflow	Element 21	Constant	1.000	Lion Elastomers
WQ0000359-000	Inflow	Element 83	Constant	1.000	Chevron Phillips Chem.
WQ0002858-000	Inflow	Element 83	Constant	1.000	Printpack, Inc.
WQ0015029-001	Inflow	Element 36	Constant	1.000	Bayou Pines, LLC
WQ0013488-001	Inflow	Element 33	Constant	1.000	Gulflander Partners Group, LP
WQ0010051-001	Inflow	Element 38	Constant	1.000	City of Bridge City
WQ0014772-001	Inflow	Element 44	Constant	1.000	Orangefield WSC
WQ0011916-001	Inflow	Element 79	Constant	1.000	PCS Development Co.
Rainbow Bridge water level	boundary elevation	Node 1	30 minutes	Not Applicable	Downstream boundary

4.3 RMA2 Calibration and Validation

The hydrodynamic models were calibrated to quality-assured water level and flow data collected during an intensive survey performed during the late spring and summer of 2004. The calibration was then verified by comparison to data from a second intensive survey performed approximately one month after the first. Each survey lasted more than 48 hours, covering multiple tidal cycles.

Water levels and water quality were measured and recorded periodically (every 10 to 30 minutes) at 15 stations using sondes that incorporated vented pressure transducers. Because the primary mission of these sondes was to measure water quality mid-channel at approximately 1-m deep, the sondes were deployed in mid-channel secured on chains between an anchor and a float. The float was deployed below the surface to maintain a taut chain. The measured pressures were converted to depths based on internal algorithms programmed in the sonde, which were verified by manual measurements on deployment and retrieval. The depths were then converted to approximate elevations based on comparison of site-measured depths across the tidal cycle to measured elevations at the Rainbow Bridge tide gauge of the National Oceanic and Atmospheric Administration. Although this approach generally resulted in good quality water elevation data, in most cases there were some minor shifts in depth due to movement of the anchor. There was also some correlation between level and flow rate caused by slight “play” in the chain in concert with deflection of the float by the current. In a few cases, the water elevation data or a portion thereof was not usable because of movement by the anchor, tangling of the chain with stream-borne debris, or vandalism to the float. It should also be noted that not all sondes deployed had pressure transducers. Model calibration and validation was performed only with quality-assured data that had been validated in accordance with the QAPP.

Flow was measured by two methods. If a monitoring station was wadeable or easily accessible from a bridge, flow was measured using a Marsh-McBirney electronic meter according to TCEQ standard procedures (TCEQ, 2012). At deeper or less accessible spots, flow was measured using a boat-mounted Sontek™ Acoustic Doppler Profiler (ADP). The Marsh-McBirney measurements involve a single stream transect comprised of many individual point velocity measurements. The ADP measurements involved averaging several complete transects with continuous depth-integrated velocity measurements. In each case, the flow measurement required from 15 to 30 minutes from start to completion. Flow was constantly changing in this tidal system, and the flow measurements should be considered as 30-minute average flows over this period rather than instantaneous flows. Often, flow direction reversed during a measurement, or flow direction changed with depth or position along the transect.

Time series plots (provided in Appendix E for Adams Bayou and Appendix F for Cow Bayou) of observed and modeled water elevations and flow were used to visually evaluate model performance during calibration. Model calibration statistics such as the r^2 , ME, MAE, RMSE, and

NSE were used as quantitative measures of model fit to supplement the visual evaluation of fit. The measured flow according to the end time of measurement, was matched with the model-predicted flow for the nearest previous model time step. The model time step was 30 minutes, consistent with the approximate measurement period, but the time differential between observed and model time varied up to 30 minutes. Thus, model fit statistics in time of high flow and elevation changes may indicate a worse fit than a visual comparison implies.

During the calibration process, the primary model parameters that were adjusted were the Manning's roughness coefficients for vegetated and non-vegetated channels. In a few places, the off-channel storage volumes that were not estimable from field measurements were also modified to improve calibration. In the Adams Bayou dredged channels, Manning's roughness was calibrated to 0.06 for both vegetated and non-vegetated channels. For other channels, a Manning's roughness coefficient of 0.09 was applied, gradually increasing to 0.11 at depths less than 2 m. In Cow Bayou, the Manning's roughness coefficient was calibrated to 0.03 in the broad dredged channels, increasing to 0.04 at depths less than 2 m. In the natural channels, the coefficient was calibrated to 0.04 increasing to 0.05 depending on depth. In narrow channels of less than 10-m width, the Manning's roughness coefficient was calibrated to 0.06, increasing to 0.07 at shallow depths.

From the QAPP, the acceptance targets for goodness-of-fit of RMA2 simulation of tidal water levels and flow were as follows:

- The RMSE of simulated tidal water levels to be less than 33 percent of the observed daily tidal range for the calibration and validation periods.
- The RMSE of simulated tidal flows to be less than 33 percent of the range of measured flows at each site where the flow range is greater than 2 cubic meter per second (cms), and less than 50 percent of the range of measured flows at each site where the flow range is 2 cms or less for the calibration and validation periods.

Tables 4-4 and 4-5 provide the model calibration and validation statistics for water elevation at Adams Bayou and Cow Bayou locations. For Adams Bayou locations, the RMSE was on average approximately 0.03 m, or 1.2 inch. The error in the validation model run was slightly higher than that from the calibration period, but still within acceptable limits given a tidal range of more than one foot. It was also noticeable that the model error tended to be greater in the more upstream tidal portions of the system during the validation run. In part, this may be due to a major rainfall event before the second intensive survey, which caused large freshwater inflows. It appears that the HSPF model may have under simulated the runoff from this rainfall event due to inaccuracies in the precipitation input. The influence of runoff and tributary inflow, relative to tide-driven flow, is greater in the narrow and shallow upstream reaches of the bayous. The goodness-of-fit RMSE target was met at all monitoring stations.

Table 4-4 Water level error statistics for the RMA2 hydrodynamic model of Adam Bayou

Acceptable RMSE/Range values in black font and unacceptable values in bold red font

Monitoring Station	Calibration Period (May 25 - 28, 2004)								Validation Period (June 28 – July 1, 2004)							
	N [†]	r ²	Range‡	ME	MAE	NSE	RMSE	RMSE/Range	N	r ²	Range	ME	MAE	NSE	RMSE	RMSE/Range
	none	none	m	m	m	None	m	%	none	none	m	m	m	None	m	%
AB2	-	-	-	-	-	-	-	-	246	0.964	0.32	-0.008	0.021	0.920	0.028	8.6%
AB3	242	0.904	0.33	0.018	0.026	0.845	0.029	9.0%	250	0.981	0.32	-0.005	0.015	0.961	0.019	5.9%
AB4	114	0.931	0.24	0.017	0.020	0.818	0.027	11.6%	254	0.978	0.33	0.000	0.015	0.961	0.019	5.8%
AB6	-	-	-	-	-	-	-	-	125	0.954	0.32	0.022	0.026	0.891	0.031	9.5%
AB8	235	0.878	0.30	-0.005	0.023	0.873	0.028	9.4%	250	0.868	0.39	0.081	0.083	0.209	0.090	22.8%
Gum Gully	252	0.912	0.40	-0.005	0.021	0.908	0.025	6.4%	-	-	-	-	-	-	-	-

[†]number of measurements

‡ maximum measured value – minimum measured value

Table 4-5 Water level error statistics for the RMA2 hydrodynamic model of Cow Bayou

Acceptable RMSE/Range values in black font and unacceptable values in bold red font

Monitoring Station	Calibration Period (July 19 – 22, 2004)								Validation Period (August 23 – 26, 2004)							
	N [†]	r ²	Range‡	ME	MAE	NSE	RMSE	RMSE/Range	N	r ²	Range	ME	MAE	NSE	RMSE	RMSE/Range
	none	none	m	m	m	None	m	%	none	none	m	m	m	None	m	%
CB0.5	-	-	-	-	-	-	-	-	133	0.969	0.43	0.001	0.021	0.966	0.025	5.9%
CB1	248	0.959	0.39	-0.003	0.018	0.958	0.021	5.4%	263	0.938	0.44	0.001	0.033	0.936	0.039	8.9%
CB2	249	0.922	0.39	-0.001	0.023	0.924	0.029	7.5%	261	0.968	0.44	0.000	0.023	0.966	0.026	5.9%
CB3	252	0.952	0.42	-0.001	0.020	0.951	0.024	5.8%	260	0.957	0.44	0.000	0.026	0.954	0.030	6.9%
CB3.5	255	0.948	0.42	-0.001	0.019	0.952	0.024	5.8%	-	-	-	-	-	-	-	-
CB4	238	0.814	0.41	0.001	0.036	0.810	0.046	11.2%	254	0.888	0.44	-0.001	0.043	0.878	0.048	11.0%
CB5	256	0.912	0.38	0.001	0.023	0.907	0.029	7.5%	265	0.966	0.44	0.006	0.021	0.960	0.026	5.9%
Coon Bayou	140	0.959	0.34	0.000	0.016	0.959	0.019	5.6%	253	0.971	0.46	0.002	0.020	0.973	0.025	5.4%
Terry Gully	-	-	-	-	-	-	-	-	254	0.865	0.30	-0.029	0.053	0.583	0.066	22.1%

[†]number of measurements

‡ maximum measured value – minimum measured value

On average, the RMSE was approximately 0.025 m, or 1 inch for Cow Bayou (Table 4-5), similar to that for the Adams Bayou model. Also similar to the Adams Bayou model, error was greater in the upstream portions of the model. The goodness-of-fit RMSE target was met at all monitoring stations.

Tables 4-6 and 4-7 present the error statistics for model flow predictions for Adams Bayou and Cow Bayou, respectively. At most sites the model errors were small relative to the range of flows observed. It was interesting to note that all Adams Bayou sites, including sites considered by TCEQ to be representative of Adams Bayou Above Tidal, exhibited tidal flow patterns. The goodness-of-fit RMSE target was met at all monitoring stations of the Adams Bayou system.

The goodness-of-fit RMSE target (RMSE/measured range), however, was not met at all monitoring stations of the Cow Bayou system. The RMSE values in the Cow Bayou system not meeting the target are provided in bold red font in Table 4-7. For monitoring stations CB4, CB5, and Coon Bayou, the missed RMSE target can reasonably attributed as an artifact of the monitoring. At all three of these monitoring stations, only three flow measurements were made and each occurred on ebb (or downstream-directed flow) for the simulated period in which the performance target was not met. The flow monitoring at these stations resulted in an artificially small flow range during these periods, which explains why the target was missed and could not be met through reasonable adjustments during the calibration process. Also of note at these three stations, water-level tidal fluctuations were well simulated and the flow RMSE target was met during the other simulated period (either calibration or validation) where measured flow data provided a more reasonable range.

This explanation of limited flow measurements cannot explain the missed RMSE target at Terry Gully, where seven measurements were made during the calibration period and eight measurements were made during the validation period. The model performance and measured data at the Terry Gully site remained an anomaly without ready explanation. Water levels were only measured during the validation period at Terry Gully (Table 4-5). During this period, the measured Terry Gully water levels show a low-water bench below which levels do not drop in an uncharacteristic manner (Figure F-34) compared to all other measured water levels of Cow Bayou stations and, also, Adams Bayou stations. The measured water-level response seems to indicate some type of obstruction, such as a sedimentation sill, that precludes the decrease of water levels beyond some minimum elevation of around -0.25 ft relative to mean sea level. The absence of a measured flow reversal with no upstream directed flows (Figures F-33 and F-35) further supports something obstructing tidal propagation into Terry Gully.

Table 4-6 Flow error statistics for the RMA2 hydrodynamic model of Adams Bayou

Acceptable RMSE/Range values in black font and unacceptable values in bold red font

Monitoring Station	Calibration Period (May 25 - 28, 2004)								Validation Period (June 28 – July 1, 2004)							
	N [†]	r ²	Range‡	ME	MAE	NSE	RMSE	RMSE/Range	N	r ²	Range	ME	MAE	NSE	RMSE	RMSE/Range
	None	None	cms	cms	cms	None	cms	%	None	None	cms	cms	cms	None	cms	%
AB2	7	0.909	38.62	-0.72	2.12	0.89	3.50	9.1%	8	0.909	38.62	-0.67	2.76	0.87	3.39	8.8%
AB3	7	0.759	26.36	-0.95	2.53	-0.55	3.35	12.7%	8	0.650	26.36	1.54	3.77	0.49	4.63	17.6%
AB4	4	0.741	19.00	-1.43	1.43	0.33	2.32	12.2%	8	0.824	19.00	1.38	2.85	0.68	3.45	18.2%
AB5	3	0.964	16.14	-0.37	0.66	0.91	0.90	5.6%	8	0.864	16.14	1.03	2.32	0.74	2.61	16.2%
AB6	8	0.864	8.66	-0.04	0.70	0.15	0.77	8.9%	8	0.840	8.66	1.41	1.63	0.49	1.84	21.2%
AB7	9	0.191	5.55	-0.49	0.79	-4.33	0.95	17.1%	9	0.665	5.55	0.42	0.95	0.49	1.10	19.9%
AB8	9	0.416	3.80	-0.15	0.20	-0.05	0.23	6.2%	9	0.885	3.80	0.56	0.87	0.29	1.02	26.9%
Gum Gully	5	0.585	0.96	-0.02	0.02	-0.46	0.03	3.1%	5	0.100	0.96	-0.22	0.29	-0.47	0.36	37.1%
Hudson Gully	9	0.203	0.20	0.01	0.03	-0.36	0.04	18.2%	7	0.489	0.20	0.04	0.04	-0.43	0.05	26.2%

[†] number of measurements

‡ maximum measured value minus minimum measured value

Table 4-7 Flow error statistics for the RMA2 hydrodynamic model of Cow Bayou

Acceptable RMSE/Range values in black font and unacceptable values in bold red font

Monitoring Station	Calibration Period (May 25 - 28, 2004)								Validation Period (June 28 – July 1, 2004)							
	N [†]	r ²	Range‡	ME	MAE	NSE	RMSE	RMSE/Range	N	r ²	Range	ME	MAE	NSE	RMSE	RMSE/Range
	None	None	cms	cms	cms	None	cms	%	None	None	cms	cms	cms	None	cms	%
CB0.5	4	0.933	77	7.30	8.87	0.80	12.88	16.8%	7	0.736	78.86	4.79	18.24	0.72	21.63	27.4%
CB1	5	0.857	67	0.46	8.25	0.85	8.84	13.1%	7	0.888	60.94	3.05	7.26	0.85	10.17	16.7%
CB2	5	0.838	46	2.37	6.22	0.79	7.26	16.0%	7	0.778	46.07	-0.45	7.69	0.77	8.92	19.4%
CB2.5	5	0.955	24	-2.25	3.00	0.86	3.30	13.7%	7	0.945	28.23	1.80	3.19	0.89	3.56	12.6%
CB3	6	0.938	20	-1.23	2.69	0.80	2.82	13.9%	7	0.828	21.78	-0.68	4.55	0.70	4.71	21.6%
CB3.5	5	0.763	9	0.00	1.15	0.75	1.54	17.5%	7	0.786	12.52	0.16	2.41	0.74	2.62	21.0%
CB4	4	0.570	1.1	-0.30	0.33	-0.60	0.39	34.3%	3	0.632	0.69	-0.30	0.33	-0.60	0.39	56.3%
CB5	3	0.995	0.1	-0.05	0.10	-1.12	0.10	66.6%	6	0.340	0.64	0.06	0.19	0.18	0.24	37.3%
Coon Bayou	3	0.183	0.5	-0.13	0.25	-0.68	0.26	55.7%	5	0.466	0.86	-0.03	0.22	0.42	0.24	27.4%
Terry Gully	7	0.773	0.5	-0.43	0.43	-8.91	0.50	98.4%	8	0.664	0.41	-0.22	0.30	-6.64	0.48	117.8%

[†]number of measurements

[‡] maximum measured value minus minimum measured value

No obstruction could be documented along Terry Gully based on review of digital elevation model datafiles, satellite and aerial imagery, nor in the input data used in the flood plain studies of Carroll and Blackmann (Carroll and Blackmann, 2015). Communications with Orange County Drainage District staff also failed to produce any evidence of an obstruction in Terry Gully. It would be highly likely that modifying the RMA2 model to represent a physical obstruction between the Terry Gully monitoring station and its downstream entry into Cow Bayou would have benefitted the model performance. There was, however, no justification for making such a modification to the model other than what the measured data showed. Since Terry Gully (AU 0511E_01) is not impaired for depressed DO and, therefore, not an area of focus in the modeling system, the decision was made to leave the RMA2 model as it was constructed based on best available data and to accept the poor performance at this location regarding flow.

Tables 4-8 and 4-9 show the model parameters used for the Adams Bayou and Cow Bayou RMA2 models, respectively.

Table 4-8 Parameters of the Adams Bayou RMA2 model

Parameter	Units	Source ¹	Value or Range
EX - Turbulent Exchange Coefficient, X-direction	Pascal-second	L	5000
EY - Turbulent Exchange Coefficient, Y-direction	Pascal-second	L	5000
AO - bottom elevation	m	F	-15.0 – -1.3
WIDTH - channel width at zero depth	m	F	2 - 43
SS1 - left side slope	m	F	0.5 – 19.7
SS2 - right side slope	m	F	0.5 – 19.7
WIDS - off-channel storage width	m/m	F	0 – 200
WSCRIT – water surface elevation to activate off-channel storage	m	F	-2.4 – 0
SSS - side slope for off channel storage	m	F	0 - 200
RDR0 – maximum Manning’s “n” ² value for non-vegetated water	complex	C	0.06 – 0.09
RDD0 – depth at which vegetation affects roughness	m	L	2
RDRM – Manning’s n-value for vegetated water	complex	C	0.06 – 0.11
RDCOEF – roughness by depth coefficient	none	L	1E-14
DSET – depth at which nodes are considered dry and deactivated	m	L	0.084
DSETD – depth at which nodes become active when rewetted	m	L	0.183

¹ F = collected data, L = literature, C=calibration

² automatic roughness assignment based on depth

Table 4-9 Parameters of the Cow Bayou RMA2 model

Parameter	Units	Source ¹	Value or Range
EX - Turbulent Exchange Coefficient, X-direction	Pascal-second	L	5000
EY - Turbulent Exchange Coefficient, Y-direction	Pascal-second	L	5000
AO - bottom elevation	m	F	-15.0 – -1.1
WIDTH - channel width at zero depth	m	F	1 – 100
SS1 - left side slope	m	F	0.5 – 10
SS2 - right side slope	m	F	0.5 – 10
WIDS - off-channel storage width	m/m	F	0 – 200
WSCRIT – water surface elevation to activate off-channel storage	m	F	-10 – 0
SSS - side slope for off channel storage	m	F	0 – 200
RDR0 – maximum Manning’s “n” ² value for non-vegetated water	complex	C	0.03 – 0.06
RDD0 – depth at which vegetation affects roughness	m	L	2
RDRM – Manning’s n-value for vegetated water	complex	C	0.04 – 0.07
RDCOEF – roughness by depth coefficient	none	L	1E-14
DSET – depth at which nodes are considered dry and deactivated	m	L	0.084
DSETD – depth at which nodes become active when rewetted	m	L	0.183

¹ F = collected data, L = literature, C=calibration

² automatic roughness assignment based on depth

5. WASP Water Quality Model

WASP is a generalized framework for simulating water quality in surface waters and the underlying sediments. It can be applied in one, two or three dimensions. The time-varying processes of advection, dispersion, point- and nonpoint-source pollutant loading, and boundary exchange are included in the basic program. Several independent WASP modules are provided. The EUTRO module is designed to simulate nutrients, DO, and eutrophication. The advanced eutrophication module also simulates nutrients, DO, and eutrophication, but also permits simulation of three groups of phytoplankton and cBOD, periphyton, and includes a linked sediment diagenesis module. The TOXI module simulates organic contaminant fate and transport. The HEAT module simulates temperature and salinity. The mercury module simulates various mercury species and sediment balances.

5.1 WASP Model Description

For this project, the eutrophication module in WASP version 7.52 was applied to simulate DO in two separate models, one for each bayou system. Table 5-1 summarizes key WASP modeling parameters. Figures 5-1 (a-c) and 5-2 (a-e) show the segmentation of the Adams and Cow models, respectively, and Tables 5-2 and 5-3 describe the physical dimensions of WASP reaches. Segmentation of the RMA2 and WASP models was based on the TCEQ boundary map of AUs allowing association of the segmentation to the representation of each AU in the boundary map.

Table 5-1 WASP model summary

Item	Description
Version/Date	WASP 7.52 (1/24/2013 2:10 PM)
Model Period	1/1/2002 – 12/31/2012
Time Step	dynamic; input frequency varies; set to output daily
Segments	118 (Adams Bayou); 136 (Cow Bayou)
Simulated constituents	Salinity, TSS, NH ₃ N, NO ₃ N, OrgN, Detrital N, PO ₄ P, OrgP, Detrital P, CBOD (ultimate), Detrital C, Phytoplankton Chla, DO
Point source wastewater discharges	Active: 2 to Adams Bayou (WQ0010626-001 and WQ0010240-001 are combined since they discharge to the same WASP segment). 9 to Cow Bayou (WQ0010808-001 and WQ0002835-000 are included in the HSPF model and WQ0000359-000 and WQ0002858-000 are combined since they discharge to the same WASP segment).

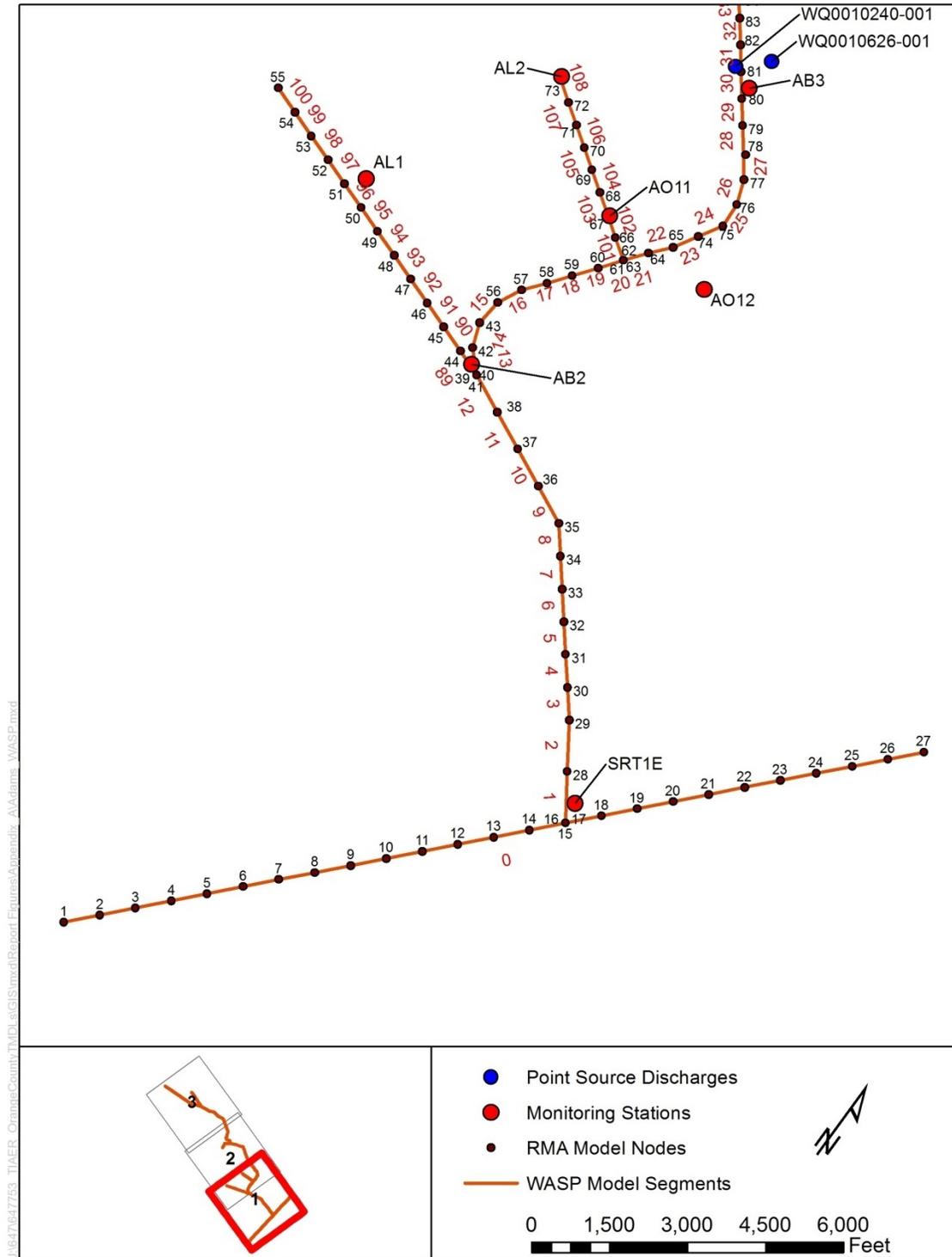


Figure 5-1a Adams Bayou WASP model segments

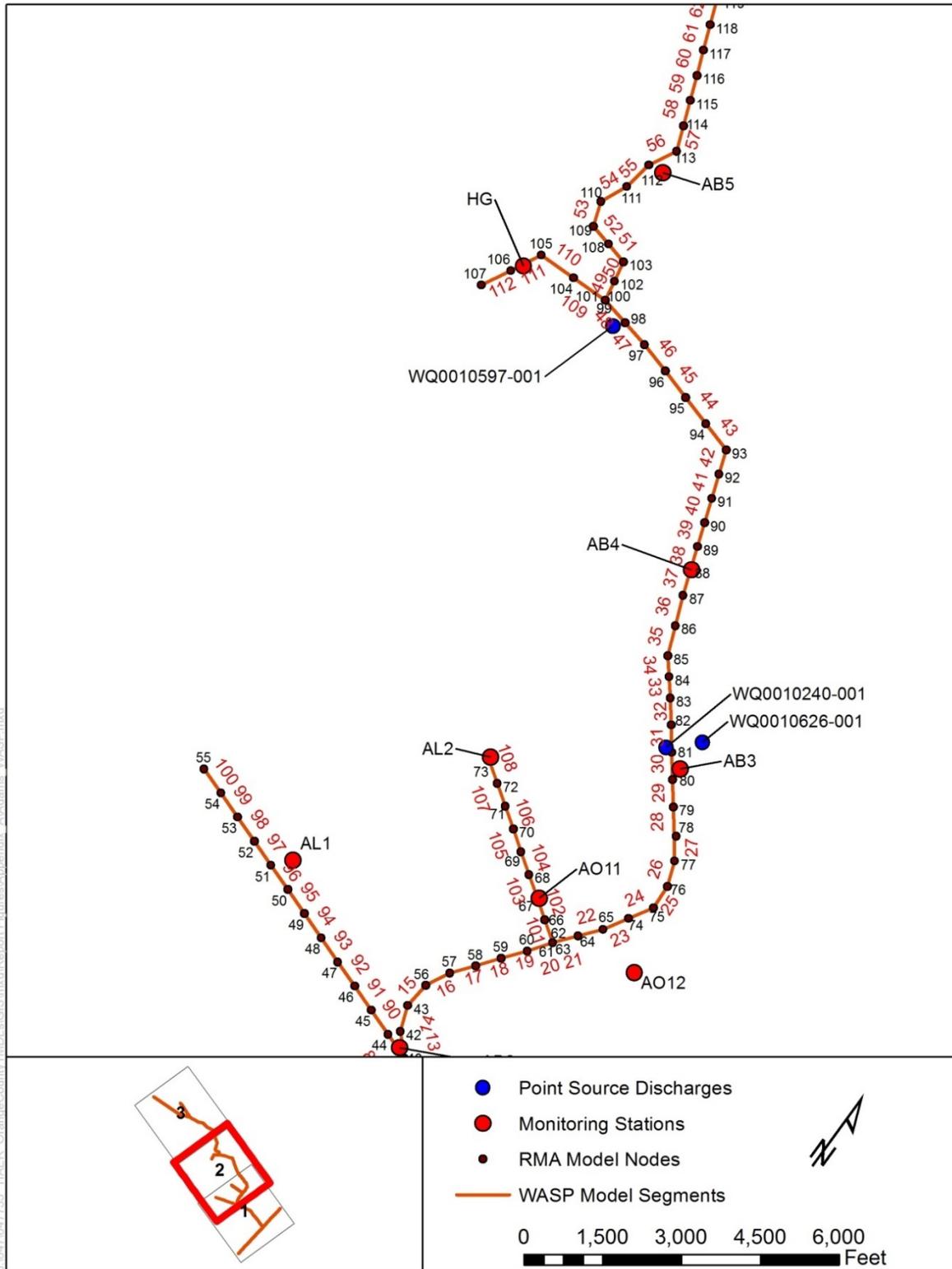


Figure 5-1b Adams Bayou WASP model segments

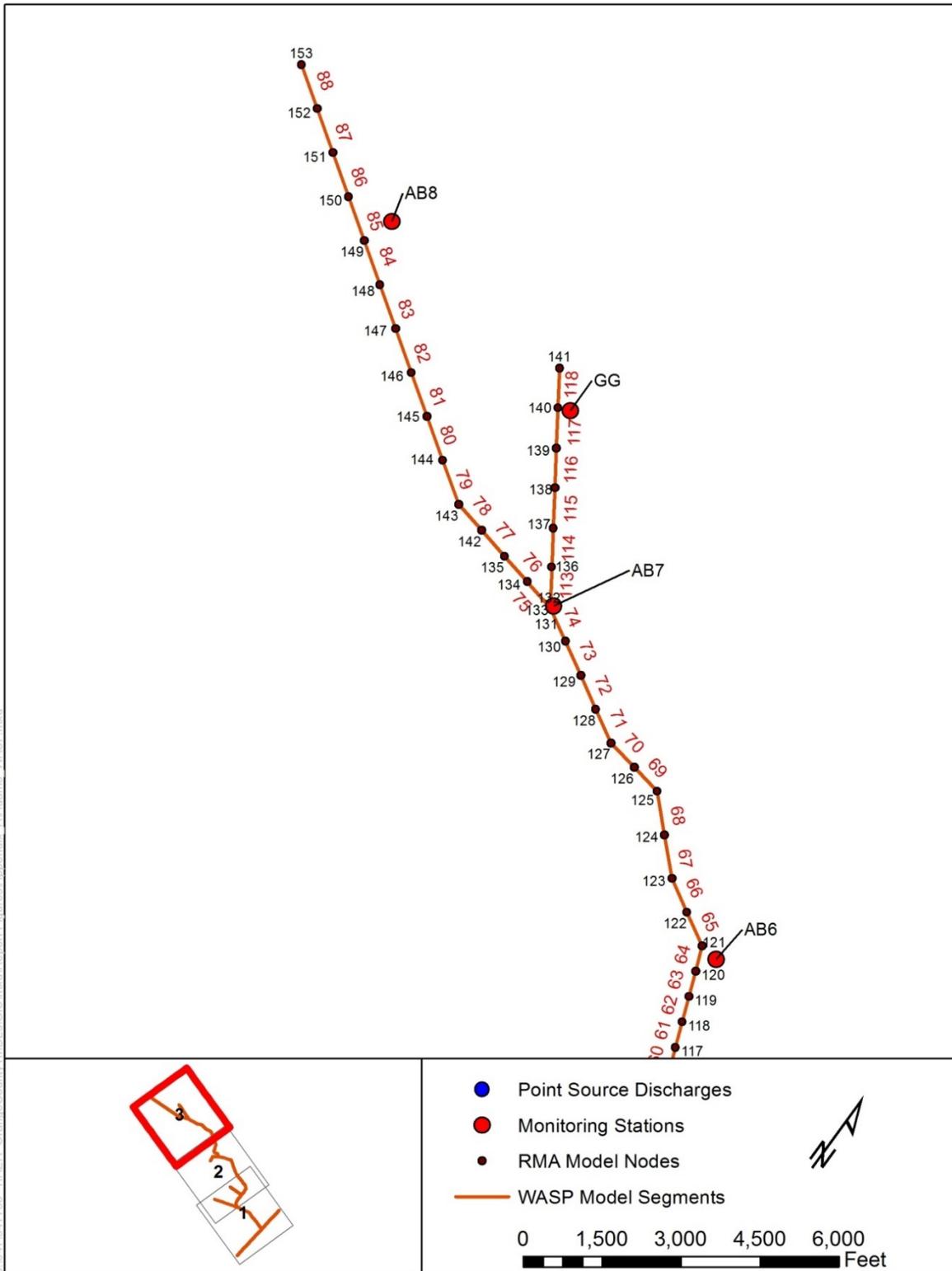


Figure 5-1c Adams Bayou WASP model segments

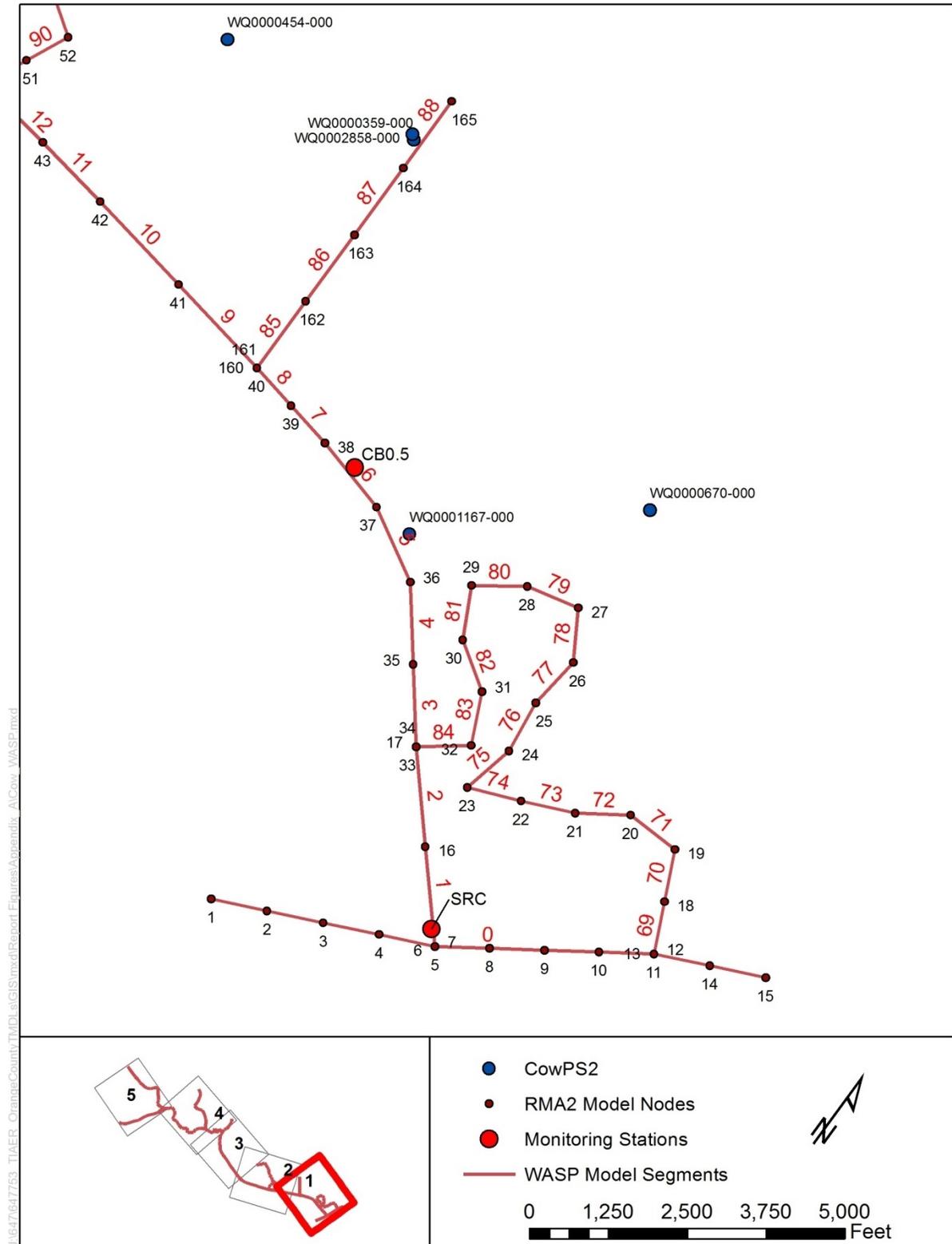


Figure 5-2a Cow Bayou WASP model segments

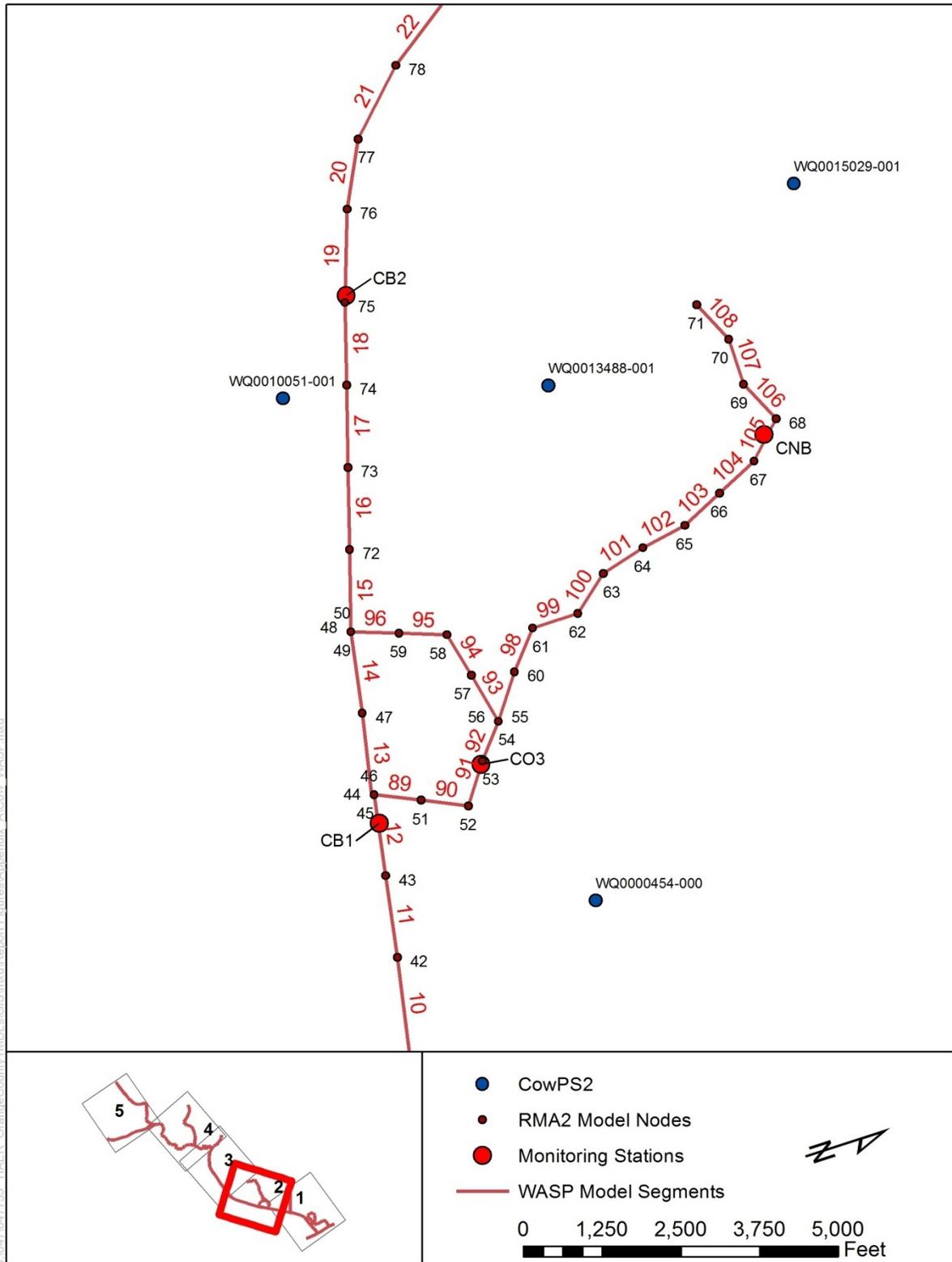


Figure 5-2b Cow Bayou WASP model segments

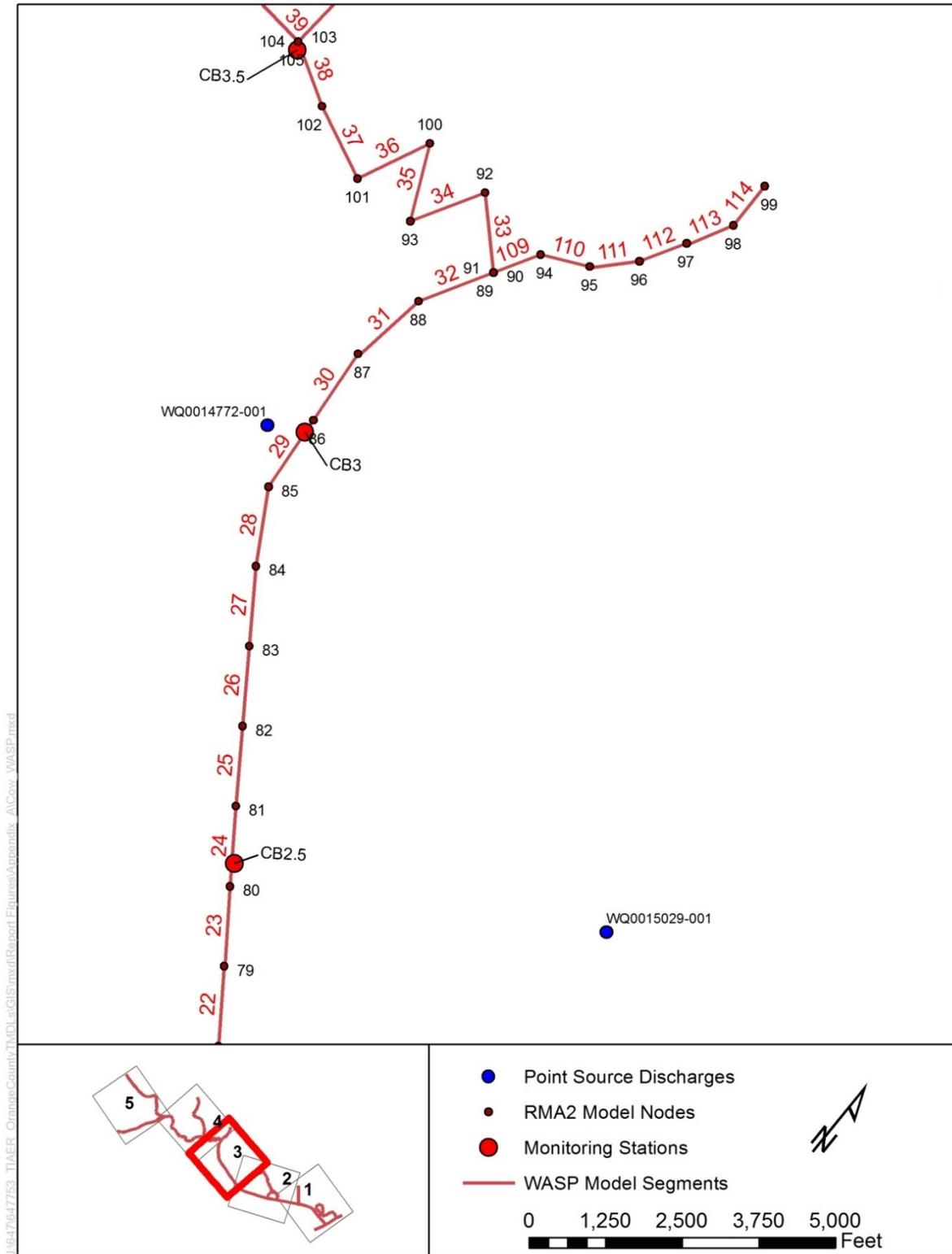


Figure 5-2c Cow Bayou WASP model segments

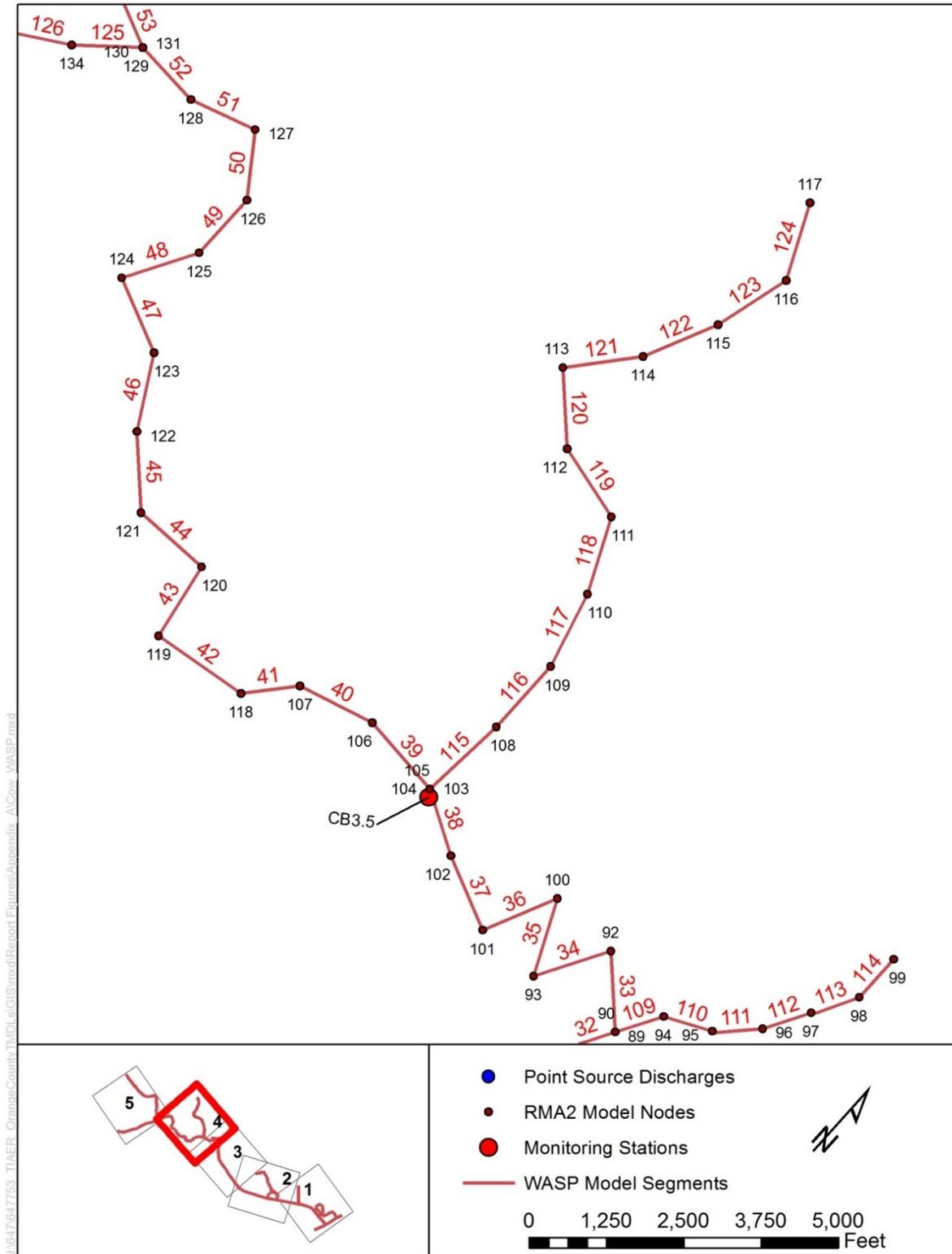


Figure 5-2d Cow Bayou WASP model segments

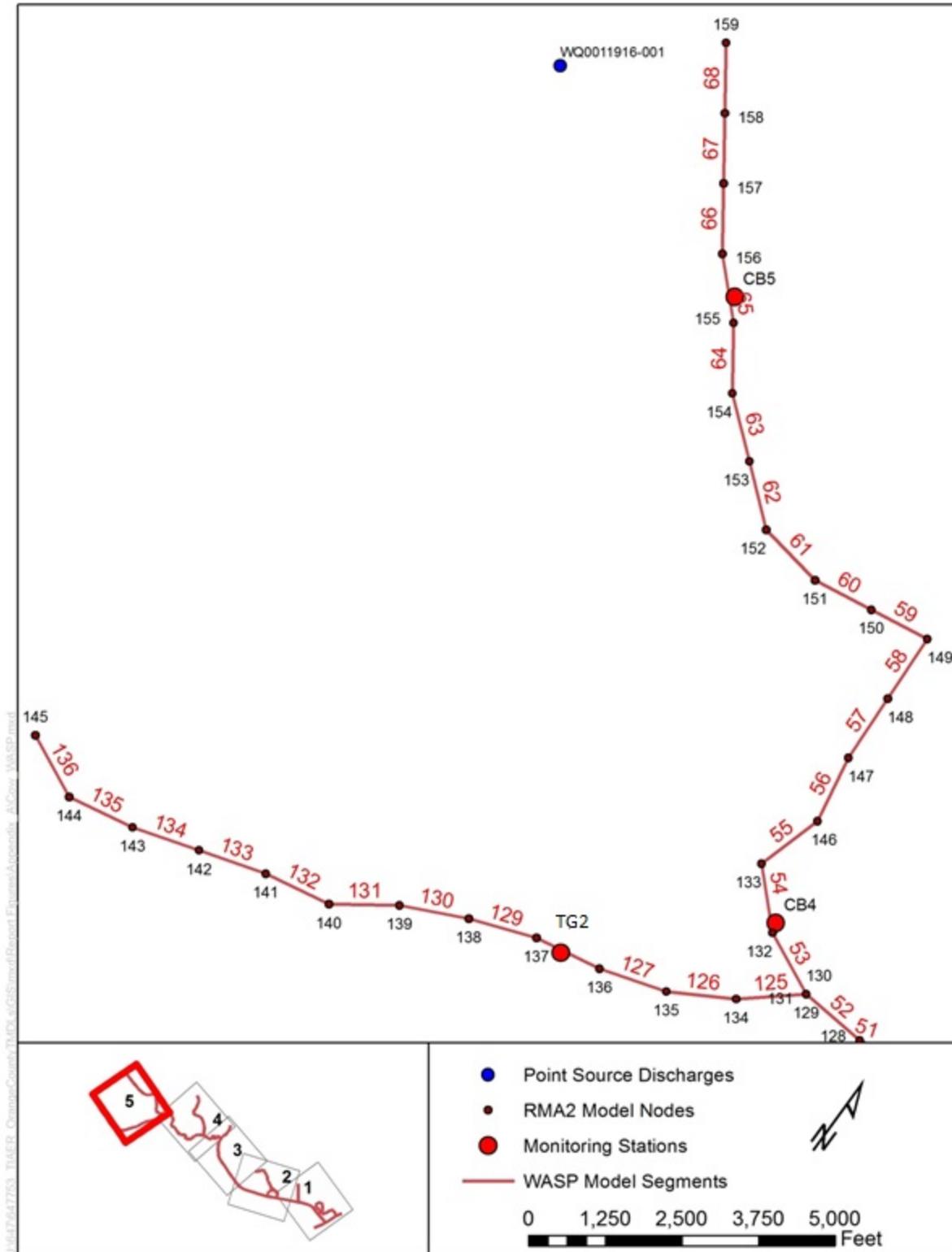


Figure 5-2e Cow Bayou WASP model segments

Table 5-2 Physical properties of Adams Bayou WASP model segments

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Segment Depth below Mean Sea Level (m)	Length (m)	Width (m)
1	Adams Bayou Tidal	0508_01		144,552	5.2	413	43
2	Adams Bayou Tidal	0508_01		60,247	4.8	193	43
3	Adams Bayou Tidal	0508_01		108,436	4.8	193	43
4	Adams Bayou Tidal	0508_01		137,354	4.8	193	43
5	Adams Bayou Tidal	0508_01		118,074	4.8	193	43
6	Adams Bayou Tidal	0508_01		118,074	4.8	193	43
7	Adams Bayou Tidal	0508_01		99,993	4.8	193	39
8	Adams Bayou Tidal	0508_01		81,913	4.8	193	35
9	Adams Bayou Tidal	0508_01		105,899	4.8	249	35
10	Adams Bayou Tidal	0508_01		102,972	4.8	249	33
11	Adams Bayou Tidal	0508_01		118,739	4.8	249	30
12	Adams Bayou Tidal	0508_01		132,371	4.7	249	27
13	Adams Bayou Tidal	0508_01	10441 (AB2)	52,491	4.7	160	21
14	Adams Bayou Tidal	0508_01		46,019	4.7	155	18
15	Adams Bayou Tidal	0508_01		38,509	4.7	158	18
16	Adams Bayou Tidal	0508_01		30,271	4.6	158	18
17	Adams Bayou Tidal	0508_01		29,124	4.6	154	18
18	Adams Bayou Tidal	0508_01		29,141	4.5	156	18
19	Adams Bayou Tidal	0508_01		28,991	4.5	157	18
20	Adams Bayou Tidal	0508_01		28,469	4.4	156	18
21	Adams Bayou Tidal	0508_01		26,315	4.4	153	15
22	Adams Bayou Tidal	0508_01		33,235	4.3	149	12
23	Adams Bayou Tidal	0508_01		47,094	4.3	161	11
24	Adams Bayou Tidal	0508_01		45,879	4.3	157	10
25	Adams Bayou Tidal	0508_01		35,827	4.3	149	10
26	Adams Bayou Tidal	0508_01		28,848	4.2	153	10
27	Adams Bayou Tidal	0508_01		27,419	4.2	146	10
28	Adams Bayou Tidal	0508_02		33,314	4.2	172	11
29	Adams Bayou Tidal	0508_02		37,885	4.2	158	13.5
30	Adams Bayou Tidal	0508_02	10442 (AB3)	44,178	4.2	158	15
31	Adams Bayou Tidal	0508_02		44,182	4.2	158	15

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Segment Depth below Mean Sea Level (m)	Length (m)	Width (m)
32	Adams Bayou Tidal	0508_02		38,566	4.2	158	12.5
33	Adams Bayou Tidal	0508_02		32,620	3.9	158	10
34	Adams Bayou Tidal	0508_02		16,922	3.6	87	10
35	Adams Bayou Tidal	0508_03		35,895	3.6	217	10
36	Adams Bayou Tidal	0508_03		24,167	3.6	147	10
37	Adams Bayou Tidal	0508_03		25,541	3.6	147	7.5
38	Adams Bayou Tidal	0508_03	16059 (AB4)	24,217	3.5	147	5.0
39	Adams Bayou Tidal	0508_03		21,856	3.6	147	5.0
40	Adams Bayou Tidal	0508_03		19,495	3.7	147	5.0
41	Adams Bayou Tidal	0508_03		19,494	3.7	147	5.0
42	Adams Bayou Tidal	0508_03		16,559	3.7	147	5.0
43	Adams Bayou Tidal	0508_03		17,945	3.7	193	5.0
44	Adams Bayou Tidal	0508_03		17,944	3.7	193	5.0
45	Adams Bayou Tidal	0508_03		17,944	3.7	193	5.0
46	Adams Bayou Tidal	0508_03		17,944	3.7	193	5.0
47	Adams Bayou Tidal	0508_03		17,944	3.7	193	5.0
48	Adams Bayou Tidal	0508_03		14,094	3.7	152	5.0
49	Adams Bayou Tidal	0508_04		25,602	3.8	145	5.0
50	Adams Bayou Tidal	0508_04		17,718	3.8	105	5.0
51	Adams Bayou Tidal	0508_04		22,799	3.9	135	5.0
52	Adams Bayou Tidal	0508_04		23,233	4	135	5.0
53	Adams Bayou Tidal	0508_04		33,832	4.1	151	5.0
54	Adams Bayou Tidal	0508_04		47,414	4.1	172	5.0
55	Adams Bayou Tidal	0508_04		55,263	4.1	182	4.5
56	Adams Bayou Tidal	0508_04	14990 (AB5)	50,431	4.1	180	4.0
57	Adams Bayou Tidal	0508_04		32,653	4.1	152	4.5
58	Adams Bayou Tidal	0508_04		30,400	4.1	152	5.0
59	Adams Bayou Tidal	0508_04		21,403	4.1	152	5.0
60	Adams Bayou Tidal	0508_04		11,264	4.1	152	5.0
61	Adams Bayou Tidal	0508_04		10,124	4.1	152	5.0
62	Adams Bayou Tidal	0508_04		10,367	4.1	152	5.0
63	Adams Bayou Tidal	0508_04		10,899	3.9	152	7.4

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Segment Depth below Mean Sea Level (m)	Length (m)	Width (m)
64	Adams Bayou Tidal	0508_04	10443 (AB6)	12,708	3.6	152	9.8
65	Adams Bayou Tidal	0508_04		18,062	3.6	215	7.4
66	Adams Bayou Tidal	0508_04		13,595	3.5	215	5.0
67	Adams Bayou Tidal	0508_04		11,483	3.4	215	6.5
68	Adams Bayou Tidal	0508_04		16,389	3.3	308	8.6
69	Adams Bayou above Tidal	0508A_01		9,978	3.2	198	9.1
70	Adams Bayou above Tidal	0508A_01		10,373	3.1	215	9.1
71	Adams Bayou above Tidal	0508A_01		9,744	3.1	215	8.8
72	Adams Bayou above Tidal	0508A_01		9,356	3.1	215	8.5
73	Adams Bayou above Tidal	0508A_01		9,357	3	215	8.5
74	Adams Bayou above Tidal	0508A_01	15107 (AB7)	9,812	2.8	224	9.9
75	Adams Bayou above Tidal	0508A_01		7,603	2.5	193	9.9
76	Adams Bayou above Tidal	0508A_01		7,047	2.3	200	8.5
77	Adams Bayou above Tidal	0508A_01		6,520	2.2	200	8.5
78	Adams Bayou above Tidal	0508A_01		9,064	2.1	200	8.5
79	Adams Bayou above Tidal	0508A_01		11,343	2	271	8.3
80	Adams Bayou above Tidal	0508A_01		6,548	1.9	271	8.0
81	Adams Bayou above Tidal	0508A_01		6,136	1.8	271	8.0
82	Adams Bayou above Tidal	0508A_01		5,734	1.7	271	8.0
83	Adams Bayou above Tidal	0508A_01		5,344	1.6	271	8.0
84	Adams Bayou above Tidal	0508A_01		4,964	1.5	271	8.0

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Segment Depth below Mean Sea Level (m)	Length (m)	Width (m)
85	Adams Bayou above Tidal	0508A_01	14964 (AB8)	4,777	1.5	271	8.0
86	Adams Bayou above Tidal	0508A_01		4,686	1.5	271	8.0
87	Adams Bayou above Tidal	0508A_01		4,152	1.5	271	7.0
88	Adams Bayou above Tidal	0508A_01		7,600	1.4	271	5.0
89	Adams Bayou Lateral 1			11,665	2.5	171	6.3
90	Adams Bayou Lateral 1			11,358	2.4	171	6.3
91	Adams Bayou Lateral 1			7,973	2.3	171	6.3
92	Adams Bayou Lateral 1			4,768	2.2	171	6.3
93	Adams Bayou Lateral 1			3,667	2.1	171	6.3
94	Adams Bayou Lateral 1			2,584	2	171	6.3
95	Adams Bayou Lateral 1			2,370	1.9	171	6.3
96	Adams Bayou Lateral 1		16057 (AL1)	2,170	1.8	171	6.3
97	Adams Bayou Lateral 1			3,031	1.7	171	6.2
98	Adams Bayou Lateral 1			2,832	1.6	171	5.9
99	Adams Bayou Lateral 1			1,578	1.5	171	5.7
100	Adams Bayou Lateral 1			3,169	1.4	171	5.3
101	Adams Bayou Lateral 2			7,098	1.8	140	8.0
102	Adams Bayou Lateral 2			7,098	1.8	140	8.0
103	Adams Bayou Lateral 2			4,531	1.7	140	7.3
104	Adams Bayou Lateral 2			1,865	1.6	140	6.6
105	Adams Bayou Lateral 2			1,674	1.5	140	6.6
106	Adams Bayou Lateral 2			1,499	1.4	140	6.6
107	Adams Bayou Lateral 2			1,398	1.4	140	6.6
108	Adams Bayou Lateral 2		16053 (AL2)	1,701	1.4	140	6.6
109	Hudson Gully	0508C_01		3,231	1.7	247	5.0
110	Hudson Gully	0508C_01		2,479	1.6	212	5.0
111	Hudson Gully	0508C_01	16041 (HG)	2,139	1.5	198	4.3
112	Hudson Gully	0508C_01		2,021	1.4	192	3.6
113	Gum Gully	0508B_01		2,568	1.8	223	2.0

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Segment Depth below Mean Sea Level (m)	Length (m)	Width (m)
114	Gum Gully	0508B_01		2,235	1.7	232	2.0
115	Gum Gully	0508B_01		1,715	1.6	232	2.0
116	Gum Gully	0508B_01		1,239	1.5	232	2.0
117	Gum Gully	0508B_01	16049 (GG)	1,065	1.5	232	1.9
118	Gum Gully	0508B_01		2,888	1.4	232	1.8

Table 5-3 Physical properties of Cow Bayou WASP model segments

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Segment Depth below Mean Sea Level (m)	Length (m)	Width (m)
1	Cow Bayou Tidal	0511_01		164,093	5.0	488	101
2	Cow Bayou Tidal	0511_01		185,222	4.8	488	99
3	Cow Bayou Tidal	0511_01		136,426	4.8	400	73
4	Cow Bayou Tidal	0511_01		282,546	4.8	400	98
5	Cow Bayou Tidal	0511_01		148,982	4.9	400	98
6	Cow Bayou Tidal	0511_01	18374 (CB0.5)	286,623	4.9	400	99
7	Cow Bayou Tidal	0511_01		95,051	5.0	245	100
8	Cow Bayou Tidal	0511_01		180,669	5.1	245	102
9	Cow Bayou Tidal	0511_01		220,288	5.2	554	101
10	Cow Bayou Tidal	0511_01		412,392	5.3	554	99
11	Cow Bayou Tidal	0511_01		160,334	5.4	400	99
12	Cow Bayou Tidal	0511_01	10449 (CB1)	301,587	5.4	400	100
13	Cow Bayou Tidal	0511_01		141,528	5.0	400	91
14	Cow Bayou Tidal	0511_01		375,692	4.9	400	86
15	Cow Bayou Tidal	0511_01		115,974	4.8	400	78
16	Cow Bayou Tidal	0511_01		305,722	4.7	400	69
17	Cow Bayou Tidal	0511_01		101,260	4.7	400	64
18	Cow Bayou Tidal	0511_01		296,860	4.7	400	58
19	Cow Bayou Tidal	0511_01	10451 (CB2)	111,046	4.6	400	66
20	Cow Bayou Tidal	0511_02		260,026	4.5	455	75
21	Cow Bayou Tidal	0511_02		111,809	4.5	347	68

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Depth below Mean Sea Level (m)	Length (m)	Width (m)
22	Cow Bayou Tidal	0511_02		320,678	4.4	400	64
23	Cow Bayou Tidal	0511_02		135,228	4.4	400	93
24	Cow Bayou Tidal	0511_02	10452 (CB2.5)	339,272	4.3	400	119
25	Cow Bayou Tidal	0511_02		146,274	4.3	400	101
26	Cow Bayou Tidal	0511_02		339,446	4.3	400	101
27	Cow Bayou Tidal	0511_02		120,413	4.3	400	97
28	Cow Bayou Tidal	0511_02		295,014	4.3	400	73
29	Cow Bayou Tidal	0511_02	10453 (CB3)	82,120	4.8	400	60
30	Cow Bayou Tidal	0511_02		68,926	5.3	400	60
31	Cow Bayou Tidal	0511_02		67,187	4.8	400	65
32	Cow Bayou Tidal	0511_02		62,876	4.3	400	58
33	Cow Bayou Tidal	0511_02		41,187	4.0	400	46
34	Cow Bayou Tidal	0511_02		41,470	3.9	400	35
35	Cow Bayou Tidal	0511_02		38,385	3.8	400	35
36	Cow Bayou Tidal	0511_02		38,780	3.7	400	34
37	Cow Bayou Tidal	0511_02		33,303	3.7	400	30
38	Cow Bayou Tidal	0511_02	10454 (CB3.5)	27,713	3.6	345	26
39	Cow Bayou Tidal	0511_02		31,188	3.5	435	25
40	Cow Bayou Tidal	0511_02		43,458	3.4	400	25
41	Cow Bayou Tidal	0511_02		19,530	3.3	293	25
42	Cow Bayou Tidal	0511_03		51,461	3.2	496	24
43	Cow Bayou Tidal	0511_03		24,687	3.1	400	24
44	Cow Bayou Tidal	0511_03		30,695	3.0	400	24
45	Cow Bayou Tidal	0511_03		22,810	2.9	400	23
46	Cow Bayou Tidal	0511_03		24,360	2.8	400	22
47	Cow Bayou Tidal	0511_03		20,179	2.7	400	22
48	Cow Bayou Tidal	0511_03		20,596	2.6	400	22
49	Cow Bayou Tidal	0511_03		15,581	2.5	350	22
50	Cow Bayou Tidal	0511_03		16,573	2.4	350	21
51	Cow Bayou Tidal	0511_03		14,159	2.4	350	21
52	Cow Bayou Tidal	0511_03		13,664	2.3	350	21
53	Cow Bayou Tidal	0511_03		10,279	2.3	350	18

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Depth below Mean Sea Level (m)	Length (m)	Width (m)
54	Cow Bayou Tidal	0511_03	13781 (CB4)	9,998	2.2	350	16
55	Cow Bayou Tidal	0511_03		9,383	2.2	350	16
56	Cow Bayou Tidal	0511_03		8,750	2.1	350	16
57	Cow Bayou Tidal	0511_03		8,270	2.0	355	15
58	Cow Bayou Tidal	0511_03		7,706	2.0	355	14
59	Cow Bayou Tidal	0511_04		6,488	1.9	315	14
60	Cow Bayou Tidal	0511_04		10,273	1.9	315	13
61	Cow Bayou Tidal	0511_04		6,362	1.8	350	12
62	Cow Bayou Tidal	0511_04		10,380	1.7	350	11
63	Cow Bayou Tidal	0511_04		5,683	1.7	350	12
64	Cow Bayou Tidal	0511_04		10,378	1.6	350	13
65	Cow Bayou Tidal	0511_04	10457 (CB5)	5,822	1.7	350	13
66	Cow Bayou Tidal	0511_04		11,320	1.7	350	13
67	Cow Bayou Tidal	0511_04		6,552	1.7	350	13
68	Cow Bayou Tidal	0511_04		40,414	1.7	350	13
69	Cow Bayou Oxbow 1			40,650	3.7	258	48
70	Cow Bayou Oxbow 1			63,783	3.7	258	48
71	Cow Bayou Oxbow 1			39,925	3.7	271	48
72	Cow Bayou Oxbow 1			57,988	3.7	268	48
73	Cow Bayou Oxbow 1			39,359	3.7	267	48
74	Cow Bayou Oxbow 1			57,935	3.7	268	48
75	Cow Bayou Oxbow 1			39,473	3.7	268	48
76	Cow Bayou Oxbow 1			57,736	3.7	267	48
77	Cow Bayou Oxbow 1			39,313	3.7	267	48
78	Cow Bayou Oxbow 1			65,724	3.7	266	48
79	Cow Bayou Oxbow 1			39,568	3.7	269	48
80	Cow Bayou Oxbow 1			58,005	3.7	268	48
81	Cow Bayou Oxbow 1			39,303	3.7	267	48
82	Cow Bayou Oxbow 1			57,980	3.7	2688	48
83	Cow Bayou Oxbow 1			39,254	3.7	267	48
84	Cow Bayou Oxbow 1			57,548	3.7	266	48
85	Unnamed Tributary to Cow Bayou Tidal	0511D_01		5,894	1.4	400	14.2

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Depth below Mean Sea Level (m)	Length (m)	Width (m)
86	Unnamed Tributary to Cow Bayou Tidal	0511D_01		3,805	1.3	400	11.1
87	Unnamed Tributary to Cow Bayou Tidal	0511D_01		3,525	1.3	400	8.9
88	Unnamed Tributary to Cow Bayou Tidal	0511D_01		5,769	1.2	400	8.2
89	Cow Bayou Oxbow 3			19,581	2.3	230	47
90	Cow Bayou Oxbow 3			23,488	2.3	230	47
91	Cow Bayou Oxbow 3			19,595	2.3	230	47
92	Cow Bayou Oxbow 3			28,086	2.3	208	47
93	Cow Bayou Oxbow 3			35,167	2.3	260	47
94	Cow Bayou Oxbow 3			19,601	2.3	230	47
95	Cow Bayou Oxbow 3			27,197	2.3	232	47
96	Cow Bayou Oxbow 3			19,770	2.3	232	47
97	Coon Bayou	0511B_01		8,475	2.3	253	16.5
98	Coon Bayou	0511B_01		28,155	2.2	231	16.3
99	Coon Bayou	0511B_01		7,156	2.2	230	16.2
100	Coon Bayou	0511B_01		12,225	2.1	230	16.0
101	Coon Bayou	0511B_01		6,446	2.0	230	15.9
102	Coon Bayou	0511B_01		11,516	1.9	230	15.6
103	Coon Bayou	0511B_01		4,883	1.8	230	15.3
104	Coon Bayou	0511B_01		12,114	1.7	230	12.9
105	Coon Bayou	0511B_01	16052 (CNB)	3,374	1.6	230	10.6
106	Coon Bayou	0511B_01		11,275	1.5	231	9.8
107	Coon Bayou	0511B_01		2,513	1.4	230	8.4
108	Coon Bayou	0511B_01		24,479	1.3	230	7.6
109	Sandy Creek			3,397	1.8	250	9.4
110	Sandy Creek			3,039	1.7	250	8.8
111	Sandy Creek			2,679	1.6	250	8.3
112	Sandy Creek			2,344	1.5	250	7.8
113	Sandy Creek			2,096	1.4	250	7.3
114	Sandy Creek			4,821	1.3	250	6.8
115	Cole Creek	0511C_01		3,086	2.0	449	4.9

Segment	Segment Name	AU	TCEQ Monitoring Site ID (Label)	Volume (m ³)	Average Maximum Depth below Mean Sea Level (m)	Length (m)	Width (m)
116	Cole Creek	0511C_01		2,487	1.9	400	4.5
117	Cole Creek	0511C_01		2,244	1.8	400	4.4
118	Cole Creek	0511C_01		2,017	1.7	400	4.1
119	Cole Creek	0511C_01		1,885	1.7	400	3.9
120	Cole Creek	0511C_01		1,762	1.7	400	3.7
121	Cole Creek	0511C_01		1,641	1.6	400	3.6
122	Cole Creek	0511C_01		1,529	1.6	400	3.4
123	Cole Creek	0511C_01		1,519	1.6	400	3.2
124	Cole Creek	0511C_01		7,151	1.5	400	3.0
125	Terry Gully	0511E_01		7,652	1.8	350	13.1
126	Terry Gully	0511E_01		7,199	1.7	350	13.0
127	Terry Gully	0511E_01		6,989	1.7	350	12.8
128	Terry Gully	0511E_01		6,778	1.6	350	12.8
129	Terry Gully	0511E_01	18377 (TG2)	6,286	1.6	350	12.4
130	Terry Gully	0511E_01		5,808	1.6	350	11.6
131	Terry Gully	0511E_01		5,116	1.5	350	11.0
132	Terry Gully	0511E_01		4,429	1.5	350	10.5
133	Terry Gully	0511E_01		3,948	1.5	350	9.5
134	Terry Gully	0511E_01		3,461	1.5	350	8.5
135	Terry Gully	0511E_01		3,117	1.5	350	7.5
136	Terry Gully	0511E_01		31,391	1.5	350	6.5

In WASP, the eutrophication module can be run with various levels of complexity, simulating the transport and transformations of up to 28 state variables. A listing of these state variables is included in Table 5-4, with those actively simulated in the Adams Bayou and Cow Bayou models noted.

Table 5-4 WASP state variables

Variable	Units	Active
salinity	ppt	✓
pH	standard units	✗
alkalinity	mg/L as CaCO ₃	✗
DO	mg/L	✓
cBOD group 1 (cBOD1)	mg/L	✓
cBOD group 2 (cBOD2)	mg/L	✗
cBOD group 3 (cBOD3)	mg/L	✗
NH ₃ N	mg/L	✓
NO ₃ N	mg/L	✓
OrgN	mg/L	✓
PO ₄ P	mg/L	✓
OrgP	mg/L	✓
inorganic silica	mg/L	✗
dissolved organic silica	mg/L	✗
phytoplankton group 1	µg/L as chla	✓
phytoplankton group 2	µg/L as chla	✗
phytoplankton group 3	µg/L as chla	✗
detrital nitrogen (DETN)	mg/L	✓
detrital phosphorus (DETP)	mg/L	✓
detrital carbon (DETC)	mg/L	✓
detrital silica	mg/L	✗
total detritus	mg/L	✓
inorganic suspended solids group 1 (sand)	mg/L	✓
inorganic suspended solids group 2 (silt)	mg/L	✓
inorganic suspended solids group 3 (clay)	mg/L	✓
benthic algae	g/m ²	✗
periphyton cell quota nitrogen	mg/g	✗
periphyton cell quota phosphorus	mg/g	✗

Two issues associated with the reaeration computations in WASP7.52 necessitate discussion at this point in the report. First, WASP7.52 restricts the user to input of a single minimum for the reaeration rate (K_a) with the units of day⁻¹ that is applicable to all model segments. It is the long-

standing practice of TCEQ to compute the minimum K_a based on a minimum value of the oxygen transfer coefficient (K_L) of 0.6 m day^{-1} . Under this practice, the minimum K_a would be computed as $K_a = K_L/\text{water depth}$ and would vary with the simulated depths of each model segment. Since K_a cannot be varied across WASP segments, it is not possible to tailor the minimum K_a to individual WASP segments through the input options available in the software. The minimum K_a will either be close to correct for the deepest portions of the channel and too small for the shallower portions, or about correct for shallow portions and too small for the deeper portions.

Second, K_a is being computed for this WASP application under the model option to use the larger of the K_a value determined from wind-induced oxygen transfer or flow-induced (water velocity) oxygen transfer. It was discovered during the modeling process, and confirmed in December 2018 by EPA Region 4 staff who oversaw the WASP modeling software, that the wind-induced K_a was incorrectly programmed in WASP, and that the error was that the computation did not include division by water depth. Thus, the model was computing wind-induced K_a values that were too large for all water depths $> 1 \text{ m}$. The WASP software was, in fact, computing K_L , the oxygen transfer coefficient instead of K_a . Average water depths along the tidal portions of Adams and Cow Bayous range from 2 m to 5 m (Tables 5-2 and 5-3) resulting in an appreciable over prediction in the model's computation of wind-induced K_a . For many stream systems, the wind-induced K_a is not important, because water velocities are sufficiently high that the flow-induced K_a values are predominately greater than the wind-induced values, and the higher flow-induced values are used by the model. However, Adams and Cow Bayous are, in essence, tidal backwater systems with low streamflows relative to stream cross-sectional area, which results in low water velocities under many circumstances. Thus, computed flow-induced K_a is often less than wind-induced K_a , and the wind-induced K_a becomes an important term in the model for Adams and Cow Bayous.

Since the source code to the old version of WASP could not be corrected, the initial approach to the second issue was to use a newer version of WASP (i.e., version 8.3) for which the error in computation of the wind-induced K_a had been corrected. However, even with assistance from EPA Region 4 staff, the conversion of the input data being used in this modeling effort into WASP version 8.3 was unsuccessful and a working model in the latest version could not readily be developed without extensive rework and substantial time and resource expenditures. Even with this newer version of WASP, the first issue regarding definition of a minimum K_a consistent with TCEQ protocol would not have been addressed (i.e., a single K_a is still applicable to all WASP 8.3 model segments). Therefore, the approach shifted to adjusting input to the existing WASP 7.52 model to compensate for the global K_a limitation in WASP and to correct for the error in computing wind-induced K_a .

Both of these reaeration issues in WASP7.52 were addressed through user modifications to the wind input to the model, which included a time series of wind speed and a multiplier to the wind speed that can be specified by model segment. To address the minimum K_a issue, a wind speed

was determined that provided a K_L value of 0.6 m day^{-1} . Wind-induced K_a in WASP is computed using one of three formulas that are a function of wind speed, air and water temperature, and, if programmed correctly, water depth. For wind speeds $< 6 \text{ m/s}$, the formula used is a linear function of wind speed with some slight non-linearities due to air and water temperature. For wind speeds $> 6 \text{ m/s}$, the formulas involve non-linear functions of wind speed that resulted in values increasing with wind speed faster than the linear function. WASP output of wind-induced K_a was analyzed for multiple segments having a range of depths. These wind-induced K_a values were actually K_L values because of the coding error wherein the computations did not include division by depth. Visual review of scatterplots of K_L (corrected to $20 \text{ }^\circ\text{C}$) with wind speed, indicated that a value of $K_L = 0.6 \text{ m day}^{-1}$ occurred at very close to the same wind speed regardless of segment selection and occurred in the linear portion of the graph for wind speeds $< 6 \text{ m/s}$. Highly significant linear regression equations with $r^2 > 0.98$ were developed for each segment investigated representing the range in depths in the WASP models, and each regression equation indicated that a wind speed of 2.5 m/s (5.6 mph) resulted in computation of a $K_L = 0.6 \text{ m day}^{-1}$.

To address the first issue regarding appropriate computation of a minimum K_a , the correction was relatively simple. Since the WASP option selected for K_a was to use the maximum of the wind-induced or flow-induced K_a , limiting the wind-induced K_a to a minimum giving a $K_L = 0.6 \text{ m day}^{-1}$ provided the needed adjustment. This adjustment was implemented by setting the minimum wind speed model input for any hour to 2.5 m/s . Therefore, the minimum K_a was being specified by restricting the computation of the wind-induced K_a to the value obtained from the minimum wind speed.

The remaining issue was how to correct the wind-induced K_a computed in the model for the mistake wherein division did not occur by segment water depth. Because of the coding error, WASP version 7.52 is actually computing wind-induced K_L and not wind-induced K_a . To address the error in coding, the segment-level wind multiplier input option was used. The reciprocal of the median depth of each segment was used to compute the wind multiplier for each segment. The median depth was computed using hourly output of the water depth of each segment in the Adams Bayou and Cow Bayou models for the simulated period of January 1, 2002 through December 31, 2012, or about 100,000 individual depths per segment. The wind multiplier essentially results in the computed wind-induced K_L being divided by depth, thus, giving the desired K_a . This correction through the wind multiplier provides a very workable solution to overcome the coding error in WASP; however, this is not a perfect solution. The simulated water levels of each segment are not static, but time varying. Using the median depth to compute the multiplier, therefore, means that half the time this correction gives K_a values that are too large and half the time the values are too small. Because the domain of the WASP model is the tidal streams of the Adams Bayou and Cow Bayou watersheds where stream cross-sectional areas are large compared to streamflows under most conditions and tidal fluctuations are relatively weak, for the majority of segments in both models, 90 percent of the simulated depths of each segment

were determined to be within +/- 0.35 m of the median depth, and 50 percent of the simulated depths were within +/- 0.13 m of the median depth. Not to minimize the limitations of the single wind multiplier correction for each segment, for the majority of the simulation period, the errors introduced by using the wind multiplier correction are not highly significant, because of the relatively narrow range of water depth variations in the tidal system.

5.2 WASP Input Data

Dynamic WASP model inputs include the hydrodynamic parameters generated by the RMA2 model, water quality constituent concentrations at upstream and downstream boundaries, loads of water quality constituents from point and nonpoint sources, and meteorological data.

5.2.1 Lower Boundary Condition

The concentrations of water quality constituents at the lower (Sabine River) boundary of the models were estimated based on concentrations reported to the TCEQ Surface Water Quality Monitoring Information System (SWQMIS). Primarily, this consisted of routine water quality measurements collected monthly by the Sabine River Authority or TCEQ regional office at one or more of the following stations:

Station ID	Description
Station ID 10391	Sabine River at channel CAN 3 1866 M downstream from mouth of new Cow Bayou
Station ID 10392	Sabine River at Cow Bayou confluence
Station ID 10393	Sabine River at channel light 13 2030 M upstream from mouth of new Cow Bayou
Station ID 18055	Sabine River at channel light 20 495 M upstream of the confluence of Adams Bayou and 70 M from the east bank

For most water quality constituents, the reported concentrations from these stations were averaged over the simulation period and this average concentration was used as a constant boundary condition in the WASP models. However, salinity exhibited a statistically significant relationship with flow, and a simple power function was developed to explain the majority of the variance in salinity:

$$\text{Salinity} = 2338 * Q_7^{-1.571}$$

where Q_7 is the average flow (in cms) over the preceding 7-day period. The predicted salinity from this relationship was manually limited to the range 0.05 to 20 parts per thousand (ppt) to reflect natural limits. At times the relationship predicted salinities that deviated substantially from measured values, so this predicted salinity time series was averaged with a second time series of measured salinity values, with the values for dates between measurements interpolated between them.

5.2.2 Carbonaceous Biochemical Oxygen Demand

As is typical, most laboratory measurements of cBOD were 5-day measurements (cBOD₅) at 20°C with suppression of nitrification. However, the WASP model simulates ultimate cBOD (UBOD), the total oxygen demand for biochemical conversion of all organic carbonaceous material to oxidized forms. Ultimate cBOD was estimated in the following manner. In a subset of 14 ambient water samples from several locations on each bayou on several dates, cBOD was measured after incubations of 5, 15, and 20 days. The 20-day cBOD was assumed to be equivalent to UBOD. A first-order rate curve was then fit to the data. Figure 5.3 illustrates the measured cBOD after these three periods. Figure 5.4 illustrates the range of cBOD decay rates estimated from these samples from the first-order rate equation $\ln(C/C_0) = -k \cdot t$. The ratio of UBOD:cBOD₅ ranged from 1.06 to 5.75, with an average of 3.0 and a standard deviation of 1.3. The rate of cBOD decay averaged 0.097 day⁻¹ with a standard deviation of 0.044 day⁻¹. A conversion factor of 3 was applied to all point source loads and measured ambient concentrations to convert from cBOD₅ to UBOD. The variability in this conversion factor, as well as the frequency of censored data (e.g., <3 mg/L cBOD₅) in the analytical dataset, provided a challenge to calibration.

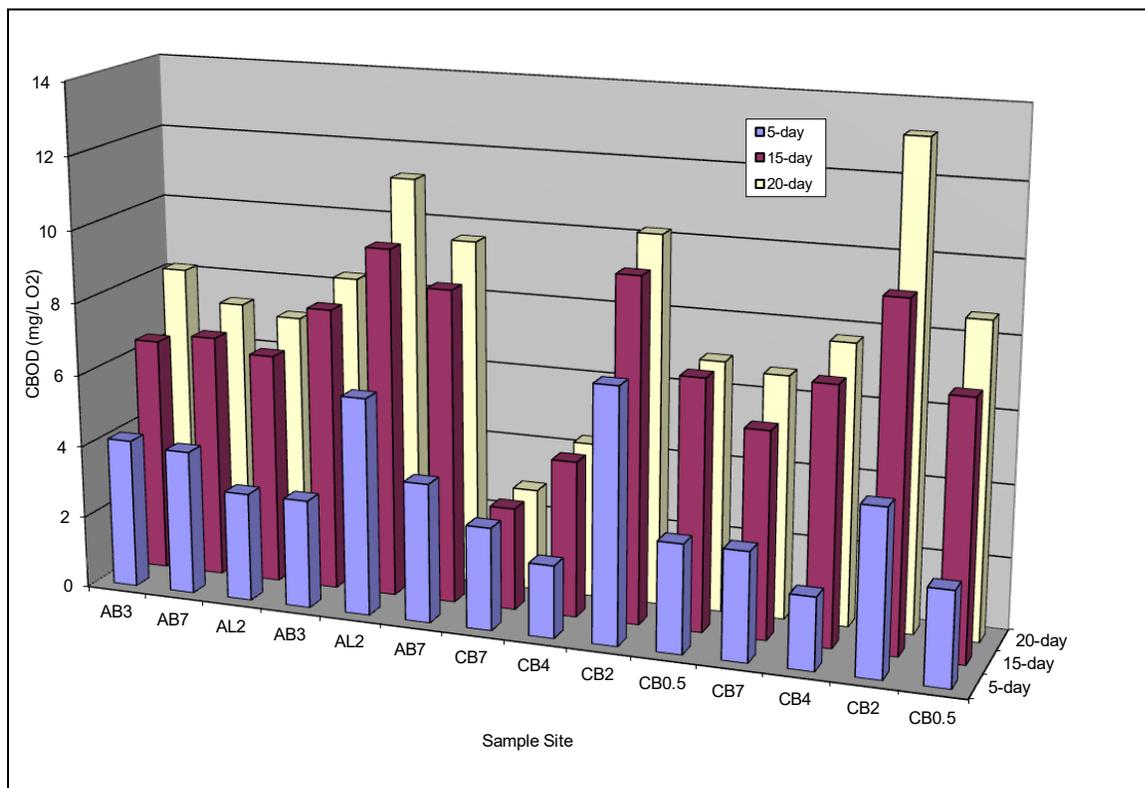


Figure 5.3 Carbonaceous BOD after 5, 15, and 20 days

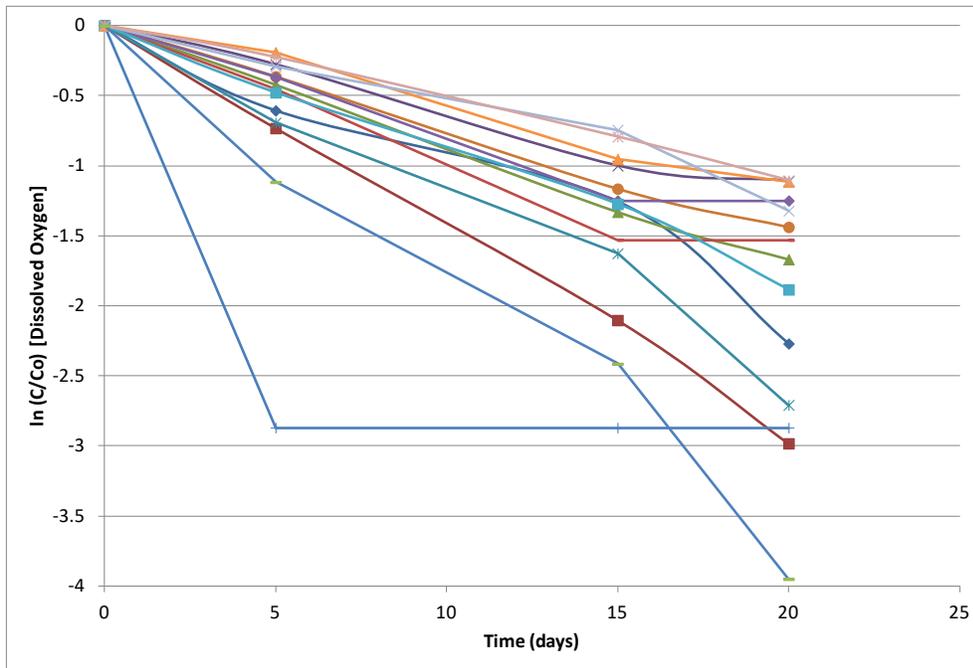


Figure 5.4 Measured rates of cBOD decay in laboratory incubations

5.2.3 WASP Linkage to the RMA2 Hydrodynamic Model

Due to the influence of tides on hydrodynamics in the bayous, an external hydrodynamic model was required to simulate water movement through the system. Historically, the external hydrodynamic model used with WASP was DYNHYD. Due to the limitations of DYNHYD, other models such as EFDC and RMA2 have been used with WASP. The hydrodynamic inputs to WASP are the segment volumes at the beginning of each time step, the average inter-segment flows during each time step, and average segment depths and velocities. WASP uses the inter-segment flows to calculate mass transport, and the volumes to calculate concentrations. The segment depths and velocities are used in calculating sediment transport, volatilization, and reaeration.

RMA2 is a link-node hydrodynamic model with a spatial network and temporal resolution equivalent to the WASP model. The RMA2 solution file reports, for each node and time step, the depth, x-velocity, and y-velocity. An RMA2 post-processor performs the tasks of calculating from these outputs the segment volumes and inter-segment flows, mapping the RMA2 nodes to WASP segments, and re-writing the output to a binary format external hydrodynamic file required by WASP model. It also performs some other useful diagnostic functions. WASP also requires that the hydrodynamic file be in a specific binary format. A utility program named Hydrolink, provided with WASP, performs the conversion from an ASCII-based hydrodynamic file to a binary format.

5.2.4 WASP Linkage to the HSPF Model and Point-Source Loads

The HSPF model is linked to the WASP model in multiple ways. First, the HSPF model is linked to the WASP model indirectly, through the RMA2 hydrodynamic model. HSPF also directly provides

WASP with the boundary water quality constituent concentrations at all upstream tidal segments of the WASP models. HSPF also provides the loads of NPS water quality constituents in middle reaches. Finally, HSPF provides a water temperature simulation that is an input to WASP. The HSPF inputs to WASP are shown in Table 5-5 (Adams Bayou) and Table 5-6 (Cow Bayou).

Point-source loads are imported into WASP via a Microsoft Excel™ spreadsheet. The input loads for point sources to the HSPF reaches are shown in Table 5-5 (Adams Bayou) and Table 5-6 (Cow Bayou).

Table 5-5 External inputs for the Adams Bayou WASP model

Source	Type	WASP Segment	Frequency	Fraction of Total Load	Assessment Unit or Location Description
HSPF Sub-basin 1	Boundary Concentration	118	Daily	1	0508B_01
HSPF Sub-basin 2	Boundary Concentration	88	Daily	1	0508A_01
HSPF Sub-basin 3	NPS Load	113	Daily	1	0508B_01
HSPF Sub-basin 4	NPS Load	77	Daily	1	0508A_01
HSPF Sub-basin 5	NPS Load	70	Daily	0.696	0508_04
		73	Daily	0.304	0508A_01
HSPF Sub-basin 6	NPS Load	75	Daily	1	0508A_01
HSPF Sub-basin 7	NPS Load	57	Daily	1	0508_04
HSPF Sub-basin 8	Boundary Concentration	112	Daily	1	0508C_01
HSPF Sub-basin 9	Boundary Concentration	108	Daily	1	0508_01
HSPF Sub-basin 10	NPS Load	25	Daily	0.183	0508_01
		29	Daily	0.294	0508_02
		35	Daily	0.523	0508_03
HSPF Sub-basin 11	Boundary Concentration	100	Daily	1	0508_01
HSPF Sub-basin 12	NPS Load	5	Daily	1	0508_01
WQ0010597-001	PS Load	48	Constant	1	City of Pinehurst
WQ0010626-001	PS Load	31	Constant	1	City of Orange
WQ0010240-001	PS Load	31	Constant	1	Orange County WCID 2
Sabine River	Boundary Concentration	1	Half Hour	Not Applicable	Downstream boundary

Table 5-6 External inputs to the Cow Bayou WASP model

Source	Type	WASP Segment	Frequency	Fraction of Total Load	Assessment Unit or Location Description
HSPF sub-basin 7	NPS Load	124	Daily	1	0511C_01
HSPF sub-basin 8	NPS Load	64	Daily	0.131	0511_04
	Boundary Concentration	68	Daily	0.869	0511A_01
HSPF sub-basin 9	NPS Load	55	Daily	0.698	0511_03
		58	Daily	0.302	0511_04
HSPF sub-basin 10	NPS Load	122	Daily	1	0511C_01
HSPF sub-basin 11	NPS Load	114	Daily	1	0511_02
HSPF sub-basin 12	NPS Load	40	Daily	0.079	0511_02
		50	Daily	0.921	0511_03
HSPF sub-basin 13	NPS Load	136	Daily	1	0511E_01
HSPF sub-basin 14	Boundary Concentration	28	Daily	1	0511_02
HSPF sub-basin 15	NPS Load	108	Daily	1	0511B_01
HSPF sub-basin 16	NPS Load	22	Daily	0.383	0511_01
		31	Daily	0.617	0511_02
HSPF sub-basin 17	NPS Load	11	Daily	0.715	0511_01
		86	Daily	0.285	0511D_01
HSPF sub-basin 18	Boundary Concentration	3	Daily	1	0511_01
WQ0000670-000	PS Load	79	Constant	1	Honeywell International
WQ0001167-000	PS Load	5	Constant	1	ARLANXEO USA LLC
WQ0000454-000	PS Load	10	Constant	1	Lion Elastomers Orange, LLC
WQ0000359-000	PS Load	88	Constant	1	Chevron Phillips Chemical
WQ0002858-000	PS Load	88	Constant	1	Printpack, Inc.
WQ0015029-001	PS Load	107	Constant	1	Bayou Pines
WQ0013488-001	PS Load	101	Constant	1	Gulflander Partners Group
WQ0010051-001	PS Load	17	Constant	1	City of Bridge City
WQ0014772-001	PS Load	29	Constant	1	Orangefield WSC
WQ0011916-001	PS Load	67	Constant	1	PCS Development Group
Sabine River	Boundary Concentrations	1 & 69	30 minutes	Not Applicable	Downstream boundary

5.3 Calibration and Validation of the WASP Models

The WASP models were calibrated primarily to data collected during intensive surveys of Adams Bayou and Cow Bayou on May 23 - 28, 2004 and July 17 - 22, 2004, respectively. The models were also compared to other quality-assured water quality data found in TCEQ SWQMIS database from Adams and Cow Bayous from 2002 to 2012. In most years, routine monitoring by the Sabine River Authority has been limited to a single station in Adams Bayou (AB2, also known as TCEQ SWQM station 10441) and a single station in Cow Bayou (CB1, also known as TCEQ SWQM station 10449), but the Texas Parks and Wildlife Department also performed water quality monitoring of four other stations on Cow Bayou on a monthly basis during 2003 and 2004 as part of a Use Attainability Study. Water quality calibration of WASP was done in the following order:

1. salinity
2. cBOD
3. OrgN
4. NH₃N, NO₃N, and PO₄P
5. Chla
6. DO

However, there were multiple iterations of calibration. Also, model predictions of TSS were compared to measured levels after salinity calibration. The WASP eutro model does not offer parameters to adjust TSS calibration, but a fixed sedimentation flux from the water column to sediments was added.

Longitudinal plots by station with simulated and observed data and observed and modeled averages were used to visually evaluate model performance during calibration.

During the calibration process, the model parameters to which the model was most sensitive were adjusted within literature-recommended ranges or as indicated from watershed specific data. The most important model parameter was DO. The model performance target for DO was an overall RMSE of less than 1.5 mg/L for the separate calibration and validation periods. Other targets included salinity (overall RMSE < 0.6 ppt) , TSS (overall RMSE < 50% of the observed average concentration or 5 mg/L, whichever is greater), and NH₃N, NO₃N, OrgN, and PO₄P (overall RMSE < 50% of the observed average concentration or 0.25 mg/L, whichever is greater).

Following calibration, the simulation results for each calibrated model were validated by comparison to data from a second intensive survey on each bayou. These intensive surveys were performed June 29 - July 1, 2004 (Adams Bayou) and August 24 - 26, 2004 (Cow Bayou). The model performance targets for the validation period were identical to the calibration targets.

Antecedent rainfall and flow conditions were different between the two surveys on each bayou. For some parameters, the initial calibration did not result in good fit to the validation dataset. While in most cases the validation criteria were met, the models were often re-calibrated in an attempt to achieve a good fit to both of the intensive surveys (and the other datasets). There were many iterations to achieve what the modelers believes was the best practical fit.

Figures 5-5 and 5-6 illustrate the goodness of fit of the WASP DO simulation. Statistical summaries of model goodness-of-fit for Adams Bayou are included in Tables 5-7 through 5-9. Table 5-10 lists the key parameters for the Adams Bayou WASP model. Additional graphical presentations of water quality comparisons of model predicted results and measured data are provided in Appendix G.

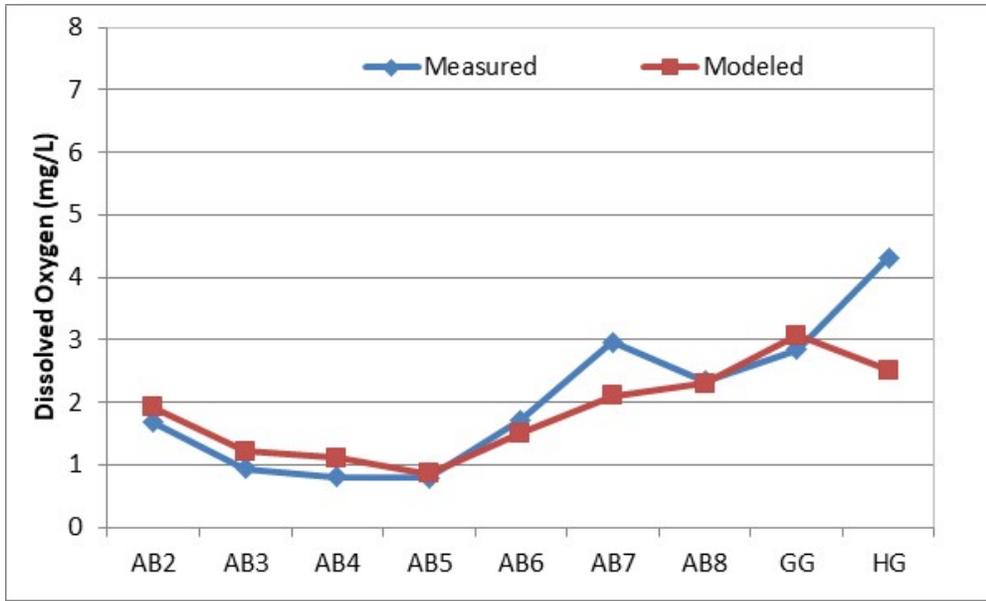


Figure 5-5 Longitudinal model fit of Adams Bayou daily average DO for the calibration period

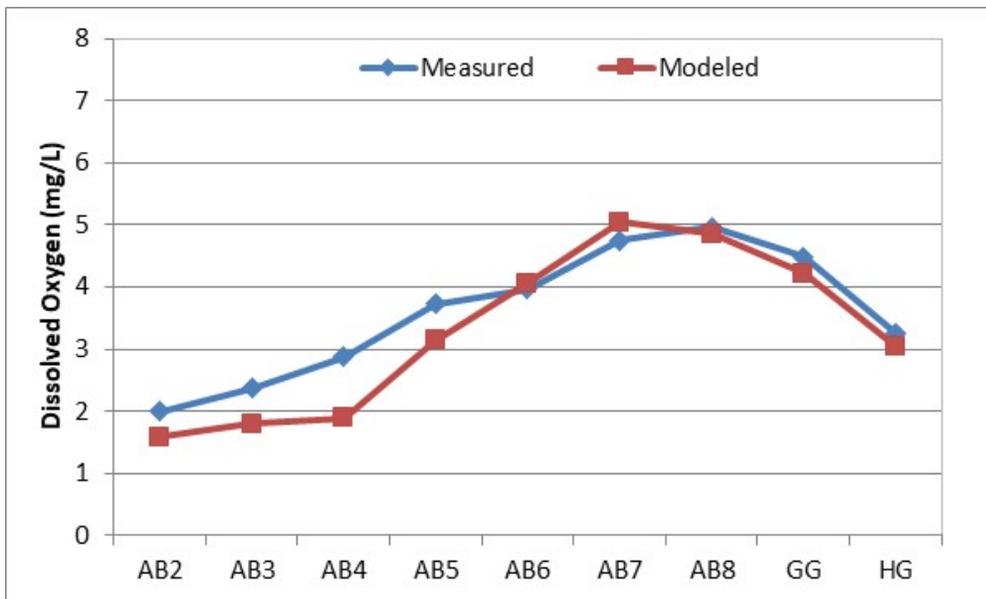


Figure 5-6 Longitudinal model fit of Adams Bayou daily average DO for the validation period

Table 5-7 Model fit statistics for daily average DO in Adams Bayou

Model performance targets based on RMSE and any station's RMSE not meeting the target is in bold red font.

Period	Station	n	Measured Average (mg/L)	Model Average (mg/L)	ME (mg/L)	MAE (mg/L)	RMSE (mg/L)
Calibration	All	18	2.04	1.85	-0.20	0.45	0.69
Validation	All	16	3.60	3.29	-0.31	0.39	0.48
All Data	AB2	4	1.84	1.75	-0.09	0.32	0.38
All Data	AB3	4	1.66	1.51	-0.15	0.43	0.52
All Data	AB4	4	1.84	1.50	-0.34	0.65	0.77
All Data	AB5	4	2.26	2.00	-0.26	0.32	0.44
All Data	AB6	4	2.84	2.79	-0.05	0.40	0.46
All Data	AB7	4	3.85	3.58	-0.28	0.86	0.93
All Data	AB8	4	3.65	3.58	-0.10	0.36	0.37
All Data	GG	2	3.67	3.65	-0.02	0.41	0.49
All Data	HG	4	3.79	2.78	-1.01	1.01	1.28

Table 5-8 Calibration statistics for the Adams Bayou WASP model

Model performance targets based on RMSE and any parameter's RMSE not meeting the target is in bold red font.

Parameter	Measured Average	Model Average	ME	MAE	RMSE
Salinity (ppt)	0.10	0.05	-0.05	0.06	0.09
TSS (mg/L)	10.20	5.58	-4.62	4.62	6.96
cBOD (ultimate, mg/L)	10.08	10.96	0.89	3.50	4.76
OrgN (mg/L)	1.23	1.12	-0.11	0.29	0.35
NH ₃ N (mg/L)	0.18	0.21	0.04	0.07	0.08
NO ₃ N (mg/L)	0.04	0.09	0.05	0.05	0.06
PO ₄ P (mg/L)	0.31	0.29	-0.02	0.07	0.08
Chla (µg/L)	13.80	9.62	-4.17	8.25	9.01

Table 5-9 Validation statistics for the Adams Bayou WASP model

Model performance targets based on RMSE and any parameter’s RMSE not meeting the target is in bold red font.

Parameter	Measured Average	Model Average	ME	MAE	RMSE	
Salinity (ppt)	0.04	0.05	0.01	0.02	0.02	
TSS (mg/L)	27.16	15.97	-11.19	11.19	13.07	
cBOD (ultimate, mg/L)	10.87	10.58	-0.28	1.27	1.57	
OrgN (mg/L)	0.79	0.90	0.11	0.18	0.25	
NH ₃ N (mg/L)	0.07	0.18	0.10	0.11	0.12	
NO ₃ N (mg/L)	0.04	0.14	0.10	0.10	0.11	
PO ₄ P (mg/L)	0.18	0.20	0.02	0.05	0.05	
Chla (µg/L)	5.19	7.82	2.63	4.11	5.49	

Table 5-10 Key parameters of the Adams Bayou WASP model

In the Source Column: F = collected data, L = literature, C=calibrated, Cf = calibrated within range of field collected data

Parameter Description	Units	Source	Value or Range
dispersion coefficient between adjacent segments	m ² /day	C	0.25 – 5.0
dispersion coefficient for pore water	cm ² /day	L	3x10 ⁻⁵
segment scale factor for wind	none	F	0.4 – 1.0
theta – reaeration temperature coefficient	none	L	1.022
minimum oxygen transfer coefficient (set using wind scale factors and specifying a minimum wind speed of 2.5 m/s in time series input)	1/day	L	≈0.6
maximum allowable calculated reaeration rate	1/day	L	10
cBOD decay rate constant @ 20°C	1/day	Cf	0.12
cBOD decay temperature coefficient	none	L	1.047
segment cBOD decay rate scale factor	none	C	1 – 2.5
cBOD decay rate constant in sediments @ 20°C	1/day	L	4x10 ⁻⁴
cBOD decay in sediments temperature coefficient	none	L	1.08
BOD half-saturation oxygen limit	mg/L O ₂	L	0 – 2.0
fraction of detritus dissolution to cBOD	none	L	1
fraction of cBOD carbon source for denitrification	none	L	1
detritus dissolution rate	1/day	C	0.4
detritus dissolution temperature coefficient	none	L	1.047

Parameter Description	Units	Source	Value or Range
OrgN mineralization rate constant (dissolved) @ 20°C	1/day	C	0.02
OrgN mineralization (dissolved) temperature coefficient	none	L	1.07
OrgN mineralization rate constant (sediments) @ 20°C	1/day	L	0.015
OrgN mineralization (in sediments) temperature coefficient	none	L	1.047
fraction of phytoplankton death recycled to OrgN	none	L	1
OrgP mineralization rate constant (dissolved) @ 20°C	1/day	C	0.15
OrgP mineralization (dissolved) temperature coefficient	none	L	1.08
OrgP mineralization rate constant (sediments) @ 20°C	1/day	L	0.015
OrgP mineralization rate (sediments) temperature coefficient	none	L	1.047
fraction of phytoplankton death recycled to OrgP	none	L	1
nitrification rate constant @ 20°C	1/day	C	0.35
nitrification temperature coefficient	none	L	1.08
half-saturation for nitrification	mg/L O ₂	L	2
segment benthic NH ₃ N flux	mg/m ² -day	C	0 - 310
denitrification rate constant @ 20°C	1/day	C	1
denitrification temperature coefficient	none	L	1.08
half-saturation for denitrification	mg/L O ₂	L	5
segment benthic PO ₄ P flux	mg/m ² -day	C	0 - 31
phytoplankton maximum growth rate constant @ 20°C	1/day	C	2
phytoplankton growth temperature coefficient	none	L	1.068
algal self-shading coefficient	none	L	0.048
algal self-shading exponent	none	L	1
phytoplankton carbon to chlorophyll ratio	none	L	35
phytoplankton half-saturation constant for nitrogen uptake	mg N/L	L	0.05
phytoplankton half-saturation constant for phosphorus uptake	mg P/L	L	0.01
phytoplankton endogenous respiration rate constant @ 20°C	1/day	C	0.075
phytoplankton respiration temperature coefficient	none	L	1.045
phytoplankton non-predatory mortality rate constant	1/day	L	0.02
phytoplankton zooplankton grazing rate constant	1/day	L	1.5
phytoplankton decay rate constant in sediments	1/day	L	0.02
phytoplankton decay in sediments temperature coefficient	none	L	1.08
phytoplankton phosphorus to carbon ratio	none	L	0.02
phytoplankton nitrogen to carbon ratio	none	L	0.25

Parameter Description	Units	Source	Value or Range
phytoplankton half-saturation for recycle of OrgN and OrgP	mg TOC/L	L	0.2
phytoplankton maximum quantum yield	Langley/day	L	720
phytoplankton optimal light saturation	Langley/day	L	360
detritus and solids light extinction multiplier	1/m	C	0.2
fraction light intercepted by canopy	none	F	0 – 0.5
segment zooplankton population	mg TOC/L	C	0.05 – 0.5
oxygen to carbon stoichiometric ratio	none	L	2.67
sediment oxygen demand (SOD)	g/m ² -day	F	1 – 4.1
temperature correction for SOD	none	L	1.047

Figures 5-7 and 5-8 illustrate the goodness of fit of the WASP DO simulation. Statistical summaries of overall model goodness-of-fit for Cow Bayou are included in Tables 5-11 through 5-13. Table 5-14 lists the key parameters for the Cow Bayou WASP model. Additional graphical presentations of water quality comparisons of model predicted results and measured data are provided in Appendix H.

For the most part, the WASP model also performed well in predicting water quality conditions in the tidal portion of Cow Bayou and its tidal tributaries. Based on goodness-of-fit targets in the QAPP, the WASP results met the DO target of RMSE < 1.5 mg/L specified for the combination of all station for the separate calibration and validation periods (Table 5-11). If this RMSE target is extended more narrowly than intended to the individual station level, the target is not met at three stations: CB2.5, CB3, and TG2. Stations CB2.5 and CB3 are located in AU 0511_02 of Cow Bayou Tidal, which is impaired for depressed DO and is located between the immediately downstream, unimpaired AU 0511_01 and impaired AUs 0511_03 and 0511_04, which are directly upstream of AU 0511_02. WASP results appear to be less robust in simulating the DO in this transition zone between depressed DO and acceptable DO. The third station with a missed DO performance target was station TG2, which is located in Terry Gully (0511E_01); an AU that is not impaired for depressed DO. The graphical presentation of results for the calibration period (Figure 5-7) and the validation period (Figure 5-8) further illustrate the reasonable predictions of DO by WASP with the less robust simulation apparent around stations CB2.5 and CB3.

For the other water quality parameters, which were based on RMSE values being less than 50 percent of the observed average for all stations, the performance targets were met for all parameters during both the calibration and validation periods (Tables 5-12 and 5-13), except for TSS during the validation period and OrgN during the calibration and validation periods. As with Adams Bayou, the results provided are after a concerted effort to improve TSS predictions.

Because TSS has only secondary implications on the primary parameter, DO, when compared to the primary parameters of cBOD and NH₃N, this missed target should have negligible implications on the ability of WASP to predict DO. OrgN does have implications on NH₃N concentration, since OrgN mineralizes into NH₃N. While the RMSE performance target was not met for OrgN, the average simulated concentrations for both the calibration and validation periods are close to the measured concentrations and on average the simulated concentrations are slightly higher affording slightly conservative predictions.

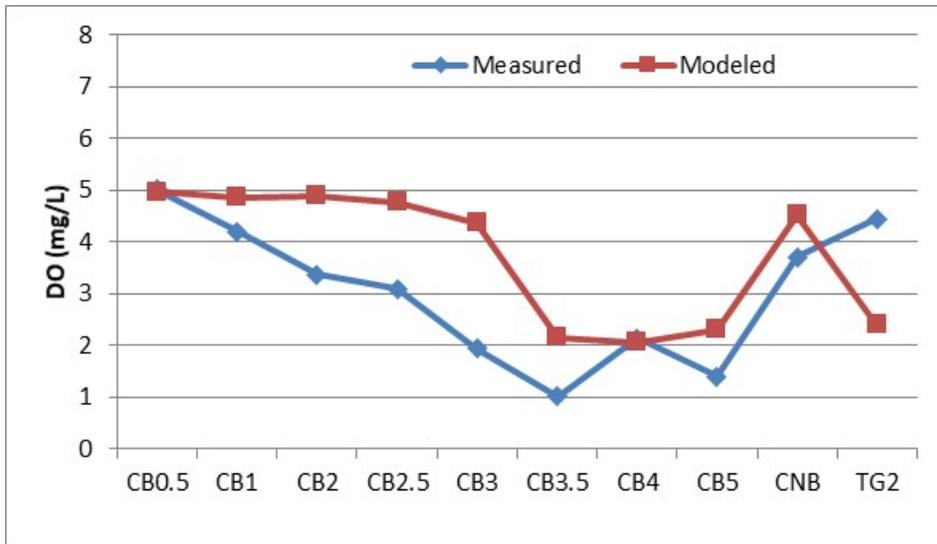


Figure 5-7 Longitudinal model fit of Cow Bayou daily average DO for the calibration period

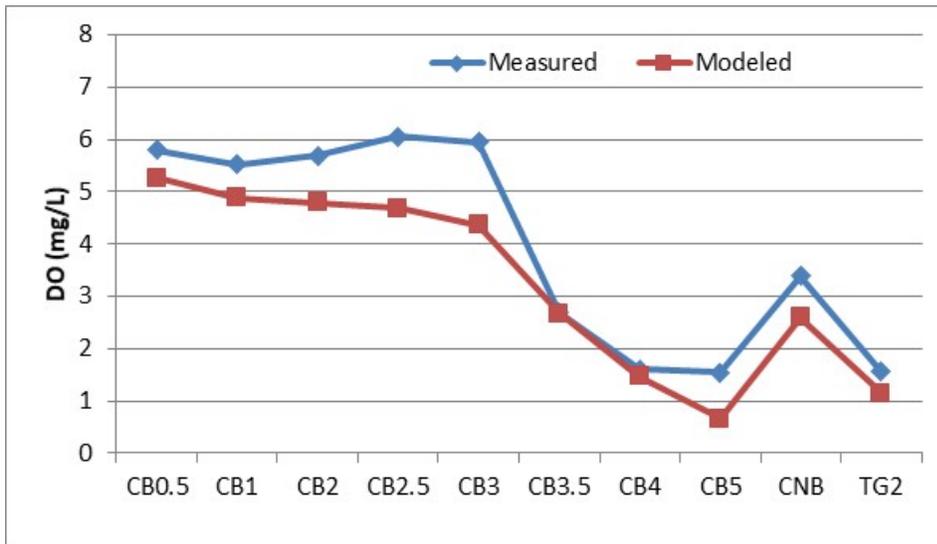


Figure 5-8 Longitudinal model fit of Cow Bayou daily average DO for the validation period

Table 5-11 Model fit statistics for daily average DO (mg/L) in Cow Bayou

Model performance targets based on RMSE and any station's RMSE not meeting the target is in bold red font.

Period	Station	n	Measured Average (mg/L)	Model Average (mg/L)	ME (mg/L)	MAE (mg/L)	RMSE (mg/L)
Calibration	All	20	3.01	3.74	0.73	1.12	1.34
Validation	All	20	4.00	3.25	-0.76	0.76	0.89
All Data	CB0.5	4	5.43	5.12	-0.31	0.38	0.43
All Data	CB1	4	4.88	4.87	-0.01	0.66	0.69
All Data	CB2	4	4.55	4.83	0.28	1.22	1.27
All Data	CB2.5	4	4.58	4.73	0.15	1.55	1.57
All Data	CB3	4	3.95	4.36	0.41	2.02	2.07
All Data	CB3.5	4	1.86	2.41	0.55	0.63	0.81
All Data	CB4	4	1.84	1.76	-0.08	0.42	0.51
All Data	CB5	4	1.46	1.49	0.03	0.91	0.95
All Data	CNB	4	3.54	3.56	0.02	0.99	1.34
All Data	TG2	4	2.96	1.78	-1.18	1.21	1.74

Table 5-12 Calibration statistics for the Cow Bayou WASP model

Model performance targets based on RMSE and any parameter's RMSE not meeting the target is in bold red font.

Parameter	Measured Average	Model Average	ME	MAE	RMSE
Salinity (ppt)	0.13	0.25	0.12	0.12	0.15
TSS (mg/L)	9.92	6.59	-2.54	3.62	4.20
cBOD (ultimate, mg/L)	11.12	9.90	-1.22	3.95	4.59
OrgN (mg/L)	0.87	0.95	0.08	0.42	0.49
NH ₃ N (mg/L)	0.14	0.09	-0.05	0.06	0.07
NO ₃ N (mg/L)	0.14	0.07	-0.06	0.07	0.08
PO ₄ P (mg/L)	0.06	0.10	0.04	0.05	0.07
Chla (µg/L)	25.42	26.96	1.55	17.28	21.92

Table 5-13 Validation statistics for the Cow Bayou WASP model

Model performance targets based on RMSE and any parameter’s RMSE not meeting the target is in bold red font.

Parameter	Measured Average	Model Average	ME	MAE	RMSE
Salinity (ppt)	1.32	1.29	-0.03	0.27	0.35
TSS (mg/L)	9.29	12.53	3.24	3.92	6.30
cBOD (ultimate, mg/L)	8.09	10.90	2.82	4.53	6.83
OrgN (mg/L)	0.60	0.61	0.01	0.28	0.36
NH ₃ N (mg/L)	0.08	0.16	0.08	0.12	0.19
NO ₃ N (mg/L)	0.08	0.11	0.02	0.05	0.06
PO ₄ P (mg/L)	0.03	0.20	0.17	0.17	0.21
Chla (µg/L)	18.54	8.54	-10.01	10.97	15.62

Table 5-14 Key parameters of the Cow Bayou WASP model

In the Source Column: F = collected data, L = literature, C=calibrated, Cf = calibrated within range of field collected data

Parameter Description	Units	Source	Value or Range
dispersion coefficient between adjacent segments	m ² /day	C	5 – 50
dispersion coefficient for pore water	cm ² /day	L	3x10 ⁻⁵
segment scale factor for wind	none	C	0.4 – 1.1
theta – reaeration temperature coefficient	none	L	1.022
minimum oxygen transfer coefficient (set using wind scale factors and specifying a minimum wind speed of 2.5 m/s in time series input)	1/day	L	≈0.6
maximum allowable calculated reaeration rate	1/day	L	10
cBOD decay rate constant @ 20°C	1/day	Cf	0.1
cBOD decay temperature coefficient	none	L	1.047
segment cBOD decay rate scale factor	none	C	0.4 – 3.0
BOD half-saturation oxygen limit	mg/L O ₂	L	0.5
fraction of detritus dissolution to cBOD	none	L	1
detritus dissolution rate	1/day	C	0.5
detritus dissolution temperature coefficient	none	L	1.047
OrgN mineralization rate constant (dissolved) @ 20°C	1/day	C	0.15
OrgN mineralization (dissolved) temperature coefficient	none	L	1.08
OrgN mineralization rate constant (sediments) @ 20°C	1/day	L	4x10 ⁻²
OrgN mineralization (in sediments) temperature coefficient	none	L	1.047

Parameter Description	Units	Source	Value or Range
OrgP mineralization rate constant (dissolved) @ 20°C	1/day	C	0.22
OrgP mineralization (dissolved) temperature coefficient	none	L	1.08
OrgP mineralization rate constant (sediments) @ 20°C	1/day	L	4x10 ⁻⁴
OrgP mineralization rate (sediments) temperature coefficient	none	L	1.047
fraction of phytoplankton death recycled to OrgP	none	C	0
nitrification rate constant @ 20°C	1/day	C	0.35
nitrification temperature coefficient	none	L	1.08
half-saturation for nitrification	mg/L O ₂	L	2
segment benthic NH ₃ N flux	mg/m ² -day	C	-100 – 100
half-saturation for denitrification	mg/L O ₂	L	5
denitrification rate constant @ 20°C	1/day	C	0.6
denitrification temperature coefficient	none	L	1.045
segment benthic PO ₄ P flux	mg/m ₂ -day	C	-10
phytoplankton maximum growth rate constant @ 20°C	1/day	C	1.4
phytoplankton growth temperature coefficient	none	L	1.068
algal self-shading coefficient	none	L	0.048
algal self-shading exponent	none	L	1
phytoplankton carbon to chlorophyll ratio	none	L	36
phytoplankton half-saturation constant for nitrogen uptake	mg N/L	L	0.05
phytoplankton half-saturation constant for phosphorus uptake	mg P/L	L	0.01
phytoplankton endogenous respiration rate constant @ 20°C	1/day	C	.075
phytoplankton respiration temperature coefficient	none	L	1.045
phytoplankton non-predatory mortality rate constant	1/day	L	0.2
phytoplankton phosphorus to carbon ratio	none	C	0.025
phytoplankton nitrogen to carbon ratio	none	L	0.25
phytoplankton maximum quantum yield	Langley/day	L	720
phytoplankton half-saturation for recycle of OrgN and OrgP	mg/L TOC	L	0.2
phytoplankton optimal light saturation	Langley/day	L	360
detritus and solids light extinction multiplier	1/m	C	0.2
fraction light intercepted by canopy	none	F	0 – 0.4
oxygen to carbon stoichiometric ratio	none	L	2.69
sediment oxygen demand	g/m ² -day	F	0.5 – 4.5
temperature correction for SOD	none	L	1.047

6. Existing Conditions and Water Quality Targets

Following calibration and validation of the modeling system, simulations were performed to evaluate the reach-specific status with respect to existing impairments of water quality criteria. These simulations were performed for the 11-year period January 1, 2002 through December 31, 2012. This long simulation period ensures that inter-annual and seasonal variability is addressed adequately. The simulations were performed using the existing HSPF NPS and, existing permit point source loads, and full permitted point source loads.

The NPS and MS4 loads simulated in HSPF were based on the 2006 NLCD land use and land cover, which provided a good basis of information for the calibration and validation, which was based predominately on data collected in 2004. Since the 2006 NLCD, the 2011 and 2016 NLCD have been developed and released. A comparison of land use and land cover from the 2006 and 2016 NLCD indicates that some land use changes are indicated to have occurred in the Adams and Cow Bayou watersheds (Table 6.1). Some of the greatest percent change has occurred for land cover categories with small acreages, e.g., barren and deciduous forest, and are largely inconsequential in the overall land cover characteristics of the watersheds. Further, the changes in certain land cover categories between the two NLDCs could be real, since there has been some small rate of population growth in the watersheds; however, some of the changes could be related to technology advances or interpretive decisions of the images used in the classification. An example of the latter is the aggregated developed land cover, which shows a small percent decrease from 2006 to 2016 in both the Adams and Cow Bayou watersheds. Such a decline seems most likely explained by changes in interpretive algorithms or imagery resolution than an actual physical decrease in developed area. Regardless, the decision was made to not go through the tedious task of updating the PERLND and IMPLND characteristics of each sub-basin within the Adams Bayou and Cow Bayou HSPF models to reflect the characteristics of the 2016 NLCD, because these changes were not considered substantial enough to warrant the resource commitment given the limited change in HSPF output expected from the land use and land cover changes.

Table 6-1 Comparison of the 2006 and 2016 NLCD land use and land cover in the Adams Bayou and Cow Bayou watersheds

NLCD Land Cover Category	Adams Bayou 2006 NLCD (acres)	Adams Bayou 2016 NLCD (acres)	Adams Bayou Percent Change 2006 to 2016 (%)	Cow Bayou 2006 NLCD (acres)	Cow Bayou 2016 NLCD (acres)	Cow Bayou Percent Change 2006 to 2016 (%)
Open Water	439	517	17.8%	1,005	1,241	23.5%
Developed, Open Space	3,560	3,264	-8.3%	10,278	8,575	-16.6%
Developed, Low Intensity	4,470	3,981	-10.9%	7,186	6,800	-5.4%
Developed, Medium Intensity	866	1,068	23.3%	1,514	1,853	22.4%
Developed, High Intensity	516	607	17.6%	878	966	10.0%
Barren Land	9	33	266.7%	64	80	25.0%
Deciduous Forest	148	10	-93.2%	102	222	117.6%
Evergreen Forest	1,234	1,216	-1.5%	15,785	18,816	19.2%
Mixed Forest	1,364	1,319	-3.3%	13,864	13,973	0.8%
Shrub/Scrub	816	700	-14.2%	8,153	7,189	-11.8%
Grassland/Herbaceous	1,403	478	-65.9%	8,204	4,059	-50.5%
Pasture Hay	6,574	7,861	19.6%	11,791	17,043	44.5%
Cultivated Crops	828	377	-54.5%	1,577	310	-80.3%
Woody Wetlands	5,951	6,495	9.1%	43,412	40,849	-5.9%
Emergent Herbaceous Wetlands	1,489	1,741	16.9%	3,397	5,234	54.1%
Aggregated Categories ¹						
Developed	9,412	8,920	-5.2%	19,856	18,194	-8.4%
Forest	2,746	2,545	-7.3%	29,751	33,011	11.0%
Agriculture	8,805	8,716	-1.0%	21,572	21,412	-0.7%
Wetlands	7,440	8,236	10.7%	46,809	46,083	-1.6%

¹ Developed = combined Open Space Developed, Low Intensity Developed, and High Intensity Developed
 Forest = combined Deciduous Forest, Evergreen Forest, and Mixed Forest
 Agriculture = combined Grassland/Herbaceous, Pasture Hay, and Cultivated Crops
 Wetlands = combined Woody Wetlands and Emergent Herbaceous Wetlands

6.1 Methodology for Calculating Pollutant Loads at AU Level

Because some HSPF sub-basins are spatially located in more than one AU in both the Adams Bayou and Cow Bayou models, the following methodology was used to map HSPF sub-basin-level loads into the proper AUs. Most sub-basins were located in a single AU, and for those sub-basins the entire loading for the HSPF sub-basin was added to that single AU. Some sub-basins, however, were geographically located in two or, in one instance, three AUs. The HSPF predicted loads of cBOD₅ and NH₃N were proportioned to the AUs using the percent of the sub-basin area in each AU. The percentages used to separate HSPF sub-basin-level pollutant loads into AUs of the Adams Bayou and Cow Bayou watersheds are provided in Table 6-2.

Table 6-2 Percentages used to separate HSPF sub-basin-level pollutant loads into AUs

HSPF Sub-basin	Percent Contribution of Sub-basin to AU	AU
Adams 1	100.0%	0508B_01
Adams 2	100.0%	0508A_01
Adams 3	100.0%	0508B_01
Adams 4	100.0%	0508A_01
Adams 5	69.6%	0508_04
	30.4%	0508A_01
Adams 6	100.0%	0508A_01
Adams 7	100.0%	0508_04
Adams 8	100.0%	0508C_01
Adams 9	100.00%	0508_01
Adams 10	18.3%	0508_01
	29.4%	0508_02
	52.3%	0508_03
Adams 11	100.0%	0508_01
Adams 12	100.0%	0508_01
Cow 1	100.0%	0511A_02
Cow 2	100.0%	0511A_02
Cow 3	100.0%	0511A_02
Cow 4	36.9%	0511A_01
	63.1%	0511A_02
Cow 5	100.0%	0511E_01
Cow 6	100.0%	0511E_01
Cow 7	100.0%	0511C_01
Cow 8	88.4%	0511_04
	11.6%	0511A_01
Cow 9	68.8%	0511_03
	30.2%	0511_04
Cow 10	100.0%	0511C_01
Cow 11	100.0%	0511_02
Cow 12	7.9%	0511_02
	92.1%	0511_03

HSPF Sub-basin	Percent Contribution of Sub-basin to AU	AU
Cow 13	100.0%	0511E_01
Cow 14	100.0%	0511_02
Cow 15	100.0%	0511B_01
Cow 16	38.3%	0511_01
	61.7%	0511_02
Cow 17	71.5%	0511_01
	28.5%	0511D_01
Cow 18	100.0%	0511_01

6.2 Water Quality Targets

The tidal AUs have a “high” aquatic life use, and the water quality criteria require that daily average DO at any site be at least 4 mg/L, with a daily minimum of at least 3 mg/L (Table 6-3). In order for water quality standards to be judged as fully supported, no more than 10 percent of daily average DO measurements can fall below this 4 mg/L daily-average criterion.

The above tidal reaches in these systems are considered intermittent water bodies with perennial pools. A “limited” aquatic life use is assumed for these water bodies, with a daily average criterion of 3 mg/L DO and a daily minimum criterion of 2 mg/L DO. In order for water quality standards to be judged as fully supported, no more than 10 percent of daily average DO measurements can fall below 3 mg/L daily-average DO.

The daily average DO criteria for aquatic life served as the instream target for calculating the necessary pollutant load reductions required by TMDLs for the tidal AUs. The daily minimum DO criterion was not evaluated, because the model was not set up or calibrated to predict diurnal fluctuations in DO, but was calibrated to simulate daily average DO.

The WASP model daily average DO results were used to assess tidal stream AUs by averaging the daily average DO results of all the segment used to represent each AU (Table 6-3). The HSPF model daily average DO results were used to assess above tidal stream AUs in a similar manner. A complicating factor is that the tidal/nontidal boundary in water bodies of the Adams Bayou and Cow Bayou systems is variable and not precisely determined. Some upstream portions of the WASP model segments are considered to be located in above tidal AUs based on water quality AU definitions in the Texas Surface Water Quality Standards; whereas the upstream segmentation of the RMA2 and WASP models, which were defined by field measurements of tidal influence observed during the intensive surveys used in model verification, included the downstream reaches of some above tidal AUs. Adams Bayou Above Tidal (AU 0508A_01), Gum Gully (AU 0508B_01), and Terry Gully (AU 0511E_01) are the above tidal water bodies that field

measurements indicated have tidal influences in their more downstream reaches, and these three AUs were, therefore, assessed using both WASP and HSPF DO results. For these three AUs, the assessment process used the daily average DO predictions from WASP and HSPF and the fraction of the length of the AU represented in WASP, with the remaining fraction of the AU assumed to be represented in HSPF. For each day of the 11-year simulated period, a daily average DO was computed for each of these AUs based on multiplying WASP derived daily average DO by the fraction of the AU length represented in WASP and adding to that value the HSPF derived daily average DO multiplied by the fraction of the AU length represented in HSPF.

Furthermore, in the WASP model, the most upstream segment in each tributary was not included in the assessment of compliance because they are heavily influenced by model boundary conditions and do not respond appropriately to changes in loading. It should be noted that extra segments were added to the upstream ends of tributaries during model development to provide a buffer to minimize the boundary effects on scenario evaluation.

Individual AUs were evaluated for compliance with the DO criteria specified in Table 6-3. In order for water quality standards to be judged as fully supported, no more than 10 percent of the model-predicted daily average DO measurements averaged across all model elements within each AU, over the period January 1, 2002 to December 31, 2012, can fall below the DO criterion specified in Table 6-3.

Table 6-3 DO criteria and modeling system connections for DO assessment

Waterbody Name	AU	Aquatic Life Use	Type	Model Element or Reach	Model	AVG/MIN DO criteria (mg/L)
Adams Bayou Tidal	0508_01	High	Tidal stream	2-27	WASP	4/3
	0508_02	High	Tidal stream	28-34	WASP	4/3
	0508_03	High	Tidal stream	35-48	WASP	4/3
	0508_04	High	Tidal stream	49-68	WASP	4/3
Adams Bayou Above Tidal	0508A_01	Limited	Intermittent with pools	2	HSPF	3/2
				69-87	WASP	3/2
Gum Gully	0508B_01	Limited	Intermittent with pools	1	HSPF	3/2
				113-117	WASP	3/2
Hudson Gully	0508C_01	High	Tidal stream	109-111	WASP	4/3
Cow Bayou Tidal	0511_01	High	Tidal stream	2-19	WASP	4/3
	0511_02	High	Tidal stream	20-41	WASP	4/3
	0511_03	High	Tidal stream	42-58	WASP	4/3
	0511_04	High	Tidal stream	59-67	WASP	4/3
Cow Bayou Above Tidal	0511A_01	Limited	Intermittent with pools	4	HSPF	3/2
	0511A_02	Limited	Intermittent with pools	1,3	HSPF	3/2
Coon Bayou	0511B_01	High	Tidal stream	97-107	WASP	4/3
Cole Creek	0511C_01	High	Tidal stream	115-123	WASP	4/3
Unnamed Trib to Cow Bayou Tidal	0511D_01	High	Tidal stream	85-87	WASP	4/3
Terry Gully	0511E_01	Limited	Intermittent with pools	6,13	HSPF	3/2
				125-135	WASP	3/2

6.3 Full Permitted Pollutant Loads

Existing pollutant loads were calculated as the average of the daily NPS loads for the entire simulation period (January 1, 2002 to December 31, 2012) and the current full permitted TPDES loads for point source discharges. Note that in addition to cBOD and NH₃N, OrgN also influences DO upon decay, but there are no permit limits or monitoring requirements for OrgN in TPDES permitted PS discharges for the Adams Bayou and Cow Bayou watersheds. For permitted municipal discharges without NH₃N permit limits, a concentration of 12 mg/L was assumed, which is what TCEQ uses in permit evaluations. For industrial facilities without NH₃N limits, a limit of 1.0 mg/L was used if historical discharge monitoring report data indicated reported concentrations not exceeding that limit. The exceptions on the industrial permits was Chevron Phillips Chemical Company, where the discharge monitoring report data supported a limit of 0.8 mg/L, and Printpak, Inc., where the data for this facility indicated higher concentrations resulting in a limit for NH₃N of 3 mg/L.

In the absence of permit limits, the following assumed values for OrgN concentrations were applied in wastewater discharges, based on best professional judgement and through consultation with TCEQ:

Domestic Facilities

If BOD ₅ /cBOD ₅ <7 and NH ₃ N < 7	OrgN = 1 mg/L
If BOD ₅ /cBOD ₅ <11 and NH ₃ N < 7	OrgN = 2 mg/L
If BOD ₅ /cBOD ₅ <11 or NH ₃ N < 7	OrgN = 3 mg/L
Otherwise	OrgN = 4 mg/L

Industrial Facilities

If measured/reported in permit application	Use average reported
Otherwise	OrgN = 0.1 mg/L

The City of Orange (TPDES Permit 10626-001) typically discharges through outfall 001 to the Sabine River. The permit allows the city to discharge through outfall 002 to Adams Bayou only if, as a result of wet weather conditions, the average discharge from the facility exceeds 11,111 gallons per minute. The City of Orange is required by their permit to provide, in their monthly discharge monitoring report, the maximum daily and average daily discharge through outfall 002. These discharge monitoring report data were used to define that dates of discharge within the 11-year simulation period. Since the available data on the discharge through outfall 002 did not provide an exact day within the month for the discharge nor the number of days of discharge, these two assumptions were made in order to define the discharge for the modeling system: (1) the discharge for any month was assigned to begin the day of maximum daily precipitation within that month based on the precipitation input record to the modeling system,(2) whenever the

reported daily maximum and daily average discharge were different values, then the discharge was assumed to occur over two successive days at the average flow. For most months in the simulation period of 2002 – 2012, the daily maximum and daily average discharge was reported as the same values, which, while not definitive, is a strong indication of only one day of discharge. There were 23 months with reported discharge over the 132 month simulated period, and in 15 of those months the reported daily maximum and average were the same value.

Table 6-4 summarizes the currently active TPDES permitted PS discharges and currently proposed Bayou Pines TPDES permitted PS discharges for selected parameters related to the DO impairments. The TPDES point source load information for municipal and industrial facilities in Table 6-4 were used as input to the modeling system. The TPDES point source loads represent the daily average full permitted loads for NH_3N and cBOD_5 .

Tables 6-5 and 6-6 summarize the full permitted loads for NH_3N and cBOD_5 , the key pollutants most closely related to DO impairments, in Adams Bayou and Cow Bayou, respectively. Loads are summarized at the individual AU level based on HSPF sub-basin output using the methodology presented in Section 6.1 and the percentage of the area of individual AUs within the HSPF subbasins. These total runoff loads are separated into unregulated and regulated stormwater components according to on the percent of each AU that is regulated stormwater area. Note that details on the estimation of the regulated area are provided in the bacteria technical support document for the Adams Bayou and Cow Bayou watershed (Hauck and Adams, 2020 [Section 2.6.1 - Regulated Sources]). The daily simulated HSPF sub-basin loads for NH_3N and cBOD_5 for the 11-year period are averaged to give a daily average load prior to being proportioned into the respective AUs.

Table 6-4 Existing full-permitted TPDES daily average PS loads to Adams and Cow Bayous

Permit	Outfall	Assessment Unit	WASP Segment	RMA2 Element	HSPF Sub-Basin	Flow MGD	BOD ₅ /cBOD ₅ mg/L (lb/day)	NH ₃ N mg/L (lb/day)	DO ¹ mg/L (lb/day)
Adams Bayou									
WQ0010597-001 City of Pinehurst	001	0508_03	48	BQE 36	NA	0.5	20 (83)	12 ² (50.1)	3.0 (12.5)
WQ0010240-001 Orange County WCID 2	001	0508_02	31	BQE 28	NA	1.22 ³	10 (102)	12 ² (153.7)	4.0 (40.7)
WQ0010626-001 City of Orange	002	0508_02	31	BQE 28	NA	7.0 ⁴	20 (1,168)	12 ² (701)	2.0 (116.8)
Cow Bayou									
WQ0001167-000 ARLANXEO USA LLC	001	0511_01	5	BQE 19	NA	6.0	3.5 (176)	1 ¹⁰ (50.1)	2.0 ² (100.1)
WQ0000670-000 Honeywell International Inc.	001	0511_01	79	BQE 14	NA	1.4	10 (117)	1 ¹⁰ (11.7)	2.0 ² (23.3)
WQ0000454-000 Lion Elastomers Orange, LLC	001 002 ⁵	0511_01	10	BQE 21	NA	1.202 -	11 (110) -	2 (20) -	2.0 ² (20) -
WQ0000359-000 Chevron Phillips Chemical Company LP	001	0511D_01	88	BQE 83	NA	3.15	17.5 (460)	0.8 ¹⁰ (21.0)	2.0 ² (20.0)
WQ0002858-000 Printpack, Inc.	001 101 ⁶	0511D_01	88	BQE 83	NA	0.085 -	10 ⁸ (7.1) -	3 ¹⁰ (2.1) -	2.0 ² (1.4) -
WQ0010051-001 City of Bridge City	001	0511_01	17	BQE 38	NA	1.6 ³	10 (133)	12 ² (160)	4.0 (53.4)
WQ0014772-001 Orangefield Water Supply Corporation	001	0511_02	29	BQE 44	NA	0.75	10 (63)	2 (13)	4.0 (25)
WQ0015029-001 (proposed) Bayou Pines	001	0511B_01	107	BQE 36	NA	0.009	30 (2.3)	8 (0.6)	4.0 (0.3)

Permit	Outfall	Assessment Unit	WASP Segment	RMA2 Element	HSPF Sub-Basin	Flow MGD	BOD ₅ /cBOD ₅ mg/L (lb/day)	NH ₃ N mg/L (lb/day)	DO ¹ mg/L (lb/day)
WQ0013488-001 Gulflander Partners Group, L.P.	001	0511B_01	101	BQE 33	NA	0.01	20 (1.7)	12 ² (1.0)	2.0 (0.17)
WQ0011916-001 P C S Development Company	001	0511_04	67	BQE 79	NA	0.09	20 (15)	12 ² (9)	2.0 (1.5)
WQ0002835-000 Miller Waste Mills, Inc.	001 ⁵ 002 003 ⁷	0511_02	NA	NA	11	– 0.116 ¹¹ –	– 20⁹ (16.9) –	– 1 ⁸ (1.0) –	– 2.0 ² (1.9) –
WQ0010808-001 Jasper County WCID 1	001	0511A_02	NA	NA	1	0.41	30 (103)	6 (21)	4.0 (13.7)

Table Notes:

NA = not applicable

Bold values represent quantities specified as limits in the permit.

¹ Permit limits for DO are applied as a minimum, rather than a daily average.

² Default value based on TCEQ guidance and values assumed in TCEQ permit evaluations.

³ Annual average flow in MGD.

⁴ Intermittent discharge. The permittee is authorized to discharge from Outfall 002 only if, as a result of wet weather conditions, the average discharge from the facility exceeds 11,111 gallons per minute. Combined average annual discharge of Outfalls 001 and 002 is not to exceed 7.0 MGD. Simulated as 7.0 MGD on all days of discharge indicated in the discharge monitoring report data for the period of January 1, 2002 – December 31, 2012. Outfall 001 discharges to the Sabine River.

⁵ Stormwater only outfall; not included as direct point source in modeling system; included through land use in HSPF model.

⁶ Internal outfall that is included in Outfall 001.

⁷ Based on discharge monitoring report data, discharges from Outfall 003 have never been reported; outfall not included in modeling effort.

⁸ Estimate based on permit renewal information.

⁹ Permit has a daily maximum limit of 26 mg/L; daily average BOD₅ based on ratio of permit limits for daily average and daily maximum total organic carbon and the daily maximum BOD₅ limit.

¹⁰ Value determined based on evaluation of discharge monitoring report data.

¹¹ Average of 2017 – 2018 discharge monitoring report data.

Table 6-5 Summary of daily average NH₃N and cBOD loads under full permitted conditons to the Adams Bayou system

Load units expressed in lbs/day; total runoff load = unregulated stormwater load + regulated stormwater load

AU	Total Runoff Load			Unregulated Stormwater Load		TPDES Point Source Load		Regulated Stormwater Load		Total Load	
	cBOD ₅	NH ₃ N	Regulated Stormwater Area (%)	cBOD ₅	NH ₃ N	cBOD ₅	NH ₃ N	cBOD ₅	NH ₃ N	cBOD ₅	NH ₃ N
0508_01	268.70	21.89	59.87	107.83	8.78	0.00	0.00	160.87	13.11	268.70	21.89
0508_02	49.19	4.15	99.85	0.07	0.01	1,270.11 ¹	823.15 ¹	49.12	4.14	1,319.30	827.30
0508_03	79.02	6.66	100.00	0.00	0.00	83.45	50.07	79.02	6.66	162.47	56.73
0508_04	325.14	26.97	76.46	76.54	6.35	0.00	0.00	248.60	20.62	325.14	26.97
0508A_01	586.33	43.50	4.21	561.65	41.67	0.00	0.00	24.68	1.83	586.33	19.73
0508B_01	100.29	7.30	2.33	97.95	7.13	0.00	0.00	2.34	0.17	100.29	7.30
0508C_01	105.47	8.71	99.32	0.72	0.06	0.00	0.00	104.75	8.65	105.47	8.71
System Total	1,514.14	119.18	NA ²	844.76	64.00	1,353.56	873.22	669.38	55.18	2,867.70	968.63

¹ Includes the loads from intermittent discharge from the City of Orange WWTF based on a flow of 7.0 MGD, though that flow only occurs infrequently during the 2001 – 2012 simulated period.

² N/A – not applicable. Adams Bayou watersheds is represented by multiple sub-basins in HSPF with each sub-basin containing a unique composition of land uses that result in differing runoff loads of CBOD₅ and NH₃N by area. Also, the loads from each sub-basin are proportioned unregulated and regulated stormwater components for individual AUs based on the percent of the sub-basin in each AU and the regulated stormwater area percent of each AU. The differing land uses comprising HSPF sub-basins and subsequent differing runoff loads by area result in spatial variability that does not allow a unique watershed-wide percent of regulated stormwater to be computed that is correct for both CBOD₅ and NH₃N runoff loads.

Table 6-6 Summary of daily average NH₃N and cBOD loads under full permitted condition to the Cow Bayou system

Load units expressed in lbs/day; total runoff load = unregulated stormwater load + regulated stormwater load

Sub-basin, TPDES permit, or AU	Total Runoff Load			Unregulated Stormwater Load		TPDES Point Source Load		Regulated Stormwater Load		Total Load	
	cBOD ₅	NH ₃ N	Regulated Stormwater Area (%)	cBOD ₅	NH ₃ N	cBOD ₅	NH ₃ N	cBOD ₅	NH ₃ N	cBOD ₅	NH ₃ N
0511_01	222.25	17.68	29.30	157.13	12.50	535.61	241.90	65.12	5.18	757.86	259.58
0511_02	362.92	28.31	9.02	330.18	25.76	81.90	13.48	32.74	2.55	444.82	41.79
0511_03	132.53	9.20	2.23	129.57	8.99	0.00	0.00	2.96	0.21	132.53	9.20
0511_04	67.46	4.54	5.61	63.68	4.29	15.01	9.01	3.78	0.25	82.47	13.55
0511A_01	613.96	40.58	1.17	606.78	40.11	0.00	0.00	7.18	0.47	613.96	40.58
0511A_02	1,059.52	69.64	0.34	1,055.92	69.40	102.58	20.52	3.60	0.24	1,162.10	90.16
0511B_01	140.19	11.11	27.87	101.12	8.01	3.92	1.60	39.07	3.10	144.11	12.71
0511C_01	297.45	20.15	1.63	292.60	19.82	0.00	0.00	4.85	0.33	297.45	20.15
0511D_01	43.61	3.76	60.52	17.22	1.48	466.83	23.15	26.39	2.28	510.44	26.91
0511E_01	657.15	45.06	18.40	536.23	36.77	0.00	0.00	120.92	8.29	657.15	45.06
System Total	3,597.04	250.03	NA ¹	3,290.43	227.13	1,205.85	309.66	306.61	22.90	4,802.89	559.69

¹ N/A – not applicable. Cow Bayou watersheds is represented by multiple sub-basins in HSPF with each sub-basin containing a unique composition of land uses that result in differing runoff loads of CBOD₅ and NH₃N by area. Also, the loads from each sub-basin are proportioned unregulated and regulated stormwater components for individual AUs based on the percent of the sub-basin in each AU and the regulated stormwater area percent of each AU. The differing land uses comprising HSPF sub-basins and subsequent differing runoff loads by area result in spatial variability that does not allow a unique watershed-wide percent of regulated stormwater to be computed that is correct for both CBOD₅ and NH₃N runoff loads.

6.4 Assessment of Compliance with Water Quality Standards under Existing Conditions and Full Permitted Conditions

Modeling system simulations of existing conditions (i.e., existing HSPF NPS and MS4 pollutant loads and existing permitted point source pollutant loads) and TPDES full permitted conditions were performed. For the existing condition scenario, the TPDES domestic and industrial WWTF discharge inputs to the modeling system were based on discharge monitoring report data and data collected during the intensive surveys used for model verification. The full permitted condition scenario was performed using the same input as the existing conditions scenarios, except the TPDES domestic and industrial WWTF discharge input were based on the information in Table 6-4. Modeling system results were post-processed to determine daily average DO concentrations for each WASP segment and each HSPF sub-basin comprising either the Adams Bayou watershed modeling system or the Cow Bayou watershed modeling system.

Statistics were calculated for each AU using the daily average DO data to quantify the:

- number of days with DO concentration less than appropriate daily average criterion for each AU during the entire simulation period;
- the 10th percentile DO concentrations during the entire simulation period; and
- average DO concentrations during the entire simulation period.

Results from both the existing conditions and full permitted conditions scenario predicted that none of the Adams Bayou system water bodies on the CWA Section 303(d) List were expected to be in compliance with water quality standards for DO for the 11-year period simulated (Table 6-7). Compliance with the water quality standards occurs when 10 percent or less of the simulated days experience depressed average DO concentrations when evaluated at the AU level. The WASP model prediction that all AUs within the Adams Bayou watershed experience depressed DO is agreement with the TCEQ assessed conditions that all the Adams Bayou watershed AUs are impaired.

In the Cow Bayou system, the DO results for the existing conditions and full permitted conditions scenario are provided in Table 6-8. The modeling system predictions of depressed DO are in agreement with the TCEQ assessment of AUs impaired because of depressed DO. Further, for AUs not considered by TCEQ as impaired, the simulated results were in agreement under the existing conditions scenario with AUs 0511_01, 0511A_01, 0511D_01, and 0511E_01 indicated to have depressed DO occurring less than 10 percent of the time. AU 0511D_01, the Unnamed Tributary to Cow Bayou Tidal was simulated as having depressed DO above 10 percent (at 27 percent) under the full permitted condition scenario. As a qualifier, it should be noted that some of the AUs assessed as unimpaired by TCEQ did not have sufficient data for proper assessment.

Table 6-7 Simulated compliance with criteria under existing conditions and full permit conditions for the Adams Bayou system

Values under Days Not Meeting Average DO Criterion that exceed 10% are shown in bold red font.

Waterbody Name	AU	Model Element or Reach	Model	24-hour Average DO criterion (mg/L)	Existing Permit Load Scenario			Full Permitted Load Scenario		
					Average DO (mg/L)	10 th Percentile DO (mg/L)	Days Not Meeting Average DO Criterion (%)	Average DO (mg/L)	10 th Percentile DO (mg/L)	Days Not Meeting Average DO Criterion (%)
Adams Bayou Tidal	0508_01	2-27	WASP	4	3.0	1.2	71	2.5	0.9	85
	0508_02	28-34	WASP	4	1.7	0.1	91	1.0	0.1	97
	0508_03	35-48	WASP	4	1.5	0.1	91	1.0	0.1	95
	0508_04	49-68	WASP	4	1.4	0.0	89	1.2	0.0	90
Adams Bayou Above Tidal	0508A_01	Combined WASP & HSPF		3	2.8	0.4	57	2.6	0.2	59
Gum Gully	0508B_01	Combined WASP & HSPF		3	4.2	1.5	24	2.9	0.2	50
Hudson Gully	0508C_01	109-111	WASP	4	1.8	0.2	88	1.5	0.1	90

Table 6-8 Simulated compliance with criteria under existing conditions and full permit conditions for the Cow Bayou system

Values under Days Not Meeting Average DO Criterion that exceed 10% are shown in bold red font.

Waterbody Name	AU	Model Element or Reach	Model	24-hour Average DO criterion (mg/L)	Existing Permit Load Scenario			Full Permitted Load Scenario		
					Average DO (mg/L)	10 th Percentile DO (mg/L)	Days Not Meeting Average DO Criterion (%)	Average DO (mg/L)	10 th Percentile DO (mg/L)	Days Not Meeting Average DO Criterion (%)
Cow Bayou Tidal	0511_01	2-19	WASP	4	5.9	4.4	1	5.7	4.2	5
	0511_02	20-41	WASP	4	5.2	3.1	27	5.0	2.9	32
	0511_03	42-58	WASP	4	4.9	1.1	40	4.7	1.0	42
	0511_04	59-67	WASP	4	5.3	0.9	37	5.0	0.7	41
Cow Bayou Above Tidal	0511A_01	4	HSPF	3	8.2	6.1	0	8.0	5.9	0
	0511A_02	1,3	HSPF	3	5.2	0.0	26	6.1	1.5	16
Coon Bayou	0511B_01	97-107	WASP	4	5.3	3.0	25	5.1	2.8	29
Cole Creek	0511C_01	115-123	WASP	4	5.8	1.8	30	5.7	1.7	32
Unnamed Trib to Cow Bayou Tidal	0511D_01	85-87	WASP	4	7.7	5.2	0	6.1	3.2	27
Terry Gully	0511E_01	Combined HSPF & WASP		3	6.5	4.5	3	6.4	4.4	3

7. DO and pH TMDL Allocations

A series of water quality loading scenarios were simulated using the calibrated modeling system to identify their impact on compliance with water quality standards for DO. The pH impairment and load reductions requirements associated with that impairment are addressed separately from the DO impairment and are provided at the end of this section.

7.1 DO Modeling Scenarios

It was assumed that reductions in loads of cBOD and OrgN would ultimately result in reductions in SOD, because SOD is derived from oxidation of settled organic matter. Similarly, reductions in the fluxes of NH₃N from sediments to the water column were assumed to result from reductions in external loading of organic matter. Modeling scenarios involving changes in loading were a two-step process. In the first step, the models were run with external load modifications of cBOD and NH₃N. In the second step, the SOD and internal fluxes of NH₃N and PO₄P from sediments to the water column were modified by a percentage equal to the percent change in the dissolved cBOD concentration in the water column. However, SOD was not reduced below a minimum level of 0.35 g/m²/day. This 0.35 g/m²/day is an estimate of background SOD, based on a memorandum of understanding between EPA and TCEQ on water quality permitting (TCEQ, 2010).

7.1.1 No Load Scenario

This scenario involved setting all PS and NPS loads to zero. Under this loading scenario, all AUs were in compliance with water quality standards except Cow Bayou Above Tidal AU 0511A_02 (Table 7-1). An evaluation of the HSPF daily average DO results for AU 0511A_02 indicated that when simulated streamflows became low, the DO in this AU was often below the 24-hour average criterion resulting in noncompliance with water quality standards. This scenario explores the physical factors constraining dissolved oxygen dynamics in the Adams Bayou and Cow Bayou stream systems. It does not represent a realistic condition, but is useful for reference purposes.

7.1.2 Pristine Condition Scenario

This scenario involved setting all PS loads to zero and setting all land uses in HSPF to a perceived “natural” condition. For this scenario, all developed land classes, cropland, pasture/hay, and septic fields were converted to the grassland/herbaceous land use category in sub-basins occurring primarily below I-10, and to mixed forest for sub-basins occurring primarily north of IH-10. Thus, there were no anthropogenic pollutant loads, but there were natural non-point source loads corresponding to a likely pre-settlement and pre-development condition. Results of pristine condition modeling scenario are presented in Table 7-2.

Table 7-1 Results of No Load Scenario

Values under Days Not Meeting Average DO Criterion that exceed 10% are shown in bold red font.

Waterbody Name	AU	Model Sub-basin or Reach	Model	24-hour Average DO criterion (mg/L)	Average DO (mg/L)	10 th Percentile DO (mg/L)	Days Not Meeting Average DO Criterion (%)
Adams Bayou Tidal	0508_01	2-27	WASP	4	7.0	5.2	0
	0508_02	28-34	WASP	4	8.1	6.5	0
	0508_03	35-48	WASP	4	8.5	7.0	0
	0508_04	49-68	WASP	4	8.9	7.4	0
Adams Bayou Above Tidal	0508A_01	Combined HSPF & WASP		3	7.5	6.2	0
Gum Gully	0508B_01	Combined HSPF & WASP		3	7.3	6.2	2
Hudson Gully	0508C_01	109-111	WASP	4	7.6	6.2	0
Cow Bayou Tidal	0511_01	2-19	WASP	4	7.0	5.2	0
	0511_02	20-41	WASP	4	7.8	6.0	0
	0511_03	42-58	WASP	4	8.8	7.2	0
	0511_04	59-67	WASP	4	8.9	7.3	0
Cow Bayou Above Tidal	0511A_01	4	HSPF	3	8.5	6.8	0
	0511A_02	1,3	HSPF	3	6.5	0.1	18
Coon Bayou	0511B_01	97-107	WASP	4	7.6	6.1	0
Cole Creek	0511C_01	115-123	WASP	4	7.6	5.1	3
Unnamed Trib to Cow Bayou Tidal	0511D_01	85-87	WASP	4	8.2	5.5	0
Terry Gully	0511E_01	Combined HSPF & WASP		3	8.1	7.1	3

Under these pristine conditions, the WASP model results show Adams Bayou Above Tidal (0508A_01), Gum Gully (0508B_01), Cow Bayou Above Tidal (0511A_02), and Terry Gully (0511E_01) are not in compliance with water quality standards. Based partly on these model results and partly on the lack of data and information available, the TCEQ decided that, for AUs 0508A_01 and 0508B_02 located in above tidal portions of the Adams Bayou watershed, additional data and analysis should be conducted, including an aquatic life use attainability

analysis, prior to proceeding with a TMDL. Therefore, no further modeling of load reductions were performed except to the extent that they were necessary to achieve water quality standards in downstream AUs. For the upstream AU of Cow Bayou Above Tidal, 0511A_02, similar to the no load scenario, simulated low DO occurred during simulated low flow conditions. Terry Gully (0511E_01) was not assessed by TCEQ as impaired due to depressed DO and was not indicated in the existing permit load and full permit load scenarios as experiencing depressed DO (Table 6-8). The noncompliance for Terry Gully under the pristine conditions scenario is also indicated to be a result of the simulated low DO occurring under low flow conditions.

Table 7-2 Results of Pristine Condition Scenario

Values under Days Not Meeting Average DO Criterion that exceed 10% are shown in bold red font.

Waterbody Name	AU	Model Sub-basin or Reach	Model	24-hour Average DO criterion (mg/L)	Average DO (mg/L)	10 th Percentile DO (mg/L)	Days Not Meeting Average DO Criterion (%)
Adams Bayou Tidal	0508_01	2-27	WASP	4	5.8	4.3	3
	0508_02	28-34	WASP	4	6.5	5.2	0
	0508_03	35-48	WASP	4	6.8	5.5	0
	0508_04	49-68	WASP	4	7.0	5.7	1
Adams Bayou Above Tidal	0508A_01	Combined HSPF & WASP		3	5.8	2.4	19
Gum Gully	0508B_01	Combined HSPF & WASP		3	5.3	0.7	21
Hudson Gully	0508C_01	109-111	WASP	4	6.0	3.2	8
Cow Bayou Tidal	0511_01	2-19	WASP	4	6.6	5.3	0
	0511_02	20-41	WASP	4	6.5	5.0	2
	0511_03	42-58	WASP	4	7.3	5.2	2
	0511_04	59-67	WASP	4	7.9	5.9	1
Cow Bayou Above Tidal	0511A_01	4	HSPF	3	8.3	6.2	0
	0511A_02	1,3	HSPF	3	5.3	0.0	34
Coon Bayou	0511B_01	97-107	WASP	4	6.9	5.5	1
Cole Creek	0511C_01	115-123	WASP	4	7.6	5.4	2
Unnamed Trib to Cow Bayou Tidal	0511D_01	85-87	WASP	4	7.0	5.6	0
Terry Gully	0511E_01	Combined HSPF & WASP		3	7.2	2.7	10.4

7.1.3 TMDL Scenarios

A series of scenarios were performed to quantify the assimilative capacity of individual AUs while simultaneously demonstrating compliance for the AUs of the Adams Bayou and Cow Bayou systems. The starting point for these scenarios was the full permit condition represented by the full permit scenario daily average loads from 2002 through 2012 for all nonpoint and MS4 sources (Tables 6-5 and 6-6) and “full permitted” conditions for all TPDES-permitted facilities, as summarized in Table 6-4. Fully permitted loads represent discharge permit limits for NH₃N and cBOD₅ (or BOD₅ where permits are written for that parameter). Loads of cBOD₅ and NH₃N to each AU were then progressively reduced in the manner shown in Table 7-3, focusing on “hot spots” of low DO, in an iterative fashion until the given AU reached attainment of the DO standard. Minor modifications were then performed to locally optimize the quantification of allowable loading.

Table 7-3 Load Reduction Progression

NPS* Reduction in NH ₃ N and CBOD ₅	Industrial PS Reduction NH ₃ N and BOD ₅ /CBOD ₅	Domestic PS Concentration	
		NH ₃ N(mg/L)	cBOD ₅ (mg/L)
0% Reduction	0% Reduction	12	20
20% Reduction	20% Reduction	12	10
40% Reduction	40% Reduction	3	10
60% Reduction	60% Reduction	2	10
70% Reduction	70% Reduction	2	7
80% Reduction	80% Reduction	2	7
90% Reduction	90% Reduction	2	5
95% Reduction	95% Reduction	1	5
100% Reduction	100% Reduction	No Discharge	No Discharge

* The term NPS is used here to represent pollutants from regulated and unregulated sources in rainfall runoff.

Additional explanations of the approach taken to reduce CBOD₅ and NH₃N loads in the scenario simulations of impaired AUs include the following:

- The reduction in industrial PS loadings was set equal to the reduction in NPS loadings; for these cases, cBOD₅ (or BOD₅) and NH₃N were reduced by the same percentage.
- The reductions in domestic PS loadings was performed according to the discrete effluent concentration hierarchy shown in Table 7-3.
- Domestic WWTF loadings were not relaxed from limits in existing permits. The input loads for the WWTFs were specified as the more stringent of (1) existing permit limits (or, in the absence of permit limits, values used to represent permit limits) or (2) the limits specified in Table 7.3.

- For domestic WWTF loadings, the level of required treatment did not increase until the next percent reduction level was reached in Table 7-3. For example, at runoff (NPS) and industrial WWTF reductions from 40 to 59 percent, the municipal permit limits are NH₃N equal to 3 mg/L and CBOD₅ equal to 10 mg/L and, for reductions between 60 and 69 percent, the limits are NH₃N equal to 2 mg/L and CBOD₅ equal to 10 mg/L;
- The minimum DO concentration specified in permits for industrial or domestic PS was assumed to be increased to 5 mg/L in all AUs for which load reductions were required;
- OrgN was not directly reduced in equal proportion to cBOD₅ and NH₃N, because it is not subject to effluent limitations in water quality permits, but was instead adjusted in accordance with the assumptions listed in Section 6.2.

The runoff (NPS) from HSPF and industrial WWTF outfalls permitted for combined stormwater and industrial process wastewater results in a duplicate representation of the stormwater component of these industrial TPDES permitted outfalls (Table 6-4) in the modeling system. Industrial outfalls that are only permitted for stormwater are represented in HSPF. Industrial outfalls that include stormwater and process wastewater are included in HSPF and specified as WWTF inputs into the modeling system. The inability to separate the flows from these industrial outfalls into distinct stormwater and process wastewater components makes this duplication unavoidable. The amount of land area actually contributing through these combined outfalls is estimated to be less than one percent of the 127,210 acres comprising the Cow Bayou watershed. There are no TPDES permitted industrial facilities in the Adams Bayou watershed. Further, the majority of the industrial facilities in the Cow Bayou watershed discharge into unimpaired AUs in the lower portion of Cow Bayou Tidal, where historical data indicate no DO impairments and where the modeling system scenarios give similar results of no DO impairments. Therefore, the duplication is not significantly impacting results and represents a conservative feature of the modeling effort.

The TMDL scenario for the Adams Bayou system involved:

- Unregulated NPS and regulated stormwater load reductions of 45 percent for Adams Bayou Tidal AU 0508_01.
- Unregulated NPS and regulated stormwater load reductions of 40 percent for Adams Bayou Tidal AUs 0508_02 and 0508_03.
- Unregulated NPS and regulated stormwater load reductions of 60 percent for Adams Bayou Tidal AU 0508_04.
- Unregulated NPS and regulated stormwater load reductions of 80 percent for Hudson Gully AU 0508C_01.
- All TPDES municipal WWTFs with daily average effluent limits at 10 mg/L CBOD₅ and 3 mg/L NH₃N, and minimum DO at 5 mg/L based on the 40 percent runoff reduction required in AUs 0508_02 and 0508_03.
- No assimilative capacity afforded for future growth.

The TMDL scenario for the Cow Bayou system involved:

- Unregulated NPS and regulated stormwater load reductions of 0 percent for Cow Bayou Tidal AU 0511_02.
- Unregulated NPS and regulated stormwater load reductions of 50 percent for Cow Bayou Tidal AU 0511_03.
- Unregulated NPS and regulated stormwater load reductions of 60 percent for Cow Bayou Tidal AU 0511_04.
- Unregulated NPS and regulated stormwater load reductions of 50 percent for Cow Bayou Above Tidal AU 0511A_02.
- Unregulated NPS and regulated stormwater load reductions of 50 percent for Coon Bayou AU 0511B_01.
- Unregulated NPS and regulated stormwater load reductions of 50 percent for Cole Creek AU 0511C_01.
- Each TPDES municipal or industrial WWTFs effluent limit was based on the runoff percent reductions computed for the AU in which the facility is located. (The AU location of each facility is in Table 6-4.) The exception was for the two industrial facilities located in 0511D_01 for which the simulation indicated that if the assumed DO in the effluent was 5 mg/L, instead of the 2 mg/L assumed in TCEQ modeling, then depressed DO was avoided in this water body. Therefore, for the two industrial facilities in 0511D_01, an effluent minimum DO of 5 mg/L was assigned to their permits for modeling purposes. CBOD₅ and NH₃N effluent limits assigned to these two industrial facilities, for modeling purposes, are based on the permit limits provided in Table 6-4.
- An assimilative capacity for future growth of 10 percent of existing loads was available for industrial and municipal facilities in AUs 0511_01, 0511_02, and 0511D_01.

A summary of the DO results for the TMDL scenario is provided in Table 7-4 for all AUs assessed by TCEQ as impaired for DO as shown on Figure 1-1. The results in Table 7-4 are provided as two sets of columns representing with and without consideration of future growth in Cow Bayou Tidal AUs 0511_01 and 0511_02. The allowance for future growth is further explained in Section 7.3.3.

Table 7-4 Results of TMDL Scenarios for conditions with and without future growth for DO impaired AUs of Adams Bayou and Cow Bayou watersheds

AUs 0511_01 and 0511D_01 are not impaired for DO but are included in this table for the purpose of showing the implications of future growth on DO in these AUs.

Waterbody Name	AU	Model Sub-basin or Reach	Model	24-hour Average DO criterion (mg/L)	Without Future Growth			With Future Growth		
					Average DO (mg/L)	10 th Percentile DO (mg/L)	Days Not Meeting Average DO Criterion (%)	Average DO (mg/L)	10 th Percentile DO (mg/L)	Days Not Meeting Average DO Criterion (%)
Adams Bayou Tidal	0508_01	2-27	WASP	4	5.6	4.0	9.2	NA	NA	NA
	0508_02	28-34	WASP	4	6.0	4.5	1.2	NA	NA	NA
	0508_03	35-48	WASP	4	6.2	4.7	1.0	NA	NA	NA
	0508_04	49-68	WASP	4	5.9	4.1	7.1	NA	NA	NA
Hudson Gully	0508C_01	109-111	WASP	4	5.8	4.2	6.9	NA	NA	NA
Cow Bayou Tidal	0511_01	2-19	WASP	4	6.1	4.5	0.1	6.0	4.4	1.0
	0511_02	20-41	WASP	4	6.3	4.2	4.5	6.2	4.0	7.7
	0511_03	42-58	WASP	4	6.9	4.1	7.9	6.9	4.0	9.9
	0511_04	59-67	WASP	4	7.3	4.1	8.2	7.3	4.1	9.1
Cow Bayou Above Tidal	0511A_02	1,3	HSPF	3	7.1	3.4	8.4	7.1	3.4	8.4
Coon Bayou	0511B_01	97-107	WASP	4	6.2	4.1	8.4	6.1	4.0	9.7
Cole Creek	0511C_01	115-123	WASP	4	7.3	4.1	8.6	7.2	4.0	9.7
Unnamed Trib to Cow Bayou Tidal	0511D_01	85-87	WASP	4	7.2	4.1	6.0	7.1	4.0	8.5

NA = not applicable, no FG available for Adams Bayou system

7.2 Margin of Safety for DO TMDLs

The MOS is used to account for uncertainty in the analysis used to develop TMDLs and thus provides a higher level of assurance that the goal of the TMDLs will be met. According to EPA guidance (EPA, 1991), the MOS can be incorporated into the TMDL using two methods:

1. Implicitly incorporating the MOS using conservative model assumptions to develop allocations; or
2. Explicitly specifying a portion of the TMDL as the MOS and using the remainder for allocations.

The margin of safety is designed to account for any uncertainty that may arise in specifying water quality control strategies for the complex environmental processes that affect water quality. Accounting for this uncertainty, to the extent possible, is the basis for assigning a margin of safety.

The DO TMDLs incorporate an implicit MOS based on conservative model assumptions. The conservative model assumptions include:

- The fact that the evaluation was performed under full permitted limits for point source discharges, which are seldom reached in practice.
- The models predict that DO levels are greater than required to meet water quality standards in most AUs. That is, in order to meet the criteria 90 percent of the time in several of the impaired AUs, the DO levels in adjacent AUs meet the criteria more than 90 percent of the time.
- A multiplier of 3.0 was used to convert CBOD₅ to ultimate carbonaceous biochemical oxygen demand for all TPDES municipal and industrial WWTFs inputs included in the modeling system. A default value of 2.3 is used as the multiplier in TCEQ permit evaluations. The multiplier of 3.0 was based on statistical analysis of simultaneously collected five, fifteen, and twenty-day carbonaceous biochemical oxygen demand in ambient water samples obtained during the intensive surveys used for verification of the modeling systems.
- Stormwater runoff loads for some industrial facilities are accounted for in both the HSPF and WASP models.

7.3 Pollutant Load Allocation for DO

The TMDL represents the maximum amount of a pollutant that the stream can receive in a single day without exceeding water quality standards. The pollutant load allocations for the selected scenarios were calculated using the TMDL equation, repeated here for clarity:

$$\text{TMDL} = \text{WLA} + \text{LA} + \text{FG} + \text{MOS}$$

Where:

WLA = wasteload allocation, the amount of pollutant allowed by regulated dischargers

LA = load allocation, the amount of pollutant allowed by unregulated sources

FG = loadings associated with future growth from potential regulated facilities

MOS = margin of safety load

As stated in 40 CFR 130.2(i), TMDLs can be expressed in terms of mass per time, toxicity, or other appropriate measures. For DO impairments, TMDLs are expressed as pounds per day of pollutants affecting DO dynamics and represent the maximum one-day load the water body can assimilate while still attaining the DO criteria specified in the Texas Surface Water Quality Standards.

The TMDL component for each impaired AU covered in this report is derived using the daily average loads from the 11-year simulations of flow and water quality in the streams of Adams Bayou and Cow Bayou watersheds. The pollutant load reduction scenarios of each watershed, for which DO conditions are summarized in Table 7-4, provides the basis of the DO TMDLs. The following sections will present an explanation of each TMDL component first, followed by the TMDL results.

7.3.1 Wasteload Allocation for DO

As previously mentioned, the WLA consists of two parts—the wasteload that is allocated to TPDES-regulated WWTFs (WLA_{WWTF}) and the wasteload that is allocated to regulated stormwater dischargers (WLA_{SW}).

$$WLA = WLA_{WWTF} + WLA_{SW}$$

7.3.1.1 WWTFs

TPDES-permitted WWTFs are allocated a daily wasteload (WLA_{WWTF}) in pounds per day (lbs/day) for CBOD₅ and NH₃N calculated as the full permitted discharge in MGD multiplied by the permit limit in mg/L determined from application of the TMDL modeling system for the pollutant load reduction scenarios. This is expressed in the following equation:

$$WLA_{WWTF} = \text{Flow} * \text{Permit Limit} * \text{Conversion Factor}$$

Where:

Flow (MGD) = full permitted flow

Permit limit for CBOD₅, NH₃N, or DO in mg/L

Conversion factor (to lbs/day) = $3.78541E6 \text{ (L/day)/MGD} * 2.20462E-6 \text{ lbs/mg} = 8.34 \text{ lbs/(mg/L)/MGD}$

7.3.1.2 Regulated Stormwater

Stormwater discharges from MS4, industrial, and construction areas are considered regulated point sources. Therefore, the WLA calculations must also include an allocation for regulated stormwater discharges (WLA_{SW}). A simplified approach for estimating the WLA for these areas was used in the development of these TMDLs because the modeling system output for stormwater is at the HSPF subbasin level, which includes both regulated and unregulated land areas.

The determination of WLA_{SW} from the HSPF subbasin level simulations occurred through a two-step process. First, the stormwater load output from each HSPF subbasin is proportioned into the AUs represented in the subbasin based on the percentage of the AUs in each subbasin. The total stormwater load for each AU is computed as the sum of the component parts from each HSPF subbasin in which the AU was located. Second, the percentage of each AU watershed that is under the jurisdiction of stormwater permits is used to estimate the amount of the overall runoff load to be allocated as the regulated stormwater contribution in the WLA_{SW} component of the TMDL. The percentage of each AU watershed that is under the jurisdiction of stormwater permits is based on the information in Section 2.6.1.3 and Table 10 of the bacteria technical support document (Hauck and Adams, 2020).

7.3.2 Load Allocation

As with the WLA_{SW} component, LA is computed at the AU level for the AUs impaired for depressed DO. The LA component of the TMDL corresponds to the unregulated portion of the direct nonpoint runoff and is the difference between the total load from stormwater runoff from HSPF simulations and the portion allocated to WLA_{SW} .

7.3.3 Allowance for Future Growth for DO TMDLS

The FG component of the TMDL equation addresses the necessity to explore for the effects of future loadings that may occur due to population growth, changes in community infrastructure, and development. Specifically, this TMDL component takes into account the probability that new flows from WWTF discharges may occur in the future. Any allowance for future growth will result in protection of existing uses and conform to Texas's antidegradation policy.

In AUs that required load reductions as indicated by TMDL modeling system simulations, no allowance for FG was assigned. Nevertheless, in some of these AUs there is some room for future loading increases in localized areas. However, the amount of the permissible additional loading depends on the location of the discharge within the AU. Any proposed additional loading must be evaluated using the TMDL models to ensure that it will not result in non-compliance with

water quality standards. Similarly, there is flexibility to modify the permitted loading of CBOD₅ or NH₃N, provided that either constituent's impacts on DO are balanced by reductions of one versus the other. These evaluations must be performed via model simulations.

In AUs for which no load reductions were required in the TMDL modeling system simulations, FG loads were added into the simulations. This was only the case for Cow Bayou watershed AUs 0511_01, 0511_02, and 0511D_01, where no load reductions were required in the simulations to meet the DO criterion. For the purposes of the TMDL, the flow of each municipal and industrial WWTF within these AUs was increased by 10 percent, representing a commensurate 10 percent increase in loading of CBOD₅ and NH₃N, as well as, DO. As noted above, any proposed additional loadings from either permit expansions or new permits must be evaluated using the modeling system to ensure that compliance with water quality standards is maintained. Nonetheless, for AUs 0511_01, 0511_02, and 0511D_01, an FG component is provided in the TMDL allocations. Also, the FG of 10 percent for existing TPDES permitted facilities is for illustrative purposes to demonstrate capacity and should not be interpreted as being assigned solely to each facility.

7.3.4 TMDL Calculations for DO

Based on the assigned permit limits for municipal and industrial WWTFs used as input into the pollutant load allocations, wasteload loadings can be assigned to each WWTF in lbs/day. The WLA_{WWTF} assigned to each facility, including CBOD₅ and NH₃N, as well as DO, are provided in Table 7-5 for municipal WWTFs and Table 7-6 for industrial WWTFs. In Tables 7-5 and 7-6, the CBOD₅, NH₃N, and DO concentrations are provided in addition to the WLA_{WWTF} load.

The regulated stormwater (WLA_{SW}) and unregulated stormwater (LA) components of the TMDL are provided in Table 7-7 based on the 11-year simulation results from the HSPF watershed models. To maintain a watershed approach, certain AUs include upstream AUs, if those upstream AUs were not impaired due to depressed DO. In the Adams Bayou watershed, 0508_04 also includes 0508A_01 and 0508B_01. In the Cow Bayou watershed, 0511_04 includes 0511A_01 and 0511_03 includes 0511E_01 as upstream contributing AUs that were not impaired due to depressed DO. For each of the impaired AUs, the regulated stormwater area percent in Table 7-7 was based on the combined areas of the impaired AU and all upstream unimpaired AUs.

Table 7-5 Wasteload allocations for regulated domestic WWTFs in the Adams Bayou and Cow Bayou watersheds

Permit	TPDES No. (NPDES No.)	AU	Outfall	Daily Average Flow (MGD)	Daily Average CBOD ₅ mg/L (lbs/day)	Daily Average NH ₃ N mg/L (lbs/day)	Minimum DO mg/L (lbs/day)
Jasper County WCID 1	WQ0010808001 (TX0021300)	0511A_02	001	0.41	10 (34.19)	3 (10.26)	5 (17.10)
Orangefield Water Supply Corporation	WQ0014772001 (TX0129313)	0511_02	001	0.75	10 (62.55)	2 (12.51)	4 (25.02)
PCS Development Company	WQ0011916001 (TX0074250)	0511_04	001	0.09	10 (7.51)	2 (1.50)	5 (3.75)
Bayou Pines LLC	WQ0015029001 (TX0133418)	0511B_01	001	0.009	10 (0.75)	3 (0.23)	5 (0.38)
Gulflander Partners Group, L.P.	WQ0013488001 (TX0106437)	0511B_01	001	0.01	10 (0.83)	3 (0.25)	5 (0.42)
City of Bridge City	WQ0010051001 (TX0025500)	0511_01	001	1.6 ¹	10 (133.44)	12 (160.13) ²	4 (53.38)
City of Pinehurst	WQ0010597001 (TX0024171)	0508_03	001	0.5	10 (41.70)	3 (12.51)	5 (20.85)
City of Orange ³	WQ0010626001 (TX0073423)	0508_02	002	7.0 ³	10 (583.80)	3 (175.14)	5 (291.90)
Orange County WCID 2	WQ0010240001 (TX0054810)	0508_02	001	1.22 ¹	10 (101.75)	3 (30.52)	5 (50.87)

¹ Annual average flow in MGD.

² Determined using a default value assumed in TCEQ permit evaluations.

³ Intermittent discharge. The permittee is authorized to discharge from Outfall 002 only if, as a result of wet weather conditions, the average discharge from the facility exceeds 11,111 gallons per minute. Combined average annual discharge of Outfalls 001 and 002 is not to exceed 7.0 MGD. Simulated as 7.0 MGD on all days of discharge indicated in the DMR data for the period of January 1, 2002 – December 31, 2012. Outfall 001 discharges to the Sabine River.

Table 7-6 Wasteload allocations for regulated industrial WWTFs in the Adams Bayou and Cow Bayou watersheds

Permit	TPDES No. (NPDES No.)	AU	Outfall	Daily Average Flow (MGD)	Daily Average CBOD ₅ mg/L (lbs/day)	Daily Average NH ₃ N mg/L (lbs/day)	Minimum DO mg/L (lbs/day)
Miller Waste Mills, Inc.	WQ0002835000 (TX0104710)	0511_02	001 ¹ 002 003 ²	- 0.116 ³ -	- 20 (19.35) -	- 1 (0.97) -	- 2 (1.93) -
Lion Elastomers Orange, LLC	WQ0000454000 (TX0002968)	0511_01	001 002 ¹	1.202 -	11 (110.27) -	2 (20.05) -	2 (20.05) -
Chevron Phillips Chemical Company LP	WQ0000359000 (TX0004839)	0511D_01	001	3.15	17.5 (459.74)	0.8 (21.02)	5 (131.36)
Printpack, Inc.	WQ0002858000 (TX0101192)	0511D_01	001 101 ⁴	0.085 -	10 (7.09) -	3 (2.13) -	5 (3.54) -
Honeywell International Inc.	WQ0000670000 (TX0007897)	0511_01	001	1.4	10 (116.76)	1 (11.68)	2 (23.35)
ARLANXEO USA LLC	WQ0001167000 (TX0003654)	0511_01	001	6.0	3.5 (175.14)	1 (50.04)	2 (100.08)

¹ Stormwater only outfall; not included as direct point source in modeling system; no new limits assigned in the pollutant load reduction scenario.

² Based on DMR data, discharge from Outfall 003 has not occurred; therefore, discharge has never been reported; no new limits assigned in the pollutant load reduction scenario.

³ Average of 2017 – 2018 DMR data.

⁴ Internal outfall that is included in Outfall 001; no new limits assigned in the pollutant load reduction scenario.

Table 7-7 Regulated and unregulated stormwater calculations for impaired AUs of Adams Bayou, Cow Bayou and associated tributaries

All loads expressed in lbs/day.

AU	Total Runoff CBOD ₅	Total Runoff NH ₃ N	Regulated Stormwater Area (%)	WLA _{SW} CBOD ₅	WLA _{SW} NH ₃ N	LA CBOD ₅	LA NH ₃ N
0508_01	177.29	14.53	59.87	106.14	8.7	71.15	5.83
0508_02	47.41	4.00	99.85	47.34	3.99	0.07	0.01
0508_03	84.34	7.11	100.00	84.34	7.11	0.00	0.00
0508_04	348.46	26.37	11.93	41.57	3.15	306.89	23.22
0508C_01	21.10	1.74	99.32	20.96	1.73	0.14	0.01
Adams Bayou Total	678.60	53.75	NA¹	300.35	24.68	378.25	29.07
0511_01 ²	222.25	17.68	29.30	65.12	5.18	157.13	12.50
0511_02	359.70	28.08	9.02	32.44	2.53	327.26	25.55
0511_03	394.82	27.16	15.54	61.36	4.22	333.46	22.94
0511_04	191.41	12.71	4.07	7.79	0.52	183.62	12.19
0511A_02	613.40	40.33	0.34	2.09	0.14	611.31	40.19
0511B_01	70.11	5.56	27.87	19.54	1.55	50.57	4.01
0511C_01	148.72	10.05	1.63	2.42	0.16	146.30	9.89
0511D_01 ²	43.61	3.76	60.52	26.39	2.28	17.22	1.48
Cow Bayou Total	2,044.02	145.32	NA¹	217.15	16.58	1,826.87	128.75

¹ N/A – not applicable. Adams Bayou and Cow Bayou watersheds are each represented by multiple sub-basins in HSPF with each sub-basin containing a unique composition of land uses that result in differing runoff loads of CBOD₅ and NH₃N by area. Also, the loads from each sub-basin are proportioned into WLA_{SW} and LA terms for individual AUs based on the percent of the sub-basin in each AU and the regulated stormwater area percent of each AU. The differing land uses comprising HSPF sub-basins and subsequent differing runoff loads by area result in spatial variability that does not allow a unique watershed-wide percent of regulated stormwater to be computed that is correct for both CBOD₅ and NH₃N loads.

² AUs 0511_01 and 0511D_01 are not impaired for DO and are included for purposes of showing implications of future growth on DO in these AUs.

7.3.5 Summary of TMDL Calculations for DO

Table 7-8 summarizes the TMDL calculations for the five impaired AUs of the Adams Bayou watershed and the six impaired AUs of the Cow Bayou watershed. The TMDLs were calculated based on the application of the TMDL modeling system of the Adams Bayou watershed and the TMDL modeling system of the Cow Bayou watershed. The values are based on the reductions required to support a high aquatic life use for all tidal streams with a 24-hour daily average DO criterion of 4 mg/L and a limited aquatic life use for freshwater streams with a 24-hour daily average DO criterion of 3 mg/L. The summary of TMDL calculations includes AUs 0511_01 and 0511D_01 to illustrate the FG term for AU 0511_01 and because the TMDL modeling system showed exceedance of the DO criterion in 0511D_01 at the fully permitted loads scenario, requiring permitted DO effluent loadings for facilities discharging to this AU (0511D_01).

The final TMDL allocations needed to comply with the requirements of 40 CFR 130.7 (Table 7-9) include the FG component within the WLA_{WWTf} and excludes Cow Bayou Tidal 0511_01, which is unimpaired for DO and in which the TMDL modeling system showed additional capacity to assimilate $CBOD_5$ and NH_3N loads while complying with the 24-hour daily average DO criterion.

7.4 Pollutant Load Allocations for pH

As a measure of the hydrogen ion content (acidity) of water, pH is also an impairment in Cow Bayou Tidal AU 0511_04 requiring a TMDL. General water quality uses are not met due to observed pH levels below the acceptable range of water quality criteria (6.0–8.5) for AU 0511_04. Five of the 23 pH measurements (22 percent) taken in AU 0511_04 from 1994 to 1999 in the upper tidal reaches of Cow Bayou were lower than the minimum of 6.0, resulting in the non-support listing.

It is difficult to simulate pH through water quality modeling. A large number of natural processes affect pH levels—watershed soil and bedrock type, watershed vegetation type, loading of organic matter, wastewater effluent discharges, temperature, seasonality, photosynthesis by phytoplankton and other aquatic plants, and respiration of organic matter. Algal photosynthesis consumes hydrogen ions, raising the pH. Respiration reverses this process, releasing hydrogen ions and lowering pH. The pH parameter varies less as alkalinity (buffering capacity) increases, but these bayous have low levels of alkalinity. In particular, at approximately 22 km upstream of the Sabine River, the median levels of total alkalinity are 20 mg/L as calcium carbonate. Further, the lower tidal portions of both bayous are more strongly buffered by the salts found in seawater.

Table 7-8 TMDL allocation summary for AUs of Adams Bayou, Cow Bayou and associated tributaries

All loads expressed in lbs/day.

Columns for CBOD₅ and NH₃N MOS not included; implicit MOS based on conservative model system assumptions.

AU	TMDL CBOD ₅	TMDL NH ₃ N	WLA _{WWTF} CBOD ₅	WLA _{WWTF} NH ₃ N	WLA _{SW} CBOD ₅	WLA _{SW} NH ₃ N	LA CBOD ₅	LA NH ₃ N	FG CBOD ₅	FG NH ₃ N
0508_01	177.29	14.53	0.00	0.00	106.14	8.70	71.15	5.83	0.00	0.00
0508_02	732.96	209.66	685.55	205.66	47.34	3.99	0.07	0.01	0.00	0.00
0508_03	126.04	19.62	41.70	12.51	84.34	7.11	0.00	0.00	0.00	0.00
0508_04	348.46	26.37	0.00	0.00	41.57	3.15	306.89	23.22	0.00	0.00
0508C_01	21.10	1.74	0.00	0.00	20.96	1.73	0.14	0.01	0.00	0.00
Adams Bayou Total	1,405.85	271.92	727.25	218.17	300.35	24.68	378.25	29.07	0.00	0.00
0511_01 ¹	811.40	283.75	535.61	241.90	65.12	5.18	157.13	12.50	53.54	24.17
0511_02	449.79	42.90	81.90	13.48	32.44	2.53	327.26	25.55	8.19	1.34
0511_03	394.82	27.16	0.00	0.00	61.36	4.22	333.46	22.94	0.00	0.00
0511_04	198.92	14.21	7.51	1.50	7.79	0.52	183.62	12.19	0.00	0.00
0511A_02	647.59	50.59	34.19	10.26	2.09	0.14	611.31	40.19	0.00	0.00
0511B_01	71.69	6.04	1.58	0.48	19.54	1.55	50.57	4.01	0.00	0.00
0511C_01	148.72	10.05	0.00	0.00	2.42	0.16	146.30	9.89	0.00	0.00
0511D_01 ¹	557.13	29.22	466.83	23.15	26.39	2.28	17.22	1.48	46.69	2.31
Cow Bayou Total	3,280.06	463.92	1,127.62	290.77	217.15	16.58	1,826.87	128.75	108.42	27.82

¹ AUs 0511_01 and 0511D_01 are not impaired for DO and are included for purposes of showing implications of future growth on DO in these AUs.

Table 7-9 Final TMDL allocations for impaired AUs of Adams Bayou, Cow Bayou and associated tributaries

All loads expressed in lbs/day.

Columns for CBOD₅ and NH₃N MOS not included; implicit MOS based on conservative model system assumptions.

AU	TMDL CBOD ₅	TMDL NH ₃ N	WLA _{WWTF} CBOD ₅ ¹	WLA _{WWTF} NH ₃ N ¹	WLA _{SW} CBOD ₅	WLA _{SW} NH ₃ N	LA CBOD ₅	LA NH ₃ N
0508_01	177.29	14.53	0.00	0.00	106.14	8.70	71.15	5.83
0508_02	732.96	209.66	685.55	205.66	47.34	3.99	0.07	0.01
0508_03	126.04	19.62	41.70	12.51	84.34	7.11	0.00	0.00
0508_04	348.46	26.37	0.00	0.00	41.57	3.15	306.89	23.22
0508C_01	21.10	1.74	0.00	0.00	20.96	1.73	0.14	0.01
Adams Bayou Total	1,405.85	271.92	727.25	218.17	300.35	24.68	378.25	29.07
0511_02	449.79	42.90	90.09	14.82	32.44	2.53	327.26	25.55
0511_03	394.82	27.16	0.00	0.00	61.36	4.22	333.46	22.94
0511_04	198.92	14.21	7.51	1.50	7.79	0.52	183.62	12.19
0511A_02	647.59	50.59	34.19	10.26	2.09	0.14	611.31	40.19
0511B_01	71.69	6.04	1.58	0.48	19.54	1.55	50.57	4.01
0511C_01	148.72	10.05	0.00	0.00	2.42	0.16	146.30	9.89
Cow Bayou Total²	1,911.53	150.95	133.37	27.06	125.64	9.12	1,652.52	114.77

¹WLA_{WWTF} includes the FG component.

²CBOD₅ and NH₃N loads for unimpaired AUs 0511_01 and 0511D_01 are excluded from this table, though these loads were provided in Table 7-8.

HSPF and more recent versions of the WASP do simulate pH. To properly and accurately simulate pH, the modeling system would have necessitated including not only pH as a state variable in both models, but also adding carbon dioxide, total inorganic carbon, and alkalinity. Including pH to simulation capabilities was not reasonable due to data constraints for proper model development. Instead an indirect approach based on well understood water-chemistry processes was applied to address the pH issues of Cow Bayou Tidal AU 0511_04.

The primary process responsible for lower pH in many systems is the respiration of organic matter. Primary production by aquatic plants, on the other hand, is the key process raising the pH level in many systems. Low pH levels tend to occur in poorly buffered systems where respiration exceeds primary production. Another potential source of low pH is un-neutralized point source discharges, though such a source is not known to occur in the areas of impairment.

The modeling conducted as part of this TMDL exercise shows the source of low pH in Cow Bayou Tidal AU 0511_04 appears to be the degradation of organic matter, which is also the primary source of low DO levels. Figure 7-1 shows that the changes in average pH levels with distance downstream in Cow Bayou vary inversely with the cBOD levels. Thus, the low pH values tend to occur where cBOD levels are highest, likely due to the degradation of the organic matter comprising cBOD. For this reason, it is reasonable to assume that the same measures intended to raise DO levels will also raise pH values to meet water quality standards.

Given that the DO criteria are not met in Cow Bayou far more frequently than the pH criteria, it follows logically that a TMDL involving sufficient reductions in oxygen demanding organic matter to meet water quality standards for DO will in all likelihood also lead to attainment of the pH standard. Therefore, the TMDL for attainment of the pH criteria in Cow Bayou Tidal requires the same allocations for cBOD and NH₃N for attainment of the DO criteria (Tables 7-8 and 7-9).

7.5 Consideration of Seasonal Variation for DO and pH

Previous studies conducted on Adams Bayou and Cow Bayou have examined seasonal variation in water quality parameters, including DO and pH. A 2002 historical review of water quality data collected on Adams Bayou, Cow Bayou and associated tributaries concluded that DO levels were lowest during the summer season when water temperatures are higher and stream flows are lower (Parsons, 2002). The report, which looked at historical data from 1969 to 2002, also showed seasonal variation in pH, with the lowest pH values occurring in mid to late summer. In 2008, Contreras and Whisenant used Analysis of Similarity (ANOSIM), a nonparametric statistical test analogous to the parametric-based ANOVA test, to analyze seasonality in water quality data collected during the aquatic life use attainability analysis conducted on Cow Bayou. Cow Bayou samples were different among seasons as revealed by the results of the ANOSIM test (Global R value was 0.234, *p* value was less than 0.001). The difference is driven primarily by the disparity between spring and summer samples, with the lowest DO and pH values occurring in summer

samples when elevated water temperatures and higher specific conductance values are also most prevalent (TPWD, 2008).

The time period modeled by the Adams Bayou and Cow Bayou TMDL modeling system (January 1, 2002 through December 31, 2012) includes over a decade of seasonal variation. By simulating a complete 11-year period, the modeling system and TMDLs implicitly consider inter-annual and seasonal variation.

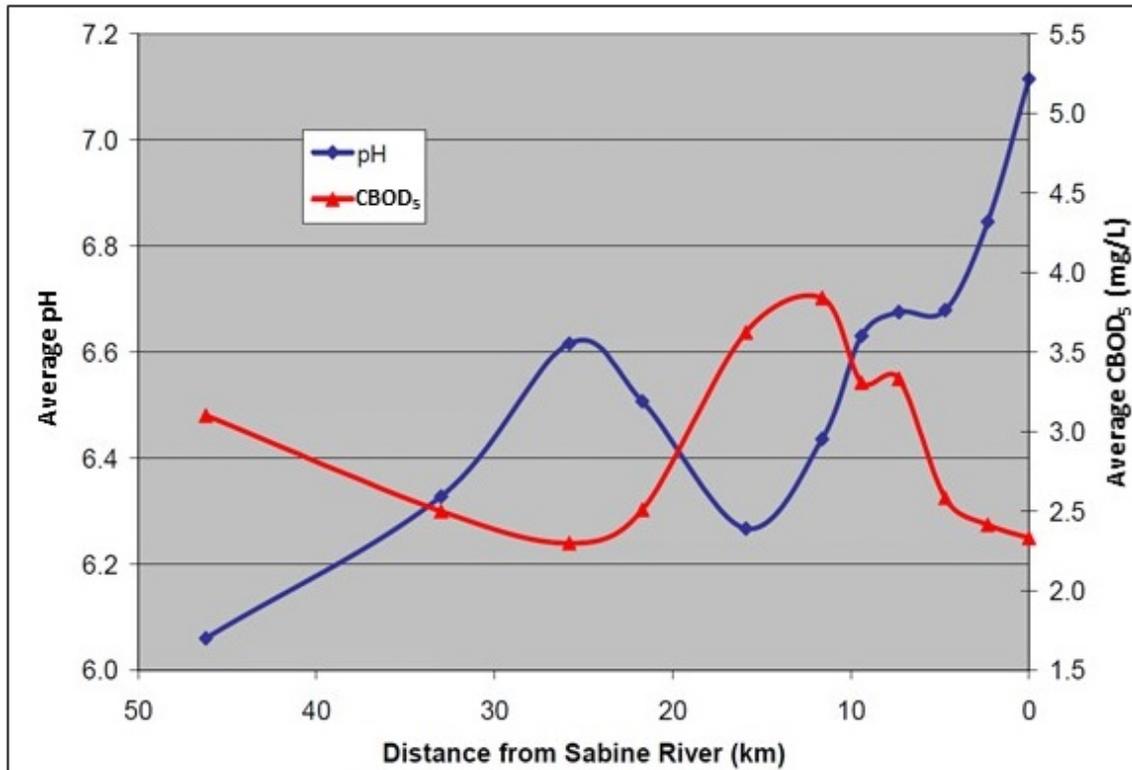


Figure 7-1 Average measured pH and cBOD₅ in Cow Bayou with distance upstream during the summer 2004 summer intensive surveys used for RMA2 and WASP validation

8. References

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Appendix A Adams Bayou HSPF User Control Interface File

Note: The annotations that were added to this print version for clarity may prevent it from running. It may be necessary to strip out some comment lines that begin with three asterisks.

RUN

GLOBAL

UCI Created by KIRK DEAN/Nabin Basnet for the Adams Bayou watershed
START 2001/01/01 00:00 END 2012/12/31 23:00
RUN INTERP OUTPT LEVELS 3 3
RESUME 0 RUN 1 UNITS 1
END GLOBAL

FILES

<FILE>	<UN#>	***<----FILE NAME----->
MESSU	24	adams_lt.ech
	91	adams_lt.out
WDM1	25	adams_out1.wdm
WDM2	26	adams_meteorol.wdm
BINO	92	adams_meteorol.hbn
WDM3	27	adams_source.wdm

END FILES

OPN SEQUENCE

INGRP	INDELT	01:00
PERLND	101	
PERLND	102	
PERLND	103	
PERLND	104	
PERLND	105	
PERLND	106	
PERLND	107	
PERLND	108	
PERLND	109	
PERLND	110	
PERLND	111	
PERLND	112	
PERLND	113	
PERLND	114	
PERLND	115	
PERLND	116	
PERLND	117	
IMPLND	101	
IMPLND	102	
IMPLND	103	
IMPLND	104	
RCHRES	1	
RCHRES	2	
RCHRES	3	
RCHRES	4	
RCHRES	6	
RCHRES	5	
RCHRES	7	
RCHRES	8	
RCHRES	9	
RCHRES	10	
RCHRES	11	

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

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RCHRES      12
COPY        1
COPY        2
COPY        3
COPY        4
COPY        5
COPY        6
COPY        7
COPY        8
COPY        9
COPY       10
COPY       11
COPY       12

END INGRP
END OPN SEQUENCE

PERLND
ACTIVITY
*** <PLS >
*** x - x ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC ***
101 117 1 0 1 1 1 1 0 0 0 0 0
END ACTIVITY

PRINT-INFO
*** < PLS>
*** x - x ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC PIVL PYR
101 117 4 4 4 4 4 4 4 4 4 4 4 1 12
END PRINT-INFO

BINARY-INFO
*** < PLS>
*** x - x ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC PIVL PYR
101 117 4 4 4 4 4 4 4 4 4 4 4 1 12
END BINARY-INFO

GEN-INFO
***
*** <PLS >
*** x - x
101 Developed Open Space 1 1 0 0 92 0
102 Developed Low Intens 1 1 0 0 92 0
103 Developed Medium Int 1 1 0 0 92 0
104 Developed High Inten 1 1 0 0 92 0
105 Barren 1 1 0 0 92 0
106 Deciduous Forest 1 1 0 0 92 0
107 Evergreen Forest 1 1 0 0 92 0
108 Mixed Forest 1 1 0 0 92 0
109 Pasture/Hay 1 1 0 0 92 0
110 Cropland 1 1 0 0 92 0
111 Grassland/Herbaceous 1 1 0 0 92 0
112 Shrub/Scrub 1 1 0 0 92 0
113 Open Water 1 1 0 0 92 0
114 Woody Wetlands 1 1 0 0 92 0
115 Herbaceous Wetlands 1 1 0 0 92 0
116 Septic Fields 1 1 0 0 92 0
117 Future Unused 2 1 1 0 0 92 0
END GEN-INFO

ATEMP-DAT
*** <PLS >
*** x - x ELDAT AIRTEMP
101 117 (ft) (deg F)
101 117 -6. 33.
END ATEMP-DAT

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

```

PWAT-PARM1
*** <PLS >
*** x - x CSNO RTOP UZFG VCS VUZ VNN VIFW VIRC VLE IFFC HWT IRRG IFRD
101 114 0 1 1 1 1 0 0 0 1 0 0 0 0
115 0 2 1 1 0 0 0 0 1 0 1 0 0
116 117 0 1 1 1 1 0 0 0 1 0 0 0 0
END PWAT-PARM1

```

```

PWAT-PARM2
*** < PLS> FOREST LZSN INFILT LSUR SLSUR KVARY AGWRC
*** x - x (in) (in/hr) (ft) (1/in) (1/day)
101 0. 5. 0.25 500. 0.002 5. 0.96
102 0. 5. 0.25 500. 0.002 5. 0.96
103 0. 5. 0.25 500. 0.002 5. 0.96
104 0. 5. 0.25 500. 0.002 5. 0.96
105 0. 5. 0.25 500. 0.002 5. 0.96
106 0. 5. 0.25 500. 0.002 5. 0.96
107 0. 5. 0.25 500. 0.002 5. 0.96
108 0. 5. 0.25 500. 0.002 5. 0.96
109 0. 5. 0.25 500. 0.002 5. 0.96
110 0. 5. 0.25 500. 0.002 5. 0.96
111 0. 5. 0.25 500. 0.002 5. 0.96
112 0. 5. 0.25 500. 0.002 5. 0.96
113 0. 5. 0.25 200. 0.001 5. 0.96
114 0. 5. 0.25 500. 0.002 5. 0.96
115 0. 5. 0.25 500. 0.001 5. 0.96
116 0. 5. 0.25 500. 0.002 5. 0.96
117 0. 5. 0.25 500. 0.002 5. 0.96
END PWAT-PARM2

```

```

PWAT-PARM3
*** < PLS> PETMAX PETMIN INFEXP INFILD DEEPFR BASETP AGWETP
*** x - x (deg F) (deg F)
101 40. 35. 2. 2. 0.10 0.10 0.2
102 40. 35. 2. 2. 0.10 0.10 0.2
103 40. 35. 2. 2. 0.10 0.10 0.2
104 40. 35. 2. 2. 0.10 0.10 0.2
105 40. 35. 2. 2. 0.10 0.10 0.2
106 40. 35. 2. 2. 0.10 0.10 0.2
107 40. 35. 2. 2. 0.10 0.10 0.2
108 40. 35. 2. 2. 0.10 0.10 0.2
109 40. 35. 2. 2. 0.10 0.10 0.2
110 40. 35. 2. 2. 0.10 0.10 0.2
111 40. 35. 2. 2. 0.10 0.10 0.2
112 40. 35. 2. 2. 0.10 0.10 0.2
113 40. 35. 2. 2. 0.10 0.10 0.2
114 40. 35. 2. 2. 0.10 0.10 0.2
115 40. 35. 2. 2. 0.10 0.10 0.2
116 40. 35. 2. 2. 0.10 0.10 0.2
117 40. 35. 2. 2. 0.10 0.10 0.2
END PWAT-PARM3

```

```

PWAT-PARM4
*** <PLS > CEPSC UZSN NSUR INTFW IRC LZETP
*** x - x (in) (in) (1/day)
101 0.15 0.6 0.4 10. 0.75 0.5
102 0.15 0.6 0.4 10. 0.75 0.5
103 0.15 0.6 0.4 10. 0.75 0.5
104 0.15 0.6 0.4 10. 0.75 0.5
105 0.15 0.6 0.4 10. 0.75 0.5
106 0.15 0.6 0.4 10. 0.75 0.5
107 0.15 0.6 0.4 10. 0.75 0.5

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

108	0.15	0.6	0.4	10.	0.75	0.5
109	0.15	0.6	0.4	10.	0.75	0.5
110	0.15	0.6	0.4	10.	0.75	0.5
111	0.15	0.6	0.4	10.	0.75	0.5
112	0.15	0.6	0.4	10.	0.75	0.5
113	0.01	0.6	0.4	10.	0.75	0.5
114	0.15	0.6	0.4	10.	0.75	0.5
115	0.15	0.6	0.4	10.	0.75	0.5
116	0.15	0.6	0.4	10.	0.75	0.5
117	0.15	0.6	0.4	10.	0.75	0.5

END PWAT-PARM4

PWAT-PARM6

*** < PLS >	MELEV	BELV	GWDATM	PCW	PGW	UPGW
*** x - x	(ft)	(ft)	(ft)			
101	53.	37.3	0.	0.3	0.1	0.15
102	53.	37.3	0.	0.3	0.1	0.15
103	53.	37.3	0.	0.3	0.1	0.15
104	51.3	37.3	0.	0.3	0.1	0.15
105	45.6	37.3	0.	0.3	0.1	0.15
106	41.9	37.3	0.	0.3	0.1	0.15
107	45.8	37.3	0.	0.3	0.1	0.15
108	43.5	37.3	0.	0.3	0.1	0.15
109	53.	37.3	0.	0.3	0.1	0.15
110	53.	37.3	0.	0.3	0.1	0.15
111	53.	37.3	0.	0.3	0.1	0.15
112	53.	37.3	0.	0.3	0.1	0.15
113	41.1	37.3	0.	0.3	0.1	0.15
114	39.4	37.3	0.	0.3	0.1	0.15
115	44.	37.3	0.	0.3	0.1	0.15
116	53.	37.3	0.	0.3	0.1	0.15
117	50.	37.3	0.	0.3	0.1	0.15

END PWAT-PARM6

PWAT-PARM7

*** < PLS >	STABNO	SRRC	SREXP	IFWSC	DELTA	UELFAC	LLEFAC
*** x - x		(/hr)		(in)	(in)		
101	0.	0.1	1.	0.5	0.002	4.	2.5
102	0.	0.1	1.	0.5	0.002	4.	2.5
103	0.	0.1	1.	0.5	0.002	4.	2.5
104	0.	0.1	1.	0.5	0.002	4.	2.5
105	0.	0.1	1.	0.5	0.002	4.	2.5
106	0.	0.1	1.	0.5	0.002	4.	2.5
107	0.	0.1	1.	0.5	0.002	4.	2.5
108	0.	0.1	1.	0.5	0.002	4.	2.5
109	0.	0.1	1.	0.5	0.002	4.	2.5
110	0.	0.1	1.	0.5	0.002	4.	2.5
111	0.	0.1	1.	0.5	0.002	4.	2.5
112	0.	0.1	1.	0.5	0.002	4.	2.5
113	0.	0.1	1.	0.5	0.002	4.	2.5
114	0.	0.1	1.	0.5	0.002	4.	2.5
115	0.	0.1	1.	0.5	0.002	4.	2.5
116	0.	0.1	1.	0.5	0.002	4.	2.5
117	0.	0.1	1.	0.5	0.002	4.	2.5

END PWAT-PARM7

PWAT-STATE1

*** < PLS >	PWATER state variables (in)						
*** x - x	CEPS	SURS	UZS	IFWS	LZS	AGWS	GWVS
101 117	0.01	0.01	0.1	0.1	4.	2.5	0.

END PWAT-STATE1

MON-INTERCEP

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

```

*** <PLS > Interception storage capacity at start of each month (in)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
101 0.05 0.05 0.05 0.09 0.11 0.15 0.15 0.15 0.15 0.13 0.09 0.05
102 0.05 0.05 0.05 0.09 0.11 0.15 0.15 0.15 0.15 0.13 0.09 0.05
103 0.05 0.05 0.05 0.09 0.11 0.15 0.15 0.15 0.15 0.13 0.09 0.05
104 0.05 0.05 0.05 0.09 0.11 0.15 0.15 0.15 0.15 0.13 0.09 0.05
105 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01
106 0.03 0.03 0.05 0.18 0.26 0.28 0.28 0.28 0.28 0.25 0.18 0.03
107 0.10 0.10 0.10 0.15 0.20 0.25 0.25 0.25 0.25 0.20 0.15 0.10
108 0.05 0.05 0.07 0.16 0.23 0.26 0.26 0.26 0.26 0.22 0.16 0.05
109 0.05 0.05 0.06 0.08 0.12 0.15 0.15 0.15 0.15 0.10 0.08 0.05
110 0.01 0.01 0.04 0.08 0.12 0.15 0.15 0.15 0.15 0.05 0.01 0.01
111 0.05 0.05 0.06 0.10 0.15 0.20 0.20 0.20 0.20 0.15 0.10 0.05
112 0.03 0.03 0.06 0.12 0.22 0.22 0.22 0.22 0.18 0.16 0.12 0.05
113 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01
114 0.05 0.05 0.07 0.16 0.20 0.22 0.22 0.22 0.22 0.20 0.16 0.05
115 0.05 0.05 0.06 0.08 0.12 0.15 0.15 0.15 0.15 0.10 0.08 0.05
116 0.05 0.05 0.05 0.09 0.11 0.15 0.15 0.15 0.15 0.13 0.09 0.05
117 0.05 0.05 0.05 0.09 0.11 0.13 0.13 0.13 0.13 0.13 0.09 0.05
END MON-INTERCEP

```

```

MON-UZSN
*** <PLS > Upper zone storage at start of each month (inches)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
101 117 0.5 0.1 0.1 0.4 0.7 1.0 1.2 1.3 1.2 1.0 1.0 1.0
END MON-UZSN

```

```

MON-LZETPARAM
*** <PLS > Lower zone evapotransp param at start of each month
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
101 117 0.10 0.10 0.17 0.69 0.86 0.90 0.90 0.90 0.90 0.49 0.26 0.10
END MON-LZETPARAM

```

```

SED-PARM1
*** <PLS > Sediment parameters 1
*** x - x CRV VSIV SDOP
101 115 1 0 1
END SED-PARM1

```

```

SED-PARM2
*** <PLS > SMPF KRER JRER AFFIX COVER NVSI
*** x - x (/day) lb/ac-day
101 105 1. 0.43 2. 0.01 0.88 1.
106 107 1. 0.43 2. 0.002 0.88 2.
108 1. 0.43 2. 0.002 0.88 2.
109 1. 0.43 2. 0.01 0.88 1.
110 1. 0.43 2. 0.01 0.88 2.
111 1. 0.43 2. 0.01 0.88 1.
112 1. 0.43 2. 0.01 0.88 1.
113 1. 0.43 2. 0.002 0.88 0.
114 1. 0.28 2. 0.002 0.88 2.
115 1. 0.43 2. 0.002 0.88 1.
116 1. 0.43 2. 0.01 0.88 1.
117 1. 0.43 2. 0.01 0.88 1.
END SED-PARM2

```

```

SED-PARM3
*** <PLS > Sediment parameter 3
*** x - x KSER JSER KGER JGER
101 0.50 2. 0. 2.
102 0.50 2. 0.01 2.
103 0.62 2. 0.07 2.
104 0.84 2. 0.125 2.

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

```

105      5.00      2.      0.25      2.
106      0.55      2.      0.      2.
107      0.55      2.      0.      2.
108      0.55      2.      0.      2.
109      1.60      2.      0.3      2.
110      5.00      1.3      5.      1.3
111      0.80      2.      0.      2.
112      1.00      2.      0.      2.
113      0.00      2.      0.      2.
114      0.50      2.      0.      2.
115      0.50      2.      0.      2.
116      0.50      2.      0.01     2.
117      0.50      2.      0.      2.
END SED-PARM3

```

MON-COVER

```

*** <PLS > Monthly values for erosion related cover
*** x - x  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP  OCT  NOV  DEC
101 103 0.90 0.90 0.90 0.91 0.93 0.93 0.93 0.93 0.91 0.90 0.90
104      0.90 0.90 0.90 0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.90 0.90
105      0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01
106      0.80 0.80 0.80 0.94 0.97 0.97 0.97 0.97 0.97 0.97 0.91 0.85
107      0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97
108      0.94 0.94 0.94 0.95 0.97 0.97 0.97 0.97 0.97 0.97 0.96 0.94
109      0.90 0.90 0.90 0.91 0.92 0.93 0.92 0.91 0.90 0.90 0.90 0.90
110      0.70 0.70 0.50 0.50 0.60 0.75 0.80 0.90 0.90 0.70 0.70 0.70
111      0.90 0.90 0.90 0.91 0.92 0.93 0.94 0.94 0.93 0.92 0.91 0.90
112      0.80 0.80 0.80 0.91 0.92 0.93 0.94 0.94 0.93 0.92 0.91 0.85
113      1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
114      0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97
115      0.90 0.90 0.90 0.91 0.93 0.93 0.94 0.94 0.93 0.92 0.91 0.90
116      0.90 0.90 0.90 0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.90 0.90
117      0.90 0.90 0.90 0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.90 0.90
END MON-COVER

```

SED-STOR

```

*** <PLS > Detached sediment storage (tons/acre)
*** x - x      DETS
101      0.4
102      0.4
103      0.4
104      0.4
105      0.5
106      0.1
107      0.1
108      0.1
109      0.2
110      0.5
111      0.2
112      0.1
113      0.
114      0.1
115      0.1
116      0.4
117      0.4
END SED-STOR

```

PSTEMP-PARM1

```

*** <PLS > Flags for section PSTEMP
*** x - x  SLTV ULTV LGTV TSOP
101 117  0  0  0  1
END PSTEMP-PARM1

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

```

PSTEMP-PARM2
*** <PLS >      ASLT      BSLT      ULTP1      ULTP2      LGTP1      LGTP2
*** x - x      (deg F)    (deg F)          (deg F)          (deg F)
101 117      35.      0.4      40.      0.3      65.      0.
END PSTEMP-PARM2

PSTEMP-TEMPS
*** <PLS > Initial temperatures (deg F)
*** x - x      AIRTC      SLTMP      ULTMP      LGTMP
101 117      40.      45.      50.      69.
END PSTEMP-TEMPS

PWT-PARM1
*** <PLS > Flags for section PWTGAS
*** x - x      IDV      ICV      GDV      GVC
101 117      0      0      0      0
END PWT-PARM1

PWT-PARM2
***          Second group of PWTGAS parms
*** <PLS >      ELEV      IDOXP      ICO2P      ADOXP      ACO2P
*** x - x      (ft)      (mg/l)    (mg C/l)    (mg/l)    (mg C/l)
101 117      25.      4.0      0.15      4.0      0.15
END PWT-PARM2

PWT-TEMPS
*** <PLS > Initial water temperatures (deg F)
*** x - x      SOTMP      IOTMP      AOTMP
101 117      45.      50.      69.
END PWT-TEMPS

PWT-GASES
***          Initial DO and CO2 concentrations
*** <PLS >      SODOX      SOCO2      IODOX      IOCO2      AODOX      AOCO2
*** x - x      (mg/l)    (mg C/l)    (mg/l)    (mg C/l)    (mg/l)    (mg C/l)
101 117      8.8      0.15      4.0      0.15      4.0      0.15
END PWT-GASES

NQUALS
*** <PLS >
*** x - xNQUAL
101 117      4
END NQUALS

PQL-AD-FLAGS
***          Atmospheric Deposition Flags
*** < PLS> QUAL1  QUAL2  QUAL3  QUAL4  QUAL5  QUAL6  QUAL7  QUAL8  QUAL9  QUAL10
*** x - x <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C>
101 117 -1 0 -1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
END PQL-AD-FLAGS

QUAL-PROPS
*** <PLS > Identifiers and Flags
*** x - x      QUALID      QTID      QSD      VPFW      VPFS      QSO      VQO      QIFW      VIQC      QAGW      VAQC
101 117NH3+NH4      LBS      0      0      0      1      0      1      0      1      0
END QUAL-PROPS

QUAL-INPUT
***          Storage on surface and nonseasonal parameters
***          SQO      POTFW      POTFS      ACQOP      SQOLIM      WSQOP      IOQC      AOQC
*** <PLS > qty/ac qty/ton qty/ton      qty/      qty/ac      in/hr qty/ft3 qty/ft3
*** x - x          ac.day
101          0.1      0.      0.      0.0817      0.3      1.2 1.6E-05 4.0E-06
  
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

```

102      0.1      0.      0.      0.0841      0.3      1.2 1.6E-05 4.0E-06
103      0.1      0.      0.      0.0846      0.3      1.2 1.6E-05 4.0E-06
104      0.1      0.      0.      0.0860      0.3      1.2 1.6E-05 4.0E-06
105      0.0      0.      0.      0.0010      0.1      0.4 1.6E-05 4.0E-06
106      0.1      0.      0.      0.0900      0.2      1.4 1.6E-05 4.0E-06
107      0.1      0.      0.      0.0900      0.2      1.4 1.6E-05 4.0E-06
108      0.1      0.      0.      0.0900      0.2      1.4 1.6E-05 4.0E-06
109      0.1      0.      0.      0.0140      0.1      1.2 1.6E-05 4.0E-06
110      0.1      0.      0.      0.0140      0.3      0.4 1.6E-05 4.0E-06
111      0.1      0.      0.      0.0140      0.1      1.2 1.6E-05 4.0E-06
112      0.1      0.      0.      0.0140      0.1      1.2 1.6E-05 4.0E-06
113      0.01     0.      0.      0.0010      0.1      0.4 1.6E-05 4.0E-06
114      0.1      0.      0.      0.0900      0.2      1.4 1.6E-05 4.0E-06
115      0.1      0.      0.      0.0140      0.1      1.4 1.6E-05 4.0E-06
116      1.0      0.      0.      0.0841      3.0      1.2 1.6E-04 4.0E-05
117      0.1      0.      0.      0.0817      0.3      1.2 1.6E-05 4.0E-06
END QUAL-INPUT

```

```

QUAL-PROPS
*** <PLS > Identifiers and Flags
*** x - x      QUALID      QTID  QSD  VPFW  VPFS  QSO  VQO  QIFW  VIQC  QAGW  VAQC
101 117NO3      LBS    0    0    0    1    0    1    0    1    0
END QUAL-PROPS

```

```

QUAL-INPUT
*** Storage on surface and nonseasonal parameters
***      SQO  POTFW  POTFS  ACQOP  SQOLIM  WSQOP  IOQC  AOQC
*** <PLS > qty/ac qty/ton qty/ton  qty/  qty/ac  in/hr  qty/ft3  qty/ft3
*** x - x      ac.day
101 117      0.05      0.      0.      0.0057      0.1      0.7 6.2E-06 6.2E-06
END QUAL-INPUT

```

```

QUAL-PROPS
*** <PLS > Identifiers and Flags
*** x - x      QUALID      QTID  QSD  VPFW  VPFS  QSO  VQO  QIFW  VIQC  QAGW  VAQC
101 117ORTHO P  LBS    0    0    0    1    0    1    0    1    0
END QUAL-PROPS

```

```

QUAL-INPUT
*** Storage on surface and nonseasonal parameters
***      SQO  POTFW  POTFS  ACQOP  SQOLIM  WSQOP  IOQC  AOQC
*** <PLS > qty/ac qty/ton qty/ton  qty/  qty/ac  in/hr  qty/ft3  qty/ft3
*** x - x      ac.day
101      0.1      0.      0.      0.0750      0.2      1.2 3.2E-06 1.0E-06
102      0.1      0.      0.      0.0770      0.2      1.2 3.2E-06 1.0E-06
103      0.1      0.      0.      0.0780      0.2      1.2 3.2E-06 1.0E-06
104      0.1      0.      0.      0.0800      0.2      1.2 3.2E-06 1.0E-06
105      0.1      0.      0.      0.0010      0.1      0.4 3.2E-06 1.0E-06
106 107      0.1      0.      0.      0.0076      0.1      1.4 3.2E-06 1.0E-06
108      0.1      0.      0.      0.0076      0.1      1.4 3.2E-06 1.0E-06
109      0.1      0.      0.      0.0088      0.1      1.2 3.2E-06 1.0E-06
110      0.1      0.      0.      0.0088      0.1      0.4 3.2E-06 1.0E-06
111 112      0.1      0.      0.      0.0088      0.1      1.2 3.2E-06 1.0E-06
113      0.01     0.      0.      0.0010      0.1      1.2 3.2E-06 1.0E-06
114      0.1      0.      0.      0.0076      0.1      1.4 3.2E-06 1.0E-06
115      0.1      0.      0.      0.0088      0.1      1.4 3.2E-06 1.0E-06
116      1.0      0.      0.      0.0770      2.0      1.2 3.2E-05 1.0E-05
117      0.1      0.      0.      0.0770      0.2      1.2 3.2E-06 1.0E-06
END QUAL-INPUT

```

```

QUAL-PROPS
*** <PLS > Identifiers and Flags
*** x - x      QUALID      QTID  QSD  VPFW  VPFS  QSO  VQO  QIFW  VIQC  QAGW  VAQC

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

```

101 117BOD          LBS      0      0      0      1      0      1      0      1      0
END QUAL-PROPS

QUAL-INPUT
*** Storage on surface and nonseasonal parameters
***      SQO      POTFW      POTFS      ACQOP      SQOLIM      WSQOP      IOQC      AOQC
*** <PLS > qty/ac qty/ton qty/ton qty/ ac.day qty/ac in/hr qty/ft3 qty/ft3
*** x - x
101      1.      0.      0.      0.65      5.      0.7 2.5E-04 6.2E-05
102      1.      0.      0.      0.69      5.      0.7 2.5E-04 6.2E-05
103      1.      0.      0.      0.70      5.      0.7 2.5E-04 6.2E-05
104      1.      0.      0.      0.73      5.      0.5 2.5E-04 6.2E-05
105      0.1     0.      0.      0.03      1.      0.5 2.5E-04 6.2E-05
106      1.      0.      0.      0.43      5.      1.4 2.5E-04 6.2E-05
107      1.      0.      0.      0.43      5.      1.4 2.5E-04 6.2E-05
108      1.      0.      0.      0.43      5.      1.4 2.5E-04 6.2E-05
109      1.      0.      0.      0.19      3.      0.7 2.5E-04 6.2E-05
110      1.      0.      0.      0.19      5.      0.7 2.5E-04 6.2E-05
111      1.      0.      0.      0.19      3.      0.7 2.5E-04 6.2E-05
112      1.      0.      0.      0.19      3.      0.7 2.5E-04 6.2E-05
113      0.1     0.      0.      0.01      0.1     0.7 2.5E-04 6.2E-05
114      1.      0.      0.      0.43      5.      1.4 2.5E-04 6.2E-05
115      1.      0.      0.      0.19      3.      1.4 2.5E-04 6.2E-05
116      10.     0.      0.      0.69      50.     0.7 2.5E-03 6.2E-04
117      1.      0.      0.      0.69      5.      1.1 2.5E-04 6.2E-05
END QUAL-INPUT

END PERLND

IMPLND
ACTIVITY
*** <ILS > Active Sections
*** x - x ATMP SNOW IWAT SLD IWG IQAL
101 104 1 0 1 1 1 1
END ACTIVITY

PRINT-INFO
*** <ILS > ***** Print-flags ***** PIVL PYR
*** x - x ATMP SNOW IWAT SLD IWG IQAL *****
101 104 4 4 4 4 4 1 12
END PRINT-INFO

BINARY-INFO
*** <ILS > **** Binary-Output-flags **** PIVL PYR
*** x - x ATMP SNOW IWAT SLD IWG IQAL *****
101 104 4 4 4 4 4 1 12
END BINARY-INFO

GEN-INFO
*** Name Unit-systems Printer BinaryOut
*** <ILS > t-series Engl Metr Engl Metr
*** x - x in out
101 Developed Open Space 1 1 0 0 92 0
102 Developed Low Intens 1 1 0 0 92 0
103 Developed Medium Int 1 1 0 0 92 0
104 Developed High Inten 1 1 0 0 92 0
END GEN-INFO

ATEMP-DAT
*** <ILS > ELDAT AIRTEMP
*** x - x (ft) (deg F)
101 104 -6. 33.
END ATEMP-DAT

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

```
IWAT-PARM1
*** <ILS >           Flags
*** x - x CSNO RTOP  VRS  VNN  RTLI
    101 104   0   1   0   0   0
    END IWAT-PARM1

IWAT-PARM2
*** <ILS >           LSUR           SLSUR           NSUR           RETSC
*** x - x           (ft)           0.0028           0.07           (in)
    101 104   100.           0.0028           0.07           0.07
    END IWAT-PARM2

IWAT-PARM3
*** <ILS >           PETMAX           PETMIN
*** x - x           (deg F)           (deg F)
    101 104   40.           35.
    END IWAT-PARM3

IWAT-STATE1
*** <ILS > IWATER state variables (inches)
*** x - x           RETS           SURS
    101 104   0.           0.
    END IWAT-STATE1

SLD-PARM1
*** <ILS >           Flags
*** x - x VASD VRSD SDOP
    101 104   0   0   1
    END SLD-PARM1

SLD-PARM2
*** <ILS >           KEIM           JEIM           ACCSDP           REMSDP
*** x - x           0.2           2.           ac.day           /day
    101 104   0.2           2.           0.010           0.01
    END SLD-PARM2

SLD-STOR
*** <ILS > Solids storage (tons/acre)
*** x - x
    101 104   0.01
    END SLD-STOR

IWT-PARM1
*** <ILS > Flags for section IWTGAS
*** x - x WTFV CSNO
    101 104   0   0
    END IWT-PARM1

IWT-PARM2
*** <ILS >           Second group of IWTGAS parms
*** x - x           ELEV           AWTF           BWTF
*** x - x           (ft)           (deg F)           (deg F/F)
    101 104   20.           40.           0.3
    END IWT-PARM2

NQUALS
*** <ILS >
*** x - xNQUAL
    101 104   4
    END NQUALS
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

```

IQL-AD-FLAGS
***
***           Atmospheric Deposition Flags
*** < ILS>  QUAL1  QUAL2  QUAL3  QUAL4  QUAL5  QUAL6  QUAL7  QUAL8  QUAL9  QUAL10
*** x  - x <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C>
101 104 -1 0 -1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
END IQL-AD-FLAGS

```

```

QUAL-PROPS
*** < ILS >  Identifiers and Flags
*** x  - x      QUALID  QTID  QSD  VPFW  QSO  VQO
101 104NH3+NH4      LBS    0    0    1    0
END QUAL-PROPS

```

```

QUAL-INPUT
***           Storage on surface and nonseasonal parameters
***           SQO  POTFW  ACQOP  SQOLIM  WSQOP
*** < ILS >  qty/ac qty/ton  qty/  qty/ac  in/hr
*** x  - x           ac.day
101 104 0.10      0.    0.08    0.3    0.3
END QUAL-INPUT

```

```

QUAL-PROPS
*** < ILS >  Identifiers and Flags
*** x  - x      QUALID  QTID  QSD  VPFW  QSO  VQO
101 104NO3      LBS    0    0    1    0
END QUAL-PROPS

```

```

QUAL-INPUT
***           Storage on surface and nonseasonal parameters
***           SQO  POTFW  ACQOP  SQOLIM  WSQOP
*** < ILS >  qty/ac qty/ton  qty/  qty/ac  in/hr
*** x  - x           ac.day
101 104 0.10      0.    0.01    0.20    0.2
END QUAL-INPUT

```

```

QUAL-PROPS
*** < ILS >  Identifiers and Flags
*** x  - x      QUALID  QTID  QSD  VPFW  QSO  VQO
101 104ORTHO P  LBS    0    0    1    0
END QUAL-PROPS

```

```

QUAL-INPUT
***           Storage on surface and nonseasonal parameters
***           SQO  POTFW  ACQOP  SQOLIM  WSQOP
*** < ILS >  qty/ac qty/ton  qty/  qty/ac  in/hr
*** x  - x           ac.day
101 104 0.10      0.    0.08    0.20    0.3
END QUAL-INPUT

```

```

QUAL-PROPS
*** < ILS >  Identifiers and Flags
*** x  - x      QUALID  QTID  QSD  VPFW  QSO  VQO
101 104BOD      LBS    0    0    1    0
END QUAL-PROPS

```

```

QUAL-INPUT
***           Storage on surface and nonseasonal parameters
***           SQO  POTFW  ACQOP  SQOLIM  WSQOP
*** < ILS >  qty/ac qty/ton  qty/  qty/ac  in/hr
*** x  - x           ac.day
101 104 1.0       0.    0.70    5.    0.3
END QUAL-INPUT

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

END IMPLND

RCHRES

ACTIVITY
 *** RCHRES Active sections
 *** x - x HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG
 1 12 1 2 0 1 1 0 1 1 1 0
 END ACTIVITY

PRINT-INFO
 *** RCHRES Printout level flags
 *** x - x HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR
 1 12 4 4 4 4 4 4 4 4 1 12
 END PRINT-INFO

BINARY-INFO
 *** RCHRES Binary Output level flags
 *** x - x HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR
 1 12 4 4 4 4 4 4 4 4 1 12
 END BINARY-INFO

GEN-INFO
 *** Name Nexits Unit Systems Printer
 *** RCHRES t-series Engr Metr LKFG
 *** x - x in out
 1 Gum Gully 1 1 1 91 0 0 92 0
 2 Adams Headwaters 1 1 1 91 0 0 92 0
 3 Gum Gully Lower Rch 1 1 1 91 0 0 92 0
 4 Adams Lateral 8 1 1 1 91 0 0 92 0
 5 Adams Bayou abv I10 1 1 1 91 0 0 92 0
 6 Adams abv confl Gum 1 1 1 91 0 0 92 0
 7 Adams Bayou abv Park 1 1 1 91 0 0 92 0
 8 Hudson Gully 1 1 1 91 0 0 92 0
 9 Adams Lateral 2 1 1 1 91 0 0 92 0
 10 Adams above Western 1 1 1 91 0 0 92 0
 11 Adams Lateral 1 1 1 1 91 0 0 92 0
 12 Adams Bayou mouth 1 1 1 91 0 0 92 0
 END GEN-INFO

HYDR-PARM1
 *** Flags for HYDR section
 ***RC HRES VC A1 A2 A3 ODFVFG for each *** ODGTFG for each FUNCT for each
 *** x - x FG FG FG FG possible exit *** possible exit possible exit
 1 12 0 1 1 1 4 0 0 0 0 0 0 0 0 0 0 0 1 1 1 1 1
 END HYDR-PARM1

HYDR-PARM2
 *** RCHRES FTBW FTBU LEN DELTH STCOR KS DB50
 *** x - x (miles) (ft) (ft) (in)
 1 0. 1. 1.85 9. 3.2 0.5 0.004
 2 0. 2. 5.75 15. 3.2 0.5 0.004
 3 0. 3. 0.6 0.1 3.2 0.5 0.004
 4 0. 4. 1.5 9.5 3.2 0.5 0.004
 5 0. 5. 1.41 2.8 3.2 0.5 0.004
 6 0. 6. 1.09 0.1 3.2 0.5 0.004
 7 0. 7. 2.03 0.2 3.2 0.5 0.004
 8 0. 8. 0.98 6.9 3.2 0.5 0.004
 9 0. 9. 1.4 4. 3.2 0.5 0.004
 10 0. 10. 3.25 1.6 3.2 0.5 0.004
 11 0. 11. 2.43 7.5 3.2 0.5 0.004
 12 0. 12. 2.42 0.1 3.2 0.5 0.004
 END HYDR-PARM2

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

```

HYDR-INIT
***      Initial conditions for HYDR section
***RC HRES      VOL  CAT Initial value of COLIND      initial value of OUTDGT
*** x  - x      ac-ft      for each possible exit  for each possible exit,ft3
    1  12      0.01      4.2 4.5 4.5 4.5 4.2      2.1 1.2 0.5 1.2 1.8
END HYDR-INIT

ADCALC-DATA
*** RCHRES Data for section ADCALC
*** x  - x      CRRAT      VOL (ac-ft)
    1  12      1.7      100.
END ADCALC-DATA

HT-BED-FLAGS
*** RCHRES Bed Heat Conductance Flags
*** x  - x BDFG TGFG TSTP
    1  12      1      3      55
END HT-BED-FLAGS

HEAT-PARM
*** RCHRES      ELEV      ELDAT      CFSAXE      KATRAD      KCOND      KEVAP
*** x  - x      (ft)      (ft)
    1      0.      -16.      0.05      9.37      6.12      2.24
    2      0.      -16.      0.35      9.37      6.12      2.24
    3      0.      -16.      0.15      9.37      6.12      2.24
    4      0.      -16.      0.25      9.37      6.12      2.24
    5      0.      -16.      0.45      9.37      6.12      2.24
    6      0.      -16.      0.45      9.37      6.12      2.24
    7      0.      -16.      0.45      9.37      6.12      2.24
    8      0.      -16.      0.25      9.37      6.12      2.24
    9      0.      -16.      0.25      9.37      6.12      2.24
   10      0.      -16.      0.65      9.37      6.12      2.24
   11      0.      -16.      0.25      9.37      6.12      2.24
   12      0.      -16.      0.75      9.37      6.12      2.24
END HEAT-PARM

HT-BED-PARM
***      Bed Heat Conduction Parameters for Single and Two-layer Methods
*** RCHRES      MUDDEP      TGRND      KMUD      KGRND
*** x  - x      (ft)      (deg F)      (kcal/m2/C/hr)
    1  12      0.8      70.      20.      1.4
END HT-BED-PARM

MON-HT-TGRND
*** RCHRES Monthly values of ground temperatures (deg F)
*** x  - x TG1 TG2 TG3 TG4 TG5 TG6 TG7 TG8 TG9 TG10 TG11 TG12
    1  12 56. 55. 58. 63. 68. 74. 79. 82. 81. 75. 68. 60.
END MON-HT-TGRND

HEAT-INIT
*** RCHRES      TW      AIRTMP
*** x  - x      (deg F)      (deg F)
    1  12      48.      40.
END HEAT-INIT

SANDFG
*** RCHRES
*** x  - x SNDFG
    1  12      3
END SANDFG

SED-GENPARG
*** RCHRES      BEDWID      BEDWRN      POR

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

```

*** x - x      (ft)      (ft)
    1          13.       6.       0.3
    2          40.       6.       0.3
    3          14.       6.       0.3
    4          12.       6.       0.3
    5          90.       6.       0.35
    6          60.       6.       0.28
    7         190.       6.       0.43
    8          16.       6.       0.3
    9          25.       6.       0.3
   10         230.       6.       0.49
   11          22.       6.       0.3
   12         220.       6.       0.55
    
```

END SED-GENPARM

SAND-PM

```

*** RCHRES      D          W          RHO          KSAND          EXPSND
*** x - x      (in)      (in/sec)  (gm/cm3)
    1          0.0100      1.0       2.65          0.8            3.2
    2          0.0100      1.0       2.65          0.8            3.2
    3          0.0100      1.0       2.65          0.8            3.2
    4          0.0100      1.0       2.65          0.8            3.2
    5          0.0100      1.0       2.65          0.8            3.2
    6          0.0100      1.0       2.65          0.8            3.2
    7          0.0100      1.0       2.65          0.8            3.2
    8          0.0100      1.0       2.65          0.8            3.2
    9          0.0100      1.0       2.65          0.8            3.2
   10          0.0100      1.0       2.65          0.8            3.2
   11          0.0100      1.0       2.65          0.8            3.2
   12          0.0100      1.0       2.65          0.8            3.2
    
```

END SAND-PM

SILT-CLAY-PM

```

*** RCHRES      D          W          RHO          TAUCD          TAUCS          M
*** x - x      (in)      (in/sec)  gm/cm3      lb/ft2         lb/ft2         lb/ft2.d
    1          0.00063      0.003     2.20         0.02           0.050          0.05
    2          0.00063      0.003     2.20         0.02           0.050          0.05
    3          0.00063      0.003     2.20         0.01           0.020          0.05
    4          0.00063      0.003     2.20         0.02           0.050          0.05
    5          0.00063      0.003     2.20         0.02           0.050          0.05
    6          0.00063      0.003     2.20         0.02           0.050          0.05
    7          0.00063      0.003     2.20         0.02           0.050          0.05
    8          0.00063      0.003     2.20         0.02           0.050          0.05
    9          0.00063      0.003     2.20         0.02           0.050          0.05
   10          0.00063      0.003     2.20         0.02           0.050          0.05
   11          0.00063      0.003     2.20         0.02           0.050          0.05
   12          0.00063      0.003     2.20         0.02           0.050          0.05
    
```

END SILT-CLAY-PM

SILT-CLAY-PM

```

*** RCHRES      D          W          RHO          TAUCD          TAUCS          M
*** x - x      (in)      (in/sec)  gm/cm3      lb/ft2         lb/ft2         lb/ft2.d
    1          0.00006      0.00002   2.00         0.015          0.045          0.05
    2          0.00006      0.00002   2.00         0.015          0.045          0.05
    3          0.00006      0.00002   2.00         0.010          0.020          0.05
    4          0.00006      0.00002   2.00         0.015          0.045          0.05
    5          0.00006      0.00002   2.00         0.015          0.045          0.05
    6          0.00006      0.00002   2.00         0.015          0.045          0.05
    7          0.00006      0.00002   2.00         0.015          0.045          0.05
    8          0.00006      0.00002   2.00         0.015          0.045          0.05
    9          0.00006      0.00002   2.00         0.015          0.045          0.05
   10          0.00006      0.00002   2.00         0.015          0.045          0.05
   11          0.00006      0.00002   2.00         0.015          0.045          0.05
    
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

```

12          0.00006  0.00002    2.00    0.015    0.045    0.05
END SILT-CLAY-PM

SSED-INIT
*** RCHRES      Suspended sed concs (mg/l)
*** x - x      Sand      Silt      Clay
1  12          1.        5.        10.
END SSED-INIT

BED-INIT
*** RCHRES      BEDDEP  Initial bed composition
*** x - x      (ft)     Sand      Silt      Clay
1              1.5     0.96     0.02     0.02
2              1.5     0.96     0.02     0.02
3              1.5     0.50     0.25     0.25
4              1.5     0.96     0.02     0.02
5              1.5     0.70     0.15     0.15
6              1.5     0.70     0.15     0.15
7              1.5     0.66     0.15     0.19
8              1.5     0.96     0.02     0.02
9              1.5     0.96     0.02     0.02
10             1.5     0.63     0.08     0.29
11             1.5     0.86     0.05     0.09
12             1.5     0.36     0.10     0.54
END BED-INIT

BENTH-FLAG
*** RCHRES      Benthic release flag
*** x - x      BENF
1  12          1
END BENTH-FLAG

OX-FLAGS
*** RCHRES      Oxygen flags
*** x - x      REAM
1  12          2
END OX-FLAGS

OX-GENPARM
*** RCHRES      KBOD20      TCBOD      KODSET      SUPSAT
*** x - x      /hr          ft/hr
1  12          0.002      1.047      0.001      1.
END OX-GENPARM

OX-BENPARM
*** RCHRES      BENOD      TCBEN      EXPOD      BRBOD (1)  BRBOD (2)  EXPREL
*** x - x      mg/m2.hr    mg/m2.hr  mg/m2.hr  mg/m2.hr  mg/m2.hr
1  12          150.      1.074      1.22      0.1      0.1      2.82
END OX-BENPARM

OX-TCGINV
*** RCHRES      Temperature Correction Coefficient
*** x - x      TCGINV
1  12          1.047
END OX-TCGINV

OX-INIT
*** RCHRES      DOX      BOD      SATDO
*** x - x      mg/l     mg/l     mg/l
1  12          8.      3.5     13.5
END OX-INIT

NUT-FLAGS

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

```

*** RCHRES Nutrient flags
*** x - x NH3 NO2 PO4 AMV DEN ADNH ADPO PHFL
      1 12 1 0 1 0 1 0 1 2
END NUT-FLAGS

CONV-VAL1
*** RCHRES CVBO CVBPC CVBPN BPCNTC
*** x - x mg/mg mols/mol mols/mol
      1 12 1.63 106. 16. 49.
END CONV-VAL1

NUT-BENPARM
*** RCHRES BRNIT(1) BRNIT(2) BRPO4(1) BRPO4(2) ANAER
*** x - x mg/m2.hr mg/m2.hr mg/m2.hr mg/m2.hr mg/l
      1 12 0. 0. 0. 0. 0.1
END NUT-BENPARM

NUT-NITDENIT
*** RCHRES KTAM20 KNO220 TCNIT KNO320 TCDEN DENOXT
*** x - x /hr /hr /hr /hr mg/l
      1 12 0.01 0.002 1.07 0.02 1.04 5.
END NUT-NITDENIT

NUT-ADSPARM
*** RCHRES Partition coefficients for NH4 AND PO4 (ml/g)
*** x - x NH4-sand NH4-silt NH4-clay PO4-sand PO4-silt PO4-clay
      1 12 1E-10 1E-10 1E-10 1E-10 0.1 50.
END NUT-ADSPARM

NUT-DINIT
*** RCHRES NO3 TAM NO2 PO4 PHVAL
*** x - x mg/l mg/l mg/l mg/l
      1 12 0.1 0.1 0.01 0.05 7.
END NUT-DINIT

PLNK-FLAGS
*** RCHRES Plankton flags
*** x - x PHYF ZOOF BALF SDLT AMRF DECF NSFQ ZFOO BNP
      1 12 1 0 1 0 0 1 1 2 0
END PLNK-FLAGS

PLNK-PARM1
***RC HRES RATCLP NONREF LITSED ALNPR EXTB MALGR PARADF
*** x - x 1/mg.ft /ft /hr
      1 12 0.68 0.5 0. 0.75 0.3 0.085 1.
END PLNK-PARM1

PLNK-PARM2
***RC HRES CMLLT CMMN CMMNP CMP TALGRH TALGRL TALGRM
*** x - x ly/min mg/l mg/l mg/l deg F deg F deg F
      1 12 0.01 0.025 0.0001 0.005 95. -20. 86.
END PLNK-PARM2

PLNK-PARM3
*** RCHRES ALR20 ALDH ALDL OXALD NALDH PALDH
*** x - x /hr /hr /hr /hr mg/l mg/l
      1 12 0.005 0.020 0.001 0.03 0.010 0.002
END PLNK-PARM3

PHYTO-PARM
*** RCHRES SEED MXSTAY OREF CLALDH PHYSET REFSET
*** x - x mg/l mg/l ft3/s ug/l ft/hr ft/hr
      1 12 1. 2. 100. 20. 0.020 0.025
  
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

END PHYTO-PARM

BENAL-PARM

***RC	HRES	MBAL	CFBALR	CFBALG	MINBAL	CAMPR	FRAVL	NMAXFX
*** x	- x	mg/m2			mg/m2	mg/l		mg/l
1	12	2500.	0.35	1.	0.0001	0.001	0.	10.

END BENAL-PARM

PLNK-INIT

***	RCHRES	PHYTO	ZOO	BENAL	ORN	ORP	ORC
*** x	- x	mg/l	org/l	mg/m2	mg/l	mg/l	mg/l
1	12	0.5	0.03	2500.	0.5	0.1	0.5

END PLNK-INIT

END RCHRES

FTABLES

FTABLE 1

rows	cols				***
8	4				
depth	area	volume	outflow1	***	
0.	0.	0.	0.		
1.	0.45	0.2	0.		
2.	1.39	1.1	0.		
3.	1.61	2.6	0.1		
5.	3.6	7.8	3.		
6.	4.5	11.9	37.		
8.	44.8	61.2	410.		
11.	112.1	296.7	3969.		

END FTABLE 1

FTABLE 2

rows	cols				***
8	4				
depth	area	volume	outflow1	***	
0.	0.	0.	0.		
1.	6.	3.	0.		
2.	22.3	17.1	0.		
3.	25.8	41.2	0.1		
5.	32.1	99.	3.		
8.	41.8	209.9	211.		
11.	348.5	795.3	1712.		
14.	697.	2363.5	10173.		

END FTABLE 2

FTABLE 3

rows	cols				***
8	4				
depth	area	volume	outflow1	***	
0.	0.	0.	0.		
1.	0.15	0.1	0.		
2.	0.45	0.4	0.		
3.	0.52	0.9	1.18		
5.	1.2	2.5	11.		
6.	1.5	3.9	37.		
8.	14.5	19.9	410.		
11.	36.4	96.2	3969.		

END FTABLE 3

FTABLE 4

rows	cols				***
8	4				

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

depth	area	volume	outflow1	***
0.	0.	0.	0.	
1.	0.36	0.2	0.	
2.	1.13	0.9	0.	
3.	1.31	2.1	0.1	
5.	2.9	6.4	3.	
6.	3.6	9.6	37.	
8.	36.4	49.6	410.	
11.	90.9	240.5	3969.	

END FTABLE 4

FTABLE 6

rows cols ***
9 4

depth	area	volume	outflow1	***
0.	0.	0.	0.	
1.	3.17	2.	0.	
2.	3.57	5.4	0.	
3.	5.95	10.1	0.7	
5.	7.3	23.3	18.	
7.	8.5	39.	89.	
9.	9.5	57.	302.	
12.	79.3	190.2	2159.	
15.	158.5	546.9	12419.	

END FTABLE 6

FTABLE 5

rows cols ***
11 4

depth	area	volume	outflow1	***
0.	0.	0.	0.	
1.	6.3	2.6	0.	
2.	7.7	9.6	0.	
4.	10.2	27.5	0.	
6.	12.	49.7	0.	
8.	12.8	74.5	0.	
10.	14.2	101.5	0.	
12.	16.4	132.1	77.	
14.	18.8	167.3	294.	
17.	68.4	298.1	1221.	
20.	170.9	657.	7688.	

END FTABLE 5

FTABLE 7

rows cols ***
11 4

depth	area	volume	outflow1	***
0.	0.	0.	0.	
1.	3.42	1.7	0.	
2.	5.98	6.4	0.	
4.	8.55	20.9	0.	
6.	19.7	49.1	0.	
8.	27.3	96.1	0.	
10.	34.2	157.7	0.	
12.	37.8	229.6	134.	
14.	68.4	335.8	589.	
17.	136.7	643.4	2635.	
20.	170.9	1104.8	12929.	

END FTABLE 7

FTABLE 8

rows cols ***
7 4

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

```

depth      area      volume  outflow1 ***
0.          0.         0.       0.
1.         1.88        1.7      0.
2.         1.92        3.6      0.
3.         2.14        5.6      4.71
5.         2.4         10.1     26.
6.        35.6        29.1     172.
8.       118.8       183.5    3090.
END FTABLE 8

```

```

FTABLE      9
rows cols          ***
 7      4
depth      area      volume  outflow1 ***
0.          0.         0.       0.
1.         4.24        3.9      0.
2.         4.41        8.2      0.
4.         4.58       17.2     10.15
6.         5.1         26.9     48.
8.        33.9        65.9     272.
10.       84.8       184.7    2177.
END FTABLE 9

```

```

FTABLE      10
rows cols          ***
11      4
depth      area      volume  outflow1 ***
0.          0.         0.       0.
1.         5.13        2.6      0.
2.        11.96       11.1     0.
4.        15.38       38.5     0.
6.        23.9       77.8     0.
8.        27.3       129.     0.
10.       37.6       194.     0.
12.       41.        273.     160.
14.       44.4       358.     629.
17.       68.4       527.     2160.
22.      256.4      1339.    15670.
END FTABLE 10

```

```

FTABLE      11
rows cols          ***
 9      4
depth      area      volume  outflow1 ***
0.          0.         0.       0.
1.         3.83        1.8      0.
2.         6.19        6.8      0.
3.         6.48       13.1     0.
5.         6.8         26.4     9.
7.         7.1         40.2     41.
9.         8.8         56.1     133.
11.        117.8      182.8    931.
14.       235.6      712.9    7262.
END FTABLE 11

```

```

FTABLE      12
rows cols          ***
11      4
depth      area      volume  outflow1 ***
0.          0.         0.       0.
1.         4.1         2.1      0.
2.         5.98        7.1      0.
4.         8.55       21.6     0.

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

```

6.      11.1     41.3     0.
8.      20.5     72.9     0.
10.     23.9     117.3    0.
12.     28.2     169.5    99.
14.     33.      230.6   405.
17.     102.5   433.9   1777.
22.     341.8   1544.8  18078.
  
```

END FTABLE 12
 END FTABLES

COPY
 TIMESERIES
 Copy-opn***
 *** x - x NPT NMN
 1 12 0 7
 END TIMESERIES

END COPY

EXT SOURCES

```

<-Volume-> <Member> SsysSgap<--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name> x <Name> x tem strg<-factor->strg <Name> x x <Name> x x ***
*** Met Seg ORANGE
WDM2 27 PREC ENGL SAME PERLND 101 117 EXTNL PREC
WDM2 28 ATEM ENGL SAME PERLND 101 117 EXTNL GATMP
WDM2 29 DEWP ENGL SAME PERLND 101 117 EXTNL DTMPG
WDM2 25 WIND ENGL SAME PERLND 101 117 EXTNL WINMOV
WDM2 26 SOLR ENGL SAME PERLND 101 117 EXTNL SOLRAD
WDM2 31 PEVT ENGL SAME PERLND 101 117 EXTNL PETINP
*** Met Seg ORANGE
WDM2 27 PREC ENGL SAME IMPLND 101 104 EXTNL PREC
WDM2 28 ATEM ENGL SAME IMPLND 101 104 EXTNL GATMP
WDM2 29 DEWP ENGL SAME IMPLND 101 104 EXTNL DTMPG
WDM2 25 WIND ENGL SAME IMPLND 101 104 EXTNL WINMOV
WDM2 26 SOLR ENGL SAME IMPLND 101 104 EXTNL SOLRAD
WDM2 31 PEVT ENGL SAME IMPLND 101 104 EXTNL PETINP
*** Met Seg ORANGE
WDM2 27 PREC ENGL SAME RCHRES 1 12 EXTNL PREC
WDM2 28 ATEM ENGL SAME RCHRES 1 12 EXTNL GATMP
WDM2 29 DEWP ENGL SAME RCHRES 1 12 EXTNL DEWTMP
WDM2 25 WIND ENGL SAME RCHRES 1 12 EXTNL WIND
WDM2 26 SOLR ENGL SAME RCHRES 1 12 EXTNL SOLRAD
WDM2 30 CLOU ENGL SAME RCHRES 1 12 EXTNL CLOUD
WDM2 34 EVAP ENGL SAME RCHRES 1 12 EXTNL POTEV
WDM3 8011 BOD ENGL 9.9DIV RCHRES 1 INFLOW OXIF 2
WDM3 8012 TSS ENGL 9.9DIV RCHRES 1 INFLOW ISED 2
WDM3 8014 DNH3 ENGL 9.9DIV RCHRES 1 INFLOW NUIF1 2
WDM3 8015 DPO4 ENGL 9.9DIV RCHRES 1 INFLOW NUIF1 4
WDM3 7001 FLOW ENGL 0DIV RCHRES 1 INFLOW IVOL
WDM3 7002 BOD ENGL 0DIV RCHRES 1 INFLOW OXIF 2
WDM3 7003 DNH3 ENGL 0DIV RCHRES 1 INFLOW NUIF1 2
WDM3 8011 BOD ENGL 54.3DIV RCHRES 2 INFLOW OXIF 2
WDM3 8012 TSS ENGL 54.3DIV RCHRES 2 INFLOW ISED 2
WDM3 8014 DNH3 ENGL 54.3DIV RCHRES 2 INFLOW NUIF1 2
WDM3 8015 DPO4 ENGL 54.3DIV RCHRES 2 INFLOW NUIF1 4
WDM3 7001 FLOW ENGL 0DIV RCHRES 2 INFLOW IVOL
WDM3 7002 BOD ENGL 0DIV RCHRES 2 INFLOW OXIF 2
WDM3 7003 DNH3 ENGL 0DIV RCHRES 2 INFLOW NUIF1 2
WDM3 8011 BOD ENGL 8.3DIV RCHRES 3 INFLOW OXIF 2
WDM3 8012 TSS ENGL 8.3DIV RCHRES 3 INFLOW ISED 2
WDM3 8014 DNH3 ENGL 8.3DIV RCHRES 3 INFLOW NUIF1 2
WDM3 8015 DPO4 ENGL 8.3DIV RCHRES 3 INFLOW NUIF1 4
WDM3 7001 FLOW ENGL 0DIV RCHRES 3 INFLOW IVOL
  
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

WDM3	7002	BOD	ENGL	0DIV	RCHRES	3	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	3	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	8.2DIV	RCHRES	4	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	8.2DIV	RCHRES	4	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	8.2DIV	RCHRES	4	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	8.2DIV	RCHRES	4	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	4	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0DIV	RCHRES	4	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	4	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	6.2DIV	RCHRES	6	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	6.2DIV	RCHRES	6	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	6.2DIV	RCHRES	6	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	6.2DIV	RCHRES	6	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	6	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0DIV	RCHRES	6	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	6	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	3.2DIV	RCHRES	5	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	3.2DIV	RCHRES	5	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	3.2DIV	RCHRES	5	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	3.2DIV	RCHRES	5	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	5	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0DIV	RCHRES	5	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	5	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	0.1DIV	RCHRES	7	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	0.1DIV	RCHRES	7	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	0.1DIV	RCHRES	7	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	0.1DIV	RCHRES	7	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	7	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0DIV	RCHRES	7	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	7	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	3.3DIV	RCHRES	8	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	3.3DIV	RCHRES	8	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	3.3DIV	RCHRES	8	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	3.3DIV	RCHRES	8	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	8	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0DIV	RCHRES	8	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	8	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	0.1DIV	RCHRES	9	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	0.1DIV	RCHRES	9	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	0.1DIV	RCHRES	9	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	0.1DIV	RCHRES	9	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	9	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0DIV	RCHRES	9	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	9	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	0.7DIV	RCHRES	10	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	0.7DIV	RCHRES	10	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	0.7DIV	RCHRES	10	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	0.7DIV	RCHRES	10	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	10	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0DIV	RCHRES	10	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	10	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	1.9DIV	RCHRES	11	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	1.9DIV	RCHRES	11	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	1.9DIV	RCHRES	11	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	1.9DIV	RCHRES	11	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	11	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0DIV	RCHRES	11	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0DIV	RCHRES	11	INFLOW	NUIF1	2
WDM3	8011	BOD	ENGL	0.1DIV	RCHRES	12	INFLOW	OXIF	2
WDM3	8012	TSS	ENGL	0.1DIV	RCHRES	12	INFLOW	ISED	2
WDM3	8014	DNH3	ENGL	0.1DIV	RCHRES	12	INFLOW	NUIF1	2
WDM3	8015	DPO4	ENGL	0.1DIV	RCHRES	12	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0DIV	RCHRES	12	INFLOW	IVOL	

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

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WDM3 7002 BOD ENGL 0DIV RCHRES 12 INFLOW OXIF 2
WDM3 7003 DNH3 ENGL 0DIV RCHRES 12 INFLOW NUIF1 2
*** 6205 and 6206 are atmospheric deposition loads of NH3N and NO3N
WDM3 6206 NO3N ENGL DIV PERLND 101 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 101 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 102 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 102 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 103 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 103 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 104 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 104 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 105 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 105 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 106 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 106 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 107 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 107 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 108 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 108 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 109 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 109 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 110 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 110 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 111 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 111 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 112 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 112 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 113 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 113 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 114 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 114 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 115 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 115 EXTNL PQADFX 1 1
*** FAILING OSSF LOADS TO PERLND 116
*** 0.9 multiplier is fraction not flowing direct via pipe to ditch & stream
WDM3 8011 BOD ENGL 0.9DIV PERLND 116 EXTNL SLIQO 4
WDM3 8012 TSS ENGL 0.9DIV PERLND 116 EXTNL SLSSED 1
WDM3 8013 FLOW ENGL 0.9DIV PERLND 116 EXTNL SURLI 1
WDM3 8014 DNH3 ENGL 0.9DIV PERLND 116 EXTNL SLIQO 1
WDM3 8015 DPO4 ENGL 0.9DIV PERLND 116 EXTNL SLIQO 3
*** 6205 and 6206 are atmospheric deposition loads of NH3N and NO3N
WDM3 6206 NO3N ENGL DIV PERLND 116 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 116 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV PERLND 117 EXTNL PQADFX 2 1
WDM3 6205 NH3N ENGL DIV PERLND 117 EXTNL PQADFX 1 1
WDM3 6206 NO3N ENGL DIV IMPLND 101 EXTNL IQADFX 2 1
WDM3 6205 NH3N ENGL DIV IMPLND 101 EXTNL IQADFX 1 1
WDM3 6206 NO3N ENGL DIV IMPLND 102 EXTNL IQADFX 2 1
WDM3 6205 NH3N ENGL DIV IMPLND 102 EXTNL IQADFX 1 1
WDM3 6206 NO3N ENGL DIV IMPLND 103 EXTNL IQADFX 2 1
WDM3 6205 NH3N ENGL DIV IMPLND 103 EXTNL IQADFX 1 1
WDM3 6206 NO3N ENGL DIV IMPLND 104 EXTNL IQADFX 2 1
WDM3 6205 NH3N ENGL DIV IMPLND 104 EXTNL IQADFX 1 1
END EXT SOURCES

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SCHEMATIC

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***SOURCE ACRES TARGET MASS LINKAGE
PERLND 101 212 RCHRES 1 2
PERLND 102 87 RCHRES 1 2
PERLND 103 2 RCHRES 1 2
PERLND 104 0 RCHRES 1 2
PERLND 105 3 RCHRES 1 2
PERLND 106 0 RCHRES 1 2

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Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

PERLND 107	75	RCHRES	1	2
PERLND 108	18	RCHRES	1	2
PERLND 109	1127	RCHRES	1	2
PERLND 110	7	RCHRES	1	2
PERLND 111	0	RCHRES	1	2
PERLND 112	49	RCHRES	1	2
PERLND 113	14	RCHRES	1	2
PERLND 114	181	RCHRES	1	2
PERLND 115	7	RCHRES	1	2
PERLND 116	10	RCHRES	1	2
IMPLND 101	26	RCHRES	1	1
IMPLND 102	42	RCHRES	1	1
IMPLND 103	4	RCHRES	1	1
IMPLND 104	0	RCHRES	1	1
PERLND 101	931	RCHRES	2	2
PERLND 102	385	RCHRES	2	2
PERLND 103	26	RCHRES	2	2
PERLND 104	2	RCHRES	2	2
PERLND 105	0	RCHRES	2	2
PERLND 106	6	RCHRES	2	2
PERLND 107	778	RCHRES	2	2
PERLND 108	919	RCHRES	2	2
PERLND 109	3425	RCHRES	2	2
PERLND 110	500	RCHRES	2	2
PERLND 111	1044	RCHRES	2	2
PERLND 112	743	RCHRES	2	2
PERLND 113	22	RCHRES	2	2
PERLND 114	3792	RCHRES	2	2
PERLND 115	608	RCHRES	2	2
PERLND 116	54	RCHRES	2	2
IMPLND 101	115	RCHRES	2	1
IMPLND 102	182	RCHRES	2	1
IMPLND 103	41	RCHRES	2	1
IMPLND 104	11	RCHRES	2	1
PERLND 101	27	RCHRES	3	2
PERLND 102	64	RCHRES	3	2
PERLND 103	4	RCHRES	3	2
PERLND 104	0	RCHRES	3	2
PERLND 105	0	RCHRES	3	2
PERLND 106	0	RCHRES	3	2
PERLND 107	87	RCHRES	3	2
PERLND 108	37	RCHRES	3	2
PERLND 109	421	RCHRES	3	2
PERLND 110	0	RCHRES	3	2
PERLND 111	26	RCHRES	3	2
PERLND 112	2	RCHRES	3	2
PERLND 113	0	RCHRES	3	2
PERLND 114	417	RCHRES	3	2
PERLND 115	10	RCHRES	3	2
PERLND 116	8	RCHRES	3	2
IMPLND 101	3	RCHRES	3	1
IMPLND 102	31	RCHRES	3	1
IMPLND 103	7	RCHRES	3	1
IMPLND 104	0	RCHRES	3	1
RCHRES 1		RCHRES	3	3
PERLND 101	242	RCHRES	4	2
PERLND 102	164	RCHRES	4	2
PERLND 103	6	RCHRES	4	2
PERLND 104	1	RCHRES	4	2
PERLND 105	0	RCHRES	4	2
PERLND 106	0	RCHRES	4	2
PERLND 107	0	RCHRES	4	2
PERLND 108	0	RCHRES	4	2

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

PERLND 109	277	RCHRES	4	2
PERLND 110	253	RCHRES	4	2
PERLND 111	22	RCHRES	4	2
PERLND 112	1	RCHRES	4	2
PERLND 113	0	RCHRES	4	2
PERLND 114	159	RCHRES	4	2
PERLND 115	14	RCHRES	4	2
PERLND 116	8	RCHRES	4	2
IMPLND 101	30	RCHRES	4	1
IMPLND 102	74	RCHRES	4	1
IMPLND 103	9	RCHRES	4	1
IMPLND 104	8	RCHRES	4	1
PERLND 101	283	RCHRES	6	2
PERLND 102	240	RCHRES	6	2
PERLND 103	24	RCHRES	6	2
PERLND 104	2	RCHRES	6	2
PERLND 105	0	RCHRES	6	2
PERLND 106	0	RCHRES	6	2
PERLND 107	30	RCHRES	6	2
PERLND 108	13	RCHRES	6	2
PERLND 109	75	RCHRES	6	2
PERLND 110	30	RCHRES	6	2
PERLND 111	8	RCHRES	6	2
PERLND 112	0	RCHRES	6	2
PERLND 113	0	RCHRES	6	2
PERLND 114	409	RCHRES	6	2
PERLND 115	0	RCHRES	6	2
PERLND 116	6	RCHRES	6	2
IMPLND 101	35	RCHRES	6	1
IMPLND 102	105	RCHRES	6	1
IMPLND 103	38	RCHRES	6	1
IMPLND 104	13	RCHRES	6	1
RCHRES 2		RCHRES	6	3
RCHRES 4		RCHRES	6	3
PERLND 101	274	RCHRES	5	2
PERLND 102	331	RCHRES	5	2
PERLND 103	36	RCHRES	5	2
PERLND 104	4	RCHRES	5	2
PERLND 105	3	RCHRES	5	2
PERLND 106	0	RCHRES	5	2
PERLND 107	5	RCHRES	5	2
PERLND 108	12	RCHRES	5	2
PERLND 109	501	RCHRES	5	2
PERLND 110	0	RCHRES	5	2
PERLND 111	1	RCHRES	5	2
PERLND 112	10	RCHRES	5	2
PERLND 113	37	RCHRES	5	2
PERLND 114	504	RCHRES	5	2
PERLND 115	30	RCHRES	5	2
PERLND 116	3	RCHRES	5	2
IMPLND 101	34	RCHRES	5	1
IMPLND 102	143	RCHRES	5	1
IMPLND 103	60	RCHRES	5	1
IMPLND 104	31	RCHRES	5	1
RCHRES 6		RCHRES	5	3
RCHRES 3		RCHRES	5	3
PERLND 101	216	RCHRES	7	2
PERLND 102	215	RCHRES	7	2
PERLND 103	32	RCHRES	7	2
PERLND 104	6	RCHRES	7	2
PERLND 105	0	RCHRES	7	2
PERLND 106	0	RCHRES	7	2
PERLND 107	10	RCHRES	7	2

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

PERLND 108	90	RCHRES	7	2
PERLND 109	28	RCHRES	7	2
PERLND 110	0	RCHRES	7	2
PERLND 111	18	RCHRES	7	2
PERLND 112	0	RCHRES	7	2
PERLND 113	25	RCHRES	7	2
PERLND 114	190	RCHRES	7	2
PERLND 115	5	RCHRES	7	2
PERLND 116	0	RCHRES	7	2
IMPLND 101	27	RCHRES	7	1
IMPLND 102	92	RCHRES	7	1
IMPLND 103	52	RCHRES	7	1
IMPLND 104	45	RCHRES	7	1
RCHRES 5		RCHRES	7	3
PERLND 101	296	RCHRES	8	2
PERLND 102	289	RCHRES	8	2
PERLND 103	25	RCHRES	8	2
PERLND 104	5	RCHRES	8	2
PERLND 105	0	RCHRES	8	2
PERLND 106	0	RCHRES	8	2
PERLND 107	59	RCHRES	8	2
PERLND 108	39	RCHRES	8	2
PERLND 109	141	RCHRES	8	2
PERLND 110	0	RCHRES	8	2
PERLND 111	61	RCHRES	8	2
PERLND 112	0	RCHRES	8	2
PERLND 113	1	RCHRES	8	2
PERLND 114	20	RCHRES	8	2
PERLND 115	1	RCHRES	8	2
PERLND 116	3	RCHRES	8	2
IMPLND 101	37	RCHRES	8	1
IMPLND 102	125	RCHRES	8	1
IMPLND 103	40	RCHRES	8	1
IMPLND 104	38	RCHRES	8	1
PERLND 101	153	RCHRES	9	2
PERLND 102	244	RCHRES	9	2
PERLND 103	20	RCHRES	9	2
PERLND 104	2	RCHRES	9	2
PERLND 105	0	RCHRES	9	2
PERLND 106	99	RCHRES	9	2
PERLND 107	5	RCHRES	9	2
PERLND 108	54	RCHRES	9	2
PERLND 109	129	RCHRES	9	2
PERLND 110	9	RCHRES	9	2
PERLND 111	31	RCHRES	9	2
PERLND 112	0	RCHRES	9	2
PERLND 113	0	RCHRES	9	2
PERLND 114	14	RCHRES	9	2
PERLND 115	0	RCHRES	9	2
PERLND 116	0	RCHRES	9	2
IMPLND 101	19	RCHRES	9	1
IMPLND 102	104	RCHRES	9	1
IMPLND 103	33	RCHRES	9	1
IMPLND 104	16	RCHRES	9	1
PERLND 101	251	RCHRES	10	2
PERLND 102	658	RCHRES	10	2
PERLND 103	90	RCHRES	10	2
PERLND 104	25	RCHRES	10	2
PERLND 105	0	RCHRES	10	2
PERLND 106	20	RCHRES	10	2
PERLND 107	48	RCHRES	10	2
PERLND 108	27	RCHRES	10	2
PERLND 109	26	RCHRES	10	2

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

PERLND 110	0	RCHRES	10	2
PERLND 111	30	RCHRES	10	2
PERLND 112	1	RCHRES	10	2
PERLND 113	133	RCHRES	10	2
PERLND 114	209	RCHRES	10	2
PERLND 115	37	RCHRES	10	2
PERLND 116	1	RCHRES	10	2
IMPLND 101	31	RCHRES	10	1
IMPLND 102	282	RCHRES	10	1
IMPLND 103	148	RCHRES	10	1
IMPLND 104	200	RCHRES	10	1
RCHRES 7		RCHRES	10	3
RCHRES 8		RCHRES	10	3
PERLND 101	225	RCHRES	11	2
PERLND 102	155	RCHRES	11	2
PERLND 103	20	RCHRES	11	2
PERLND 104	4	RCHRES	11	2
PERLND 105	1	RCHRES	11	2
PERLND 106	24	RCHRES	11	2
PERLND 107	119	RCHRES	11	2
PERLND 108	148	RCHRES	11	2
PERLND 109	384	RCHRES	11	2
PERLND 110	0	RCHRES	11	2
PERLND 111	152	RCHRES	11	2
PERLND 112	11	RCHRES	11	2
PERLND 113	1	RCHRES	11	2
PERLND 114	41	RCHRES	11	2
PERLND 115	45	RCHRES	11	2
PERLND 116	2	RCHRES	11	2
IMPLND 101	28	RCHRES	11	1
IMPLND 102	67	RCHRES	11	1
IMPLND 103	33	RCHRES	11	1
IMPLND 104	30	RCHRES	11	1
PERLND 101	76	RCHRES	12	2
PERLND 102	188	RCHRES	12	2
PERLND 103	50	RCHRES	12	2
PERLND 104	8	RCHRES	12	2
PERLND 105	1	RCHRES	12	2
PERLND 106	0	RCHRES	12	2
PERLND 107	20	RCHRES	12	2
PERLND 108	15	RCHRES	12	2
PERLND 109	8	RCHRES	12	2
PERLND 110	27	RCHRES	12	2
PERLND 111	6	RCHRES	12	2
PERLND 112	6	RCHRES	12	2
PERLND 113	205	RCHRES	12	2
PERLND 114	16	RCHRES	12	2
PERLND 115	739	RCHRES	12	2
PERLND 116	0	RCHRES	12	2
IMPLND 101	9	RCHRES	12	1
IMPLND 102	81	RCHRES	12	1
IMPLND 103	81	RCHRES	12	1
IMPLND 104	65	RCHRES	12	1
RCHRES 10		RCHRES	12	3
RCHRES 11		RCHRES	12	3
RCHRES 9		RCHRES	12	3
***Sum the loads from all land segments in subbasin 1				
PERLND 101	212	COPY	1	4
PERLND 102	87	COPY	1	4
PERLND 103	2	COPY	1	4
PERLND 104	0	COPY	1	4
PERLND 105	3	COPY	1	4
PERLND 106	0	COPY	1	4

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

PERLND 107	75	COPY	1	4
PERLND 108	18	COPY	1	4
PERLND 109	1127	COPY	1	4
PERLND 110	7	COPY	1	4
PERLND 111	0	COPY	1	4
PERLND 112	49	COPY	1	4
PERLND 113	14	COPY	1	4
PERLND 114	181	COPY	1	4
PERLND 115	7	COPY	1	4
PERLND 116	10	COPY	1	4
IMPLND 101	26	COPY	1	5
IMPLND 102	42	COPY	1	5
IMPLND 103	4	COPY	1	5
IMPLND 104	0	COPY	1	5
***Sum the loads from all land segments in subbasin 2			2	
PERLND 101	931	COPY	2	4
PERLND 102	385	COPY	2	4
PERLND 103	26	COPY	2	4
PERLND 104	2	COPY	2	4
PERLND 105	0	COPY	2	4
PERLND 106	6	COPY	2	4
PERLND 107	778	COPY	2	4
PERLND 108	919	COPY	2	4
PERLND 109	3425	COPY	2	4
PERLND 110	500	COPY	2	4
PERLND 111	1044	COPY	2	4
PERLND 112	743	COPY	2	4
PERLND 113	22	COPY	2	4
PERLND 114	3792	COPY	2	4
PERLND 115	608	COPY	2	4
PERLND 116	54	COPY	2	4
IMPLND 101	115	COPY	2	5
IMPLND 102	182	COPY	2	5
IMPLND 103	41	COPY	2	5
IMPLND 104	11	COPY	2	5
***Sum the loads from all land segments in subbasin 3			3	
PERLND 101	27	COPY	3	4
PERLND 102	64	COPY	3	4
PERLND 103	4	COPY	3	4
PERLND 104	0	COPY	3	4
PERLND 105	0	COPY	3	4
PERLND 106	0	COPY	3	4
PERLND 107	87	COPY	3	4
PERLND 108	37	COPY	3	4
PERLND 109	421	COPY	3	4
PERLND 110	0	COPY	3	4
PERLND 111	26	COPY	3	4
PERLND 112	2	COPY	3	4
PERLND 113	0	COPY	3	4
PERLND 114	417	COPY	3	4
PERLND 115	10	COPY	3	4
PERLND 116	8	COPY	3	4
IMPLND 101	3	COPY	3	5
IMPLND 102	31	COPY	3	5
IMPLND 103	7	COPY	3	5
IMPLND 104	0	COPY	3	5
***Sum the loads from all land segments in subbasin 4			4	
PERLND 101	242	COPY	4	4
PERLND 102	164	COPY	4	4
PERLND 103	6	COPY	4	4
PERLND 104	1	COPY	4	4
PERLND 105	0	COPY	4	4
PERLND 106	0	COPY	4	4

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

PERLND 107	0	COPY	4	4
PERLND 108	0	COPY	4	4
PERLND 109	277	COPY	4	4
PERLND 110	253	COPY	4	4
PERLND 111	22	COPY	4	4
PERLND 112	1	COPY	4	4
PERLND 113	0	COPY	4	4
PERLND 114	159	COPY	4	4
PERLND 115	14	COPY	4	4
PERLND 116	8	COPY	4	4
IMPLND 101	30	COPY	4	5
IMPLND 102	74	COPY	4	5
IMPLND 103	9	COPY	4	5
IMPLND 104	8	COPY	4	5
***Sum the loads from all land segments in subbasin 5				
PERLND 101	274	COPY	5	4
PERLND 102	331	COPY	5	4
PERLND 103	36	COPY	5	4
PERLND 104	4	COPY	5	4
PERLND 105	3	COPY	5	4
PERLND 106	0	COPY	5	4
PERLND 107	5	COPY	5	4
PERLND 108	12	COPY	5	4
PERLND 109	501	COPY	5	4
PERLND 110	0	COPY	5	4
PERLND 111	1	COPY	5	4
PERLND 112	10	COPY	5	4
PERLND 113	37	COPY	5	4
PERLND 114	504	COPY	5	4
PERLND 115	30	COPY	5	4
PERLND 116	3	COPY	5	4
IMPLND 101	34	COPY	5	5
IMPLND 102	143	COPY	5	5
IMPLND 103	60	COPY	5	5
IMPLND 104	31	COPY	5	5
***Sum the loads from all land segments in subbasin 6				
PERLND 101	283	COPY	6	4
PERLND 102	240	COPY	6	4
PERLND 103	24	COPY	6	4
PERLND 104	2	COPY	6	4
PERLND 105	0	COPY	6	4
PERLND 106	0	COPY	6	4
PERLND 107	30	COPY	6	4
PERLND 108	13	COPY	6	4
PERLND 109	75	COPY	6	4
PERLND 110	30	COPY	6	4
PERLND 111	8	COPY	6	4
PERLND 112	0	COPY	6	4
PERLND 113	0	COPY	6	4
PERLND 114	409	COPY	6	4
PERLND 115	0	COPY	6	4
PERLND 116	6	COPY	6	4
IMPLND 101	35	COPY	6	5
IMPLND 102	105	COPY	6	5
IMPLND 103	38	COPY	6	5
IMPLND 104	13	COPY	6	5
***Sum the loads from all land segments in subbasin 7				
PERLND 101	216	COPY	7	4
PERLND 102	215	COPY	7	4
PERLND 103	32	COPY	7	4
PERLND 104	6	COPY	7	4
PERLND 105	0	COPY	7	4
PERLND 106	0	COPY	7	4

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

PERLND 107	10	COPY	7	4
PERLND 108	90	COPY	7	4
PERLND 109	28	COPY	7	4
PERLND 110	0	COPY	7	4
PERLND 111	18	COPY	7	4
PERLND 112	0	COPY	7	4
PERLND 113	25	COPY	7	4
PERLND 114	190	COPY	7	4
PERLND 115	5	COPY	7	4
PERLND 116	0	COPY	7	4
IMPLND 101	27	COPY	7	5
IMPLND 102	92	COPY	7	5
IMPLND 103	52	COPY	7	5
IMPLND 104	45	COPY	7	5
***Sum the loads from all land segments in subbasin 8				
PERLND 101	296	COPY	8	4
PERLND 102	289	COPY	8	4
PERLND 103	25	COPY	8	4
PERLND 104	5	COPY	8	4
PERLND 105	0	COPY	8	4
PERLND 106	0	COPY	8	4
PERLND 107	59	COPY	8	4
PERLND 108	39	COPY	8	4
PERLND 109	141	COPY	8	4
PERLND 110	0	COPY	8	4
PERLND 111	61	COPY	8	4
PERLND 112	0	COPY	8	4
PERLND 113	1	COPY	8	4
PERLND 114	20	COPY	8	4
PERLND 115	1	COPY	8	4
PERLND 116	3	COPY	8	4
IMPLND 101	37	COPY	8	5
IMPLND 102	125	COPY	8	5
IMPLND 103	40	COPY	8	5
IMPLND 104	38	COPY	8	5
***Sum the loads from all land segments in subbasin 9				
PERLND 101	153	COPY	9	4
PERLND 102	244	COPY	9	4
PERLND 103	20	COPY	9	4
PERLND 104	2	COPY	9	4
PERLND 105	0	COPY	9	4
PERLND 106	99	COPY	9	4
PERLND 107	5	COPY	9	4
PERLND 108	54	COPY	9	4
PERLND 109	129	COPY	9	4
PERLND 110	9	COPY	9	4
PERLND 111	31	COPY	9	4
PERLND 112	0	COPY	9	4
PERLND 113	0	COPY	9	4
PERLND 114	14	COPY	9	4
PERLND 115	0	COPY	9	4
PERLND 116	0	COPY	9	4
IMPLND 101	19	COPY	9	5
IMPLND 102	104	COPY	9	5
IMPLND 103	33	COPY	9	5
IMPLND 104	16	COPY	9	5
***Sum the loads from all land segments in subbasin 10				
PERLND 101	251	COPY	10	4
PERLND 102	658	COPY	10	4
PERLND 103	90	COPY	10	4
PERLND 104	25	COPY	10	4
PERLND 105	0	COPY	10	4
PERLND 106	20	COPY	10	4

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

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PERLND 107          48      COPY      10      4
PERLND 108          27      COPY      10      4
PERLND 109          26      COPY      10      4
PERLND 110           0      COPY      10      4
PERLND 111          30      COPY      10      4
PERLND 112           1      COPY      10      4
PERLND 113         133      COPY      10      4
PERLND 114         209      COPY      10      4
PERLND 115          37      COPY      10      4
PERLND 116           1      COPY      10      4
IMPLND 101          31      COPY      10      5
IMPLND 102         282      COPY      10      5
IMPLND 103         148      COPY      10      5
IMPLND 104         200      COPY      10      5
***Sum the loads from all land segments in subbasin 11
PERLND 101         225      COPY      11      4
PERLND 102         155      COPY      11      4
PERLND 103          20      COPY      11      4
PERLND 104           4      COPY      11      4
PERLND 105           1      COPY      11      4
PERLND 106          24      COPY      11      4
PERLND 107         119      COPY      11      4
PERLND 108         148      COPY      11      4
PERLND 109         384      COPY      11      4
PERLND 110           0      COPY      11      4
PERLND 111         152      COPY      11      4
PERLND 112          11      COPY      11      4
PERLND 113           1      COPY      11      4
PERLND 114          41      COPY      11      4
PERLND 115          45      COPY      11      4
PERLND 116           2      COPY      11      4
IMPLND 101          28      COPY      11      5
IMPLND 102          67      COPY      11      5
IMPLND 103          33      COPY      11      5
IMPLND 104          30      COPY      11      5
***Sum the loads from all land segments in subbasin 12
PERLND 101          76      COPY      12      4
PERLND 102         188      COPY      12      4
PERLND 103          50      COPY      12      4
PERLND 104           8      COPY      12      4
PERLND 105           1      COPY      12      4
PERLND 106           0      COPY      12      4
PERLND 107          20      COPY      12      4
PERLND 108          15      COPY      12      4
PERLND 109           8      COPY      12      4
PERLND 110          27      COPY      12      4
PERLND 111           6      COPY      12      4
PERLND 112           6      COPY      12      4
PERLND 113         205      COPY      12      4
PERLND 114          16      COPY      12      4
PERLND 115         739      COPY      12      4
PERLND 116           0      COPY      12      4
IMPLND 101           9      COPY      12      5
IMPLND 102          81      COPY      12      5
IMPLND 103          81      COPY      12      5
IMPLND 104          65      COPY      12      5
END SCHEMATIC

```

EXT TARGETS

```

<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Volume-> <Member> Tsys Aggr Amd ***
<Name> x <Name> x x<-factor->strg <Name> x <Name>qf tem strg strg***
*** INSTREAM CONCENTRATIONS in mg/L except CHLA(ug/L), TEMP(deg F), Flow(cfs)
RCHRES 1 HYDR RO 1 1 AVER WDM1 2001 RO 1 METR AGGR REPL

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Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

RCHRES	1	OXR	DOX	1	1	AVER	WDM1	3001	DO	1	ENGL	AGGR	REPL
RCHRES	1	OXR	DOX	1	1	MIN	WDM1	4001	DO	1	ENGL	AGGR	REPL
RCHRES	1	SEDTRN	SSED	1	1	AVER	WDM1	1505	SAND	1	ENGL	AGGR	REPL
RCHRES	1	SEDTRN	SSED	2	1	AVER	WDM1	1506	SILT	1	ENGL	AGGR	REPL
RCHRES	1	SEDTRN	SSED	3	1	AVER	WDM1	1507	CLAY	1	ENGL	AGGR	REPL
RCHRES	1	OXR	BOD	1	1	AVER	WDM1	1404	BOD	1	ENGL	AGGR	REPL
RCHRES	1	NUTRX	DNUST	1	1	AVER	WDM1	1401	DNO3	1	ENGL	AGGR	REPL
RCHRES	1	NUTRX	DNUST	2	1	AVER	WDM1	1402	DNH3	1	ENGL	AGGR	REPL
RCHRES	1	NUTRX	DNUST	4	1	AVER	WDM1	1403	DPO4	1	ENGL	AGGR	REPL
RCHRES	1	PLANK	PHYCLA	1	1	AVER	WDM1	1406	CHLA	1	ENGL	AGGR	REPL
RCHRES	1	PLANK	PKST3	4	1	AVER	WDM1	1407	ORGN	1	ENGL	AGGR	REPL
RCHRES	1	PLANK	PKST3	5	1	AVER	WDM1	1408	ORGP	1	ENGL	AGGR	REPL
RCHRES	1	PLANK	PKST3	1	1	AVER	WDM1	1601	DETN	1	ENGL	AGGR	REPL
RCHRES	1	PLANK	PKST3	2	1	AVER	WDM1	1602	DETP	1	ENGL	AGGR	REPL
RCHRES	1	PLANK	PKST3	3	1	AVER	WDM1	1603	DETC	1	ENGL	AGGR	REPL
RCHRES	1	SEDTRN	SSED	4	1	AVER	WDM1	1021	TSS	1	ENGL	AGGR	REPL
RCHRES	2	HYDR	RO	1	1	AVER	WDM1	2002	RO	1	METR	AGGR	REPL
RCHRES	2	OXR	DOX	1	1	AVER	WDM1	3002	DO	1	ENGL	AGGR	REPL
RCHRES	2	OXR	DOX	1	1	MIN	WDM1	4002	DO	1	ENGL	AGGR	REPL
RCHRES	2	SEDTRN	SSED	1	1	AVER	WDM1	1508	SAND	1	ENGL	AGGR	REPL
RCHRES	2	SEDTRN	SSED	2	1	AVER	WDM1	1509	SILT	1	ENGL	AGGR	REPL
RCHRES	2	SEDTRN	SSED	3	1	AVER	WDM1	1510	CLAY	1	ENGL	AGGR	REPL
RCHRES	2	OXR	BOD	1	1	AVER	WDM1	1414	BOD	1	ENGL	AGGR	REPL
RCHRES	2	NUTRX	DNUST	1	1	AVER	WDM1	1411	DNO3	1	ENGL	AGGR	REPL
RCHRES	2	NUTRX	DNUST	2	1	AVER	WDM1	1412	DNH3	1	ENGL	AGGR	REPL
RCHRES	2	NUTRX	DNUST	4	1	AVER	WDM1	1413	DPO4	1	ENGL	AGGR	REPL
RCHRES	2	PLANK	PHYCLA	1	1	AVER	WDM1	1416	CHLA	1	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	4	1	AVER	WDM1	1417	ORGN	1	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	5	1	AVER	WDM1	1418	ORGP	1	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	1	1	AVER	WDM1	1604	DETN	1	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	2	1	AVER	WDM1	1605	DETP	1	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	3	1	AVER	WDM1	1606	DETC	1	ENGL	AGGR	REPL
RCHRES	2	SEDTRN	SSED	4	1	AVER	WDM1	1045	TSS	1	ENGL	AGGR	REPL
RCHRES	3	HYDR	RO	1	1	AVER	WDM1	2003	RO	1	METR	AGGR	REPL
RCHRES	3	OXR	DOX	1	1	AVER	WDM1	3003	DO	1	ENGL	AGGR	REPL
RCHRES	3	OXR	DOX	1	1	MIN	WDM1	4003	DO	1	ENGL	AGGR	REPL
RCHRES	4	HYDR	RO	1	1	AVER	WDM1	2004	RO	1	METR	AGGR	REPL
RCHRES	4	OXR	DOX	1	1	AVER	WDM1	3004	DO	1	ENGL	AGGR	REPL
RCHRES	4	OXR	DOX	1	1	MIN	WDM1	4004	DO	1	ENGL	AGGR	REPL
RCHRES	6	HYDR	RO	1	1	AVER	WDM1	2006	RO	1	METR	AGGR	REPL
RCHRES	6	OXR	DOX	1	1	AVER	WDM1	3006	DO	1	ENGL	AGGR	REPL
RCHRES	6	OXR	DOX	1	1	MIN	WDM1	4006	DO	1	ENGL	AGGR	REPL
RCHRES	5	HYDR	RO	1	1	AVER	WDM1	2005	RO	1	METR	AGGR	REPL
RCHRES	5	OXR	DOX	1	1	AVER	WDM1	3005	DO	1	ENGL	AGGR	REPL
RCHRES	5	OXR	DOX	1	1	MIN	WDM1	4005	DO	1	ENGL	AGGR	REPL
RCHRES	7	HYDR	RO	1	1	AVER	WDM1	2007	RO	1	METR	AGGR	REPL
RCHRES	7	OXR	DOX	1	1	AVER	WDM1	3007	DO	1	ENGL	AGGR	REPL
RCHRES	7	OXR	DOX	1	1	MIN	WDM1	4007	DO	1	ENGL	AGGR	REPL
RCHRES	8	HYDR	RO	1	1	AVER	WDM1	2008	RO	1	METR	AGGR	REPL
RCHRES	8	OXR	DOX	1	1	AVER	WDM1	3008	DO	1	ENGL	AGGR	REPL
RCHRES	8	OXR	DOX	1	1	MIN	WDM1	4008	DO	1	ENGL	AGGR	REPL
RCHRES	8	SEDTRN	SSED	1	1	AVER	WDM1	1511	SAND	1	ENGL	AGGR	REPL
RCHRES	8	SEDTRN	SSED	2	1	AVER	WDM1	1512	SILT	1	ENGL	AGGR	REPL
RCHRES	8	SEDTRN	SSED	3	1	AVER	WDM1	1513	CLAY	1	ENGL	AGGR	REPL
RCHRES	8	OXR	BOD	1	1	AVER	WDM1	1212	BOD	1	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	1	1	AVER	WDM1	1209	DNO3	1	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	2	1	AVER	WDM1	1210	DNH3	1	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	4	1	AVER	WDM1	1211	DPO4	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PHYCLA	1	1	AVER	WDM1	1215	CHLA	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	4	1	AVER	WDM1	1236	ORGN	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	5	1	AVER	WDM1	1101	ORGP	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	1	1	AVER	WDM1	1607	DETN	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	2	1	AVER	WDM1	1608	DETP	1	ENGL	AGGR	REPL

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

RCHRES	8	PLANK	PKST3	3	1	AVER	WDM1	1609	DETC	1	ENGL	AGGR	REPL
RCHRES	8	SEDTRN	SSED	4	1	AVER	WDM1	1093	TSS	1	ENGL	AGGR	REPL
RCHRES	9	HYDR	RO	1	1	AVER	WDM1	2009	RO	1	METR	AGGR	REPL
RCHRES	9	OXR	DOX	1	1	AVER	WDM1	3009	DO	1	ENGL	AGGR	REPL
RCHRES	9	OXR	DOX	1	1	MIN	WDM1	4009	DO	1	ENGL	AGGR	REPL
RCHRES	9	SEDTRN	SSED	1	1	AVER	WDM1	1514	SAND	1	ENGL	AGGR	REPL
RCHRES	9	SEDTRN	SSED	2	1	AVER	WDM1	1515	SILT	1	ENGL	AGGR	REPL
RCHRES	9	SEDTRN	SSED	3	1	AVER	WDM1	1516	CLAY	1	ENGL	AGGR	REPL
RCHRES	9	OXR	BOD	1	1	AVER	WDM1	1448	BOD	1	ENGL	AGGR	REPL
RCHRES	9	NUTRX	DNUST	1	1	AVER	WDM1	1445	DNO3	1	ENGL	AGGR	REPL
RCHRES	9	NUTRX	DNUST	2	1	AVER	WDM1	1446	DNH3	1	ENGL	AGGR	REPL
RCHRES	9	NUTRX	DNUST	4	1	AVER	WDM1	1447	DPO4	1	ENGL	AGGR	REPL
RCHRES	9	PLANK	PHYCLA	1	1	AVER	WDM1	1450	CHLA	1	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	4	1	AVER	WDM1	1451	ORGN	1	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	5	1	AVER	WDM1	1452	ORGP	1	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	1	1	AVER	WDM1	1610	DETN	1	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	2	1	AVER	WDM1	1611	DETP	1	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	3	1	AVER	WDM1	1612	DETC	1	ENGL	AGGR	REPL
RCHRES	9	SEDTRN	SSED	4	1	AVER	WDM1	1117	TSS	1	ENGL	AGGR	REPL
RCHRES	10	HYDR	RO	1	1	AVER	WDM1	2010	RO	1	METR	AGGR	REPL
RCHRES	10	OXR	DOX	1	1	AVER	WDM1	3010	DO	1	ENGL	AGGR	REPL
RCHRES	10	OXR	DOX	1	1	MIN	WDM1	4010	DO	1	ENGL	AGGR	REPL
RCHRES	10	HTRCH	TW	1	1	AVER	WDM1	1296	TW	1	METR	AGGR	REPL
RCHRES	11	HYDR	RO	1	1	AVER	WDM1	2011	RO	1	METR	AGGR	REPL
RCHRES	11	OXR	DOX	1	1	AVER	WDM1	3011	DO	1	ENGL	AGGR	REPL
RCHRES	11	OXR	DOX	1	1	MIN	WDM1	4011	DO	1	ENGL	AGGR	REPL
RCHRES	11	SEDTRN	SSED	1	1	AVER	WDM1	1517	SAND	1	ENGL	AGGR	REPL
RCHRES	11	SEDTRN	SSED	2	1	AVER	WDM1	1518	SILT	1	ENGL	AGGR	REPL
RCHRES	11	SEDTRN	SSED	3	1	AVER	WDM1	1519	CLAY	1	ENGL	AGGR	REPL
RCHRES	11	OXR	BOD	1	1	AVER	WDM1	1240	BOD	1	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	1	1	AVER	WDM1	1217	DNO3	1	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	2	1	AVER	WDM1	1218	DNH3	1	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	4	1	AVER	WDM1	1219	DPO4	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PHYCLA	1	1	AVER	WDM1	1249	CHLA	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	4	1	AVER	WDM1	1237	ORGN	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	5	1	AVER	WDM1	1102	ORGP	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	1	1	AVER	WDM1	1613	DETN	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	2	1	AVER	WDM1	1614	DETP	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	3	1	AVER	WDM1	1615	DETC	1	ENGL	AGGR	REPL
RCHRES	11	SEDTRN	SSED	4	1	AVER	WDM1	1141	TSS	1	ENGL	AGGR	REPL
RCHRES	12	HYDR	RO	1	1	AVER	WDM1	2012	RO	1	METR	AGGR	REPL
RCHRES	12	OXR	DOX	1	1	AVER	WDM1	3012	DO	1	ENGL	AGGR	REPL
RCHRES	12	OXR	DOX	1	1	MIN	WDM1	4012	DO	1	ENGL	AGGR	REPL

*** In the following COPY statements

*** multiplier of 1.008 converts from ac*in/hr to cfs

*** MULTIPLIER OF 907 CONVERTS FROM TONS TO KG

*** multiplier of 0.454 CONVERTS FROM LBS TO KG

*** output flows and loads from sub-basin 1

COPY	1	OUTPUT	MEAN	1	1	0.02855	WDM1	9006	PERO	1	METR	AGGR	REPL
COPY	1	OUTPUT	MEAN	2	1	907	WDM1	9000	TSS	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	3	1	0.454	WDM1	9002	NH3N	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	4	1	0.454	WDM1	9003	NO3N	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	5	1	0.454	WDM1	9004	PO4P	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	6	1	0.454	WDM1	9005	BOD	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	7	1	0.454	WDM1	9001	DO	1	ENGL	AGGR	REPL

***output flows and loads from sub-basin 2

COPY	2	OUTPUT	MEAN	1	1	0.02855	WDM1	9016	PERO	1	METR	AGGR	REPL
COPY	2	OUTPUT	MEAN	2	1	907	WDM1	9010	TSS	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	3	1	0.454	WDM1	9012	NH3N	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	4	1	0.454	WDM1	9013	NO3N	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	5	1	0.454	WDM1	9014	PO4P	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	6	1	0.454	WDM1	9015	BOD	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	7	1	0.454	WDM1	9011	DO	1	ENGL	AGGR	REPL

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A*

```

***output flows and loads from sub-basin 3
COPY      3 OUTPUT MEAN    1 1    0.02855    WDM1  9026 PERO    1 METR AGGR REPL
COPY      3 OUTPUT MEAN    2 1         907    WDM1  9020 TSS     1 ENGL AGGR REPL
COPY      3 OUTPUT MEAN    3 1    0.454    WDM1  9022 NH3N    1 ENGL AGGR REPL
COPY      3 OUTPUT MEAN    4 1    0.454    WDM1  9023 NO3N    1 ENGL AGGR REPL
COPY      3 OUTPUT MEAN    5 1    0.454    WDM1  9024 PO4P    1 ENGL AGGR REPL
COPY      3 OUTPUT MEAN    6 1    0.454    WDM1  9025 BOD     1 ENGL AGGR REPL
COPY      3 OUTPUT MEAN    7 1    0.454    WDM1  9021 DO      1 ENGL AGGR REPL
***output flows and loads from sub-basin 4
COPY      4 OUTPUT MEAN    1 1    0.02855    WDM1  9036 PERO    1 METR AGGR REPL
COPY      4 OUTPUT MEAN    2 1         907    WDM1  9030 TSS     1 ENGL AGGR REPL
COPY      4 OUTPUT MEAN    3 1    0.454    WDM1  9032 NH3N    1 ENGL AGGR REPL
COPY      4 OUTPUT MEAN    4 1    0.454    WDM1  9033 NO3N    1 ENGL AGGR REPL
COPY      4 OUTPUT MEAN    5 1    0.454    WDM1  9034 PO4P    1 ENGL AGGR REPL
COPY      4 OUTPUT MEAN    6 1    0.454    WDM1  9035 BOD     1 ENGL AGGR REPL
COPY      4 OUTPUT MEAN    7 1    0.454    WDM1  9031 DO      1 ENGL AGGR REPL
***output flows and loads from sub-basin 5
COPY      5 OUTPUT MEAN    1 1    0.02855    WDM1  9046 PERO    1 METR AGGR REPL
COPY      5 OUTPUT MEAN    2 1         907    WDM1  9040 TSS     1 ENGL AGGR REPL
COPY      5 OUTPUT MEAN    3 1    0.454    WDM1  9042 NH3N    1 ENGL AGGR REPL
COPY      5 OUTPUT MEAN    4 1    0.454    WDM1  9043 NO3N    1 ENGL AGGR REPL
COPY      5 OUTPUT MEAN    5 1    0.454    WDM1  9044 PO4P    1 ENGL AGGR REPL
COPY      5 OUTPUT MEAN    6 1    0.454    WDM1  9045 BOD     1 ENGL AGGR REPL
COPY      5 OUTPUT MEAN    7 1    0.454    WDM1  9041 DO      1 ENGL AGGR REPL
***output flows and loads from sub-basin 6
COPY      6 OUTPUT MEAN    1 1    0.02855    WDM1  9056 PERO    1 METR AGGR REPL
COPY      6 OUTPUT MEAN    2 1         907    WDM1  9050 TSS     1 ENGL AGGR REPL
COPY      6 OUTPUT MEAN    3 1    0.454    WDM1  9052 NH3N    1 ENGL AGGR REPL
COPY      6 OUTPUT MEAN    4 1    0.454    WDM1  9053 NO3N    1 ENGL AGGR REPL
COPY      6 OUTPUT MEAN    5 1    0.454    WDM1  9054 PO4P    1 ENGL AGGR REPL
COPY      6 OUTPUT MEAN    6 1    0.454    WDM1  9055 BOD     1 ENGL AGGR REPL
COPY      6 OUTPUT MEAN    7 1    0.454    WDM1  9051 DO      1 ENGL AGGR REPL
***output flows and loads from sub-basin 7
COPY      7 OUTPUT MEAN    1 1    0.02855    WDM1  9066 PERO    1 METR AGGR REPL
COPY      7 OUTPUT MEAN    2 1         907    WDM1  9060 TSS     1 ENGL AGGR REPL
COPY      7 OUTPUT MEAN    3 1    0.454    WDM1  9062 NH3N    1 ENGL AGGR REPL
COPY      7 OUTPUT MEAN    4 1    0.454    WDM1  9063 NO3N    1 ENGL AGGR REPL
COPY      7 OUTPUT MEAN    5 1    0.454    WDM1  9064 PO4P    1 ENGL AGGR REPL
COPY      7 OUTPUT MEAN    6 1    0.454    WDM1  9065 BOD     1 ENGL AGGR REPL
COPY      7 OUTPUT MEAN    7 1    0.454    WDM1  9061 DO      1 ENGL AGGR REPL
***output flows and loads from sub-basin 8
COPY      8 OUTPUT MEAN    1 1    0.02855    WDM1  9076 PERO    1 METR AGGR REPL
COPY      8 OUTPUT MEAN    2 1         907    WDM1  9070 TSS     1 ENGL AGGR REPL
COPY      8 OUTPUT MEAN    3 1    0.454    WDM1  9072 NH3N    1 ENGL AGGR REPL
COPY      8 OUTPUT MEAN    4 1    0.454    WDM1  9073 NO3N    1 ENGL AGGR REPL
COPY      8 OUTPUT MEAN    5 1    0.454    WDM1  9074 PO4P    1 ENGL AGGR REPL
COPY      8 OUTPUT MEAN    6 1    0.454    WDM1  9075 BOD     1 ENGL AGGR REPL
COPY      8 OUTPUT MEAN    7 1    0.454    WDM1  9071 DO      1 ENGL AGGR REPL
***output flows and loads from sub-basin 9
COPY      9 OUTPUT MEAN    1 1    0.02855    WDM1  9086 PERO    1 METR AGGR REPL
COPY      9 OUTPUT MEAN    2 1         907    WDM1  9080 TSS     1 ENGL AGGR REPL
COPY      9 OUTPUT MEAN    3 1    0.454    WDM1  9082 NH3N    1 ENGL AGGR REPL
COPY      9 OUTPUT MEAN    4 1    0.454    WDM1  9083 NO3N    1 ENGL AGGR REPL
COPY      9 OUTPUT MEAN    5 1    0.454    WDM1  9084 PO4P    1 ENGL AGGR REPL
COPY      9 OUTPUT MEAN    6 1    0.454    WDM1  9085 BOD     1 ENGL AGGR REPL
COPY      9 OUTPUT MEAN    7 1    0.454    WDM1  9081 DO      1 ENGL AGGR REPL
***output flows and loads from sub-basin 10
COPY     10 OUTPUT MEAN    1 1    0.02855    WDM1  9096 PERO    1 METR AGGR REPL
COPY     10 OUTPUT MEAN    2 1         907    WDM1  9090 TSS     1 ENGL AGGR REPL
COPY     10 OUTPUT MEAN    3 1    0.454    WDM1  9092 NH3N    1 ENGL AGGR REPL
COPY     10 OUTPUT MEAN    4 1    0.454    WDM1  9093 NO3N    1 ENGL AGGR REPL
COPY     10 OUTPUT MEAN    5 1    0.454    WDM1  9094 PO4P    1 ENGL AGGR REPL
COPY     10 OUTPUT MEAN    6 1    0.454    WDM1  9095 BOD     1 ENGL AGGR REPL

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix A

```

COPY 10 OUTPUT MEAN 7 1 0.454 WDM1 9091 DO 1 ENGL AGGR REPL
***output flows and loads from sub-basin 11
COPY 11 OUTPUT MEAN 1 1 0.02855 WDM1 9106 PERO 1 METR AGGR REPL
COPY 11 OUTPUT MEAN 2 1 907 WDM1 9100 TSS 1 ENGL AGGR REPL
COPY 11 OUTPUT MEAN 3 1 0.454 WDM1 9102 NH3N 1 ENGL AGGR REPL
COPY 11 OUTPUT MEAN 4 1 0.454 WDM1 9103 NO3N 1 ENGL AGGR REPL
COPY 11 OUTPUT MEAN 5 1 0.454 WDM1 9104 PO4P 1 ENGL AGGR REPL
COPY 11 OUTPUT MEAN 6 1 0.454 WDM1 9105 BOD 1 ENGL AGGR REPL
COPY 11 OUTPUT MEAN 7 1 0.454 WDM1 9101 DO 1 ENGL AGGR REPL
***output flows and loads from sub-basin 12
COPY 12 OUTPUT MEAN 1 1 0.02855 WDM1 9116 PERO 1 METR AGGR REPL
COPY 12 OUTPUT MEAN 2 1 907 WDM1 9110 TSS 1 ENGL AGGR REPL
COPY 12 OUTPUT MEAN 3 1 0.454 WDM1 9112 NH3N 1 ENGL AGGR REPL
COPY 12 OUTPUT MEAN 4 1 0.454 WDM1 9113 NO3N 1 ENGL AGGR REPL
COPY 12 OUTPUT MEAN 5 1 0.454 WDM1 9114 PO4P 1 ENGL AGGR REPL
COPY 12 OUTPUT MEAN 6 1 0.454 WDM1 9115 BOD 1 ENGL AGGR REPL
COPY 12 OUTPUT MEAN 7 1 0.454 WDM1 9111 DO 1 ENGL AGGR REPL
END EXT TARGETS
  
```

MASS-LINK

```

MASS-LINK 3
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
RCHRES ROFLOW RCHRES INFLOW
END MASS-LINK 3
  
```

```

MASS-LINK 4
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWATER PERO COPY INPUT MEAN 1
PERLND SEDMNT SOSED 1 COPY INPUT MEAN 2
PERLND PQUAL POQUAL 1 COPY INPUT MEAN 3
PERLND PQUAL POQUAL 2 COPY INPUT MEAN 4
PERLND PQUAL POQUAL 3 COPY INPUT MEAN 5
PERLND PQUAL POQUAL 4 COPY INPUT MEAN 6
PERLND PWTGAS PODOXM COPY INPUT MEAN 7
END MASS-LINK 4
  
```

```

MASS-LINK 5
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO COPY INPUT MEAN 1
IMPLND SOLIDS SOSLD 1 COPY INPUT MEAN 2
IMPLND IQUAL SOQUAL 1 COPY INPUT MEAN 3
IMPLND IQUAL SOQUAL 2 COPY INPUT MEAN 4
IMPLND IQUAL SOQUAL 3 COPY INPUT MEAN 5
IMPLND IQUAL SOQUAL 4 COPY INPUT MEAN 6
IMPLND IWTGAS SODOXM COPY INPUT MEAN 7
END MASS-LINK 5
  
```

```

MASS-LINK 1
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO 0.0833333 RCHRES INFLOW IVOL
IMPLND SOLIDS SOSLD 1 0.05 RCHRES INFLOW ISED 1
IMPLND SOLIDS SOSLD 1 0.55 RCHRES INFLOW ISED 2
IMPLND SOLIDS SOSLD 1 0.4 RCHRES INFLOW ISED 3
IMPLND IWTGAS SODOXM RCHRES INFLOW OXIF 1
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT 1
IMPLND IQUAL SOQUAL 1 RCHRES INFLOW NUIF1 2
IMPLND IQUAL SOQUAL 2 RCHRES INFLOW NUIF1 1
  
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix A

```

IMPLND    IQUAL    SOQUAL    3                RCHRES    INFLOW    NUIF1    4
IMPLND    IQUAL    SOQUAL    4                RCHRES    INFLOW    OXIF     2
IMPLND    IQUAL    SOQUAL    4                0.1       RCHRES    INFLOW    PKIF     3
IMPLND    IQUAL    SOQUAL    4                0.015    RCHRES    INFLOW    PKIF     4
IMPLND    IQUAL    SOQUAL    4                0.5       RCHRES    INFLOW    PKIF     5
    END MASS-LINK    1

    MASS-LINK    2
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name>      <Name> x x<-factor-> <Name>      <Name> x x ***
PERLND      PWATER  PERO      0.0833333 RCHRES    INFLOW    IVOL
PERLND      SEDMNT  SOSED    1          0.05     RCHRES    INFLOW    ISED    1
PERLND      SEDMNT  SOSED    1          0.55     RCHRES    INFLOW    ISED    2
PERLND      SEDMNT  SOSED    1          0.4      RCHRES    INFLOW    ISED    3
PERLND      PWTGAS  PODOXM   RCHRES    INFLOW    OXIF    1
PERLND      PWTGAS  POHT     RCHRES    INFLOW    IHEAT   1
PERLND      PWTGAS  POHT     RCHRES    INFLOW    IHEAT   1
PERLND      PQUAL   POQUAL   1          RCHRES    INFLOW    NUIF1   2
PERLND      PQUAL   POQUAL   2          RCHRES    INFLOW    NUIF1   1
PERLND      PQUAL   POQUAL   3          RCHRES    INFLOW    NUIF1   4
PERLND      PQUAL   POQUAL   4          RCHRES    INFLOW    OXIF    2
PERLND      PQUAL   POQUAL   4          0.1      RCHRES    INFLOW    PKIF    3
PERLND      PQUAL   POQUAL   4          0.015    RCHRES    INFLOW    PKIF    4
PERLND      PQUAL   POQUAL   4          0.5      RCHRES    INFLOW    PKIF    5
    END MASS-LINK    2
END MASS-LINK

END RUN

```

Appendix B Cow Bayou HSPF User Control Interface File

Note: The annotations that were added to this print version for clarity may prevent it from running. It may be necessary to strip out extra comment lines that begin with three asterisks.

```
RUN

GLOBAL
  UCI Created by Kirk Dean/Nabin Basnet for the Cow Bayou watershed
  START      2001/01/01 01:00  END      2013/01/31 23:00
  RUN INTERP  OUTPT LEVELS  10   10
  RESUME     0 RUN      1
  UNITS      1
END GLOBAL

FILES
<FILE> <UN#>***<----FILE NAME----->
MESSU   24   cow_lt.ech
        91   cow_lt.out
WDM1    25   cow_out.wdm
WDM2    26   cow_meteorol.wdm
WDM3    27   cow_source.wdm
BINO    92   cow_lt.hbn
END FILES

OPN SEQUENCE
  INGRP          INDELT 01:00
  PERLND        101
  PERLND        102
  PERLND        103
  PERLND        104
  PERLND        105
  PERLND        106
  PERLND        107
  PERLND        108
  PERLND        109
  PERLND        110
  PERLND        111
  PERLND        112
  PERLND        113
  PERLND        114
  PERLND        115
  PERLND        116
  PERLND        117
  IMPLND        101
  IMPLND        102
  IMPLND        103
  IMPLND        104
  RCHRES        1
  RCHRES        2
  RCHRES        3
  RCHRES        4
  RCHRES        5
  RCHRES        6
  RCHRES        7
  RCHRES        8
  RCHRES        9
  RCHRES        10
  RCHRES        11
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

RCHRES      13
RCHRES      12
RCHRES      14
RCHRES      15
RCHRES      16
RCHRES      17
RCHRES      18
COPY        1
COPY        2
COPY        3
COPY        4
COPY        5
COPY        6
COPY        7
COPY        8
COPY        9
COPY       10
COPY       11
COPY       12
COPY       13
COPY       14
COPY       15
COPY       16
COPY       17
COPY       18
END INGRP
END OPN SEQUENCE

PERLND
ACTIVITY
*** <PLS >
*** x - x ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC ***
101 117 1 0 1 1 1 1 1 0 0 0 0 0
END ACTIVITY

PRINT-INFO
*** < PLS>
*** x - x ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC PIVL PYR
101 117 4 4 4 4 4 4 4 4 4 4 4 1 12
END PRINT-INFO

BINARY-INFO
*** < PLS>
*** x - x ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC PIVL PYR
101 117 4 4 4 4 4 4 4 4 4 4 4 1 12
END BINARY-INFO

GEN-INFO
***
*** <PLS >
*** x - x
101 Developed Open Space 1 1 0 0 92 0
102 Developed Low Intens 1 1 0 0 92 0
103 Developed Medium Int 1 1 0 0 92 0
104 Developed High Inten 1 1 0 0 92 0
105 Barren 1 1 0 0 92 0
106 Deciduous Forest 1 1 0 0 92 0
107 Evergreen Forest 1 1 0 0 92 0
108 Mixed Forest 1 1 0 0 92 0
109 Pasture/Hay 1 1 0 0 92 0
110 Cropland 1 1 0 0 92 0
111 Grassland/Herbaceous 1 1 0 0 92 0
112 Shrub/Scrub 1 1 0 0 92 0

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

113    Open Water                1    1    0    0    92    0
114    Woody Wetlands            1    1    0    0    92    0
115    Herbaceous Wetlands       1    1    0    0    92    0
116    Septic Fields             1    1    0    0    92    0
117    Future Unused             1    1    0    0    92    0
END GEN-INFO

```

```

ATEMP-DAT
*** <PLS >      ELDAT      AIRTEMP
*** x - x      (ft)      (deg F)
101 117      -6.      33.
END ATEMP-DAT

```

```

PWAT-PARM1
*** <PLS >      Flags
*** x - x CSNO RTOP UZFG VCS VUZ VMN VIFW VIRC VLE IFFC HWT IRRG IFRD
101 114      0    1    1    1    1    0    0    0    1    0    0    0    0
115          0    2    1    1    0    0    0    0    1    0    1    0    0
116 117      0    1    1    1    1    0    0    0    1    0    0    0    0
END PWAT-PARM1

```

```

PWAT-PARM2
*** < PLS>      FOREST      LZSN      INFILT      LSUR      SLSUR      KVARY      AGWRC
*** x - x      (in)      (in/hr)      (ft)      (1/in)      (1/day)
***          CAL      CAL
101          0.      5.0      0.25      500.      0.002      5.      0.96
102          0.      5.0      0.25      500.      0.002      5.      0.96
103          0.      5.0      0.25      500.      0.002      5.      0.96
104          0.      5.0      0.25      500.      0.002      5.      0.96
105          0.      5.0      0.25      500.      0.002      5.      0.96
106          0.      5.0      0.25      500.      0.002      5.      0.96
107          0.      5.0      0.25      500.      0.002      5.      0.96
108          0.      5.0      0.25      500.      0.002      5.      0.96
109          0.      5.0      0.25      500.      0.002      5.      0.96
110          0.      5.0      0.25      500.      0.003      5.      0.96
111          0.      5.0      0.25      500.      0.002      5.      0.96
112          0.      5.0      0.25      500.      0.002      5.      0.96
113          0.      5.0      0.25      500.      0.001      5.      0.96
114          0.      5.0      0.25      500.      0.002      5.      0.96
115          0.      5.0      0.25      500.      0.001      5.      0.96
116 117      0.      5.0      0.25      500.      0.002      5.      0.96
END PWAT-PARM2

```

```

PWAT-PARM3
*** < PLS>      PETMAX      PETMIN      INFEXP      INFILD      DEEPFR      BASETP      AGWETP
*** x - x      (deg F)      (deg F)
101 117      40.      35.      2.0      2.0      0.10      0.10      0.20
END PWAT-PARM3

```

```

PWAT-PARM4
*** <PLS >      CEPSC      UZSN      NSUR      INTFW      IRC      LZETP
*** x - x      (in)      (in)      (1/day)
101      0.15      0.6      0.4      10.      0.75      0.5
102      0.15      0.6      0.4      10.      0.75      0.5
103      0.15      0.6      0.4      10.      0.75      0.5
104      0.15      0.6      0.4      10.      0.75      0.5
105      0.15      0.6      0.4      10.      0.75      0.5
106      0.15      0.6      0.4      10.      0.75      0.5
107      0.15      0.6      0.4      10.      0.75      0.5
108      0.15      0.6      0.4      10.      0.75      0.5
109      0.15      0.6      0.4      10.      0.75      0.5
110      0.15      0.6      0.4      10.      0.75      0.5
111      0.15      0.6      0.4      10.      0.75      0.5

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

112          0.15      0.6      0.4      10.      0.75      0.5
113          0.01      0.6      0.4      10.      0.75      0.5
114 117      0.15      0.6      0.4      10.      0.75      0.5
END PWAT-PARM4

```

```

PWAT-PARM6
*** <PLS > MELEV      BELV      GWDATM      PCW      PGW      UPGW
*** x - x      (ft)      (ft)      (ft)
101          53.0      37.3      0.      0.30      0.10      0.15
102          53.0      37.3      0.      0.30      0.10      0.15
103          53.0      37.3      0.      0.30      0.10      0.15
104          51.3      37.3      0.      0.30      0.10      0.15
105          45.6      37.3      0.      0.30      0.10      0.15
106          41.9      37.3      0.      0.30      0.10      0.15
107          45.8      37.3      0.      0.30      0.10      0.15
108          43.5      37.3      0.      0.30      0.10      0.15
109          53.0      37.3      0.      0.30      0.10      0.15
110          53.0      37.3      0.      0.30      0.10      0.15
111          53.0      37.3      0.      0.30      0.10      0.15
112          53.0      37.3      0.      0.30      0.10      0.15
113          41.1      37.3      0.      0.30      0.10      0.15
114          39.4      37.3      0.      0.30      0.10      0.15
115          44.0      37.3      0.      0.30      0.10      0.15
116          53.0      37.3      0.      0.30      0.10      0.15
117          50.0      37.3      0.      0.30      0.10      0.15
END PWAT-PARM6

```

```

PWAT-PARM7
*** < PLS> STABNO      SRRC      SREXP      IFWSC      DELTA      UELFAC      LELFAC
*** x - x      (/hr)      (in)      (in)
***          CAL      CAL      CAL
101          0.      0.1      1.      0.5      0.002      4.      2.5
102          0.      0.1      1.      0.5      0.002      4.      2.5
103          0.      0.1      1.      0.5      0.002      4.      2.5
104          0.      0.1      1.      0.5      0.002      4.      2.5
105          0.      0.1      1.      0.5      0.002      4.      2.5
106          0.      0.1      1.      0.5      0.002      4.      2.5
107          0.      0.1      1.      0.5      0.002      4.      2.5
108          0.      0.1      1.      0.5      0.002      4.      2.5
109          0.      0.1      1.      0.5      0.002      4.      2.5
110          0.      0.1      1.      0.5      0.002      4.      2.5
111          0.      0.1      1.      0.5      0.002      4.      2.5
112          0.      0.1      1.      0.5      0.002      4.      2.5
113          0.      0.1      1.      0.5      0.002      4.      2.5
114          0.      0.1      1.      0.5      0.002      4.      2.5
115          0.      0.1      1.      0.5      0.002      4.      2.5
116          0.      0.1      1.      0.5      0.002      4.      2.5
117          0.      0.1      1.      0.5      0.002      4.      2.5
END PWAT-PARM7

```

```

PWAT-STATE1
*** < PLS> PWATER state variables (in)
*** x - x      CEPS      SURS      UZS      IFWS      LZS      AGWS      GWVS
101 117      0.01      0.01      0.1      0.1      4.      2.5      0.
END PWAT-STATE1

```

```

MON-INTERCEP
*** <PLS > Interception storage capacity at start of each month (in) CAL
*** x - x      JAN      FEB      MAR      APR      MAY      JUN      JUL      AUG      SEP      OCT      NOV      DEC
101          0.05      0.05      0.05      0.09      0.11      0.15      0.15      0.15      0.15      0.13      0.09      0.05
102          0.05      0.05      0.05      0.09      0.11      0.15      0.15      0.15      0.15      0.13      0.09      0.05
103          0.05      0.05      0.05      0.09      0.11      0.15      0.15      0.15      0.15      0.13      0.09      0.05
104          0.05      0.05      0.05      0.09      0.11      0.15      0.15      0.15      0.15      0.13      0.09      0.05

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

105      0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01
106      0.03 0.03 0.05 0.18 0.26 0.28 0.28 0.28 0.28 0.25 0.18 0.03
107      0.10 0.10 0.10 0.15 0.20 0.25 0.25 0.25 0.25 0.20 0.15 0.10
108      0.05 0.05 0.07 0.16 0.23 0.26 0.26 0.26 0.26 0.22 0.16 0.05
109      0.05 0.05 0.06 0.08 0.12 0.15 0.15 0.15 0.15 0.10 0.08 0.05
110      0.01 0.01 0.04 0.08 0.12 0.15 0.15 0.15 0.15 0.05 0.01 0.01
111      0.05 0.05 0.06 0.10 0.15 0.20 0.20 0.20 0.20 0.15 0.10 0.05
112      0.03 0.03 0.06 0.12 0.22 0.22 0.22 0.22 0.18 0.16 0.12 0.05
113      0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01
114      0.05 0.05 0.07 0.16 0.20 0.22 0.22 0.22 0.22 0.20 0.16 0.05
115      0.05 0.05 0.06 0.08 0.12 0.15 0.15 0.15 0.15 0.10 0.08 0.05
116      0.05 0.05 0.05 0.09 0.11 0.15 0.15 0.15 0.15 0.13 0.09 0.05
117      0.05 0.05 0.05 0.09 0.11 0.13 0.13 0.13 0.13 0.13 0.09 0.05
END MON-INTERCEP

MON-UZSN
*** <PLS > Upper zone storage capacity at start of each month (in) CAL
*** x - x  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP  OCT  NOV  DEC
101 117 0.5 0.1 0.1 0.4 0.7 1.0 1.2 1.3 1.2 1.0 1.0 1.0
END MON-UZSN

MON-LZETPARAM
*** <PLS > Lower zone evapotranspiration param at start of each month CAL
*** x - x  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP  OCT  NOV  DEC
101 117 0.1 0.10 0.17 0.69 0.86 0.90 0.90 0.90 0.90 0.49 0.26 0.1
END MON-LZETPARAM

SED-PARM1
*** <PLS > Sediment parameters 1
*** x - x  CRV VSIV SDOP
101 117 1 0 1
END SED-PARM1

SED-PARM2
*** <PLS > SMPF KRER JRER AFFIX COVER NVSI
*** x - x (/day) lb/ac-day
101 1. 0.43 2. 0.01 0.88 1.
102 1. 0.43 2. 0.01 0.88 1.
103 1. 0.43 2. 0.01 0.88 1.
104 1. 0.43 2. 0.01 0.88 1.
105 1. 0.43 2. 0.01 0.88 1.
106 1. 0.43 2. 0.002 0.88 2.
107 1. 0.43 2. 0.002 0.88 2.
108 1. 0.43 2. 0.002 0.88 2.
109 1. 0.43 2. 0.01 0.88 1.
110 1. 0.43 2. 0.01 0.88 2.
111 1. 0.43 2. 0.01 0.88 1.
112 1. 0.43 2. 0.01 0.88 1.
113 1. 0.43 2. 0.002 0.88 0.
114 1. 0.28 2. 0.002 0.88 2.
115 1. 0.49 2. 0.002 0.88 1.
116 1. 0.43 2. 0.01 0.88 1.
117 1. 0.43 2. 0.01 0.88 1.
END SED-PARM2

SED-PARM3
*** <PLS > Sediment parameter 3
*** x - x KSER JSER KGER JGER
101 0.5 2. 0. 2.
102 0.5 2. 0.01 2.
103 0.62 2. 0.07 2.
104 0.84 2. 0.125 2.
105 5. 2. 0.25 2.

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

106      0.55      2.      0.      2.
107      0.55      2.      0.      2.
108      0.55      2.      0.      2.
109      1.6       2.      0.3     2.
110      5.        1.3     5.      1.3
111      0.8       2.      0.      2.
112      1.0       2.      0.      2.
113      0.        2.      0.      2.
114      0.5       2.      0.      2.
115      0.5       2.      0.      2.
116      0.5       2.      0.01    2.
117      0.5       2.      0.      2.
END SED-PARM3

```

MON-COVER

```

*** <PLS > Monthly values for erosion related cover
*** x - x  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP  OCT  NOV  DEC
101      0.9  0.9  0.9  0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.9 0.9
102      0.9  0.9  0.9  0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.9 0.9
103      0.9  0.9  0.9  0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.9 0.9
104      0.9  0.9  0.9  0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.9 0.9
105      0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01
106      0.8  0.8  0.8  0.94 0.97 0.97 0.97 0.97 0.97 0.97 0.91 0.85
107      0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97
108      0.94 0.94 0.94 0.95 0.97 0.97 0.97 0.97 0.97 0.97 0.96 0.94
109      0.9  0.9  0.9  0.91 0.92 0.93 0.92 0.91 0.90 0.90 0.9 0.9
110      0.7  0.7  0.5  0.5  0.6 0.75 0.8 0.9 0.9 0.7 0.7 0.7
111      0.9  0.9  0.9  0.91 0.92 0.93 0.94 0.94 0.93 0.92 0.91 0.9
112      0.8  0.8  0.8  0.91 0.92 0.93 0.94 0.94 0.93 0.92 0.91 0.85
113      1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.    1.
114      0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.97
115      0.9  0.9  0.9  0.91 0.92 0.93 0.94 0.94 0.93 0.92 0.91 0.9
116      0.9  0.9  0.9  0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.9 0.9
117      0.9  0.9  0.9  0.91 0.93 0.93 0.93 0.93 0.93 0.91 0.9 0.9
END MON-COVER

```

SED-STOR

```

*** <PLS > Detached sediment storage (tons/acre)
*** x - x      DETS
101      0.4
102      0.4
103      0.4
104      0.4
105      0.5
106      0.1
107      0.1
108      0.1
109      0.2
110      0.5
111      0.2
112      0.1
113      0.
114      0.1
115      0.1
116      0.4
117      0.4
END SED-STOR

```

PSTEMP-PARM1

```

*** <PLS > Flags for section PSTEMP
*** x - x  SLTV ULTV LGTV TSOP
101 117   0   0   0   1
END PSTEMP-PARM1

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

PSTEMP-PARM2
*** <PLS >      ASLT      BSLT      ULTP1      ULTP2      LGTP1      LGTP2
*** x - x      (deg F)    (deg F)          (deg F)          (deg F)
   101 117      35.      0.4      40.      0.3      65.      0.
END PSTEMP-PARM2

MON-ASLT
*** <PLS > Value of ASLT at start of each month (deg F)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
   101 117 45. 45. 45. 48. 55. 65. 70. 77. 73. 68. 60. 50.
END MON-ASLT

MON-BSLT
*** <PLS > Value of BSLT at start of each month (deg F/F)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
   101 117 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15
END MON-BSLT

MON-ULTP1
*** <PLS > Value of ULTP1 at start of each month in deg F (TSOPFG=1)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
   101 117 52. 52. 52. 56. 62. 70. 77. 77. 73. 68. 60. 54.
END MON-ULTP1

MON-ULTP2
*** <PLS > Value of ULTP2 at start of each month in Deg F/F (TSOPFG=1)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
   101 117 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15 0.15
END MON-ULTP2

MON-LGTP1
*** <PLS > Value of LGTP1 at start of each month in Deg F (TSOPFG=1)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
   101 117 48. 48. 52. 58. 60. 63. 63. 64. 60. 55. 52. 48.
END MON-LGTP1

PSTEMP-TEMPS
*** <PLS > Initial temperatures (deg F)
*** x - x      AIRTC      SLTMP      ULTMP      LGTMP
   101 117      40.      45.      50.      69.
END PSTEMP-TEMPS

PWT-PARM1
*** <PLS > Flags for section PWTGAS
*** x - x IDV ICV GDV GVC
   101 117 0 0 0 0
END PWT-PARM1

PWT-PARM2
*** Second group of PWTGAS parms
*** <PLS >      ELEV      IDOXP      ICO2P      ADOXP      ACO2P
*** x - x      (ft)      (mg/l)    (mg C/l)    (mg/l)    (mg C/l)
   101 117      25.      4.0      0.15      4.0      0.15
END PWT-PARM2

MON-IFWDOX
*** <PLS > Value at start of each month for interflow DO concentration (mg/l)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
   101 117 12.7 12.7 11.2 9.70 7.40 6.60 6.20 6.20 7.00 8.40 9.40 11.6
END MON-IFWDOX

MON-GRNDDOX

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```
*** <PLS >Value at start of each month for groundwater DO concentration (mg/l)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
101 117 10.0 10.0 10.0 10.0 7.50 5.50 5.00 5.00 5.50 7.50 9.0 10.0
END MON-GRNDDOX
```

```
PWT-TEMPS
*** <PLS > Initial water temperatures (deg F)
*** x - x SOTMP IOTMP AOTMP
101 117 45. 50. 69.
END PWT-TEMPS
```

```
PWT-GASES
*** Initial DO and CO2 concentrations
*** <PLS > SODOX SOCO2 IODOX IOCO2 AODOX AOCO2
*** x - x (mg/l) (mg C/l) (mg/l) (mg C/l) (mg/l) (mg C/l)
101 117 8.8 0.15 4.0 0.15 4.0 0.15
END PWT-GASES
```

```
NQUALS
*** <PLS >
*** x - xNQUAL
101 117 4
END NQUALS
```

```
PQL-AD-FLAGS
*** Atmospheric Deposition Flags
*** < PLS> QUAL1 QUAL2 QUAL3 QUAL4 QUAL5 QUAL6 QUAL7 QUAL8 QUAL9 QUAL10
*** x - x <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C>
101 117 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
END PQL-AD-FLAGS
```

```
QUAL-PROPS
*** <PLS > Identifiers and Flags
*** x - x QUALID QTID QSD VPFW VPFS QSO VQO QIFW VIQC QAGW VAQC
101 117NH3+NH4 LBS 0 0 0 1 0 1 0 1 0
END QUAL-PROPS
```

```
QUAL-INPUT
*** Storage on surface and nonseasonal parameters
*** SQO POTFW POTFS ACQOP SQOLIM WSQOP IOQC AOQC
*** <PLS > qty/ac qty/ton qty/ton qty/ ac.day qty/ac in/hr qty/ft3 qty/ft3
*** x - x
101 0.1 0. 0. 0.1520 0.3 1.2 1.6E-05 4.0E-06
102 0.1 0. 0. 0.1530 0.3 1.2 1.6E-05 4.0E-06
103 0.1 0. 0. 0.1540 0.3 1.2 1.6E-05 4.0E-06
104 0.1 0. 0. 0.1550 0.3 1.2 1.6E-05 4.0E-06
105 0.01 0. 0. 0.0006 0.02 0.4 1.6E-05 4.0E-06
106 0.1 0. 0. 0.0900 0.2 1.4 1.6E-05 4.0E-06
107 0.1 0. 0. 0.0900 0.2 1.4 1.6E-05 4.0E-06
108 0.1 0. 0. 0.0900 0.2 1.4 1.6E-05 4.0E-06
109 0.01 0. 0. 0.0170 0.03 1.2 1.6E-05 4.0E-06
110 0.01 0. 0. 0.0080 0.02 0.4 1.6E-05 4.0E-06
111 0.01 0. 0. 0.0170 0.03 1.2 1.6E-05 4.0E-06
112 0.1 0. 0. 0.0500 0.2 1.2 1.6E-05 4.0E-06
113 0.01 0. 0. 0.001 0.01 0.4 1.6E-05 4.0E-06
114 0.1 0. 0. 0.0900 0.2 1.4 1.6E-05 4.0E-06
115 0.01 0. 0. 0.0170 0.03 1.4 1.6E-05 4.0E-06
116 1.0 0. 0. 0.1530 2.0 1.2 1.6E-04 4.0E-05
117 0.1 0. 0. 0.1530 0.3 1.2 1.6E-05 4.0E-06
END QUAL-INPUT
```

```
QUAL-PROPS
*** <PLS > Identifiers and Flags
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```
*** x - x    QUALID      QTID  QSD  VPFW  VPFS   QSO   VQO  QIFW  VIQC  QAGW  VAQC
101 117NO3      LBS    0    0    0     1     0    1    0    1    0
END QUAL-PROPS
```

QUAL-INPUT

```
***          Storage on surface and nonseasonal parameters
***          SQO   POTFW  POTFS   ACQOP  SQOLIM  WSQOP   IOQC   AOQC
*** <PLS >  qty/ac qty/ton qty/ton   qty/   qty/ac   in/hr  qty/ft3  qty/ft3
*** x - x          ac.day
101 117    0.04    0.    0.  0.0057  0.08    0.7  6.2E-06  6.2E-06
END QUAL-INPUT
```

QUAL-PROPS

```
*** <PLS > Identifiers and Flags
*** x - x    QUALID      QTID  QSD  VPFW  VPFS   QSO   VQO  QIFW  VIQC  QAGW  VAQC
101 117ORTHO P      LBS    0    0    0     1     0    1    0    1    0
END QUAL-PROPS
```

QUAL-INPUT

```
***          Storage on surface and nonseasonal parameters
***          SQO   POTFW  POTFS   ACQOP  SQOLIM  WSQOP   IOQC   AOQC
*** <PLS >  qty/ac qty/ton qty/ton   qty/   qty/ac   in/hr  qty/ft3  qty/ft3
*** x - x          ac.day
101          0.2    0.    0.  0.0740  0.2    1.2  3.2E-06  1.0E-06
102          0.2    0.    0.  0.0760  0.3    1.2  3.2E-06  1.0E-06
103          0.2    0.    0.  0.0770  0.3    1.2  3.2E-06  1.0E-06
104          0.2    0.    0.  0.0770  0.3    1.2  3.2E-06  1.0E-06
105          0.01   0.    0.  0.0010  0.1    0.4  3.2E-06  1.0E-06
106          0.1    0.    0.  0.0076  0.1    1.4  3.2E-06  1.0E-06
107          0.1    0.    0.  0.0076  0.1    1.4  3.2E-06  1.0E-06
108          0.1    0.    0.  0.0076  0.1    1.4  3.2E-06  1.0E-06
109          0.1    0.    0.  0.0110  0.1    1.2  3.2E-06  1.0E-06
110          0.01   0.    0.  0.0013  0.1    0.4  3.2E-06  1.0E-06
111          0.1    0.    0.  0.0110  0.1    1.2  3.2E-06  1.0E-06
112          0.1    0.    0.  0.0110  0.1    1.2  3.2E-06  1.0E-06
113          0.01   0.    0.  0.0010  0.1    1.2  3.2E-06  1.0E-06
114          0.1    0.    0.  0.0076  0.1    1.4  3.2E-06  1.0E-06
115          0.1    0.    0.  0.0110  0.1    1.4  3.2E-06  1.0E-06
116          2.0    0.    0.  0.0760  2.0    1.2  3.2E-05  1.0E-05
117          0.1    0.    0.  0.0760  0.3    1.2  3.2E-06  1.0E-06
END QUAL-INPUT
```

QUAL-PROPS

```
*** <PLS > Identifiers and Flags
*** x - x    QUALID      QTID  QSD  VPFW  VPFS   QSO   VQO  QIFW  VIQC  QAGW  VAQC
101 117BOD      LBS    0    0    0     1     0    1    0    1    0
END QUAL-PROPS
```

QUAL-INPUT

```
***          Storage on surface and nonseasonal parameters
***          SQO   POTFW  POTFS   ACQOP  SQOLIM  WSQOP   IOQC   AOQC
*** <PLS >  qty/ac qty/ton qty/ton   qty/   qty/ac   in/hr  qty/ft3  qty/ft3
*** x - x          ac.day
101          1.    0.    0.  0.614   3.    0.7  2.5E-04  6.2E-05
102          1.    0.    0.  0.638   5.    0.7  2.5E-04  6.2E-05
103          1.    0.    0.  0.654   5.    0.7  2.5E-04  6.2E-05
104          1.    0.    0.  0.656   5.    0.5  2.5E-04  6.2E-05
105          0.1    0.    0.  0.100   1.    0.5  2.5E-04  6.2E-05
106          1.    0.    0.  0.406   5.    1.4  2.5E-04  6.2E-05
107          1.    0.    0.  0.406   5.    1.4  2.5E-04  6.2E-05
108          1.    0.    0.  0.406   5.    1.4  2.5E-04  6.2E-05
109          1.    0.    0.  0.198   3.    0.7  2.5E-04  6.2E-05
110          1.    0.    0.  0.100   5.    0.7  2.5E-04  6.2E-05
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

111      1.      0.      0.      0.300      3.      0.7 2.5E-04 6.2E-05
112      1.      0.      0.      0.198      3.      0.7 2.5E-04 6.2E-05
113      0.1     0.      0.      0.020     0.1     0.7 2.5E-04 6.2E-05
114      1.      0.      0.      0.406      5.      1.4 2.5E-04 6.2E-05
115      1.      0.      0.      0.198      3.      1.4 2.5E-04 6.2E-05
116      10.     0.      0.      0.638     50.     0.7 2.5E-03 6.2E-04
117      1.      0.      0.      0.638      5.      1.1 2.5E-04 6.2E-05
END QUAL-INPUT

END PERLND

IMPLND
ACTIVITY
*** <ILS >           Active Sections
*** x - x ATMP SNOW IWAT  SLD  IWG IQAL
101 104  1  0  1  1  1  1
END ACTIVITY

PRINT-INFO
*** <ILS > ***** Print-flags ***** PIVL  PYR
*** x - x ATMP SNOW IWAT  SLD  IWG IQAL *****
101 104  4  4  4  4  4  4  1  12
END PRINT-INFO

BINARY-INFO
*** <ILS > ***** Binary-Output-flags ***** PIVL  PYR
*** x - x ATMP SNOW IWAT  SLD  IWG IQAL *****
101 104  4  4  4  4  4  4  1  12
END BINARY-INFO

GEN-INFO
***           Name           Unit-systems   Printer BinaryOut
*** <ILS >           t-series  Engl Metr Engl Metr
*** x - x           in  out
101   Developed Open Space   1  1  0  0  92  0
102   Developed Low Intens   1  1  0  0  92  0
103   Developed Medium Int   1  1  0  0  92  0
104   Developed High Inten   1  1  0  0  92  0
END GEN-INFO

ATEMP-DAT
*** <ILS >   ELDAT   AIRTEMP
*** x - x   (ft)   (deg F)
101 104   -6.    33.
END ATEMP-DAT

IWAT-PARM1
*** <ILS >           Flags
*** x - x CSNO RTOP  VRS  VNN RTLI
101 104  0  1  0  0  0
END IWAT-PARM1

IWAT-PARM2
*** <ILS >   LSUR   SLSUR   NSUR   RETSC
*** x - x   (ft)   (in)
101 104  100.  0.0028  0.07  0.07
END IWAT-PARM2

IWAT-PARM3
*** <ILS >   PETMAX  PETMIN
*** x - x   (deg F)  (deg F)
101 104  40.    35.
END IWAT-PARM3

```

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B*

```

IWAT-STATE1
*** <ILS > IWATER state variables (inches)
*** x - x      RETS      SURS
      101 104      0.      0.
      END IWAT-STATE1

SLD-PARM1
*** <ILS >      Flags
*** x - x VASD VRSD SDOP
      101 104      0      0      1
      END SLD-PARM1

SLD-PARM2
***
*** <ILS >      KEIM      JEIM      ACCSDP      REMSDP
*** x - x      tons/      /day
*** x - x      ac.day
      101 104      0.2      2.      0.010      0.01
      END SLD-PARM2

SLD-STOR
*** <ILS > Solids storage (tons/acre)
*** x - x
      101 104      0.01
      END SLD-STOR

IWT-PARM1
*** <ILS > Flags for section IWTGAS
*** x - x WTFV CSNO
      101 104      0      0
      END IWT-PARM1

IWT-PARM2
***
*** <ILS >      Second group of IWTGAS parms
*** x - x      ELEV      AWTF      BWTF
*** x - x      (ft)      (deg F) (deg F/F)
      101 104      20.      40.      0.3
      END IWT-PARM2

MON-AWTF
*** <ILS > Value of AWTF at start of each month (deg F)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
      101 104 29.0 29.0 30.0 34.0 54.0 63.0 65.0 64.0 60.0 48.0 35.0 30.0
      END MON-AWTF

MON-BWTF
*** <ILS > Value of BWTF at start of each month (deg F/F)
*** x - x JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC
      101 104 .55 .55 .65 .75 .90 1.1 1.2 1.1 1.0 .65 .65 .60
      END MON-BWTF

NQUALS
*** <ILS >
*** x - xNQUAL
      101 104      4
      END NQUALS

IQL-AD-FLAGS
***
*** < ILS>      Atmospheric Deposition Flags
*** x - x <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C> <F><C>
      101 104 -1 0 -1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
      END IQL-AD-FLAGS

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```
QUAL-PROPS
*** <ILS > Identifiers and Flags
*** x - x QUALID QTID QSD VPFW QSO VQO
101 104NH3+NH4 LBS 0 0 1 0
END QUAL-PROPS

QUAL-INPUT
*** Storage on surface and nonseasonal parameters
*** SQO POTFW ACQOP SQOLIM WSQOP
*** <ILS > qty/ac qty/ton qty/ qty/ac in/hr
*** x - x ac.day
101 104 0.05 0. 0.014 0.1 0.3
END QUAL-INPUT

QUAL-PROPS
*** <ILS > Identifiers and Flags
*** x - x QUALID QTID QSD VPFW QSO VQO
101 104NO3 LBS 0 0 1 0
END QUAL-PROPS

QUAL-INPUT
*** Storage on surface and nonseasonal parameters
*** SQO POTFW ACQOP SQOLIM WSQOP
*** <ILS > qty/ac qty/ton qty/ qty/ac in/hr
*** x - x ac.day
101 104 0.05 0. 0.006 0.1 0.2
END QUAL-INPUT

QUAL-PROPS
*** <ILS > Identifiers and Flags
*** x - x QUALID QTID QSD VPFW QSO VQO
101 104ORTHO P LBS 0 0 1 0
END QUAL-PROPS

QUAL-INPUT
*** Storage on surface and nonseasonal parameters
*** SQO POTFW ACQOP SQOLIM WSQOP
*** <ILS > qty/ac qty/ton qty/ qty/ac in/hr
*** x - x ac.day
101 104 0.10 0. 0.010 0.2 0.3
END QUAL-INPUT

QUAL-PROPS
*** <ILS > Identifiers and Flags
*** x - x QUALID QTID QSD VPFW QSO VQO
101 104BOD LBS 0 0 1 0
END QUAL-PROPS

QUAL-INPUT
*** Storage on surface and nonseasonal parameters
*** SQO POTFW ACQOP SQOLIM WSQOP
*** <ILS > qty/ac qty/ton qty/ qty/ac in/hr
*** x - x ac.day
101 104 1. 0. 0.13 2. 0.3
END QUAL-INPUT

END IMPLND

RCHRES
ACTIVITY
*** RCHRES Active sections
*** x - x HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

1 18 1 1 0 1 1 0 1 1 1 0
END ACTIVITY

PRINT-INFO

*** RCHRES Printout level flags
*** x - x HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR
1 18 4 4 4 4 4 4 4 4 1 12
END PRINT-INFO

BINARY-INFO

*** RCHRES Binary Output level flags
*** x - x HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR
1 18 4 4 4 4 4 4 4 4 1 12
END BINARY-INFO

GEN-INFO

*** Name Nexits Unit Systems Printer
*** RCHRES t-series Engl Metr LKFG
*** x - x in out
1 CB7upper 1 1 1 91 0 0 92 0
2 Dognash 1 1 1 91 0 0 92 0
3 CB7lower 1 1 1 91 0 0 92 0
4 CB6 1 1 1 91 0 0 92 0
5 TGupper 1 1 1 91 0 0 92 0
6 TGmidI10 1 1 1 91 0 0 92 0
7 CCupper 1 1 1 91 0 0 92 0
8 CB5 1 1 1 91 0 0 92 0
9 CB4 1 1 1 91 0 0 92 0
10 CClower 1 1 1 91 0 0 92 0
11 Sandy Creek 1 1 1 91 0 0 92 0
12 CB3_5 1 1 1 91 0 0 92 0
13 TGlower 1 1 1 91 0 0 92 0
14 CB2_5 1 1 1 91 0 0 92 0
15 CNB 1 1 1 91 0 0 92 0
16 CB2 1 1 1 91 0 0 92 0
17 CO3 1 1 1 91 0 0 92 0
18 CB0_5 1 1 1 91 0 0 92 0
END GEN-INFO

HYDR-PARM1

*** Flags for HYDR section
***RC HRES VC A1 A2 A3 ODFVFG for each *** ODGTFG for each FUNCT for each
*** x - x FG FG FG FG possible exit *** possible exit possible exit
1 18 0 1 1 1 4 0 0 0 0 0 0 0 0 0 1 1 1 1 1
END HYDR-PARM1

HYDR-PARM2

*** RCHRES FTBW FTBU LEN DELTH STCOR KS DB50
*** x - x (miles) (ft) (ft) (in)
1 0. 1. 9.04 29.5 3.2 0.5 0.008
2 0. 2. 8.58 22. 3.2 0.5 0.008
3 0. 3. 9.79 13.1 3.2 0.5 0.008
4 0. 4. 7.08 13.8 3.2 0.5 0.008
5 0. 5. 6.63 5.2 3.2 0.5 0.008
6 0. 6. 5.01 9.2 3.2 0.5 0.008
7 0. 7. 5.65 16.4 3.2 0.5 0.008
8 0. 8. 4.94 2.3 3.2 0.5 0.007
9 0. 9. 3.03 1.5 3.2 0.5 0.004
10 0. 10. 3.7 4.9 3.2 0.5 0.007
11 0. 11. 5.18 13.1 3.2 0.5 0.007
12 0. 12. 3.48 2. 3.2 0.5 0.004
13 0. 13. 5.87 8.8 3.2 0.5 0.004
14 0. 14. 4.21 1. 3.2 0.5 0.005

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

15      0. 15.      4.6      5.6      3.2      0.5      0.007
16      0. 16.      2.59     0.4      3.2      0.5      0.006
17      0. 17.      3.02     2.       3.2      0.5      0.006
18      0. 18.      3.2      0.2      3.2      0.5      0.003
END HYDR-PARM2

HYDR-INIT
***      Initial conditions for HYDR section
***RC HRES      VOL CAT Initial value of COLIND      initial value of OUTDGT
*** x - x      ac-ft      for each possible exit      for each possible exit,ft3
1 18 10.      4.2 4.5 4.5 4.5 4.2      2.1 1.2 0.5 1.2 1.8
END HYDR-INIT

ADCALC-DATA
*** RCHRES Data for section ADCALC
*** x - x      CRRAT      VOL (ac-ft)
1 18 1.7      100.
END ADCALC-DATA

HT-BED-FLAGS
*** RCHRES Bed Heat Conductance Flags
*** x - x BDFG TGFG TSTP
1 18 1 3 55
END HT-BED-FLAGS

HEAT-PARM
*** RCHRES      ELEV      ELDAT      CFSAX      KATRAD      KCOND      KEVAP
*** x - x      (ft)      (ft)
1 10.      -6.      0.2      9.37      6.12      2.24
2 10.      -6.      0.2      9.37      6.12      2.24
3 6.      -10.     0.2      9.37      6.12      2.24
4 4.      -12.     0.2      9.37      6.12      2.24
5 6.      -10.     0.2      9.37      6.12      2.24
6 4.      -12.     0.2      9.37      6.12      2.24
7 4.      -12.     0.2      9.37      6.12      2.24
8 1.      -15.     0.2      9.37      6.12      2.24
9 0.      -16.     0.2      9.37      6.12      2.24
10 0.      -16.     0.4      9.37      6.12      2.24
11 0.      -16.     0.4      9.37      6.12      2.24
12 0.      -16.     0.4      9.37      6.12      2.24
13 0.      -16.     0.4      9.37      6.12      2.24
14 0.      -16.     0.6      9.37      6.12      2.24
15 0.      -16.     0.4      9.37      6.12      2.24
16 0.      -16.     0.75     9.37      6.12      2.24
17 0.      -16.     0.75     9.37      6.12      2.24
18 0.      -16.     0.75     9.37      6.12      2.24
END HEAT-PARM

HT-BED-PARM
***      Bed Heat Conduction Parameters for Single and Two-layer Methods
*** RCHRES      MUDDEP      TGRND      KMUD      KGRND
*** x - x      (ft)      (deg F)      (kcal/m2/C/hr)
1 18 0.8      70.      20.      1.4
END HT-BED-PARM

MON-HT-TGRND
*** RCHRES Monthly values of ground temperatures (deg F)
*** x - x TG1 TG2 TG3 TG4 TG5 TG6 TG7 TG8 TG9 TG10 TG11 TG12
1 18 56. 55. 58. 63. 68. 74. 79. 82. 81. 75. 68. 60.
END MON-HT-TGRND

HEAT-INIT
*** RCHRES      TW      AIRTMP

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```
*** x - x (deg F) (deg F)
    1 18 48. 40.
END HEAT-INIT
```

```
SANDFG
*** RCHRES
*** x - x SANDFG
    1 18 3
END SANDFG
```

```
SED-GENPARM
*** RCHRES BEDWID BEDWRN POR
*** x - x (ft) (ft)
    1 15. 6. 0.3
    2 9. 6. 0.3
    3 15. 6. 0.3
    4 9. 6. 0.27
    5 8. 6. 0.3
    6 15. 6. 0.3
    7 8. 6. 0.3
    8 40. 6. 0.28
    9 50. 6. 0.51
   10 20. 6. 0.3
   11 15. 6. 0.3
   12 60. 6. 0.4
   13 30. 6. 0.4
   14 240. 6. 0.6
   15 20. 6. 0.3
   16 220. 6. 0.5
   17 100. 6. 0.5
   18 300. 6. 0.6
END SED-GENPARM
```

```
SAND-PM
*** RCHRES D W RHO KSAND EXPSND
*** x - x (in) (in/sec) (gm/cm3)
    1 18 0.0079 0.46 2.60 0.8 3.2
END SAND-PM
```

```
SILT-CLAY-PM
*** RCHRES D W RHO TAUCD TAUCS M
*** x - x (in) (in/sec) gm/cm3 lb/ft2 lb/ft2 lb/ft2.d
    1 0.00160 0.018 2.60 0.020 0.130 0.05
    2 0.00160 0.018 2.60 0.020 0.130 0.05
    3 0.00160 0.018 2.60 0.020 0.088 0.05
    4 0.00160 0.018 2.60 0.020 0.116 0.05
    5 0.00160 0.018 2.60 0.020 0.030 0.05
    6 0.00160 0.018 2.60 0.020 0.048 0.05
    7 0.00160 0.018 2.60 0.020 0.085 0.05
    8 0.00160 0.018 2.60 0.020 0.028 0.05
    9 0.00160 0.018 2.60 0.020 0.033 0.05
   10 0.00160 0.018 2.60 0.020 0.041 0.05
   11 0.00160 0.018 2.60 0.020 0.065 0.05
   12 0.00160 0.018 2.60 0.020 0.045 0.05
   13 0.00160 0.018 2.60 0.020 0.055 0.05
   14 0.00160 0.018 2.60 0.020 0.020 0.05
   15 0.00160 0.018 2.60 0.020 0.035 0.05
   16 0.00160 0.018 2.60 0.020 0.020 0.05
   17 0.00160 0.018 2.60 0.020 0.030 0.05
   18 0.00160 0.018 2.60 0.020 0.020 0.05
END SILT-CLAY-PM
```

```
SILT-CLAY-PM
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

*** RCHRES      D          W          RHO      TAUCD      TAUCS      M
*** x - x      (in)     (in/sec)   gm/cm3   lb/ft2    lb/ft2    lb/ft2.d
  1      0.00006  0.00005   2.60    0.015    0.100    0.05
  2      0.00006  0.00005   2.60    0.015    0.100    0.05
  3      0.00006  0.00005   2.60    0.015    0.065    0.05
  4      0.00006  0.00005   2.60    0.015    0.089    0.05
  5      0.00006  0.00005   2.60    0.015    0.018    0.05
  6      0.00006  0.00005   2.60    0.015    0.046    0.05
  7      0.00006  0.00005   2.60    0.015    0.070    0.05
  8      0.00006  0.00005   2.60    0.015    0.022    0.05
  9      0.00006  0.00005   2.60    0.015    0.026    0.05
 10      0.00006  0.00005   2.60    0.015    0.034    0.05
 11      0.00006  0.00005   2.60    0.015    0.035    0.05
 12      0.00006  0.00005   2.60    0.015    0.037    0.05
 13      0.00006  0.00005   2.60    0.015    0.044    0.05
 14      0.00006  0.00005   2.60    0.015    0.015    0.05
 15      0.00006  0.00005   2.60    0.015    0.016    0.05
 16      0.00006  0.00005   2.60    0.015    0.015    0.05
 17      0.00006  0.00005   2.60    0.015    0.015    0.05
 18      0.00006  0.00005   2.60    0.015    0.015    0.05
END SILT-CLAY-PM

```

```

SSED-INIT
*** RCHRES      Suspended sed concs (mg/l)
*** x - x      Sand      Silt      Clay
  1  18      1.      5.      5.
END SSED-INIT

```

```

BED-INIT
*** RCHRES      BEDDEP      Initial bed composition
*** x - x      (ft)      Sand      Silt      Clay
  1   5      1.5      0.880    0.050    0.070
  6   8      1.5      0.780    0.120    0.100
  9      1.5      0.520    0.120    0.360
 10      1.5      0.800    0.100    0.100
 11      1.5      0.800    0.100    0.100
 12      1.5      0.700    0.100    0.200
 13      1.5      0.700    0.100    0.200
 14      1.5      0.550    0.090    0.360
 15      1.5      0.700    0.100    0.200
 16  17      1.5      0.670    0.080    0.250
 18      1.5      0.500    0.170    0.330
END BED-INIT

```

```

BENTH-FLAG
*** RCHRES      Benthic release flag
*** x - x      BENF
  1  18      1
END BENTH-FLAG

```

```

OX-FLAGS
*** RCHRES      Oxygen flags
*** x - x      REAM
  1  18      2
END OX-FLAGS

```

```

OX-GENPARM
*** RCHRES      KBOD20      TCBOD      KODSET      SUPSAT
*** x - x      /hr      ft/hr
  1  18      0.002      1.047      0.001      1.
END OX-GENPARM

```

```

OX-BENPARM

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

*** RCHRES      BENOD      TCBEN      EXPOD      BRBOD (1)  BRBOD (2)  EXPREL
*** x - x      mg/m2.hr      mg/m2.hr      mg/m2.hr      mg/m2.hr
1      150.      1.074      1.22      0.1      0.1      2.82
2      150.      1.074      1.22      0.1      0.1      2.82
3      150.      1.074      1.22      0.1      0.1      2.82
4      150.      1.074      1.22      0.1      0.1      2.82
5      150.      1.074      1.22      0.1      0.1      2.82
6      150.      1.074      1.22      0.1      0.1      2.82
7      150.      1.074      1.22      0.1      0.1      2.82
8      150.      1.074      1.22      0.1      0.1      2.82
9      150.      1.074      1.22      0.1      0.1      2.82
10     150.      1.074      1.22      0.1      0.1      2.82
11     150.      1.074      1.22      0.1      0.1      2.82
12     150.      1.074      1.22      0.1      0.1      2.82
13     150.      1.074      1.22      0.1      0.1      2.82
14     150.      1.074      1.22      0.1      0.1      2.82
15     150.      1.074      1.22      0.1      0.1      2.82
16     150.      1.074      1.22      0.1      0.1      2.82
17     150.      1.074      1.22      0.1      0.1      2.82
18     150.      1.074      1.22      0.1      0.1      2.82
END OX-BENPARM
  
```

```

OX-TCGINV
*** RCHRES      Temperature correction coef
*** x - x      TCGINV
1      18      1.047
END OX-TCGINV
  
```

```

OX-REAPARM
*** RCHRES      TCGINV      REAK      EXPRED      EXPREV
*** x - x      /hr
1      18      1.024      0.2      -1.673      0.969
END OX-REAPARM
  
```

```

OX-INIT
*** RCHRES      DOX      BOD      SATDO
*** x - x      mg/l      mg/l      mg/l
1      18      8.      3.5      13.5
END OX-INIT
  
```

```

NUT-FLAGS
*** RCHRES      Nutrient flags
*** x - x      NH3      NO2      PO4      AMV      DEN      ADNH      ADPO      PHFL
1      18      1      0      1      0      1      0      1      2
END NUT-FLAGS
  
```

```

CONV-VAL1
*** RCHRES      CVBO      CVBPC      CVBPN      BPCNTC
*** x - x      mg/mg      mols/mol      mols/mol
1      18      1.63      106.      16.      49.
END CONV-VAL1
  
```

```

NUT-BENPARM
*** RCHRES      BRNIT (1)  BRNIT (2)  BRPO4 (1)  BRPO4 (2)  ANAER
*** x - x      mg/m2.hr      mg/m2.hr      mg/m2.hr      mg/m2.hr      mg/l
1      18      0.      0.      0.      0.      0.1
END NUT-BENPARM
  
```

```

NUT-NITDENIT
*** RCHRES      KTAM20      KNO220      TCNIT      KNO320      TCDEN      DENOXT
*** x - x      /hr      /hr      /hr      /hr      mg/l
1      18      0.01      0.002      1.07      0.02      1.04      2.
END NUT-NITDENIT
  
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

NUT-ADSPARM
*** RCHRES      Partition coefficients for NH4 AND PO4 (ml/g)
*** x - x NH4-sand NH4-silt NH4-clay PO4-sand PO4-silt PO4-clay
    1  18    1E-10    1E-10    1E-10    1E-10    0.1    1.
END NUT-ADSPARM

NUT-DINIT
*** RCHRES      NO3      TAM      NO2      PO4      PHVAL
*** x - x      mg/l     mg/l     mg/l     mg/l
    1  18    0.1     0.1     0.01    0.05     7.
END NUT-DINIT

PLNK-FLAGS
*** RCHRES Plankton flags
*** x - x PHYF ZOOF BALF SDLT AMRF DECF NSFG ZFOO BNP
    1  18    1    0    1    0    0    1    1    2    0
END PLNK-FLAGS

PLNK-PARM1
***RC HRES      RATCLP      NONREF      LITSED      ALNPR      EXTB      MALGR      PARADF
*** x - x      /mg.ft     /ft     /hr
    1  18    0.68    0.25     0.     0.75    0.3    0.085    1.
END PLNK-PARM1

PLNK-PARM2
***RC HRES      CMLLT      CMMN      CMMNP      CMP      TALGRH      TALGRL      TALGRM
*** x - x      ly/min     mg/l     mg/l     mg/l     deg F     deg F     deg F
    1  18    0.01    0.025    0.0001  0.005    95.    -20.    86.
END PLNK-PARM2

PLNK-PARM3
*** RCHRES      ALR20      ALDH      ALDL      OXALD      NALDH      PALDH
*** x - x      /hr     /hr     /hr     /hr     mg/l     mg/l
    1  18    0.005    0.02    0.001    0.03    0.01    0.002
END PLNK-PARM3

PHYTO-PARM
*** RCHRES      SEED      MXSTAY      OREF      CLALDH      PHYSET      REFSET
*** x - x      mg/l     mg/l     ft3/s     ug/l     ft/hr     ft/hr
    1  18    1.     2.     100.    20.    0.005    0.010
END PHYTO-PARM

BENAL-PARM
***RC HRES      MBAL      CFBALR      CFBALG      MINBAL      CAMPR      FRAVL      NMAXFX
*** x - x      mg/m2     mg/l     mg/m2     mg/l     mg/l     mg/l
    1  18    2500.    0.35     1.     0.0001  0.001    0.     10.
END BENAL-PARM

PLNK-INIT
*** RCHRES      PHYTO      ZOO      BENAL      ORN      ORP      ORC
*** x - x      mg/l     org/l     mg/m2     mg/l     mg/l     mg/l
    1  18    0.5     0.03    2500.    1.0     0.1     0.5
END PLNK-INIT

END RCHRES

FTABLES

FTABLE      1
rows cols
  16    4
depth      area      volume      outflow1 ***

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

0.	0.	0.	0.
0.2	10.	1.	0.
1.	33.	23.	0.
2.	43.	66.	24.
3.	44.	110.	40.
4.	46.	156.	56.
5.	47.	203.	111.
6.	48.	251.	184.
8.	49.	350.	287.
10.	55.	460.	419.
12.	66.	590.	647.
14.	82.	755.	896.
16.	110.	975.	1245.
18.	137.	1248.	1709.
20.	4383.	10015.	14623.
22.	7013.	24040.	37088.

END FTABLE 1

FTABLE 2

rows cols ***

16 4

depth	area	volume	outflow1	***
0.	0.	0.	0.	
0.2	4.8	0.48	0.	
1.	15.6	11.1	0.	
2.	20.3	31.4	12.	
3.	20.8	52.2	20.	
4.	21.8	74.	28.	
5.	22.4	96.	56.	
6.	22.9	119.	92.	
8.	23.4	166.	144.	
10.	26.	218.	210.	
12.	31.	280.	324.	
14.	39.	358.	448.	
16.	52.	462.	623.	
18.	65.	592.	855.	
20.	520.	1632.	7312.	
22.	1040.	3712.	13135.	

END FTABLE 2

FTABLE 3

rows cols ***

16 4

depth	area	volume	outflow1	***
0.	0.	0.	0.	
0.2	11.	1.1	0.	
1.	36.	25.4	0.	
2.	46.	72.	24.	
3.	48.	119.	41.	
4.	50.	169.	57.	
5.	51.	220.	112.	
6.	52.	272.	184.	
8.	53.	379.	288.	
10.	59.	498.	420.	
12.	71.	640.	648.	
14.	89.	818.	898.	
16.	119.	1055.	1247.	
18.	148.	1352.	1711.	
20.	4747.	10845.	14625.	
22.	7595.	26035.	37090.	

END FTABLE 3

FTABLE 4

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

rows cols                                     ***
 18     4
  depth      area      volume  outflow1 ***
  0.         0.         0.         0.
  0.2        8.         0.69        0.1
  0.4       10.6        2.92         1.
  1.        17.2       12.9         10.
  2.        27.5       42.9         40.
  3.        32.6        73.         100.
  4.        36.9       111.6        150.
  5.        41.2       150.2        210.
  6.        46.3       206.         310.
  8.        51.5       275.         500.
 10.        66.9       429.         700.
 12.        79.        515.         900.
 14.       103.        687.        1300.
 16.       112.        944.        2100.
 18.       124.       1201.        3000.
 19.5      5003.       4205.        8100.
 22.      10006.      23000.       45300.
 25.     40026.      98050.     198000.
END FTABLE 4

```

```

FTABLE 5                                     ***
rows cols                                     ***
 12     4
  depth      area      volume  outflow1 ***
  0.         0.         0.         0.
  0.2        2.8         0.3         0.07
  1.         7.3         4.8          6.
  2.         8.2        13.         16.2
  3.         9.         22.         27.
  4.        11.3        33.         50.
  5.        24.8        58.         123.
  6.        28.1        86.         257.
  8.        43.9       174.         562.
 10.        84.4       343.        1236.
 12.       563.       1468.       5662.
 14.      1125.       3718.      15267.
END FTABLE 5

```

```

FTABLE 6                                     ***
rows cols                                     ***
 12     4
  depth      area      volume  outflow1 ***
  0.         0.         0.         0.
  0.2         3.         0.3         0.1
  1.         7.9         5.2          9.
  2.         8.8        14.         23.
  3.         9.7        23.7        39.
  4.        12.1        36.         71.
  5.        26.7        63.         175.
  6.        30.4        93.         367.
  8.        47.4       188.         800.
 10.       91.1       370.        1770.
 12.       607.       1584.       8090.
 14.      1215.       4014.      21800.
END FTABLE 6

```

```

FTABLE 7                                     ***
rows cols                                     ***
 14     4
  depth      area      volume  outflow1 ***

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

0.	0.	0.	0.
0.2	3.4	0.34	0.
0.6	4.9	1.66	0.
1.	8.9	4.1	0.01
2.	9.9	12.7	1.
3.	11.	22.7	20.
4.	13.	34.2	69.7
5.	15.1	48.	136.
7.	19.2	84.	327.
9.	24.	120.	536.
10.	53.4	155.	767.
12.	102.7	300.	1694.
14.	685.	1100.	8010.
16.	1370.	2600.	21727.

END FTABLE 7

FTABLE 8				***		
rows	cols			***		
18	4	depth	area	volume	outflow1	***
		0.	0.	0.	0.	
		0.2	3.	0.3	0.	
		0.5	6.	1.5	0.	
		1.	12.	5.5	0.05	
		2.	15.	17.5	3.	
		3.	24.	36.	20.	
		4.	26.	56.	100.	
		5.	29.	82.5	200.	
		6.	32.	112.	336.	
		8.	36.	180.	585.	
		10.	47.	260.	950.	
		12.	55.	350.	1440.	
		14.	72.	470.	2130.	
		16.	78.	600.	2960.	
		18.	87.	760.	3980.	
		20.	3490.	4500.	30000.	
		22.	6980.	12000.	100000.	
		25.	28000.	70000.	600000.	

END FTABLE 8

FTABLE 9				***		
rows	cols			***		
18	4	depth	area	volume	outflow1	***
		0.	0.	0.	0.	
		0.2	3.7	0.37	0.12	
		0.4	7.3	1.84	1.9	
		1.	10.3	8.	15.5	
		2.	11.8	19.8	52.	
		3.	12.9	32.6	98.	
		4.	14.	47.	165.	
		5.	15.4	62.	236.	
		6.	16.9	79.	322.	
		8.	19.1	117.	542.	
		10.	22.	161.	834.	
		12.	34.	229.	1308.	
		14.	44.	317.	1984.	
		16.	48.	412.	2800.	
		18.	53.	519.	3800.	
		20.	2141.	4800.	37900.	
		22.	4282.	13370.	112800.	
		25.	17130.	64760.	600000.	

END FTABLE 9

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

FTABLE      10
rows cols          ***
  14      4
  depth      area      volume      outflow1 ***
    0.         0.         0.         0.
    0.2        2.7        0.27        0.12
    0.6        3.9        1.82        2.43
    1.         7.         4.6         10.3
    2.         7.8        12.4        27.7
    3.         8.6        21.         46.9
    4.        10.2        31.         83.64
    5.        11.8        43.        163.4
    7.        15.1        73.        392.
    9.        18.8       111.        643.
   10.         42.       153.        920.
   12.        80.7       314.       2033.
   14.       538.      1391.      9613.
   16.     1076.     3543.     26073.
END FTABLE 10

```

```

FTABLE      11
rows cols          ***
  13      4
  depth      area      volume      outflow1 ***
    0.         0.         0.         0.
    0.5        3.1         0.5         0.
    1.         8.2         2.9         0.
    2.         9.1        10.2         0.5
    3.        10.        19.3         5.
    4.        11.9        30.         30.
    5.        13.8        42.         100.
    6.        17.6        57.         200.
    8.        22.         95.         380.
   10.        49.        165.         800.
   12.        94.        285.        1700.
   14.       628.       1000.       7000.
   16.     1256.     2600.     20000.
END FTABLE 11

```

```

FTABLE      13
rows cols          ***
  12      4
  depth      area      volume      outflow1 ***
    0.         0.         0.         0.
    0.5        3.6         0.8         0.
    1.        17.8         6.         0.
    2.        21.        21.5         1.
    3.        27.        44.         20.
    4.        28.5        69.         80.
    5.        29.9        97.         200.
    6.        31.3       127.         400.
    8.        55.5       220.         900.
   10.       107.       380.        1920.
   12.       712.      1300.       8200.
   14.     1423.     3000.     22000.
END FTABLE 13

```

```

FTABLE      12
rows cols          ***
  18      4
  depth      area      volume      outflow1 ***
    0.         0.         0.         0.

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

0.2	4.2	0.42	0.12
1.	8.4	7.2	12.
2.	11.8	19.	44.
3.	13.5	32.5	86.
4.	14.8	47.2	123.
5.	16.	63.	195.
6.	17.7	81.	270.
8.	19.4	120.	426.
10.	21.9	164.	660.
12.	25.3	214.	965.
14.	33.7	282.	1400.
16.	51.	383.	2100.
18.	67.	518.	3100.
20.	101.	720.	4600.
22.	2459.	5639.	38800.
25.	4918.	20394.	150000.
30.	19674.	118760.	960000.

END FTABLE 12

FTABLE 14

rows cols ***

18 4

depth	area	volume	outflow1	***
0.	0.	0.	0.	
0.2	15.	1.53	0.23	
1.	26.	21.9	20.	
2.	38.	60.2	75.	
3.	61.	121.5	175.	
4.	76.	198.	280.	
5.	92.	290.	480.	
6.	102.	392.	700.	
8.	122.	637.	1200.	
10.	153.	943.	2060.	
12.	179.	1300.	3180.	
14.	189.	1680.	4500.	
16.	204.	2090.	6200.	
18.	255.	2600.	8300.	
20.	510.	3620.	12600.	
22.	2975.	9600.	36000.	
25.	5950.	27400.	109000.	
30.	23800.	146400.	860000.	

END FTABLE 14

FTABLE 15

rows cols ***

12 4

depth	area	volume	outflow1	***
0.	0.	0.	0.	
0.5	2.8	0.5	0.	
1.	13.9	7.5	0.05	
2.	14.5	22.	39.	
3.	15.1	37.	66.	
4.	15.1	52.	112.	
5.	15.1	67.	205.	
6.	15.1	82.	354.	
8.	43.5	169.	789.	
10.	83.6	336.	1750.	
12.	558.	1452.	7800.	
14.	1115.	3682.	19800.	

END FTABLE 15

FTABLE 16

rows cols ***

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

18      4
  depth      area      volume  outflow1 ***
    0.         0.         0.         0.
   0.2        9.4        0.94        0.1
    1.       15.7       13.5        31.
    2.       23.5       37.         114.
    3.       31.4       68.         244.
    4.       37.7      106.         372.
    5.       40.8      147.         608.
    6.       44.       191.         850.
    8.       47.       285.        1360.
   10.       50.       386.        2090.
   12.       53.       492.        2980.
   14.       56.       605.        4050.
   16.       63.       731.        5350.
   18.       69.       869.        6920.
   20.       94.      1057.        9090.
   22.      1830.      4718.       43580.
   25.      3660.     15700.     155000.
   30.     14640.     88900.     963000.
END FTABLE 16

```

```

FTABLE      17
rows cols                                     ***
18      4
  depth      area      volume  outflow1 ***
    0.         0.         0.         0.
   0.2        11.         1.1         0.1
    1.       18.3       15.7         28.
    2.       25.6       41.4         99.
    3.       33.       74.3        205.
    4.       40.       115.        310.
    5.       48.       162.        520.
    6.       55.       217.        750.
    8.       62.       342.       1260.
   10.       77.       495.       2070.
   12.       95.       686.       3200.
   14.      110.       905.       4700.
   16.      128.      1160.       6600.
   18.      183.      1530.       9400.
   20.      366.      2260.      15000.
   22.     2134.      6530.      47000.
   25.     4270.     19330.     147000.
   30.    17070.    105000.     875000.
END FTABLE 17

```

```

FTABLE      18
rows cols                                     ***
18      4
  depth      area      volume  outflow1 ***
    0.         0.         0.         0.
   0.2       11.6         1.2         0.1
    1.       19.4       16.7         28.
    2.       29.1       45.8        103.
    3.       46.5       92.3        240.
    4.       58.2      151.        384.
    5.       69.8      220.        665.
    6.       77.6      298.        968.
    8.       93.1      484.       1680.
   10.      101.       686.       2700.
   12.      109.       903.       4000.
   14.      116.      1140.       5500.
   16.      136.      1410.       7500.

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

18.      194.      1800.      10400.
20.      388.      2570.      16100.
22.      2260.     7090.      47700.
25.      4523.    20660.    149000.
30.     18090.   111111.   877000.
  
```

```

END FTABLE 18
END FTABLES
  
```

COPY

```

TIMESERIES
Copy-opn***
*** x - x NPT NMN
    1  18  0  7
END TIMESERIES
  
```

END COPY

EXT SOURCES

```

<-Volume-> <Member> SsysSgap<--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name> x <Name> x tem strg<-factor->strg <Name> x x <Name> x x ***
*** Met Seg EVADALE
WDM2 35 PREC ENGL SAME PERLND 101 117 EXTNL PREC
WDM2 36 ATEM ENGL SAME PERLND 101 117 EXTNL GATMP
WDM2 39 DEWP ENGL SAME PERLND 101 117 EXTNL DTMPG
WDM2 38 WIND ENGL SAME PERLND 101 117 EXTNL WINMOV
WDM2 40 SOLR ENGL SAME PERLND 101 117 EXTNL SOLRAD
WDM2 42 PEVT ENGL SAME PERLND 101 117 EXTNL PETINP
*** Met Seg EVADALE
WDM2 35 PREC ENGL SAME IMPLND 101 104 EXTNL PREC
WDM2 36 ATEM ENGL SAME IMPLND 101 104 EXTNL GATMP
WDM2 39 DEWP ENGL SAME IMPLND 101 104 EXTNL DTMPG
WDM2 38 WIND ENGL SAME IMPLND 101 104 EXTNL WINMOV
WDM2 40 SOLR ENGL SAME IMPLND 101 104 EXTNL SOLRAD
WDM2 42 PEVT ENGL SAME IMPLND 101 104 EXTNL PETINP
*** Met Seg BPT
WDM2 35 PREC ENGL SAME RCHRES 1 18 EXTNL PREC
WDM2 36 ATEM ENGL SAME RCHRES 1 18 EXTNL GATMP
WDM2 39 DEWP ENGL SAME RCHRES 1 18 EXTNL DEWTMP
WDM2 38 WIND ENGL SAME RCHRES 1 18 EXTNL WIND
WDM2 40 SOLR ENGL SAME RCHRES 1 18 EXTNL SOLRAD
WDM2 41 CLOU ENGL SAME RCHRES 1 18 EXTNL CLOUD
WDM2 43 EVAP ENGL SAME RCHRES 1 18 EXTNL POTEV

WDM3 8111 BOD ENGL 47.9DIV RCHRES 1 INFLOW OXIF 2
WDM3 8112 TSS ENGL 47.9DIV RCHRES 1 INFLOW ISED 2
WDM3 8114 DNH3 ENGL 47.9DIV RCHRES 1 INFLOW NUIF1 2
WDM3 8115 DPO4 ENGL 47.9DIV RCHRES 1 INFLOW NUIF1 4
WDM3 7001 FLOW ENGL 0.13DIV RCHRES 1 INFLOW IVOL
WDM3 7002 BOD ENGL 8.36DIV RCHRES 1 INFLOW OXIF 2
WDM3 7003 DNH3 ENGL 3.08DIV RCHRES 1 INFLOW NUIF1 2
WDM3 7004 ORGN ENGL 5.12DIV RCHRES 1 INFLOW PKIF 3
WDM3 7005 DO ENGL 5.42DIV RCHRES 1 INFLOW OXIF 1
WDM3 8111 BOD ENGL 14.6DIV RCHRES 2 INFLOW OXIF 2
WDM3 8112 TSS ENGL 14.6DIV RCHRES 2 INFLOW ISED 2
WDM3 8114 DNH3 ENGL 14.6DIV RCHRES 2 INFLOW NUIF1 2
WDM3 8115 DPO4 ENGL 14.6DIV RCHRES 2 INFLOW NUIF1 4
WDM3 7001 FLOW ENGL 0.00DIV RCHRES 2 INFLOW IVOL
WDM3 7002 BOD ENGL 0.00DIV RCHRES 2 INFLOW OXIF 2
WDM3 7003 DNH3 ENGL 0.00DIV RCHRES 2 INFLOW NUIF1 2
WDM3 7004 ORGN ENGL 0.00DIV RCHRES 2 INFLOW PKIF 3
WDM3 7005 DO ENGL 0.00DIV RCHRES 2 INFLOW OXIF 1
WDM3 8111 BOD ENGL 9.4DIV RCHRES 3 INFLOW OXIF 2
WDM3 8112 TSS ENGL 9.4DIV RCHRES 3 INFLOW ISED 2
  
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

WDM3	8114	DNH3	ENGL	9.4DIV	RCHRES	3	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	9.4DIV	RCHRES	3	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	3	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	3	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	3	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	3	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	3	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	48.6DIV	RCHRES	4	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	48.6DIV	RCHRES	4	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	48.6DIV	RCHRES	4	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	48.6DIV	RCHRES	4	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	4	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	4	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	4	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	4	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	4	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	28.7DIV	RCHRES	5	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	28.7DIV	RCHRES	5	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	28.7DIV	RCHRES	5	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	28.7DIV	RCHRES	5	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	5	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	5	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	5	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	5	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	5	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	90.0DIV	RCHRES	6	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	90.0DIV	RCHRES	6	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	90.0DIV	RCHRES	6	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	90.0DIV	RCHRES	6	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	6	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	6	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	6	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	6	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	6	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	54.6DIV	RCHRES	7	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	54.6DIV	RCHRES	7	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	54.6DIV	RCHRES	7	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	54.6DIV	RCHRES	7	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	7	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	7	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	7	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	7	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	7	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	68.7DIV	RCHRES	8	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	68.7DIV	RCHRES	8	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	68.7DIV	RCHRES	8	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	68.7DIV	RCHRES	8	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	8	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	8	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	8	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	8	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	8	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	14.1DIV	RCHRES	9	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	14.1DIV	RCHRES	9	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	14.1DIV	RCHRES	9	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	14.1DIV	RCHRES	9	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	9	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	9	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	9	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	9	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	9	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	8.1DIV	RCHRES	10	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	8.1DIV	RCHRES	10	INFLOW	ISED	2

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

WDM3	8114	DNH3	ENGL	8.1DIV	RCHRES	10	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	8.1DIV	RCHRES	10	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	10	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	10	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	10	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	10	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	10	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	4.4DIV	RCHRES	11	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	4.4DIV	RCHRES	11	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	4.4DIV	RCHRES	11	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	4.4DIV	RCHRES	11	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.20DIV	RCHRES	11	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	14.28DIV	RCHRES	11	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	1.70DIV	RCHRES	11	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	1.39DIV	RCHRES	11	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	3.40DIV	RCHRES	11	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	2.7DIV	RCHRES	12	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	2.7DIV	RCHRES	12	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	2.7DIV	RCHRES	12	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	2.7DIV	RCHRES	12	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	12	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	12	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	12	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	12	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	12	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	48.9DIV	RCHRES	13	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	48.9DIV	RCHRES	13	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	48.9DIV	RCHRES	13	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	48.9DIV	RCHRES	13	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	13	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	13	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	13	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	13	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	13	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	3.7DIV	RCHRES	14	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	3.7DIV	RCHRES	14	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	3.7DIV	RCHRES	14	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	3.7DIV	RCHRES	14	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	14	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	14	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	14	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	14	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	14	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	18.9DIV	RCHRES	15	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	18.9DIV	RCHRES	15	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	18.9DIV	RCHRES	15	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	18.9DIV	RCHRES	15	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	15	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	15	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	15	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	15	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	15	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	27.2DIV	RCHRES	16	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	27.2DIV	RCHRES	16	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	27.2DIV	RCHRES	16	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	27.2DIV	RCHRES	16	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	16	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	16	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	16	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	16	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	16	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	10.3DIV	RCHRES	17	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	10.3DIV	RCHRES	17	INFLOW	ISED	2

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B*

WDM3	8114	DNH3	ENGL	10.3DIV	RCHRES	17	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	10.3DIV	RCHRES	17	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	17	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	17	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	17	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	17	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	17	INFLOW	OXIF	1
WDM3	8111	BOD	ENGL	3.5DIV	RCHRES	18	INFLOW	OXIF	2
WDM3	8112	TSS	ENGL	3.5DIV	RCHRES	18	INFLOW	ISED	2
WDM3	8114	DNH3	ENGL	3.5DIV	RCHRES	18	INFLOW	NUIF1	2
WDM3	8115	DPO4	ENGL	3.5DIV	RCHRES	18	INFLOW	NUIF1	4
WDM3	7001	FLOW	ENGL	0.000DIV	RCHRES	18	INFLOW	IVOL	
WDM3	7002	BOD	ENGL	0.0DIV	RCHRES	18	INFLOW	OXIF	2
WDM3	7003	DNH3	ENGL	0.0DIV	RCHRES	18	INFLOW	NUIF1	2
WDM3	7004	ORGN	ENGL	0.0DIV	RCHRES	18	INFLOW	PKIF	3
WDM3	7005	DO	ENGL	0.0DIV	RCHRES	18	INFLOW	OXIF	1
*** 6205 and 6206 are atmospheric deposition loads of NH3-N and NO3-N									
WDM3	7306	NO3N	ENGL	DIV	PERLND	101	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	101	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	102	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	102	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	103	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	103	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	104	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	104	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	105	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	105	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	106	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	106	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	107	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	107	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	108	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	108	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	109	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	109	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	110	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	110	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	111	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	111	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	112	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	112	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	113	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	113	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	114	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	114	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	115	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	115	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	116	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	116	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	PERLND	117	EXTNL	PQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	PERLND	117	EXTNL	PQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	IMPLND	101	EXTNL	IQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	IMPLND	101	EXTNL	IQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	IMPLND	102	EXTNL	IQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	IMPLND	102	EXTNL	IQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	IMPLND	103	EXTNL	IQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	IMPLND	103	EXTNL	IQADFX	1 1
WDM3	7306	NO3N	ENGL	DIV	IMPLND	104	EXTNL	IQADFX	2 1
WDM3	7305	NH3N	ENGL	DIV	IMPLND	104	EXTNL	IQADFX	1 1
***FAILING OSSF LOADS TO PERLND 116									
*** 0.9 multiplier is fraction of failing septic effluent to PERLND 116 surface									
WDM3	8111	BOD	ENGL	0.9DIV	PERLND	116	EXTNL	SLIQO	4
WDM3	8112	TSS	ENGL	0.9DIV	PERLND	116	EXTNL	SLSED	1

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

WDM3	8113	FLOW	ENGL	0.9DIV	PERLND	116	EXTNL	SURLI	1
WDM3	8114	DNH3	ENGL	0.9DIV	PERLND	116	EXTNL	SLIQO	1
WDM3	8115	DPO4	ENGL	0.9DIV	PERLND	116	EXTNL	SLIQO	3

END EXT SOURCES

SCHEMATIC

<-Volume->	<--Area-->	<-Volume->	<ML#>	***	<sb>
<Name> x	<-factor-->	<Name> x		***	x x
PERLND 101	894	RCHRES 1	2		
PERLND 102	373	RCHRES 1	2		
PERLND 103	71	RCHRES 1	2		
PERLND 104	6	RCHRES 1	2		
PERLND 105	16	RCHRES 1	2		
PERLND 106	0	RCHRES 1	2		
PERLND 107	3107	RCHRES 1	2		
PERLND 108	1845	RCHRES 1	2		
PERLND 109	1663	RCHRES 1	2		
PERLND 110	271	RCHRES 1	2		
PERLND 111	1866	RCHRES 1	2		
PERLND 112	1858	RCHRES 1	2		
PERLND 113	8	RCHRES 1	2		
PERLND 114	5260	RCHRES 1	2		
PERLND 115	62	RCHRES 1	2		
PERLND 116	48	RCHRES 1	2		
PERLND 117	0	RCHRES 1	2		
IMPLND 101	110	RCHRES 1	1		
IMPLND 102	180	RCHRES 1	1		
IMPLND 103	115	RCHRES 1	1		
IMPLND 104	48	RCHRES 1	1		
PERLND 101	419	RCHRES 2	2		
PERLND 102	89	RCHRES 2	2		
PERLND 103	0	RCHRES 2	2		
PERLND 104	0	RCHRES 2	2		
PERLND 105	0	RCHRES 2	2		
PERLND 106	0	RCHRES 2	2		
PERLND 107	2702	RCHRES 2	2		
PERLND 108	1251	RCHRES 2	2		
PERLND 109	344	RCHRES 2	2		
PERLND 110	17	RCHRES 2	2		
PERLND 111	1252	RCHRES 2	2		
PERLND 112	1499	RCHRES 2	2		
PERLND 113	6	RCHRES 2	2		
PERLND 114	5553	RCHRES 2	2		
PERLND 115	145	RCHRES 2	2		
PERLND 116	15	RCHRES 2	2		
PERLND 117	0	RCHRES 2	2		
IMPLND 101	52	RCHRES 2	1		
IMPLND 102	44	RCHRES 2	1		
IMPLND 103	1	RCHRES 2	1		
IMPLND 104	0	RCHRES 2	1		
PERLND 101	195	RCHRES 3	2		
PERLND 102	22	RCHRES 3	2		
PERLND 103	3	RCHRES 3	2		
PERLND 104	0	RCHRES 3	2		
PERLND 105	0	RCHRES 3	2		
PERLND 106	0	RCHRES 3	2		
PERLND 107	2173	RCHRES 3	2		
PERLND 108	556	RCHRES 3	2		
PERLND 109	173	RCHRES 3	2		
PERLND 110	16	RCHRES 3	2		
PERLND 111	1045	RCHRES 3	2		
PERLND 112	550	RCHRES 3	2		
PERLND 113	1	RCHRES 3	2		

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

PERLND 114	5181	RCHRES	3	2
PERLND 115	68	RCHRES	3	2
PERLND 116	9	RCHRES	3	2
PERLND 117	0	RCHRES	3	2
IMPLND 101	24	RCHRES	3	1
IMPLND 102	14	RCHRES	3	1
IMPLND 103	6	RCHRES	3	1
IMPLND 104	0	RCHRES	3	1
RCHRES 1		RCHRES	3	3
PERLND 101	709	RCHRES	4	5
PERLND 102	166	RCHRES	4	5
PERLND 103	2	RCHRES	4	5
PERLND 104	0	RCHRES	4	5
PERLND 105	3	RCHRES	4	5
PERLND 106	3	RCHRES	4	5
PERLND 107	1679	RCHRES	4	5
PERLND 108	1521	RCHRES	4	5
PERLND 109	297	RCHRES	4	5
PERLND 110	76	RCHRES	4	5
PERLND 111	785	RCHRES	4	5
PERLND 112	405	RCHRES	4	5
PERLND 113	8	RCHRES	4	5
PERLND 114	6371	RCHRES	4	5
PERLND 115	227	RCHRES	4	5
PERLND 116	49	RCHRES	4	5
PERLND 117	0	RCHRES	4	5
IMPLND 101	88	RCHRES	4	4
IMPLND 102	92	RCHRES	4	4
IMPLND 103	4	RCHRES	4	4
IMPLND 104	2	RCHRES	4	4
RCHRES 2		RCHRES	4	3
RCHRES 3		RCHRES	4	3
PERLND 101	370	RCHRES	5	7
PERLND 102	40	RCHRES	5	7
PERLND 103	7	RCHRES	5	7
PERLND 104	0	RCHRES	5	7
PERLND 105	3	RCHRES	5	7
PERLND 106	6	RCHRES	5	7
PERLND 107	1503	RCHRES	5	7
PERLND 108	1054	RCHRES	5	7
PERLND 109	61	RCHRES	5	7
PERLND 110	7	RCHRES	5	7
PERLND 111	807	RCHRES	5	7
PERLND 112	1085	RCHRES	5	7
PERLND 113	0	RCHRES	5	7
PERLND 114	3501	RCHRES	5	7
PERLND 115	41	RCHRES	5	7
PERLND 116	29	RCHRES	5	7
PERLND 117	0	RCHRES	5	7
IMPLND 101	46	RCHRES	5	6
IMPLND 102	29	RCHRES	5	6
IMPLND 103	11	RCHRES	5	6
IMPLND 104	0	RCHRES	5	6
PERLND 101	755	RCHRES	6	7
PERLND 102	250	RCHRES	6	7
PERLND 103	43	RCHRES	6	7
PERLND 104	6	RCHRES	6	7
PERLND 105	2	RCHRES	6	7
PERLND 106	0	RCHRES	6	7
PERLND 107	228	RCHRES	6	7
PERLND 108	1130	RCHRES	6	7
PERLND 109	71	RCHRES	6	7
PERLND 110	33	RCHRES	6	7

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

PERLND 111	403	RCHRES	6	7
PERLND 112	222	RCHRES	6	7
PERLND 113	8	RCHRES	6	7
PERLND 114	1453	RCHRES	6	7
PERLND 115	9	RCHRES	6	7
PERLND 116	90	RCHRES	6	7
PERLND 117	0	RCHRES	6	7
IMPLND 101	93	RCHRES	6	6
IMPLND 102	146	RCHRES	6	6
IMPLND 103	70	RCHRES	6	6
IMPLND 104	51	RCHRES	6	6
RCHRES 5		RCHRES	6	3
PERLND 101	634	RCHRES	7	9
PERLND 102	232	RCHRES	7	9
PERLND 103	28	RCHRES	7	9
PERLND 104	2	RCHRES	7	9
PERLND 105	4	RCHRES	7	9
PERLND 106	0	RCHRES	7	9
PERLND 107	557	RCHRES	7	9
PERLND 108	1072	RCHRES	7	9
PERLND 109	1982	RCHRES	7	9
PERLND 110	43	RCHRES	7	9
PERLND 111	455	RCHRES	7	9
PERLND 112	602	RCHRES	7	9
PERLND 113	17	RCHRES	7	9
PERLND 114	2212	RCHRES	7	9
PERLND 115	133	RCHRES	7	9
PERLND 116	55	RCHRES	7	9
PERLND 117	0	RCHRES	7	9
IMPLND 101	78	RCHRES	7	8
IMPLND 102	123	RCHRES	7	8
IMPLND 103	46	RCHRES	7	8
IMPLND 104	13	RCHRES	7	8
PERLND 101	781	RCHRES	8	11
PERLND 102	202	RCHRES	8	11
PERLND 103	14	RCHRES	8	11
PERLND 104	0	RCHRES	8	11
PERLND 105	3	RCHRES	8	11
PERLND 106	44	RCHRES	8	11
PERLND 107	1785	RCHRES	8	11
PERLND 108	3009	RCHRES	8	11
PERLND 109	512	RCHRES	8	11
PERLND 110	46	RCHRES	8	11
PERLND 111	689	RCHRES	8	11
PERLND 112	935	RCHRES	8	11
PERLND 113	46	RCHRES	8	11
PERLND 114	3202	RCHRES	8	11
PERLND 115	164	RCHRES	8	11
PERLND 116	69	RCHRES	8	11
PERLND 117	0	RCHRES	8	11
IMPLND 101	97	RCHRES	8	10
IMPLND 102	116	RCHRES	8	10
IMPLND 103	24	RCHRES	8	10
IMPLND 104	2	RCHRES	8	10
RCHRES 4		RCHRES	8	3
PERLND 101	151	RCHRES	9	13
PERLND 102	83	RCHRES	9	13
PERLND 103	23	RCHRES	9	13
PERLND 104	0	RCHRES	9	13
PERLND 105	0	RCHRES	9	13
PERLND 106	0	RCHRES	9	13
PERLND 107	161	RCHRES	9	13
PERLND 108	271	RCHRES	9	13

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B*

PERLND 109	347	RCHRES	9	13
PERLND 110	17	RCHRES	9	13
PERLND 111	77	RCHRES	9	13
PERLND 112	133	RCHRES	9	13
PERLND 113	0	RCHRES	9	13
PERLND 114	1491	RCHRES	9	13
PERLND 115	46	RCHRES	9	13
PERLND 116	14	RCHRES	9	13
PERLND 117	0	RCHRES	9	13
IMPLND 101	19	RCHRES	9	12
IMPLND 102	42	RCHRES	9	12
IMPLND 103	37	RCHRES	9	12
IMPLND 104	1	RCHRES	9	12
RCHRES 8		RCHRES	9	3
PERLND 101	33	RCHRES	10	9
PERLND 102	68	RCHRES	10	9
PERLND 103	6	RCHRES	10	9
PERLND 104	0	RCHRES	10	9
PERLND 105	0	RCHRES	10	9
PERLND 106	12	RCHRES	10	9
PERLND 107	224	RCHRES	10	9
PERLND 108	36	RCHRES	10	9
PERLND 109	172	RCHRES	10	9
PERLND 110	10	RCHRES	10	9
PERLND 111	30	RCHRES	10	9
PERLND 112	9	RCHRES	10	9
PERLND 113	0	RCHRES	10	9
PERLND 114	1484	RCHRES	10	9
PERLND 115	21	RCHRES	10	9
PERLND 116	8	RCHRES	10	9
PERLND 117	0	RCHRES	10	9
IMPLND 101	4	RCHRES	10	8
IMPLND 102	33	RCHRES	10	8
IMPLND 103	10	RCHRES	10	8
IMPLND 104	0	RCHRES	10	8
RCHRES 7		RCHRES	10	3
PERLND 101	1036	RCHRES	11	15
PERLND 102	647	RCHRES	11	15
PERLND 103	76	RCHRES	11	15
PERLND 104	8	RCHRES	11	15
PERLND 105	0	RCHRES	11	15
PERLND 106	0	RCHRES	11	15
PERLND 107	151	RCHRES	11	15
PERLND 108	254	RCHRES	11	15
PERLND 109	964	RCHRES	11	15
PERLND 110	86	RCHRES	11	15
PERLND 111	210	RCHRES	11	15
PERLND 112	192	RCHRES	11	15
PERLND 113	39	RCHRES	11	15
PERLND 114	1198	RCHRES	11	15
PERLND 115	178	RCHRES	11	15
PERLND 116	4	RCHRES	11	15
PERLND 117	0	RCHRES	11	15
IMPLND 101	128	RCHRES	11	14
IMPLND 102	279	RCHRES	11	14
IMPLND 103	124	RCHRES	11	14
IMPLND 104	67	RCHRES	11	14
PERLND 101	303	RCHRES	12	17
PERLND 102	140	RCHRES	12	17
PERLND 103	5	RCHRES	12	17
PERLND 104	2	RCHRES	12	17
PERLND 105	4	RCHRES	12	17
PERLND 106	18	RCHRES	12	17

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

PERLND 107	30	RCHRES	12	17
PERLND 108	125	RCHRES	12	17
PERLND 109	179	RCHRES	12	17
PERLND 110	34	RCHRES	12	17
PERLND 111	139	RCHRES	12	17
PERLND 112	255	RCHRES	12	17
PERLND 113	19	RCHRES	12	17
PERLND 114	1535	RCHRES	12	17
PERLND 115	80	RCHRES	12	17
PERLND 116	3	RCHRES	12	17
PERLND 117	0	RCHRES	12	17
IMPLND 101	37	RCHRES	12	16
IMPLND 102	61	RCHRES	12	16
IMPLND 103	8	RCHRES	12	16
IMPLND 104	16	RCHRES	12	16
RCHRES 9		RCHRES	12	3
RCHRES 13		RCHRES	12	3
PERLND 101	506	RCHRES	13	7
PERLND 102	287	RCHRES	13	7
PERLND 103	60	RCHRES	13	7
PERLND 104	6	RCHRES	13	7
PERLND 105	6	RCHRES	13	7
PERLND 106	2	RCHRES	13	7
PERLND 107	1148	RCHRES	13	7
PERLND 108	1017	RCHRES	13	7
PERLND 109	1276	RCHRES	13	7
PERLND 110	630	RCHRES	13	7
PERLND 111	220	RCHRES	13	7
PERLND 112	250	RCHRES	13	7
PERLND 113	12	RCHRES	13	7
PERLND 114	2748	RCHRES	13	7
PERLND 115	38	RCHRES	13	7
PERLND 116	49	RCHRES	13	7
PERLND 117	0	RCHRES	13	7
IMPLND 101	62	RCHRES	13	6
IMPLND 102	144	RCHRES	13	6
IMPLND 103	97	RCHRES	13	6
IMPLND 104	51	RCHRES	13	6
RCHRES 6		RCHRES	13	3
PERLND 101	309	RCHRES	14	19
PERLND 102	392	RCHRES	14	19
PERLND 103	17	RCHRES	14	19
PERLND 104	2	RCHRES	14	19
PERLND 105	4	RCHRES	14	19
PERLND 106	0	RCHRES	14	19
PERLND 107	66	RCHRES	14	19
PERLND 108	299	RCHRES	14	19
PERLND 109	133	RCHRES	14	19
PERLND 110	11	RCHRES	14	19
PERLND 111	98	RCHRES	14	19
PERLND 112	48	RCHRES	14	19
PERLND 113	168	RCHRES	14	19
PERLND 114	833	RCHRES	14	19
PERLND 115	380	RCHRES	14	19
PERLND 116	4	RCHRES	14	19
PERLND 117	0	RCHRES	14	19
IMPLND 101	38	RCHRES	14	18
IMPLND 102	170	RCHRES	14	18
IMPLND 103	27	RCHRES	14	18
IMPLND 104	14	RCHRES	14	18
RCHRES 10		RCHRES	14	3
RCHRES 11		RCHRES	14	3
RCHRES 12		RCHRES	14	3

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B*

PERLND 101	1050	RCHRES	15	21
PERLND 102	538	RCHRES	15	21
PERLND 103	58	RCHRES	15	21
PERLND 104	4	RCHRES	15	21
PERLND 105	0	RCHRES	15	21
PERLND 106	6	RCHRES	15	21
PERLND 107	193	RCHRES	15	21
PERLND 108	206	RCHRES	15	21
PERLND 109	1141	RCHRES	15	21
PERLND 110	105	RCHRES	15	21
PERLND 111	50	RCHRES	15	21
PERLND 112	12	RCHRES	15	21
PERLND 113	40	RCHRES	15	21
PERLND 114	124	RCHRES	15	21
PERLND 115	35	RCHRES	15	21
PERLND 116	19	RCHRES	15	21
PERLND 117	0	RCHRES	15	21
IMPLND 101	130	RCHRES	15	20
IMPLND 102	239	RCHRES	15	20
IMPLND 103	95	RCHRES	15	20
IMPLND 104	29	RCHRES	15	20
PERLND 101	633	RCHRES	16	23
PERLND 102	595	RCHRES	16	23
PERLND 103	55	RCHRES	16	23
PERLND 104	7	RCHRES	16	23
PERLND 105	23	RCHRES	16	23
PERLND 106	2	RCHRES	16	23
PERLND 107	10	RCHRES	16	23
PERLND 108	75	RCHRES	16	23
PERLND 109	820	RCHRES	16	23
PERLND 110	76	RCHRES	16	23
PERLND 111	24	RCHRES	16	23
PERLND 112	81	RCHRES	16	23
PERLND 113	230	RCHRES	16	23
PERLND 114	643	RCHRES	16	23
PERLND 115	215	RCHRES	16	23
PERLND 116	27	RCHRES	16	23
PERLND 117	0	RCHRES	16	23
IMPLND 101	78	RCHRES	16	22
IMPLND 102	267	RCHRES	16	22
IMPLND 103	89	RCHRES	16	22
IMPLND 104	61	RCHRES	16	22
RCHRES 14		RCHRES	16	3
PERLND 101	362	RCHRES	17	25
PERLND 102	317	RCHRES	17	25
PERLND 103	107	RCHRES	17	25
PERLND 104	50	RCHRES	17	25
PERLND 105	3	RCHRES	17	25
PERLND 106	6	RCHRES	17	25
PERLND 107	42	RCHRES	17	25
PERLND 108	155	RCHRES	17	25
PERLND 109	878	RCHRES	17	25
PERLND 110	101	RCHRES	17	25
PERLND 111	82	RCHRES	17	25
PERLND 112	23	RCHRES	17	25
PERLND 113	165	RCHRES	17	25
PERLND 114	397	RCHRES	17	25
PERLND 115	583	RCHRES	17	25
PERLND 116	10	RCHRES	17	25
PERLND 117	0	RCHRES	17	25
IMPLND 101	45	RCHRES	17	24
IMPLND 102	140	RCHRES	17	24
IMPLND 103	174	RCHRES	17	24

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

IMPLND 104	409	RCHRES	17	24
RCHRES 15		RCHRES	17	3
PERLND 101	49	RCHRES	18	25
PERLND 102	74	RCHRES	18	25
PERLND 103	7	RCHRES	18	25
PERLND 104	1	RCHRES	18	25
PERLND 105	0	RCHRES	18	25
PERLND 106	0	RCHRES	18	25
PERLND 107	0	RCHRES	18	25
PERLND 108	4	RCHRES	18	25
PERLND 109	740	RCHRES	18	25
PERLND 110	0	RCHRES	18	25
PERLND 111	2	RCHRES	18	25
PERLND 112	65	RCHRES	18	25
PERLND 113	238	RCHRES	18	25
PERLND 114	68	RCHRES	18	25
PERLND 115	994	RCHRES	18	25
PERLND 116	4	RCHRES	18	25
PERLND 117	0	RCHRES	18	25
IMPLND 101	6	RCHRES	18	24
IMPLND 102	33	RCHRES	18	24
IMPLND 103	11	RCHRES	18	24
IMPLND 104	6	RCHRES	18	24
RCHRES 16		RCHRES	18	3
RCHRES 17		RCHRES	18	3
PERLND 101	894	COPY	1	27
PERLND 102	373	COPY	1	27
PERLND 103	71	COPY	1	27
PERLND 104	6	COPY	1	27
PERLND 105	16	COPY	1	27
PERLND 106	0	COPY	1	27
PERLND 107	3107	COPY	1	27
PERLND 108	1845	COPY	1	27
PERLND 109	1663	COPY	1	27
PERLND 110	271	COPY	1	27
PERLND 111	1866	COPY	1	27
PERLND 112	1858	COPY	1	27
PERLND 113	8	COPY	1	27
PERLND 114	5260	COPY	1	27
PERLND 115	62	COPY	1	27
PERLND 116	48	COPY	1	27
PERLND 117	0	COPY	1	27
IMPLND 101	110	COPY	1	26
IMPLND 102	180	COPY	1	26
IMPLND 103	115	COPY	1	26
IMPLND 104	48	COPY	1	26
PERLND 101	419	COPY	2	27
PERLND 102	89	COPY	2	27
PERLND 103	0	COPY	2	27
PERLND 104	0	COPY	2	27
PERLND 105	0	COPY	2	27
PERLND 106	0	COPY	2	27
PERLND 107	2702	COPY	2	27
PERLND 108	1251	COPY	2	27
PERLND 109	344	COPY	2	27
PERLND 110	17	COPY	2	27
PERLND 111	1252	COPY	2	27
PERLND 112	1499	COPY	2	27
PERLND 113	6	COPY	2	27
PERLND 114	5553	COPY	2	27
PERLND 115	145	COPY	2	27
PERLND 116	15	COPY	2	27
PERLND 117	0	COPY	2	27

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

IMPLND 101	52	COPY	2	26
IMPLND 102	44	COPY	2	26
IMPLND 103	1	COPY	2	26
IMPLND 104	0	COPY	2	26
PERLND 101	195	COPY	3	27
PERLND 102	22	COPY	3	27
PERLND 103	3	COPY	3	27
PERLND 104	0	COPY	3	27
PERLND 105	0	COPY	3	27
PERLND 106	0	COPY	3	27
PERLND 107	2173	COPY	3	27
PERLND 108	556	COPY	3	27
PERLND 109	173	COPY	3	27
PERLND 110	16	COPY	3	27
PERLND 111	1045	COPY	3	27
PERLND 112	550	COPY	3	27
PERLND 113	1	COPY	3	27
PERLND 114	5181	COPY	3	27
PERLND 115	68	COPY	3	27
PERLND 116	9	COPY	3	27
PERLND 117	0	COPY	3	27
IMPLND 101	24	COPY	3	26
IMPLND 102	14	COPY	3	26
IMPLND 103	6	COPY	3	26
IMPLND 104	0	COPY	3	26
PERLND 101	709	COPY	4	29
PERLND 102	166	COPY	4	29
PERLND 103	2	COPY	4	29
PERLND 104	0	COPY	4	29
PERLND 105	3	COPY	4	29
PERLND 106	3	COPY	4	29
PERLND 107	1679	COPY	4	29
PERLND 108	1521	COPY	4	29
PERLND 109	297	COPY	4	29
PERLND 110	76	COPY	4	29
PERLND 111	785	COPY	4	29
PERLND 112	405	COPY	4	29
PERLND 113	8	COPY	4	29
PERLND 114	6371	COPY	4	29
PERLND 115	227	COPY	4	29
PERLND 116	49	COPY	4	29
PERLND 117	0	COPY	4	29
IMPLND 101	88	COPY	4	28
IMPLND 102	92	COPY	4	28
IMPLND 103	4	COPY	4	28
IMPLND 104	2	COPY	4	28
PERLND 101	370	COPY	5	31
PERLND 102	40	COPY	5	31
PERLND 103	7	COPY	5	31
PERLND 104	0	COPY	5	31
PERLND 105	3	COPY	5	31
PERLND 106	6	COPY	5	31
PERLND 107	1503	COPY	5	31
PERLND 108	1054	COPY	5	31
PERLND 109	61	COPY	5	31
PERLND 110	7	COPY	5	31
PERLND 111	807	COPY	5	31
PERLND 112	1085	COPY	5	31
PERLND 113	0	COPY	5	31
PERLND 114	3501	COPY	5	31
PERLND 115	41	COPY	5	31
PERLND 116	29	COPY	5	31
PERLND 117	0	COPY	5	31

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

IMPLND 101	46	COPY	5	30
IMPLND 102	29	COPY	5	30
IMPLND 103	11	COPY	5	30
IMPLND 104	0	COPY	5	30
PERLND 101	755	COPY	6	31
PERLND 102	250	COPY	6	31
PERLND 103	43	COPY	6	31
PERLND 104	6	COPY	6	31
PERLND 105	2	COPY	6	31
PERLND 106	0	COPY	6	31
PERLND 107	228	COPY	6	31
PERLND 108	1130	COPY	6	31
PERLND 109	71	COPY	6	31
PERLND 110	33	COPY	6	31
PERLND 111	403	COPY	6	31
PERLND 112	222	COPY	6	31
PERLND 113	8	COPY	6	31
PERLND 114	1453	COPY	6	31
PERLND 115	9	COPY	6	31
PERLND 116	90	COPY	6	31
PERLND 117	0	COPY	6	31
IMPLND 101	93	COPY	6	30
IMPLND 102	146	COPY	6	30
IMPLND 103	70	COPY	6	30
IMPLND 104	51	COPY	6	30
PERLND 101	634	COPY	7	33
PERLND 102	232	COPY	7	33
PERLND 103	28	COPY	7	33
PERLND 104	2	COPY	7	33
PERLND 105	4	COPY	7	33
PERLND 106	0	COPY	7	33
PERLND 107	557	COPY	7	33
PERLND 108	1072	COPY	7	33
PERLND 109	1982	COPY	7	33
PERLND 110	43	COPY	7	33
PERLND 111	455	COPY	7	33
PERLND 112	602	COPY	7	33
PERLND 113	17	COPY	7	33
PERLND 114	2212	COPY	7	33
PERLND 115	133	COPY	7	33
PERLND 116	55	COPY	7	33
PERLND 117	0	COPY	7	33
IMPLND 101	78	COPY	7	32
IMPLND 102	123	COPY	7	32
IMPLND 103	46	COPY	7	32
IMPLND 104	13	COPY	7	32
PERLND 101	781	COPY	8	35
PERLND 102	202	COPY	8	35
PERLND 103	14	COPY	8	35
PERLND 104	0	COPY	8	35
PERLND 105	3	COPY	8	35
PERLND 106	44	COPY	8	35
PERLND 107	1785	COPY	8	35
PERLND 108	3009	COPY	8	35
PERLND 109	512	COPY	8	35
PERLND 110	46	COPY	8	35
PERLND 111	689	COPY	8	35
PERLND 112	935	COPY	8	35
PERLND 113	46	COPY	8	35
PERLND 114	3202	COPY	8	35
PERLND 115	164	COPY	8	35
PERLND 116	69	COPY	8	35
PERLND 117	0	COPY	8	35

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

IMPLND 101	97	COPY	8	34
IMPLND 102	116	COPY	8	34
IMPLND 103	24	COPY	8	34
IMPLND 104	2	COPY	8	34
PERLND 101	151	COPY	9	37
PERLND 102	83	COPY	9	37
PERLND 103	23	COPY	9	37
PERLND 104	0	COPY	9	37
PERLND 105	0	COPY	9	37
PERLND 106	0	COPY	9	37
PERLND 107	161	COPY	9	37
PERLND 108	271	COPY	9	37
PERLND 109	347	COPY	9	37
PERLND 110	17	COPY	9	37
PERLND 111	77	COPY	9	37
PERLND 112	133	COPY	9	37
PERLND 113	0	COPY	9	37
PERLND 114	1491	COPY	9	37
PERLND 115	46	COPY	9	37
PERLND 116	14	COPY	9	37
PERLND 117	0	COPY	9	37
IMPLND 101	19	COPY	9	36
IMPLND 102	42	COPY	9	36
IMPLND 103	37	COPY	9	36
IMPLND 104	1	COPY	9	36
PERLND 101	33	COPY	10	33
PERLND 102	68	COPY	10	33
PERLND 103	6	COPY	10	33
PERLND 104	0	COPY	10	33
PERLND 105	0	COPY	10	33
PERLND 106	12	COPY	10	33
PERLND 107	224	COPY	10	33
PERLND 108	36	COPY	10	33
PERLND 109	172	COPY	10	33
PERLND 110	10	COPY	10	33
PERLND 111	30	COPY	10	33
PERLND 112	9	COPY	10	33
PERLND 113	0	COPY	10	33
PERLND 114	1484	COPY	10	33
PERLND 115	21	COPY	10	33
PERLND 116	8	COPY	10	33
PERLND 117	0	COPY	10	33
IMPLND 101	4	COPY	10	32
IMPLND 102	33	COPY	10	32
IMPLND 103	10	COPY	10	32
IMPLND 104	0	COPY	10	32
PERLND 101	1036	COPY	11	39
PERLND 102	647	COPY	11	39
PERLND 103	76	COPY	11	39
PERLND 104	8	COPY	11	39
PERLND 105	0	COPY	11	39
PERLND 106	0	COPY	11	39
PERLND 107	151	COPY	11	39
PERLND 108	254	COPY	11	39
PERLND 109	964	COPY	11	39
PERLND 110	86	COPY	11	39
PERLND 111	210	COPY	11	39
PERLND 112	192	COPY	11	39
PERLND 113	39	COPY	11	39
PERLND 114	1198	COPY	11	39
PERLND 115	178	COPY	11	39
PERLND 116	4	COPY	11	39
PERLND 117	0	COPY	11	39

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

IMPLND 101	128	COPY	11	38
IMPLND 102	279	COPY	11	38
IMPLND 103	124	COPY	11	38
IMPLND 104	67	COPY	11	38
PERLND 101	303	COPY	12	41
PERLND 102	140	COPY	12	41
PERLND 103	5	COPY	12	41
PERLND 104	2	COPY	12	41
PERLND 105	4	COPY	12	41
PERLND 106	18	COPY	12	41
PERLND 107	30	COPY	12	41
PERLND 108	125	COPY	12	41
PERLND 109	179	COPY	12	41
PERLND 110	34	COPY	12	41
PERLND 111	139	COPY	12	41
PERLND 112	255	COPY	12	41
PERLND 113	19	COPY	12	41
PERLND 114	1535	COPY	12	41
PERLND 115	80	COPY	12	41
PERLND 116	3	COPY	12	41
PERLND 117	0	COPY	12	41
IMPLND 101	37	COPY	12	40
IMPLND 102	61	COPY	12	40
IMPLND 103	8	COPY	12	40
IMPLND 104	16	COPY	12	40
PERLND 101	506	COPY	13	31
PERLND 102	287	COPY	13	31
PERLND 103	60	COPY	13	31
PERLND 104	6	COPY	13	31
PERLND 105	6	COPY	13	31
PERLND 106	2	COPY	13	31
PERLND 107	1148	COPY	13	31
PERLND 108	1017	COPY	13	31
PERLND 109	1276	COPY	13	31
PERLND 110	630	COPY	13	31
PERLND 111	220	COPY	13	31
PERLND 112	250	COPY	13	31
PERLND 113	12	COPY	13	31
PERLND 114	2748	COPY	13	31
PERLND 115	38	COPY	13	31
PERLND 116	49	COPY	13	31
PERLND 117	0	COPY	13	31
IMPLND 101	62	COPY	13	30
IMPLND 102	144	COPY	13	30
IMPLND 103	97	COPY	13	30
IMPLND 104	51	COPY	13	30
PERLND 101	309	COPY	14	43
PERLND 102	392	COPY	14	43
PERLND 103	17	COPY	14	43
PERLND 104	2	COPY	14	43
PERLND 105	4	COPY	14	43
PERLND 106	0	COPY	14	43
PERLND 107	66	COPY	14	43
PERLND 108	299	COPY	14	43
PERLND 109	133	COPY	14	43
PERLND 110	11	COPY	14	43
PERLND 111	98	COPY	14	43
PERLND 112	48	COPY	14	43
PERLND 113	168	COPY	14	43
PERLND 114	833	COPY	14	43
PERLND 115	380	COPY	14	43
PERLND 116	4	COPY	14	43
PERLND 117	0	COPY	14	43

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

IMPLND 101	38	COPY	14	42
IMPLND 102	170	COPY	14	42
IMPLND 103	27	COPY	14	42
IMPLND 104	14	COPY	14	42
PERLND 101	1050	COPY	15	45
PERLND 102	538	COPY	15	45
PERLND 103	58	COPY	15	45
PERLND 104	4	COPY	15	45
PERLND 105	0	COPY	15	45
PERLND 106	6	COPY	15	45
PERLND 107	193	COPY	15	45
PERLND 108	206	COPY	15	45
PERLND 109	1141	COPY	15	45
PERLND 110	105	COPY	15	45
PERLND 111	50	COPY	15	45
PERLND 112	12	COPY	15	45
PERLND 113	40	COPY	15	45
PERLND 114	124	COPY	15	45
PERLND 115	35	COPY	15	45
PERLND 116	19	COPY	15	45
PERLND 117	0	COPY	15	45
IMPLND 101	130	COPY	15	44
IMPLND 102	239	COPY	15	44
IMPLND 103	95	COPY	15	44
IMPLND 104	29	COPY	15	44
PERLND 101	633	COPY	16	47
PERLND 102	595	COPY	16	47
PERLND 103	55	COPY	16	47
PERLND 104	7	COPY	16	47
PERLND 105	23	COPY	16	47
PERLND 106	2	COPY	16	47
PERLND 107	10	COPY	16	47
PERLND 108	75	COPY	16	47
PERLND 109	820	COPY	16	47
PERLND 110	76	COPY	16	47
PERLND 111	24	COPY	16	47
PERLND 112	81	COPY	16	47
PERLND 113	230	COPY	16	47
PERLND 114	643	COPY	16	47
PERLND 115	215	COPY	16	47
PERLND 116	27	COPY	16	47
PERLND 117	0	COPY	16	47
IMPLND 101	78	COPY	16	46
IMPLND 102	267	COPY	16	46
IMPLND 103	89	COPY	16	46
IMPLND 104	61	COPY	16	46
PERLND 101	362	COPY	17	49
PERLND 102	317	COPY	17	49
PERLND 103	107	COPY	17	49
PERLND 104	50	COPY	17	49
PERLND 105	3	COPY	17	49
PERLND 106	6	COPY	17	49
PERLND 107	42	COPY	17	49
PERLND 108	155	COPY	17	49
PERLND 109	878	COPY	17	49
PERLND 110	101	COPY	17	49
PERLND 111	82	COPY	17	49
PERLND 112	23	COPY	17	49
PERLND 113	165	COPY	17	49
PERLND 114	397	COPY	17	49
PERLND 115	583	COPY	17	49
PERLND 116	10	COPY	17	49
PERLND 117	0	COPY	17	49

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

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IMPLND 101          45      COPY      17      48
IMPLND 102         140      COPY      17      48
IMPLND 103         174      COPY      17      48
IMPLND 104         409      COPY      17      48
PERLND 101          49      COPY      18      49
PERLND 102          74      COPY      18      49
PERLND 103           7      COPY      18      49
PERLND 104           1      COPY      18      49
PERLND 105           0      COPY      18      49
PERLND 106           0      COPY      18      49
PERLND 107           0      COPY      18      49
PERLND 108           4      COPY      18      49
PERLND 109          740      COPY      18      49
PERLND 110           0      COPY      18      49
PERLND 111           2      COPY      18      49
PERLND 112          65      COPY      18      49
PERLND 113         238      COPY      18      49
PERLND 114          68      COPY      18      49
PERLND 115         994      COPY      18      49
PERLND 116           4      COPY      18      49
PERLND 117           0      COPY      18      49
IMPLND 101           6      COPY      18      48
IMPLND 102          33      COPY      18      48
IMPLND 103          11      COPY      18      48
IMPLND 104           6      COPY      18      48
END SCHEMATIC

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EXT TARGETS

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<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Volume-> <Member> Tsys Aggr Amd ***
<Name>      x      <Name> x x<-factor->strg <Name>      x <Name>qf  tem strg strg***
RCHRES  1  HYDR  RO      1  1      AVER WDM1  1315 RO      1  METR AGGR REPL
RCHRES  1  OXRX  DOX     1  1      AVER WDM1  3001 DO      1  ENGL AGGR REPL
RCHRES  1  OXRX  DOX     1  1      MIN  WDM1  4001 DO      1  ENGL AGGR REPL
RCHRES  2  HYDR  RO      1  1      AVER WDM1  1339 RO      1  METR AGGR REPL
RCHRES  2  OXRX  DOX     1  1      AVER WDM1  3002 DO      1  ENGL AGGR REPL
RCHRES  2  OXRX  DOX     1  1      MIN  WDM1  4002 DO      1  ENGL AGGR REPL
RCHRES  3  HYDR  RO      1  1      AVER WDM1  1363 RO      1  METR AGGR REPL
RCHRES  3  OXRX  DOX     1  1      AVER WDM1  3003 DO      1  ENGL AGGR REPL
RCHRES  3  OXRX  DOX     1  1      MIN  WDM1  4003 DO      1  ENGL AGGR REPL
RCHRES  4  HYDR  RO      1  1      AVER WDM1  1387 RO      1  METR AGGR REPL
RCHRES  4  OXRX  DOX     1  1      AVER WDM1  3004 DO      1  ENGL AGGR REPL
RCHRES  4  OXRX  DOX     1  1      MIN  WDM1  4004 DO      1  ENGL AGGR REPL
RCHRES  5  HYDR  RO      1  1      AVER WDM1  1411 RO      1  METR AGGR REPL
RCHRES  5  OXRX  DOX     1  1      AVER WDM1  3005 DO      1  ENGL AGGR REPL
RCHRES  5  OXRX  DOX     1  1      MIN  WDM1  4005 DO      1  ENGL AGGR REPL
RCHRES  6  HYDR  RO      1  1      AVER WDM1  1219 RO      1  METR AGGR REPL
RCHRES  6  OXRX  DOX     1  1      AVER WDM1  3006 DO      1  ENGL AGGR REPL
RCHRES  6  OXRX  DOX     1  1      MIN  WDM1  4006 DO      1  ENGL AGGR REPL
RCHRES  7  HYDR  RO      1  1      AVER WDM1  1003 RO      1  METR AGGR REPL
RCHRES  7  OXRX  DOX     1  1      AVER WDM1  3007 DO      1  ENGL AGGR REPL
RCHRES  7  OXRX  DOX     1  1      MIN  WDM1  4007 DO      1  ENGL AGGR REPL
RCHRES  7  SEDTRN SSED   4  1      AVER WDM1  1021 TSS    1  ENGL AGGR REPL
RCHRES  7  SEDTRN SSED   1  1      AVER WDM1  1505 SAND    1  ENGL AGGR REPL
RCHRES  7  SEDTRN SSED   2  1      AVER WDM1  1506 SILT    1  ENGL AGGR REPL
RCHRES  7  SEDTRN SSED   3  1      AVER WDM1  1507 CLAY    1  ENGL AGGR REPL
RCHRES  7  OXRX  BOD     1  1      AVER WDM1  1627 BOD     1  ENGL AGGR REPL
RCHRES  7  NUTRX  DNUST   2  1      AVER WDM1  1440 DNH3    1  ENGL AGGR REPL
RCHRES  7  NUTRX  DNUST   1  1      AVER WDM1  1439 DNO3    1  ENGL AGGR REPL
RCHRES  7  NUTRX  DNUST   4  1      AVER WDM1  1441 DPO4    1  ENGL AGGR REPL
RCHRES  7  PLANK  PHYCLA  1  1      AVER WDM1  1433 CHLA    1  ENGL AGGR REPL
RCHRES  7  PLANK  PKST3   4  1      AVER WDM1  1460 ORGN    1  ENGL AGGR REPL
RCHRES  7  PLANK  PKST3   5  1      AVER WDM1  1461 ORGP    1  ENGL AGGR REPL
RCHRES  7  PLANK  PKST3   1  1      AVER WDM1  1457 DETN    1  ENGL AGGR REPL

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*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B*

RCHRES	7	PLANK	PKST3	2	1	AVER	WDM1	1458	DETP	1	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST3	3	1	AVER	WDM1	1459	DETC	1	ENGL	AGGR	REPL
RCHRES	8	HYDR	RO	1	1	AVER	WDM1	1027	RO	1	METR	AGGR	REPL
RCHRES	8	OXR	DOX	1	1	AVER	WDM1	3008	DO	1	ENGL	AGGR	REPL
RCHRES	8	OXR	DOX	1	1	MIN	WDM1	4008	DO	1	ENGL	AGGR	REPL
RCHRES	8	SEDTRN	SSED	4	1	AVER	WDM1	1045	TSS	1	ENGL	AGGR	REPL
RCHRES	8	SEDTRN	SSED	1	1	AVER	WDM1	1508	SAND	1	ENGL	AGGR	REPL
RCHRES	8	SEDTRN	SSED	2	1	AVER	WDM1	1509	SILT	1	ENGL	AGGR	REPL
RCHRES	8	SEDTRN	SSED	3	1	AVER	WDM1	1510	CLAY	1	ENGL	AGGR	REPL
RCHRES	8	OXR	BOD	1	1	AVER	WDM1	1628	BOD	1	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	2	1	AVER	WDM1	1443	DNH3	1	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	1	1	AVER	WDM1	1442	DNO3	1	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	4	1	AVER	WDM1	1444	DPO4	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PHYCLA	1	1	AVER	WDM1	1434	CHLA	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	4	1	AVER	WDM1	1465	ORGN	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	5	1	AVER	WDM1	1466	ORGP	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	1	1	AVER	WDM1	1462	DETN	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	2	1	AVER	WDM1	1463	DETP	1	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	3	1	AVER	WDM1	1464	DETC	1	ENGL	AGGR	REPL
RCHRES	9	HYDR	RO	1	1	AVER	WDM1	1243	RO	1	METR	AGGR	REPL
RCHRES	10	HYDR	RO	1	1	AVER	WDM1	1051	RO	1	METR	AGGR	REPL
RCHRES	10	OXR	DOX	1	1	AVER	WDM1	3010	DO	1	ENGL	AGGR	REPL
RCHRES	10	OXR	DOX	1	1	MIN	WDM1	4010	DO	1	ENGL	AGGR	REPL
RCHRES	11	HYDR	RO	1	1	AVER	WDM1	1075	RO	1	METR	AGGR	REPL
RCHRES	11	OXR	DOX	1	1	AVER	WDM1	3011	DO	1	ENGL	AGGR	REPL
RCHRES	11	OXR	DOX	1	1	MIN	WDM1	4011	DO	1	ENGL	AGGR	REPL
RCHRES	11	SEDTRN	SSED	4	1	AVER	WDM1	1093	TSS	1	ENGL	AGGR	REPL
RCHRES	11	SEDTRN	SSED	1	1	AVER	WDM1	1511	SAND	1	ENGL	AGGR	REPL
RCHRES	11	SEDTRN	SSED	2	1	AVER	WDM1	1512	SILT	1	ENGL	AGGR	REPL
RCHRES	11	SEDTRN	SSED	3	1	AVER	WDM1	1513	CLAY	1	ENGL	AGGR	REPL
RCHRES	11	OXR	BOD	1	1	AVER	WDM1	1631	BOD	1	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	2	1	AVER	WDM1	1449	DNH3	1	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	1	1	AVER	WDM1	1448	DNO3	1	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	4	1	AVER	WDM1	1450	DPO4	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PHYCLA	1	1	AVER	WDM1	1436	CHLA	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	4	1	AVER	WDM1	1475	ORGN	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	5	1	AVER	WDM1	1476	ORGP	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	1	1	AVER	WDM1	1472	DETN	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	2	1	AVER	WDM1	1473	DETP	1	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	3	1	AVER	WDM1	1474	DETC	1	ENGL	AGGR	REPL
RCHRES	13	HYDR	RO	1	1	AVER	WDM1	1099	RO	1	METR	AGGR	REPL
RCHRES	13	OXR	DOX	1	1	AVER	WDM1	3013	DO	1	ENGL	AGGR	REPL
RCHRES	13	OXR	DOX	1	1	MIN	WDM1	4013	DO	1	ENGL	AGGR	REPL
RCHRES	13	SEDTRN	SSED	4	1	AVER	WDM1	1117	TSS	1	ENGL	AGGR	REPL
RCHRES	13	SEDTRN	SSED	1	1	AVER	WDM1	1514	SAND	1	ENGL	AGGR	REPL
RCHRES	13	SEDTRN	SSED	2	1	AVER	WDM1	1515	SILT	1	ENGL	AGGR	REPL
RCHRES	13	SEDTRN	SSED	3	1	AVER	WDM1	1516	CLAY	1	ENGL	AGGR	REPL
RCHRES	13	OXR	BOD	1	1	AVER	WDM1	1633	BOD	1	ENGL	AGGR	REPL
RCHRES	13	NUTRX	DNUST	2	1	AVER	WDM1	1452	DNH3	1	ENGL	AGGR	REPL
RCHRES	13	NUTRX	DNUST	1	1	AVER	WDM1	1451	DNO3	1	ENGL	AGGR	REPL
RCHRES	13	NUTRX	DNUST	4	1	AVER	WDM1	1453	DPO4	1	ENGL	AGGR	REPL
RCHRES	13	PLANK	PHYCLA	1	1	AVER	WDM1	1437	CHLA	1	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	4	1	AVER	WDM1	1480	ORGN	1	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	5	1	AVER	WDM1	1481	ORGP	1	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	1	1	AVER	WDM1	1477	DETN	1	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	2	1	AVER	WDM1	1478	DETP	1	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	3	1	AVER	WDM1	1479	DETC	1	ENGL	AGGR	REPL
RCHRES	12	HYDR	RO	1	1	AVER	WDM1	1267	RO	1	METR	AGGR	REPL
RCHRES	14	HYDR	RO	1	1	AVER	WDM1	1291	RO	1	METR	AGGR	REPL
RCHRES	14	HTRCH	TW	1	1	AVER	WDM1	1296	TW	1	METR	AGGR	REPL
RCHRES	15	HYDR	RO	1	1	AVER	WDM1	1123	RO	1	METR	AGGR	REPL
RCHRES	15	OXR	DOX	1	1	AVER	WDM1	3015	DO	1	ENGL	AGGR	REPL
RCHRES	15	OXR	DOX	1	1	MIN	WDM1	4015	DO	1	ENGL	AGGR	REPL

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

RCHRES	15	SEDTRN	SSED	4	1			AVER	WDM1	1141	TSS	1	ENGL	AGGR	REPL
RCHRES	15	SEDTRN	SSED	1	1			AVER	WDM1	1517	SAND	1	ENGL	AGGR	REPL
RCHRES	15	SEDTRN	SSED	2	1			AVER	WDM1	1518	SILT	1	ENGL	AGGR	REPL
RCHRES	15	SEDTRN	SSED	3	1			AVER	WDM1	1519	CLAY	1	ENGL	AGGR	REPL
RCHRES	15	OXR	BOD	1	1			AVER	WDM1	1635	BOD	1	ENGL	AGGR	REPL
RCHRES	15	NUTRX	DNUST	2	1			AVER	WDM1	1455	DNH3	1	ENGL	AGGR	REPL
RCHRES	15	NUTRX	DNUST	1	1			AVER	WDM1	1454	DNO3	1	ENGL	AGGR	REPL
RCHRES	15	NUTRX	DNUST	4	1			AVER	WDM1	1456	DPO4	1	ENGL	AGGR	REPL
RCHRES	15	PLANK	PHYCLA	1	1			AVER	WDM1	1438	CHLA	1	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	4	1			AVER	WDM1	1485	ORGN	1	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	5	1			AVER	WDM1	1486	ORGP	1	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	1	1			AVER	WDM1	1482	DETN	1	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	2	1			AVER	WDM1	1483	DETP	1	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	3	1			AVER	WDM1	1484	DETC	1	ENGL	AGGR	REPL
RCHRES	16	HYDR	RO	1	1			AVER	WDM1	1147	RO	1	METR	AGGR	REPL
RCHRES	17	HYDR	RO	1	1			AVER	WDM1	1171	RO	1	METR	AGGR	REPL
RCHRES	18	HYDR	RO	1	1			AVER	WDM1	1195	RO	1	METR	AGGR	REPL
COPY	1	OUTPUT	MEAN	1	1	0.02855			WDM1	9006	PERO	1	METR	AGGR	REPL
COPY	1	OUTPUT	MEAN	2	1	907			WDM1	9000	TSS	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	3	1	0.454			WDM1	9002	NH3N	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	4	1	0.454			WDM1	9003	NO3N	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	5	1	0.454			WDM1	9004	PO4P	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	6	1	0.454			WDM1	9005	BOD	1	ENGL	AGGR	REPL
COPY	1	OUTPUT	MEAN	7	1	0.454			WDM1	9001	DO	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	1	1	0.02855			WDM1	9016	PERO	1	METR	AGGR	REPL
COPY	2	OUTPUT	MEAN	2	1	907			WDM1	9010	TSS	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	3	1	0.454			WDM1	9012	NH3N	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	4	1	0.454			WDM1	9013	NO3N	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	5	1	0.454			WDM1	9014	PO4P	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	6	1	0.454			WDM1	9015	BOD	1	ENGL	AGGR	REPL
COPY	2	OUTPUT	MEAN	7	1	0.454			WDM1	9011	DO	1	ENGL	AGGR	REPL
COPY	3	OUTPUT	MEAN	1	1	0.02855			WDM1	9026	PERO	1	METR	AGGR	REPL
COPY	3	OUTPUT	MEAN	2	1	907			WDM1	9020	TSS	1	ENGL	AGGR	REPL
COPY	3	OUTPUT	MEAN	3	1	0.454			WDM1	9022	NH3N	1	ENGL	AGGR	REPL
COPY	3	OUTPUT	MEAN	4	1	0.454			WDM1	9023	NO3N	1	ENGL	AGGR	REPL
COPY	3	OUTPUT	MEAN	5	1	0.454			WDM1	9024	PO4P	1	ENGL	AGGR	REPL
COPY	3	OUTPUT	MEAN	6	1	0.454			WDM1	9025	BOD	1	ENGL	AGGR	REPL
COPY	3	OUTPUT	MEAN	7	1	0.454			WDM1	9021	DO	1	ENGL	AGGR	REPL
COPY	4	OUTPUT	MEAN	1	1	0.02855			WDM1	9036	PERO	1	METR	AGGR	REPL
COPY	4	OUTPUT	MEAN	2	1	907			WDM1	9030	TSS	1	ENGL	AGGR	REPL
COPY	4	OUTPUT	MEAN	3	1	0.454			WDM1	9032	NH3N	1	ENGL	AGGR	REPL
COPY	4	OUTPUT	MEAN	4	1	0.454			WDM1	9033	NO3N	1	ENGL	AGGR	REPL
COPY	4	OUTPUT	MEAN	5	1	0.454			WDM1	9034	PO4P	1	ENGL	AGGR	REPL
COPY	4	OUTPUT	MEAN	6	1	0.454			WDM1	9035	BOD	1	ENGL	AGGR	REPL
COPY	4	OUTPUT	MEAN	7	1	0.454			WDM1	9031	DO	1	ENGL	AGGR	REPL
COPY	5	OUTPUT	MEAN	1	1	0.02855			WDM1	9046	PERO	1	METR	AGGR	REPL
COPY	5	OUTPUT	MEAN	2	1	907			WDM1	9040	TSS	1	ENGL	AGGR	REPL
COPY	5	OUTPUT	MEAN	3	1	0.454			WDM1	9042	NH3N	1	ENGL	AGGR	REPL
COPY	5	OUTPUT	MEAN	4	1	0.454			WDM1	9043	NO3N	1	ENGL	AGGR	REPL
COPY	5	OUTPUT	MEAN	5	1	0.454			WDM1	9044	PO4P	1	ENGL	AGGR	REPL
COPY	5	OUTPUT	MEAN	6	1	0.454			WDM1	9045	BOD	1	ENGL	AGGR	REPL
COPY	5	OUTPUT	MEAN	7	1	0.454			WDM1	9041	DO	1	ENGL	AGGR	REPL
COPY	6	OUTPUT	MEAN	1	1	0.02855			WDM1	9056	PERO	1	METR	AGGR	REPL
COPY	6	OUTPUT	MEAN	2	1	907			WDM1	9050	TSS	1	ENGL	AGGR	REPL
COPY	6	OUTPUT	MEAN	3	1	0.454			WDM1	9052	NH3N	1	ENGL	AGGR	REPL
COPY	6	OUTPUT	MEAN	4	1	0.454			WDM1	9053	NO3N	1	ENGL	AGGR	REPL
COPY	6	OUTPUT	MEAN	5	1	0.454			WDM1	9054	PO4P	1	ENGL	AGGR	REPL
COPY	6	OUTPUT	MEAN	6	1	0.454			WDM1	9055	BOD	1	ENGL	AGGR	REPL
COPY	6	OUTPUT	MEAN	7	1	0.454			WDM1	9051	DO	1	ENGL	AGGR	REPL
COPY	7	OUTPUT	MEAN	1	1	0.02855			WDM1	9066	PERO	1	METR	AGGR	REPL
COPY	7	OUTPUT	MEAN	2	1	907			WDM1	9060	TSS	1	ENGL	AGGR	REPL
COPY	7	OUTPUT	MEAN	3	1	0.454			WDM1	9062	NH3N	1	ENGL	AGGR	REPL
COPY	7	OUTPUT	MEAN	4	1	0.454			WDM1	9063	NO3N	1	ENGL	AGGR	REPL

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

COPY	7	OUTPUT	MEAN	5	1	0.454	WDM1	9064	PO4P	1	ENGL	AGGR	REPL
COPY	7	OUTPUT	MEAN	6	1	0.454	WDM1	9065	BOD	1	ENGL	AGGR	REPL
COPY	7	OUTPUT	MEAN	7	1	0.454	WDM1	9061	DO	1	ENGL	AGGR	REPL
COPY	8	OUTPUT	MEAN	1	1	0.02855	WDM1	9076	PERO	1	METR	AGGR	REPL
COPY	8	OUTPUT	MEAN	2	1	907	WDM1	9070	TSS	1	ENGL	AGGR	REPL
COPY	8	OUTPUT	MEAN	3	1	0.454	WDM1	9072	NH3N	1	ENGL	AGGR	REPL
COPY	8	OUTPUT	MEAN	4	1	0.454	WDM1	9073	NO3N	1	ENGL	AGGR	REPL
COPY	8	OUTPUT	MEAN	5	1	0.454	WDM1	9074	PO4P	1	ENGL	AGGR	REPL
COPY	8	OUTPUT	MEAN	6	1	0.454	WDM1	9075	BOD	1	ENGL	AGGR	REPL
COPY	8	OUTPUT	MEAN	7	1	0.454	WDM1	9071	DO	1	ENGL	AGGR	REPL
COPY	9	OUTPUT	MEAN	1	1	0.02855	WDM1	9086	PERO	1	METR	AGGR	REPL
COPY	9	OUTPUT	MEAN	2	1	907	WDM1	9080	TSS	1	ENGL	AGGR	REPL
COPY	9	OUTPUT	MEAN	3	1	0.454	WDM1	9082	NH3N	1	ENGL	AGGR	REPL
COPY	9	OUTPUT	MEAN	4	1	0.454	WDM1	9083	NO3N	1	ENGL	AGGR	REPL
COPY	9	OUTPUT	MEAN	5	1	0.454	WDM1	9084	PO4P	1	ENGL	AGGR	REPL
COPY	9	OUTPUT	MEAN	6	1	0.454	WDM1	9085	BOD	1	ENGL	AGGR	REPL
COPY	9	OUTPUT	MEAN	7	1	0.454	WDM1	9081	DO	1	ENGL	AGGR	REPL
COPY	10	OUTPUT	MEAN	1	1	0.02855	WDM1	9096	PERO	1	METR	AGGR	REPL
COPY	10	OUTPUT	MEAN	2	1	907	WDM1	9090	TSS	1	ENGL	AGGR	REPL
COPY	10	OUTPUT	MEAN	3	1	0.454	WDM1	9092	NH3N	1	ENGL	AGGR	REPL
COPY	10	OUTPUT	MEAN	4	1	0.454	WDM1	9093	NO3N	1	ENGL	AGGR	REPL
COPY	10	OUTPUT	MEAN	5	1	0.454	WDM1	9094	PO4P	1	ENGL	AGGR	REPL
COPY	10	OUTPUT	MEAN	6	1	0.454	WDM1	9095	BOD	1	ENGL	AGGR	REPL
COPY	10	OUTPUT	MEAN	7	1	0.454	WDM1	9091	DO	1	ENGL	AGGR	REPL
COPY	11	OUTPUT	MEAN	1	1	0.02855	WDM1	9106	PERO	1	METR	AGGR	REPL
COPY	11	OUTPUT	MEAN	2	1	907	WDM1	9100	TSS	1	ENGL	AGGR	REPL
COPY	11	OUTPUT	MEAN	3	1	0.454	WDM1	9102	NH3N	1	ENGL	AGGR	REPL
COPY	11	OUTPUT	MEAN	4	1	0.454	WDM1	9103	NO3N	1	ENGL	AGGR	REPL
COPY	11	OUTPUT	MEAN	5	1	0.454	WDM1	9104	PO4P	1	ENGL	AGGR	REPL
COPY	11	OUTPUT	MEAN	6	1	0.454	WDM1	9105	BOD	1	ENGL	AGGR	REPL
COPY	11	OUTPUT	MEAN	7	1	0.454	WDM1	9101	DO	1	ENGL	AGGR	REPL
COPY	12	OUTPUT	MEAN	1	1	0.02855	WDM1	9116	PERO	1	METR	AGGR	REPL
COPY	12	OUTPUT	MEAN	2	1	907	WDM1	9110	TSS	1	ENGL	AGGR	REPL
COPY	12	OUTPUT	MEAN	3	1	0.454	WDM1	9112	NH3N	1	ENGL	AGGR	REPL
COPY	12	OUTPUT	MEAN	4	1	0.454	WDM1	9113	NO3N	1	ENGL	AGGR	REPL
COPY	12	OUTPUT	MEAN	5	1	0.454	WDM1	9114	PO4P	1	ENGL	AGGR	REPL
COPY	12	OUTPUT	MEAN	6	1	0.454	WDM1	9115	BOD	1	ENGL	AGGR	REPL
COPY	12	OUTPUT	MEAN	7	1	0.454	WDM1	9111	DO	1	ENGL	AGGR	REPL
COPY	13	OUTPUT	MEAN	1	1	0.02855	WDM1	9126	PERO	1	METR	AGGR	REPL
COPY	13	OUTPUT	MEAN	2	1	907	WDM1	9120	TSS	1	ENGL	AGGR	REPL
COPY	13	OUTPUT	MEAN	3	1	0.454	WDM1	9122	NH3N	1	ENGL	AGGR	REPL
COPY	13	OUTPUT	MEAN	4	1	0.454	WDM1	9123	NO3N	1	ENGL	AGGR	REPL
COPY	13	OUTPUT	MEAN	5	1	0.454	WDM1	9124	PO4P	1	ENGL	AGGR	REPL
COPY	13	OUTPUT	MEAN	6	1	0.454	WDM1	9125	BOD	1	ENGL	AGGR	REPL
COPY	13	OUTPUT	MEAN	7	1	0.454	WDM1	9121	DO	1	ENGL	AGGR	REPL
COPY	14	OUTPUT	MEAN	1	1	0.02855	WDM1	9136	PERO	1	METR	AGGR	REPL
COPY	14	OUTPUT	MEAN	2	1	907	WDM1	9130	TSS	1	ENGL	AGGR	REPL
COPY	14	OUTPUT	MEAN	3	1	0.454	WDM1	9132	NH3N	1	ENGL	AGGR	REPL
COPY	14	OUTPUT	MEAN	4	1	0.454	WDM1	9133	NO3N	1	ENGL	AGGR	REPL
COPY	14	OUTPUT	MEAN	5	1	0.454	WDM1	9134	PO4P	1	ENGL	AGGR	REPL
COPY	14	OUTPUT	MEAN	6	1	0.454	WDM1	9135	BOD	1	ENGL	AGGR	REPL
COPY	14	OUTPUT	MEAN	7	1	0.454	WDM1	9131	DO	1	ENGL	AGGR	REPL
COPY	15	OUTPUT	MEAN	1	1	0.02855	WDM1	9146	PERO	1	METR	AGGR	REPL
COPY	15	OUTPUT	MEAN	2	1	907	WDM1	9140	TSS	1	ENGL	AGGR	REPL
COPY	15	OUTPUT	MEAN	3	1	0.454	WDM1	9142	NH3N	1	ENGL	AGGR	REPL
COPY	15	OUTPUT	MEAN	4	1	0.454	WDM1	9143	NO3N	1	ENGL	AGGR	REPL
COPY	15	OUTPUT	MEAN	5	1	0.454	WDM1	9144	PO4P	1	ENGL	AGGR	REPL
COPY	15	OUTPUT	MEAN	6	1	0.454	WDM1	9145	BOD	1	ENGL	AGGR	REPL
COPY	15	OUTPUT	MEAN	7	1	0.454	WDM1	9141	DO	1	ENGL	AGGR	REPL
COPY	16	OUTPUT	MEAN	1	1	0.02855	WDM1	9156	PERO	1	METR	AGGR	REPL
COPY	16	OUTPUT	MEAN	2	1	907	WDM1	9150	TSS	1	ENGL	AGGR	REPL
COPY	16	OUTPUT	MEAN	3	1	0.454	WDM1	9152	NH3N	1	ENGL	AGGR	REPL
COPY	16	OUTPUT	MEAN	4	1	0.454	WDM1	9153	NO3N	1	ENGL	AGGR	REPL

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

COPY 16 OUTPUT MEAN 5 1 0.454 WDM1 9154 PO4P 1 ENGL AGGR REPL
COPY 16 OUTPUT MEAN 6 1 0.454 WDM1 9155 BOD 1 ENGL AGGR REPL
COPY 16 OUTPUT MEAN 7 1 0.454 WDM1 9151 DO 1 ENGL AGGR REPL
COPY 17 OUTPUT MEAN 1 1 0.02855 WDM1 9166 PERO 1 METR AGGR REPL
COPY 17 OUTPUT MEAN 2 1 907 WDM1 9160 TSS 1 ENGL AGGR REPL
COPY 17 OUTPUT MEAN 3 1 0.454 WDM1 9162 NH3N 1 ENGL AGGR REPL
COPY 17 OUTPUT MEAN 4 1 0.454 WDM1 9163 NO3N 1 ENGL AGGR REPL
COPY 17 OUTPUT MEAN 5 1 0.454 WDM1 9164 PO4P 1 ENGL AGGR REPL
COPY 17 OUTPUT MEAN 6 1 0.454 WDM1 9165 BOD 1 ENGL AGGR REPL
COPY 17 OUTPUT MEAN 7 1 0.454 WDM1 9161 DO 1 ENGL AGGR REPL
COPY 18 OUTPUT MEAN 1 1 0.02855 WDM1 9176 PERO 1 METR AGGR REPL
COPY 18 OUTPUT MEAN 2 1 907 WDM1 9170 TSS 1 ENGL AGGR REPL
COPY 18 OUTPUT MEAN 3 1 0.454 WDM1 9172 NH3N 1 ENGL AGGR REPL
COPY 18 OUTPUT MEAN 4 1 0.454 WDM1 9173 NO3N 1 ENGL AGGR REPL
COPY 18 OUTPUT MEAN 5 1 0.454 WDM1 9174 PO4P 1 ENGL AGGR REPL
COPY 18 OUTPUT MEAN 6 1 0.454 WDM1 9175 BOD 1 ENGL AGGR REPL
COPY 18 OUTPUT MEAN 7 1 0.454 WDM1 9171 DO 1 ENGL AGGR REPL
END EXT TARGETS

```

MASS-LINK

```

MASS-LINK 3
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
RCHRES ROFLOW RCHRES INFLOW
END MASS-LINK 3

```

```

MASS-LINK 2
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWATER PERO 0.0833333 RCHRES INFLOW IVOL
PERLND PWTGAS POHT RCHRES INFLOW IHEAT
PERLND PQUAL POQUAL 1 1.00 RCHRES INFLOW NUIF1 2
PERLND PQUAL POQUAL 2 RCHRES INFLOW NUIF1 1
PERLND PQUAL POQUAL 3 RCHRES INFLOW NUIF1 4
PERLND PQUAL POQUAL 4 1.00 RCHRES INFLOW OXIF 2
PERLND PQUAL POQUAL 4 0.100 RCHRES INFLOW PKIF 3
PERLND PQUAL POQUAL 4 0.015 RCHRES INFLOW PKIF 4
PERLND PQUAL POQUAL 4 0.5 RCHRES INFLOW PKIF 5
PERLND SEDMNT SOSED 1 0.05 RCHRES INFLOW ISED 1
PERLND SEDMNT SOSED 1 0.55 RCHRES INFLOW ISED 2
PERLND SEDMNT SOSED 1 0.4 RCHRES INFLOW ISED 3
PERLND PWTGAS PODOXM RCHRES INFLOW OXIF 1
PERLND PWTGAS POHT RCHRES INFLOW IHEAT 1
END MASS-LINK 2

```

```

MASS-LINK 1
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO 0.0833333 RCHRES INFLOW IVOL
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT
IMPLND IQUAL SOQUAL 1 1.00 RCHRES INFLOW NUIF1 2
IMPLND IQUAL SOQUAL 2 RCHRES INFLOW NUIF1 1
IMPLND IQUAL SOQUAL 3 RCHRES INFLOW NUIF1 4
IMPLND IQUAL SOQUAL 4 1.00 RCHRES INFLOW OXIF 2
IMPLND IQUAL SOQUAL 4 0.100 RCHRES INFLOW PKIF 3
IMPLND IQUAL SOQUAL 4 0.015 RCHRES INFLOW PKIF 4
IMPLND IQUAL SOQUAL 4 0.5 RCHRES INFLOW PKIF 5
IMPLND SOLIDS SOSLD 1 0.05 RCHRES INFLOW ISED 1
IMPLND SOLIDS SOSLD 1 0.55 RCHRES INFLOW ISED 2
IMPLND SOLIDS SOSLD 1 0.4 RCHRES INFLOW ISED 3
IMPLND IWTGAS SODOXM RCHRES INFLOW OXIF 1
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT 1

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

END MASS-LINK      1

MASS-LINK          27
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWATER PERO COPY INPUT MEAN 1
PERLND SEDMNT SOSED 1 COPY INPUT MEAN 2
PERLND PQUAL POQUAL 1 1.00 COPY INPUT MEAN 3
PERLND PQUAL POQUAL 2 COPY INPUT MEAN 4
PERLND PQUAL POQUAL 3 COPY INPUT MEAN 5
PERLND PQUAL POQUAL 4 1.00 COPY INPUT MEAN 6
PERLND PWTGAS PODOXM COPY INPUT MEAN 7
END MASS-LINK      27

MASS-LINK          26
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO COPY INPUT MEAN 1
IMPLND SOLIDS SOSLD 1 COPY INPUT MEAN 2
IMPLND IQUAL SOQUAL 1 1.00 COPY INPUT MEAN 3
IMPLND IQUAL SOQUAL 2 COPY INPUT MEAN 4
IMPLND IQUAL SOQUAL 3 COPY INPUT MEAN 5
IMPLND IQUAL SOQUAL 4 1.00 COPY INPUT MEAN 6
IMPLND IWTGAS SODOXM COPY INPUT MEAN 7
END MASS-LINK      26

MASS-LINK          5
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWATER PERO 0.0833333 RCHRES INFLOW IVOL
PERLND PWTGAS POHT RCHRES INFLOW IHEAT
PERLND PQUAL POQUAL 1 1.00 RCHRES INFLOW NUIF1 2
PERLND PQUAL POQUAL 2 RCHRES INFLOW NUIF1 1
PERLND PQUAL POQUAL 3 RCHRES INFLOW NUIF1 4
PERLND PQUAL POQUAL 4 1.00 RCHRES INFLOW OXIF 2
PERLND PQUAL POQUAL 4 0.100 RCHRES INFLOW PKIF 3
PERLND PQUAL POQUAL 4 0.015 RCHRES INFLOW PKIF 4
PERLND PQUAL POQUAL 4 0.5 RCHRES INFLOW PKIF 5
PERLND SEDMNT SOSED 1 0.05 RCHRES INFLOW ISED 1
PERLND SEDMNT SOSED 1 0.55 RCHRES INFLOW ISED 2
PERLND SEDMNT SOSED 1 0.4 RCHRES INFLOW ISED 3
PERLND PWTGAS PODOXM RCHRES INFLOW OXIF 1
PERLND PWTGAS POHT RCHRES INFLOW IHEAT 1
END MASS-LINK      5

MASS-LINK          4
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO 0.0833333 RCHRES INFLOW IVOL
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT
IMPLND IQUAL SOQUAL 1 1.00 RCHRES INFLOW NUIF1 2
IMPLND IQUAL SOQUAL 2 RCHRES INFLOW NUIF1 1
IMPLND IQUAL SOQUAL 3 RCHRES INFLOW NUIF1 4
IMPLND IQUAL SOQUAL 4 1.00 RCHRES INFLOW OXIF 2
IMPLND IQUAL SOQUAL 4 0.100 RCHRES INFLOW PKIF 3
IMPLND IQUAL SOQUAL 4 0.015 RCHRES INFLOW PKIF 4
IMPLND IQUAL SOQUAL 4 0.5 RCHRES INFLOW PKIF 5
IMPLND SOLIDS SOSLD 1 0.05 RCHRES INFLOW ISED 1
IMPLND SOLIDS SOSLD 1 0.55 RCHRES INFLOW ISED 2
IMPLND SOLIDS SOSLD 1 0.4 RCHRES INFLOW ISED 3
IMPLND IWTGAS SODOXM RCHRES INFLOW OXIF 1
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT 1
END MASS-LINK      4

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

    MASS-LINK          29
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWTGAS PERO COPY INPUT MEAN 1
PERLND SEDMNT SOSED 1 COPY INPUT MEAN 2
PERLND PQUAL POQUAL 1 1.00 COPY INPUT MEAN 3
PERLND PQUAL POQUAL 2 COPY INPUT MEAN 4
PERLND PQUAL POQUAL 3 COPY INPUT MEAN 5
PERLND PQUAL POQUAL 4 1.00 COPY INPUT MEAN 6
PERLND PWTGAS PODOXM COPY INPUT MEAN 7
    END MASS-LINK 29
    
```

```

    MASS-LINK          28
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO COPY INPUT MEAN 1
IMPLND SOLIDS SOSLD 1 COPY INPUT MEAN 2
IMPLND IQUAL SOQUAL 1 1.00 COPY INPUT MEAN 3
IMPLND IQUAL SOQUAL 2 COPY INPUT MEAN 4
IMPLND IQUAL SOQUAL 3 COPY INPUT MEAN 5
IMPLND IQUAL SOQUAL 4 1.00 COPY INPUT MEAN 6
IMPLND IWTGAS SODOXM COPY INPUT MEAN 7
    END MASS-LINK 28
    
```

```

    MASS-LINK          7
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWTGAS PERO 0.0833333 RCHRES INFLOW IVOL
PERLND PWTGAS POHT RCHRES INFLOW IHEAT
PERLND PQUAL POQUAL 1 1.00 RCHRES INFLOW NUIF1 2
PERLND PQUAL POQUAL 2 RCHRES INFLOW NUIF1 1
PERLND PQUAL POQUAL 3 RCHRES INFLOW NUIF1 4
PERLND PQUAL POQUAL 4 1.00 RCHRES INFLOW OXIF 2
PERLND PQUAL POQUAL 4 0.100 RCHRES INFLOW PKIF 3
PERLND PQUAL POQUAL 4 0.015 RCHRES INFLOW PKIF 4
PERLND PQUAL POQUAL 4 0.5 RCHRES INFLOW PKIF 5
PERLND SEDMNT SOSED 1 0.05 RCHRES INFLOW ISED 1
PERLND SEDMNT SOSED 1 0.55 RCHRES INFLOW ISED 2
PERLND SEDMNT SOSED 1 0.4 RCHRES INFLOW ISED 3
PERLND PWTGAS PODOXM RCHRES INFLOW OXIF 1
PERLND PWTGAS POHT RCHRES INFLOW IHEAT 1
    END MASS-LINK 7
    
```

```

    MASS-LINK          6
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO 0.0833333 RCHRES INFLOW IVOL
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT
IMPLND IQUAL SOQUAL 1 1.00 RCHRES INFLOW NUIF1 2
IMPLND IQUAL SOQUAL 2 RCHRES INFLOW NUIF1 1
IMPLND IQUAL SOQUAL 3 RCHRES INFLOW NUIF1 4
IMPLND IQUAL SOQUAL 4 1.00 RCHRES INFLOW OXIF 2
IMPLND IQUAL SOQUAL 4 0.100 RCHRES INFLOW PKIF 3
IMPLND IQUAL SOQUAL 4 0.015 RCHRES INFLOW PKIF 4
IMPLND IQUAL SOQUAL 4 0.5 RCHRES INFLOW PKIF 5
IMPLND SOLIDS SOSLD 1 0.05 RCHRES INFLOW ISED 1
IMPLND SOLIDS SOSLD 1 0.55 RCHRES INFLOW ISED 2
IMPLND SOLIDS SOSLD 1 0.4 RCHRES INFLOW ISED 3
IMPLND IWTGAS SODOXM RCHRES INFLOW OXIF 1
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT 1
    END MASS-LINK 6
    
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

    MASS-LINK          31
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWATER PERO COPY INPUT MEAN 1
PERLND SEDMNT SOSED 1 COPY INPUT MEAN 2
PERLND PQUAL POQUAL 1 1.00 COPY INPUT MEAN 3
PERLND PQUAL POQUAL 2 COPY INPUT MEAN 4
PERLND PQUAL POQUAL 3 COPY INPUT MEAN 5
PERLND PQUAL POQUAL 4 1.00 COPY INPUT MEAN 6
PERLND PWTGAS PODOXM COPY INPUT MEAN 7
    END MASS-LINK 31
    
```

```

    MASS-LINK          30
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO COPY INPUT MEAN 1
IMPLND SOLIDS SOSLD 1 COPY INPUT MEAN 2
IMPLND IQUAL SOQUAL 1 1.00 COPY INPUT MEAN 3
IMPLND IQUAL SOQUAL 2 COPY INPUT MEAN 4
IMPLND IQUAL SOQUAL 3 COPY INPUT MEAN 5
IMPLND IQUAL SOQUAL 4 1.00 COPY INPUT MEAN 6
IMPLND IWTGAS SODOXM COPY INPUT MEAN 7
    END MASS-LINK 30
    
```

```

    MASS-LINK          9
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWATER PERO 0.0833333 RCHRES INFLOW IVOL
PERLND PWTGAS POHT RCHRES INFLOW IHEAT
PERLND PQUAL POQUAL 1 1.00 RCHRES INFLOW NUIF1 2
PERLND PQUAL POQUAL 2 RCHRES INFLOW NUIF1 1
PERLND PQUAL POQUAL 3 RCHRES INFLOW NUIF1 4
PERLND PQUAL POQUAL 4 1.00 RCHRES INFLOW OXIF 2
PERLND PQUAL POQUAL 4 0.100 RCHRES INFLOW PKIF 3
PERLND PQUAL POQUAL 4 0.015 RCHRES INFLOW PKIF 4
PERLND PQUAL POQUAL 4 0.5 RCHRES INFLOW PKIF 5
PERLND SEDMNT SOSED 1 0.05 RCHRES INFLOW ISED 1
PERLND SEDMNT SOSED 1 0.55 RCHRES INFLOW ISED 2
PERLND SEDMNT SOSED 1 0.4 RCHRES INFLOW ISED 3
PERLND PWTGAS PODOXM RCHRES INFLOW OXIF 1
PERLND PWTGAS POHT RCHRES INFLOW IHEAT 1
    END MASS-LINK 9
    
```

```

    MASS-LINK          8
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO 0.0833333 RCHRES INFLOW IVOL
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT
IMPLND IQUAL SOQUAL 1 1.00 RCHRES INFLOW NUIF1 2
IMPLND IQUAL SOQUAL 2 RCHRES INFLOW NUIF1 1
IMPLND IQUAL SOQUAL 3 RCHRES INFLOW NUIF1 4
IMPLND IQUAL SOQUAL 4 1.00 RCHRES INFLOW OXIF 2
IMPLND IQUAL SOQUAL 4 0.100 RCHRES INFLOW PKIF 3
IMPLND IQUAL SOQUAL 4 0.015 RCHRES INFLOW PKIF 4
IMPLND IQUAL SOQUAL 4 0.5 RCHRES INFLOW PKIF 5
IMPLND SOLIDS SOSLD 1 0.05 RCHRES INFLOW ISED 1
IMPLND SOLIDS SOSLD 1 0.55 RCHRES INFLOW ISED 2
IMPLND SOLIDS SOSLD 1 0.4 RCHRES INFLOW ISED 3
IMPLND IWTGAS SODOXM RCHRES INFLOW OXIF 1
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT 1
    END MASS-LINK 8
    
```

MASS-LINK 33

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWATER PERO COPY INPUT MEAN 1
PERLND SEDMNT SOSED 1 COPY INPUT MEAN 2
PERLND PQUAL POQUAL 1 1.00 COPY INPUT MEAN 3
PERLND PQUAL POQUAL 2 COPY INPUT MEAN 4
PERLND PQUAL POQUAL 3 COPY INPUT MEAN 5
PERLND PQUAL POQUAL 4 1.00 COPY INPUT MEAN 6
PERLND PWTGAS PODOXM COPY INPUT MEAN 7
    END MASS-LINK 33
    
```

```

MASS-LINK 32
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO COPY INPUT MEAN 1
IMPLND SOLIDS SOSLD 1 COPY INPUT MEAN 2
IMPLND IQUAL SOQUAL 1 1.00 COPY INPUT MEAN 3
IMPLND IQUAL SOQUAL 2 COPY INPUT MEAN 4
IMPLND IQUAL SOQUAL 3 COPY INPUT MEAN 5
IMPLND IQUAL SOQUAL 4 1.00 COPY INPUT MEAN 6
IMPLND IWTGAS SODOXM COPY INPUT MEAN 7
    END MASS-LINK 32
    
```

```

MASS-LINK 11
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND PWATER PERO 0.0833333 RCHRES INFLOW IVOL
PERLND PWTGAS POHT RCHRES INFLOW IHEAT
PERLND PQUAL POQUAL 1 1.00 RCHRES INFLOW NUIF1 2
PERLND PQUAL POQUAL 2 RCHRES INFLOW NUIF1 1
PERLND PQUAL POQUAL 3 RCHRES INFLOW NUIF1 4
PERLND PQUAL POQUAL 4 1.00 RCHRES INFLOW OXIF 2
PERLND PQUAL POQUAL 4 0.100 RCHRES INFLOW PKIF 3
PERLND PQUAL POQUAL 4 0.015 RCHRES INFLOW PKIF 4
PERLND PQUAL POQUAL 4 0.5 RCHRES INFLOW PKIF 5
PERLND SEDMNT SOSED 1 0.05 RCHRES INFLOW ISED 1
PERLND SEDMNT SOSED 1 0.55 RCHRES INFLOW ISED 2
PERLND SEDMNT SOSED 1 0.4 RCHRES INFLOW ISED 3
PERLND PWTGAS PODOXM RCHRES INFLOW OXIF 1
PERLND PWTGAS POHT RCHRES INFLOW IHEAT 1
    END MASS-LINK 11
    
```

```

MASS-LINK 10
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND IWATER SURO 0.0833333 RCHRES INFLOW IVOL
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT
IMPLND IQUAL SOQUAL 1 1.00 RCHRES INFLOW NUIF1 2
IMPLND IQUAL SOQUAL 2 RCHRES INFLOW NUIF1 1
IMPLND IQUAL SOQUAL 3 RCHRES INFLOW NUIF1 4
IMPLND IQUAL SOQUAL 4 1.00 RCHRES INFLOW OXIF 2
IMPLND IQUAL SOQUAL 4 0.100 RCHRES INFLOW PKIF 3
IMPLND IQUAL SOQUAL 4 0.015 RCHRES INFLOW PKIF 4
IMPLND IQUAL SOQUAL 4 0.5 RCHRES INFLOW PKIF 5
IMPLND SOLIDS SOSLD 1 0.05 RCHRES INFLOW ISED 1
IMPLND SOLIDS SOSLD 1 0.55 RCHRES INFLOW ISED 2
IMPLND SOLIDS SOSLD 1 0.4 RCHRES INFLOW ISED 3
IMPLND IWTGAS SODOXM RCHRES INFLOW OXIF 1
IMPLND IWTGAS SOHT RCHRES INFLOW IHEAT 1
    END MASS-LINK 10
    
```

```

MASS-LINK 35
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
    
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

<Name>          <Name> x x<-factor->          <Name>          <Name> x x ***
PERLND  PWATER  PERO          COPY          INPUT  MEAN  1
PERLND  SEDMNT  SOSED  1          COPY          INPUT  MEAN  2
PERLND  PQUAL  POQUAL  1          1.00         COPY          INPUT  MEAN  3
PERLND  PQUAL  POQUAL  2          COPY          INPUT  MEAN  4
PERLND  PQUAL  POQUAL  3          COPY          INPUT  MEAN  5
PERLND  PQUAL  POQUAL  4          1.00         COPY          INPUT  MEAN  6
PERLND  PWTGAS  PODOXM          COPY          INPUT  MEAN  7
  END MASS-LINK  35

  MASS-LINK  34
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->          <Name>          <Name> x x ***
IMPLND  IWATER  SURO          COPY          INPUT  MEAN  1
IMPLND  SOLIDS  SOSLD  1          COPY          INPUT  MEAN  2
IMPLND  IQUAL  SOQUAL  1          1.00         COPY          INPUT  MEAN  3
IMPLND  IQUAL  SOQUAL  2          COPY          INPUT  MEAN  4
IMPLND  IQUAL  SOQUAL  3          COPY          INPUT  MEAN  5
IMPLND  IQUAL  SOQUAL  4          1.00         COPY          INPUT  MEAN  6
IMPLND  IWTGAS  SODOXM          COPY          INPUT  MEAN  7
  END MASS-LINK  34

  MASS-LINK  13
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->          <Name>          <Name> x x ***
PERLND  PWATER  PERO          0.0833333    RCHRES          INFLOW  IVOL
PERLND  PWTGAS  POHT          RCHRES          INFLOW  IHEAT
PERLND  PQUAL  POQUAL  1          1.00         RCHRES          INFLOW  NUIF1  2
PERLND  PQUAL  POQUAL  2          RCHRES          INFLOW  NUIF1  1
PERLND  PQUAL  POQUAL  3          RCHRES          INFLOW  NUIF1  4
PERLND  PQUAL  POQUAL  4          1.00         RCHRES          INFLOW  OXIF  2
PERLND  PQUAL  POQUAL  4          0.100        RCHRES          INFLOW  PKIF  3
PERLND  PQUAL  POQUAL  4          0.015        RCHRES          INFLOW  PKIF  4
PERLND  PQUAL  POQUAL  4          0.5          RCHRES          INFLOW  PKIF  5
PERLND  SEDMNT  SOSED  1          0.05         RCHRES          INFLOW  ISED  1
PERLND  SEDMNT  SOSED  1          0.55         RCHRES          INFLOW  ISED  2
PERLND  SEDMNT  SOSED  1          0.4          RCHRES          INFLOW  ISED  3
PERLND  PWTGAS  PODOXM          RCHRES          INFLOW  OXIF  1
PERLND  PWTGAS  POHT          RCHRES          INFLOW  IHEAT  1
  END MASS-LINK  13

  MASS-LINK  12
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->          <Name>          <Name> x x ***
IMPLND  IWATER  SURO          0.0833333    RCHRES          INFLOW  IVOL
IMPLND  IWTGAS  SOHT          RCHRES          INFLOW  IHEAT
IMPLND  IQUAL  SOQUAL  1          1.00         RCHRES          INFLOW  NUIF1  2
IMPLND  IQUAL  SOQUAL  2          RCHRES          INFLOW  NUIF1  1
IMPLND  IQUAL  SOQUAL  3          RCHRES          INFLOW  NUIF1  4
IMPLND  IQUAL  SOQUAL  4          1.00         RCHRES          INFLOW  OXIF  2
IMPLND  IQUAL  SOQUAL  4          0.100        RCHRES          INFLOW  PKIF  3
IMPLND  IQUAL  SOQUAL  4          0.015        RCHRES          INFLOW  PKIF  4
IMPLND  IQUAL  SOQUAL  4          0.5          RCHRES          INFLOW  PKIF  5
IMPLND  SOLIDS  SOSLD  1          0.05         RCHRES          INFLOW  ISED  1
IMPLND  SOLIDS  SOSLD  1          0.55         RCHRES          INFLOW  ISED  2
IMPLND  SOLIDS  SOSLD  1          0.4          RCHRES          INFLOW  ISED  3
IMPLND  IWTGAS  SODOXM          RCHRES          INFLOW  OXIF  1
IMPLND  IWTGAS  SOHT          RCHRES          INFLOW  IHEAT  1
  END MASS-LINK  12

  MASS-LINK  37
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->          <Name>          <Name> x x ***

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

PERLND  PWATER  PERO                COPY          INPUT  MEAN  1
PERLND  SEDMNT  SOSED  1                COPY          INPUT  MEAN  2
PERLND  PQUAL  POQUAL 1          1.00         COPY          INPUT  MEAN  3
PERLND  PQUAL  POQUAL 2                COPY          INPUT  MEAN  4
PERLND  PQUAL  POQUAL 3                COPY          INPUT  MEAN  5
PERLND  PQUAL  POQUAL 4          1.00         COPY          INPUT  MEAN  6
PERLND  PWTGAS  PODOXM          COPY          INPUT  MEAN  7
  END MASS-LINK  37

  MASS-LINK  36
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND  IWATER  SURO                COPY          INPUT  MEAN  1
IMPLND  SOLIDS  SOSLD  1                COPY          INPUT  MEAN  2
IMPLND  IQUAL  SOQUAL 1          1.00         COPY          INPUT  MEAN  3
IMPLND  IQUAL  SOQUAL 2                COPY          INPUT  MEAN  4
IMPLND  IQUAL  SOQUAL 3                COPY          INPUT  MEAN  5
IMPLND  IQUAL  SOQUAL 4          1.00         COPY          INPUT  MEAN  6
IMPLND  IWTGAS  SODOXM          COPY          INPUT  MEAN  7
  END MASS-LINK  36

  MASS-LINK  15
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND  PWATER  PERO                0.08333333  RCHRES       INFLOW  IVOL
PERLND  PWTGAS  POHT                RCHRES       INFLOW  IHEAT
PERLND  PQUAL  POQUAL 1          1.00         RCHRES       INFLOW  NUIF1  2
PERLND  PQUAL  POQUAL 2                RCHRES       INFLOW  NUIF1  1
PERLND  PQUAL  POQUAL 3                RCHRES       INFLOW  NUIF1  4
PERLND  PQUAL  POQUAL 4          1.00         RCHRES       INFLOW  OXIF  2
PERLND  PQUAL  POQUAL 4          0.100        RCHRES       INFLOW  PKIF  3
PERLND  PQUAL  POQUAL 4          0.015        RCHRES       INFLOW  PKIF  4
PERLND  PQUAL  POQUAL 4          0.5          RCHRES       INFLOW  PKIF  5
PERLND  SEDMNT  SOSED  1          0.05         RCHRES       INFLOW  ISED  1
PERLND  SEDMNT  SOSED  1          0.55         RCHRES       INFLOW  ISED  2
PERLND  SEDMNT  SOSED  1          0.4          RCHRES       INFLOW  ISED  3
PERLND  PWTGAS  PODOXM          RCHRES       INFLOW  OXIF  1
PERLND  PWTGAS  POHT                RCHRES       INFLOW  IHEAT  1
  END MASS-LINK  15

  MASS-LINK  14
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND  IWATER  SURO                0.08333333  RCHRES       INFLOW  IVOL
IMPLND  IWTGAS  SOHT                RCHRES       INFLOW  IHEAT
IMPLND  IQUAL  SOQUAL 1          1.00         RCHRES       INFLOW  NUIF1  2
IMPLND  IQUAL  SOQUAL 2                RCHRES       INFLOW  NUIF1  1
IMPLND  IQUAL  SOQUAL 3                RCHRES       INFLOW  NUIF1  4
IMPLND  IQUAL  SOQUAL 4          1.00         RCHRES       INFLOW  OXIF  2
IMPLND  IQUAL  SOQUAL 4          0.100        RCHRES       INFLOW  PKIF  3
IMPLND  IQUAL  SOQUAL 4          0.015        RCHRES       INFLOW  PKIF  4
IMPLND  IQUAL  SOQUAL 4          0.5          RCHRES       INFLOW  PKIF  5
IMPLND  SOLIDS  SOSLD  1          0.05         RCHRES       INFLOW  ISED  1
IMPLND  SOLIDS  SOSLD  1          0.55         RCHRES       INFLOW  ISED  2
IMPLND  SOLIDS  SOSLD  1          0.4          RCHRES       INFLOW  ISED  3
IMPLND  IWTGAS  SODOXM          RCHRES       INFLOW  OXIF  1
IMPLND  IWTGAS  SOHT                RCHRES       INFLOW  IHEAT  1
  END MASS-LINK  14

  MASS-LINK  39
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND  PWATER  PERO                COPY          INPUT  MEAN  1
  
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B

```

PERLND  SEDMNT  SOSED  1          COPY          INPUT  MEAN  2
PERLND  PQUAL  POQUAL  1          1.00  COPY          INPUT  MEAN  3
PERLND  PQUAL  POQUAL  2          COPY          INPUT  MEAN  4
PERLND  PQUAL  POQUAL  3          COPY          INPUT  MEAN  5
PERLND  PQUAL  POQUAL  4          1.00  COPY          INPUT  MEAN  6
PERLND  PWTGAS  PODOXM  COPY          INPUT  MEAN  7
  END MASS-LINK  39

  MASS-LINK  38
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND  IWATER  SURO          COPY          INPUT  MEAN  1
IMPLND  SOLIDS  SOSLD  1          COPY          INPUT  MEAN  2
IMPLND  IQUAL  SOQUAL  1          1.00  COPY          INPUT  MEAN  3
IMPLND  IQUAL  SOQUAL  2          COPY          INPUT  MEAN  4
IMPLND  IQUAL  SOQUAL  3          COPY          INPUT  MEAN  5
IMPLND  IQUAL  SOQUAL  4          1.00  COPY          INPUT  MEAN  6
IMPLND  IWTGAS  SODOXM  COPY          INPUT  MEAN  7
  END MASS-LINK  38

  MASS-LINK  17
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND  PWATER  PERO          0.0833333  RCHRES        INFLOW  IVOL
PERLND  PWTGAS  POHT          RCHRES        INFLOW  IHEAT
PERLND  PQUAL  POQUAL  1          1.00  RCHRES        INFLOW  NUIF1  2
PERLND  PQUAL  POQUAL  2          RCHRES        INFLOW  NUIF1  1
PERLND  PQUAL  POQUAL  3          RCHRES        INFLOW  NUIF1  4
PERLND  PQUAL  POQUAL  4          1.00  RCHRES        INFLOW  OXIF  2
PERLND  PQUAL  POQUAL  4          0.100  RCHRES        INFLOW  PKIF  3
PERLND  PQUAL  POQUAL  4          0.015  RCHRES        INFLOW  PKIF  4
PERLND  PQUAL  POQUAL  4          0.5    RCHRES        INFLOW  PKIF  5
PERLND  SEDMNT  SOSED  1          0.05  RCHRES        INFLOW  ISED  1
PERLND  SEDMNT  SOSED  1          0.55  RCHRES        INFLOW  ISED  2
PERLND  SEDMNT  SOSED  1          0.4   RCHRES        INFLOW  ISED  3
PERLND  PWTGAS  PODOXM  RCHRES        INFLOW  OXIF  1
PERLND  PWTGAS  POHT          RCHRES        INFLOW  IHEAT  1
  END MASS-LINK  17

  MASS-LINK  16
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND  IWATER  SURO          0.0833333  RCHRES        INFLOW  IVOL
IMPLND  IWTGAS  SOHT          RCHRES        INFLOW  IHEAT
IMPLND  IQUAL  SOQUAL  1          1.00  RCHRES        INFLOW  NUIF1  2
IMPLND  IQUAL  SOQUAL  2          RCHRES        INFLOW  NUIF1  1
IMPLND  IQUAL  SOQUAL  3          RCHRES        INFLOW  NUIF1  4
IMPLND  IQUAL  SOQUAL  4          1.00  RCHRES        INFLOW  OXIF  2
IMPLND  IQUAL  SOQUAL  4          0.100  RCHRES        INFLOW  PKIF  3
IMPLND  IQUAL  SOQUAL  4          0.015  RCHRES        INFLOW  PKIF  4
IMPLND  IQUAL  SOQUAL  4          0.5    RCHRES        INFLOW  PKIF  5
IMPLND  SOLIDS  SOSLD  1          0.05  RCHRES        INFLOW  ISED  1
IMPLND  SOLIDS  SOSLD  1          0.55  RCHRES        INFLOW  ISED  2
IMPLND  SOLIDS  SOSLD  1          0.4   RCHRES        INFLOW  ISED  3
IMPLND  IWTGAS  SODOXM  RCHRES        INFLOW  OXIF  1
IMPLND  IWTGAS  SOHT          RCHRES        INFLOW  IHEAT  1
  END MASS-LINK  16

  MASS-LINK  41
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND  PWATER  PERO          COPY          INPUT  MEAN  1
PERLND  SEDMNT  SOSED  1          COPY          INPUT  MEAN  2

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

PERLND    PQUAL    POQUAL 1          1.00    COPY          INPUT    MEAN    3
PERLND    PQUAL    POQUAL 2          1.00    COPY          INPUT    MEAN    4
PERLND    PQUAL    POQUAL 3          1.00    COPY          INPUT    MEAN    5
PERLND    PQUAL    POQUAL 4          1.00    COPY          INPUT    MEAN    6
PERLND    PWTGAS   PODOXM          COPY          INPUT    MEAN    7
  END MASS-LINK    41

  MASS-LINK    40
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND    IWATER   SURO          COPY          INPUT    MEAN    1
IMPLND    SOLIDS   SOSLD 1          1.00    COPY          INPUT    MEAN    2
IMPLND    IQUAL    SOQUAL 1          1.00    COPY          INPUT    MEAN    3
IMPLND    IQUAL    SOQUAL 2          1.00    COPY          INPUT    MEAN    4
IMPLND    IQUAL    SOQUAL 3          1.00    COPY          INPUT    MEAN    5
IMPLND    IQUAL    SOQUAL 4          1.00    COPY          INPUT    MEAN    6
IMPLND    IWTGAS   SODOXM          COPY          INPUT    MEAN    7
  END MASS-LINK    40

  MASS-LINK    19
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND    PWATER   PERO          0.0833333    RCHRES        INFLOW   IVOL
PERLND    PWTGAS   POHT          RCHRES        INFLOW   IHEAT
PERLND    PQUAL    POQUAL 1          1.00    RCHRES        INFLOW   NUIF1  2
PERLND    PQUAL    POQUAL 2          RCHRES        INFLOW   NUIF1  1
PERLND    PQUAL    POQUAL 3          RCHRES        INFLOW   NUIF1  4
PERLND    PQUAL    POQUAL 4          1.00    RCHRES        INFLOW   OXIF   2
PERLND    PQUAL    POQUAL 4          0.100    RCHRES        INFLOW   PKIF   3
PERLND    PQUAL    POQUAL 4          0.015    RCHRES        INFLOW   PKIF   4
PERLND    PQUAL    POQUAL 4          0.5      RCHRES        INFLOW   PKIF   5
PERLND    SEDMNT   SOSED 1          0.05    RCHRES        INFLOW   ISED   1
PERLND    SEDMNT   SOSED 1          0.55    RCHRES        INFLOW   ISED   2
PERLND    SEDMNT   SOSED 1          0.4     RCHRES        INFLOW   ISED   3
PERLND    PWTGAS   PODOXM          RCHRES        INFLOW   OXIF   1
PERLND    PWTGAS   POHT          RCHRES        INFLOW   IHEAT   1
  END MASS-LINK    19

  MASS-LINK    18
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND    IWATER   SURO          0.0833333    RCHRES        INFLOW   IVOL
IMPLND    IWTGAS   SOHT          RCHRES        INFLOW   IHEAT
IMPLND    IQUAL    SOQUAL 1          1.00    RCHRES        INFLOW   NUIF1  2
IMPLND    IQUAL    SOQUAL 2          RCHRES        INFLOW   NUIF1  1
IMPLND    IQUAL    SOQUAL 3          RCHRES        INFLOW   NUIF1  4
IMPLND    IQUAL    SOQUAL 4          1.00    RCHRES        INFLOW   OXIF   2
IMPLND    IQUAL    SOQUAL 4          0.100    RCHRES        INFLOW   PKIF   3
IMPLND    IQUAL    SOQUAL 4          0.015    RCHRES        INFLOW   PKIF   4
IMPLND    IQUAL    SOQUAL 4          0.5      RCHRES        INFLOW   PKIF   5
IMPLND    SOLIDS   SOSLD 1          0.05    RCHRES        INFLOW   ISED   1
IMPLND    SOLIDS   SOSLD 1          0.55    RCHRES        INFLOW   ISED   2
IMPLND    SOLIDS   SOSLD 1          0.4     RCHRES        INFLOW   ISED   3
IMPLND    IWTGAS   SODOXM          RCHRES        INFLOW   OXIF   1
IMPLND    IWTGAS   SOHT          RCHRES        INFLOW   IHEAT   1
  END MASS-LINK    18

  MASS-LINK    43
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND    PWATER   PERO          COPY          INPUT    MEAN    1
PERLND    SEDMNT   SOSED 1          COPY          INPUT    MEAN    2
PERLND    PQUAL    POQUAL 1          1.00    COPY          INPUT    MEAN    3
  
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

PERLND    PQUAL    POQUAL 2                COPY                INPUT MEAN 4
PERLND    PQUAL    POQUAL 3                COPY                INPUT MEAN 5
PERLND    PQUAL    POQUAL 4                1.00              COPY                INPUT MEAN 6
PERLND    PWTGAS   PODOXM                COPY                INPUT MEAN 7
    END MASS-LINK 43

    MASS-LINK 42
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND    IWATER   SURO                COPY                INPUT MEAN 1
IMPLND    SOLIDS   SOSLD 1                COPY                INPUT MEAN 2
IMPLND    IQUAL    SOQUAL 1                1.00              COPY                INPUT MEAN 3
IMPLND    IQUAL    SOQUAL 2                COPY                INPUT MEAN 4
IMPLND    IQUAL    SOQUAL 3                COPY                INPUT MEAN 5
IMPLND    IQUAL    SOQUAL 4                1.00              COPY                INPUT MEAN 6
IMPLND    IWTGAS   SODOXM                COPY                INPUT MEAN 7
    END MASS-LINK 42

    MASS-LINK 21
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND    PWATER   PERO                0.0833333        RCHRES             INFLOW IVOL
PERLND    PWTGAS   POHT                RCHRES             INFLOW IHEAT
PERLND    PQUAL    POQUAL 1                1.00              RCHRES             INFLOW NUIF1 2
PERLND    PQUAL    POQUAL 2                RCHRES             INFLOW NUIF1 1
PERLND    PQUAL    POQUAL 3                RCHRES             INFLOW NUIF1 4
PERLND    PQUAL    POQUAL 4                1.00              RCHRES             INFLOW OXIF 2
PERLND    PQUAL    POQUAL 4                0.100            RCHRES             INFLOW PKIF 3
PERLND    PQUAL    POQUAL 4                0.015            RCHRES             INFLOW PKIF 4
PERLND    PQUAL    POQUAL 4                0.5               RCHRES             INFLOW PKIF 5
PERLND    SEDMNT   SOSED 1                0.05              RCHRES             INFLOW ISED 1
PERLND    SEDMNT   SOSED 1                0.55              RCHRES             INFLOW ISED 2
PERLND    SEDMNT   SOSED 1                0.4               RCHRES             INFLOW ISED 3
PERLND    PWTGAS   PODOXM                RCHRES             INFLOW OXIF 1
PERLND    PWTGAS   POHT                RCHRES             INFLOW IHEAT 1
    END MASS-LINK 21

    MASS-LINK 20
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND    IWATER   SURO                0.0833333        RCHRES             INFLOW IVOL
IMPLND    IWTGAS   SOHT                RCHRES             INFLOW IHEAT
IMPLND    IQUAL    SOQUAL 1                1.00              RCHRES             INFLOW NUIF1 2
IMPLND    IQUAL    SOQUAL 2                RCHRES             INFLOW NUIF1 1
IMPLND    IQUAL    SOQUAL 3                RCHRES             INFLOW NUIF1 4
IMPLND    IQUAL    SOQUAL 4                1.00              RCHRES             INFLOW OXIF 2
IMPLND    IQUAL    SOQUAL 4                0.100            RCHRES             INFLOW PKIF 3
IMPLND    IQUAL    SOQUAL 4                0.015            RCHRES             INFLOW PKIF 4
IMPLND    IQUAL    SOQUAL 4                0.5               RCHRES             INFLOW PKIF 5
IMPLND    SOLIDS   SOSLD 1                0.05              RCHRES             INFLOW ISED 1
IMPLND    SOLIDS   SOSLD 1                0.55              RCHRES             INFLOW ISED 2
IMPLND    SOLIDS   SOSLD 1                0.4               RCHRES             INFLOW ISED 3
IMPLND    IWTGAS   SODOXM                RCHRES             INFLOW OXIF 1
IMPLND    IWTGAS   SOHT                RCHRES             INFLOW IHEAT 1
    END MASS-LINK 20

    MASS-LINK 45
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND    PWATER   PERO                COPY                INPUT MEAN 1
PERLND    SEDMNT   SOSED 1                COPY                INPUT MEAN 2
PERLND    PQUAL    POQUAL 1                1.00              COPY                INPUT MEAN 3
PERLND    PQUAL    POQUAL 2                COPY                INPUT MEAN 4
    
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
 Appendix B

```

PERLND    PQUAL    POQUAL 3                COPY          INPUT MEAN 5
PERLND    PQUAL    POQUAL 4                1.00          COPY          INPUT MEAN 6
PERLND    PWTGAS   PODOXM                COPY          INPUT MEAN 7
  END MASS-LINK 45

  MASS-LINK 44
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND    IWATER   SURO                COPY          INPUT MEAN 1
IMPLND    SOLIDS   SOSLD 1                COPY          INPUT MEAN 2
IMPLND    IQUAL    SOQUAL 1                1.00          COPY          INPUT MEAN 3
IMPLND    IQUAL    SOQUAL 2                COPY          INPUT MEAN 4
IMPLND    IQUAL    SOQUAL 3                COPY          INPUT MEAN 5
IMPLND    IQUAL    SOQUAL 4                1.00          COPY          INPUT MEAN 6
IMPLND    IWTGAS   SODOXM                COPY          INPUT MEAN 7
  END MASS-LINK 44

  MASS-LINK 23
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND    PWATER   PERO                0.08333333   RCHRES        INFLOW IVOL
PERLND    PWTGAS   POHT                RCHRES        INFLOW IHEAT
PERLND    PQUAL    POQUAL 1                1.00          RCHRES        INFLOW NUIF1 2
PERLND    PQUAL    POQUAL 2                RCHRES        INFLOW NUIF1 1
PERLND    PQUAL    POQUAL 3                RCHRES        INFLOW NUIF1 4
PERLND    PQUAL    POQUAL 4                1.00          RCHRES        INFLOW OXIF 2
PERLND    PQUAL    POQUAL 4                0.100         RCHRES        INFLOW PKIF 3
PERLND    PQUAL    POQUAL 4                0.015         RCHRES        INFLOW PKIF 4
PERLND    PQUAL    POQUAL 4                0.5           RCHRES        INFLOW PKIF 5
PERLND    SEDMNT   SOSED 1                0.05          RCHRES        INFLOW ISED 1
PERLND    SEDMNT   SOSED 1                0.55          RCHRES        INFLOW ISED 2
PERLND    SEDMNT   SOSED 1                0.4           RCHRES        INFLOW ISED 3
PERLND    PWTGAS   PODOXM                RCHRES        INFLOW OXIF 1
PERLND    PWTGAS   POHT                RCHRES        INFLOW IHEAT 1
  END MASS-LINK 23

  MASS-LINK 22
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND    IWATER   SURO                0.08333333   RCHRES        INFLOW IVOL
IMPLND    IWTGAS   SOHT                RCHRES        INFLOW IHEAT
IMPLND    IQUAL    SOQUAL 1                1.00          RCHRES        INFLOW NUIF1 2
IMPLND    IQUAL    SOQUAL 2                RCHRES        INFLOW NUIF1 1
IMPLND    IQUAL    SOQUAL 3                RCHRES        INFLOW NUIF1 4
IMPLND    IQUAL    SOQUAL 4                1.00          RCHRES        INFLOW OXIF 2
IMPLND    IQUAL    SOQUAL 4                0.100         RCHRES        INFLOW PKIF 3
IMPLND    IQUAL    SOQUAL 4                0.015         RCHRES        INFLOW PKIF 4
IMPLND    IQUAL    SOQUAL 4                0.5           RCHRES        INFLOW PKIF 5
IMPLND    SOLIDS   SOSLD 1                0.05          RCHRES        INFLOW ISED 1
IMPLND    SOLIDS   SOSLD 1                0.55          RCHRES        INFLOW ISED 2
IMPLND    SOLIDS   SOSLD 1                0.4           RCHRES        INFLOW ISED 3
IMPLND    IWTGAS   SODOXM                RCHRES        INFLOW OXIF 1
IMPLND    IWTGAS   SOHT                RCHRES        INFLOW IHEAT 1
  END MASS-LINK 22

  MASS-LINK 47
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND    PWATER   PERO                COPY          INPUT MEAN 1
PERLND    SEDMNT   SOSED 1                COPY          INPUT MEAN 2
PERLND    PQUAL    POQUAL 1                1.00          COPY          INPUT MEAN 3
PERLND    PQUAL    POQUAL 2                COPY          INPUT MEAN 4
PERLND    PQUAL    POQUAL 3                COPY          INPUT MEAN 5
  
```

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B*

```

PERLND    PQUAL    POQUAL 4          1.00    COPY          INPUT MEAN 6
PERLND    PWTGAS   PODOXM          COPY          INPUT MEAN 7
  END MASS-LINK 47

  MASS-LINK 46
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND    IWATER   SURO          COPY          INPUT MEAN 1
IMPLND    SOLIDS   SOSLD 1          COPY          INPUT MEAN 2
IMPLND    IQUAL    SOQUAL 1          1.00    COPY          INPUT MEAN 3
IMPLND    IQUAL    SOQUAL 2          COPY          INPUT MEAN 4
IMPLND    IQUAL    SOQUAL 3          COPY          INPUT MEAN 5
IMPLND    IQUAL    SOQUAL 4          1.00    COPY          INPUT MEAN 6
IMPLND    IWTGAS   SODOXM          COPY          INPUT MEAN 7
  END MASS-LINK 46

  MASS-LINK 25
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND    PWATER   PERO          0.0833333   RCHRES        INFLOW IVOL
PERLND    PWTGAS   POHT          RCHRES        INFLOW IHEAT
PERLND    PQUAL    POQUAL 1          1.00    RCHRES        INFLOW NUIF1 2
PERLND    PQUAL    POQUAL 2          RCHRES        INFLOW NUIF1 1
PERLND    PQUAL    POQUAL 3          RCHRES        INFLOW NUIF1 4
PERLND    PQUAL    POQUAL 4          1.00    RCHRES        INFLOW OXIF 2
PERLND    PQUAL    POQUAL 4          0.100   RCHRES        INFLOW PKIF 3
PERLND    PQUAL    POQUAL 4          0.015   RCHRES        INFLOW PKIF 4
PERLND    PQUAL    POQUAL 4          0.5     RCHRES        INFLOW PKIF 5
PERLND    SEDMNT   SOSED 1          0.05    RCHRES        INFLOW ISED 1
PERLND    SEDMNT   SOSED 1          0.55    RCHRES        INFLOW ISED 2
PERLND    SEDMNT   SOSED 1          0.4     RCHRES        INFLOW ISED 3
PERLND    PWTGAS   PODOXM          RCHRES        INFLOW OXIF 1
PERLND    PWTGAS   POHT          RCHRES        INFLOW IHEAT 1
  END MASS-LINK 25

  MASS-LINK 24
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND    IWATER   SURO          0.0833333   RCHRES        INFLOW IVOL
IMPLND    IWTGAS   SOHT          RCHRES        INFLOW IHEAT
IMPLND    IQUAL    SOQUAL 1          1.00    RCHRES        INFLOW NUIF1 2
IMPLND    IQUAL    SOQUAL 2          RCHRES        INFLOW NUIF1 1
IMPLND    IQUAL    SOQUAL 3          RCHRES        INFLOW NUIF1 4
IMPLND    IQUAL    SOQUAL 4          1.00    RCHRES        INFLOW OXIF 2
IMPLND    IQUAL    SOQUAL 4          0.100   RCHRES        INFLOW PKIF 3
IMPLND    IQUAL    SOQUAL 4          0.015   RCHRES        INFLOW PKIF 4
IMPLND    IQUAL    SOQUAL 4          0.5     RCHRES        INFLOW PKIF 5
IMPLND    SOLIDS   SOSLD 1          0.05    RCHRES        INFLOW ISED 1
IMPLND    SOLIDS   SOSLD 1          0.55    RCHRES        INFLOW ISED 2
IMPLND    SOLIDS   SOSLD 1          0.4     RCHRES        INFLOW ISED 3
IMPLND    IWTGAS   SODOXM          RCHRES        INFLOW OXIF 1
IMPLND    IWTGAS   SOHT          RCHRES        INFLOW IHEAT 1
  END MASS-LINK 24

  MASS-LINK 49
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name> <Name> x x<-factor-> <Name> <Name> x x ***
PERLND    PWATER   PERO          COPY          INPUT MEAN 1
PERLND    SEDMNT   SOSED 1          COPY          INPUT MEAN 2
PERLND    PQUAL    POQUAL 1          1.00    COPY          INPUT MEAN 3
PERLND    PQUAL    POQUAL 2          COPY          INPUT MEAN 4
PERLND    PQUAL    POQUAL 3          COPY          INPUT MEAN 5
PERLND    PQUAL    POQUAL 4          1.00    COPY          INPUT MEAN 6

```

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix B*

```

PERLND      PWTGAS  PODOXM
  END MASS-LINK  49

      MASS-LINK      48
<-Volume-> <-Grp> <-Member-><--Mult--> <-Target vols> <-Grp> <-Member-> ***
<Name>      <Name> x x<-factor-> <Name> <Name> x x ***
IMPLND      IWATER  SURO      COPY      INPUT  MEAN  1
IMPLND      SOLIDS  SOSLD  1      COPY      INPUT  MEAN  2
IMPLND      IQUAL   SOQUAL 1      1.00     COPY      INPUT  MEAN  3
IMPLND      IQUAL   SOQUAL 2      COPY      INPUT  MEAN  4
IMPLND      IQUAL   SOQUAL 3      COPY      INPUT  MEAN  5
IMPLND      IQUAL   SOQUAL 4      1.00     COPY      INPUT  MEAN  6
IMPLND      IWTGAS  SODOXM COPY      INPUT  MEAN  7
  END MASS-LINK  48
END MASS-LINK

END RUN

```

Appendix C Adams Bayou RMA2 Geometry and Boundary Condition Files

```

T1 Adams Bayou Model B Long Term Run GFGEN input file
T2 Geometry input file
T3
SI 1
$L 3
GE 1 1 2 3 0 0 0 0 0 1 0.0
GE 2 3 4 5 0 0 0 0 0 1 0.0
GE 3 5 6 7 0 0 0 0 0 1 0.0
GE 4 7 8 9 0 0 0 0 0 1 0.0
GE 5 9 10 11 0 0 0 0 0 1 0.0
GE 6 11 12 13 0 0 0 0 0 1 0.0
GE 7 13 14 15 0 0 0 0 0 1 0.0
GE 57 15 16 17 0 0 0 0 0 901 0.0
GE 8 16 18 19 0 0 0 0 0 1 0.0
GE 9 19 20 21 0 0 0 0 0 1 0.0
GE 10 21 22 23 0 0 0 0 0 1 0.0
GE 11 23 24 25 0 0 0 0 0 1 0.0
GE 12 25 26 27 0 0 0 0 0 1 0.0
GE 13 17 28 29 0 0 0 0 0 1 0.0
GE 14 29 30 31 0 0 0 0 0 1 0.0
GE 15 31 32 33 0 0 0 0 0 1 0.0
GE 16 33 34 35 0 0 0 0 0 1 0.0
GE 17 35 36 37 0 0 0 0 0 1 0.0
GE 18 37 38 39 0 0 0 0 0 1 0.0
GE 58 39 40 41 0 0 0 0 0 901 0.0
GE 59 41 44 45 0 0 0 0 0 2 0.0
GE 60 45 46 47 0 0 0 0 0 2 0.0
GE 61 47 48 49 0 0 0 0 0 3 0.0
GE 62 49 50 51 0 0 0 0 0 3 0.0
GE 63 51 52 53 0 0 0 0 0 3 0.0
GE 64 53 54 55 0 0 0 0 0 3 0.0
GE 19 40 42 43 0 0 0 0 0 1 0.0
GE 20 43 56 57 0 0 0 0 0 1 0.0
GE 21 57 58 59 0 0 0 0 0 1 0.0
GE 22 59 60 61 0 0 0 0 0 1 0.0
GE 65 61 62 63 0 0 0 0 0 901 0.0
GE 23 62 64 65 0 0 0 0 0 1 0.0
GE 66 63 66 67 0 0 0 0 0 1 0.0
GE 67 67 68 69 0 0 0 0 0 3 0.0
GE 68 69 70 71 0 0 0 0 0 3 0.0
GE 69 71 72 73 0 0 0 0 0 3 0.0
GE 24 65 74 75 0 0 0 0 0 1 0.0
GE 25 75 76 77 0 0 0 0 0 1 0.0
GE 26 77 78 79 0 0 0 0 0 1 0.0
GE 27 79 80 81 0 0 0 0 0 1 0.0
GE 28 81 82 83 0 0 0 0 0 1 0.0
GE 29 83 84 85 0 0 0 0 0 1 0.0
GE 30 85 86 87 0 0 0 0 0 1 0.0
GE 31 87 88 89 0 0 0 0 0 1 0.0
GE 32 89 90 91 0 0 0 0 0 2 0.0
GE 33 91 92 93 0 0 0 0 0 2 0.0
GE 34 93 94 95 0 0 0 0 0 2 0.0
GE 35 95 96 97 0 0 0 0 0 2 0.0
GE 36 97 98 99 0 0 0 0 0 2 0.0
GE 70 99 100 101 0 0 0 0 0 901 0.0
GE 37 100 102 103 0 0 0 0 0 2 0.0
    
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

GE	71	101	104	105	0	0	0	0	0	3	0.0
GE	72	105	106	107	0	0	0	0	0	3	0.0
GE	38	103	108	109	0	0	0	0	0	2	0.0
GE	39	109	110	111	0	0	0	0	0	2	0.0
GE	40	111	112	113	0	0	0	0	0	2	0.0
GE	41	113	114	115	0	0	0	0	0	2	0.0
GE	42	115	116	117	0	0	0	0	0	2	0.0
GE	43	117	118	119	0	0	0	0	0	2	0.0
GE	44	119	120	121	0	0	0	0	0	2	0.0
GE	45	121	122	123	0	0	0	0	0	2	0.0
GE	46	123	124	125	0	0	0	0	0	2	0.0
GE	47	125	126	127	0	0	0	0	0	2	0.0
GE	48	127	128	129	0	0	0	0	0	2	0.0
GE	49	129	130	131	0	0	0	0	0	2	0.0
GE	73	131	132	133	0	0	0	0	0	901	0.0
GE	50	132	134	135	0	0	0	0	0	2	0.0
GE	74	133	136	137	0	0	0	0	0	2	0.0
GE	75	137	138	139	0	0	0	0	0	3	0.0
GE	76	139	140	141	0	0	0	0	0	3	0.0
GE	51	135	142	143	0	0	0	0	0	2	0.0
GE	52	143	144	145	0	0	0	0	0	2	0.0
GE	53	145	146	147	0	0	0	0	0	3	0.0
GE	54	147	148	149	0	0	0	0	0	3	0.0
GE	55	149	150	151	0	0	0	0	0	3	0.0
GE	56	151	152	153	0	0	0	0	0	3	0.0
GNN	1			2101191.16				7340222.73			-15
GNN	2			2101336.81				7340379.97			-15
GNN	3			2101482.46				7340537.22			-15
GNN	4			2101628.11				7340694.46			-15
GNN	5			2101773.76				7340851.71			-15
GNN	6			2101919.40				7341008.96			-15
GNN	7			2102065.05				7341166.20			-15
GNN	8			2102210.70				7341323.45			-15
GNN	9			2102356.35				7341480.69			-15
GNN	10			2102502.00				7341637.94			-15
GNN	11			2102647.65				7341795.19			-15
GNN	12			2102793.29				7341952.43			-15
GNN	13			2102938.94				7342109.68			-15
GNN	14			2103084.59				7342266.93			-15
GNN	15			2103230.24				7342424.17			-15
GNN	16			2103230.24				7342424.17			-15
GNN	17			2103230.24				7342424.17			-5.5
GNN	18			2103375.89				7342581.42			-15
GNN	19			2103521.54				7342738.66			-15
GNN	20			2103667.18				7342895.91			-15
GNN	21			2103812.83				7343053.16			-15
GNN	22			2103958.48				7343210.40			-15
GNN	23			2104104.13				7343367.65			-15
GNN	24			2104249.78				7343524.89			-15
GNN	25			2104395.42				7343682.14			-15
GNN	26			2104541.07				7343839.39			-15
GNN	27			2104686.72				7343996.63			-15
GNN	28			2103108.87				7342573.92			-4.7
GNN	29			2102987.50				7342723.67			-4.7
GNN	30			2102866.13				7342873.42			-4.7
GNN	31			2102744.75				7343023.17			-4.7
GNN	32			2102623.38				7343172.92			-4.7
GNN	33			2102502.01				7343322.67			-4.7
GNN	34			2102380.64				7343472.42			-4.7
GNN	35			2102259.27				7343622.17			-4.7
GNN	36			2102033.74				7343728.18			-4.7
GNN	37			2101808.21				7343834.20			-4.7
GNN	38			2101582.67				7343940.22			-4.7

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

GNN	39	2101357.14	7344046.23	-4.6
GNN	40	2101357.14	7344046.23	-4.6
GNN	41	2101357.14	7344046.23	-2.4
GNN	42	2101244.00	7344159.00	-4.6
GNN	43	2101191.00	7344305.00	-4.6
GNN	44	2101196.17	7344102.69	-2.4
GNN	45	2101035.20	7344159.15	-2.3
GNN	46	2100874.23	7344215.61	-2.2
GNN	47	2100713.26	7344272.07	-2.1
GNN	48	2100552.29	7344328.53	-2
GNN	49	2100391.32	7344384.99	-1.9
GNN	50	2100230.35	7344441.45	-1.8
GNN	51	2100069.38	7344497.91	-1.7
GNN	52	2099908.41	7344554.37	-1.6
GNN	53	2099747.44	7344610.83	-1.5
GNN	54	2099586.47	7344667.29	-1.4
GNN	55	2099425.50	7344723.75	-1.3
GNN	56	2101207.00	7344462.00	-4.5
GNN	57	2101278.00	7344603.00	-4.5
GNN	58	2101374.00	7344723.00	-4.4
GNN	59	2101468.00	7344847.00	-4.4
GNN	60	2101565.00	7344970.00	-4.3
GNN	61	2101657.10	7345095.51	-4.3
GNN	62	2101657.10	7345095.51	-4.3
GNN	63	2101657.10	7345095.51	-1.7
GNN	64	2101752.60	7345215.02	-4.2
GNN	65	2101848.49	7345328.53	-4.2
GNN	66	2101542.12	7345175.62	-1.7
GNN	67	2101427.15	7345255.73	-1.7
GNN	68	2101312.17	7345335.84	-1.6
GNN	69	2101197.20	7345415.95	-1.5
GNN	70	2101082.22	7345496.06	-1.4
GNN	71	2100967.25	7345576.17	-1.3
GNN	72	2100852.27	7345656.28	-1.3
GNN	73	2100737.30	7345736.39	-1.3
GNN	74	2101929.77	7345467.23	-4.2
GNN	75	2102011.31	7345601.92	-4.2
GNN	76	2102004.00	7345751.19	-4.1
GNN	77	2101951.78	7345895.42	-4.1
GNN	78	2101855.33	7346020.88	-4.1
GNN	79	2101758.87	7346146.35	-4.1
GNN	80	2101662.42	7346271.81	-4.1
GNN	81	2101565.97	7346397.27	-4.1
GNN	82	2101469.51	7346522.74	-4.1
GNN	83	2101373.06	7346648.20	-4.1
GNN	84	2101276.61	7346773.67	-4
GNN	85	2101180.15	7346899.13	-3.5
GNN	86	2101131.16	7347037.51	-3.5
GNN	87	2101082.16	7347175.89	-3.5
GNN	88	2101033.16	7347314.27	-3.4
GNN	89	2100984.17	7347452.65	-3.4
GNN	90	2100935.17	7347591.03	-3.6
GNN	91	2100886.17	7347729.41	-3.6
GNN	92	2100837.17	7347867.78	-3.6
GNN	93	2100788.18	7348006.16	-3.6
GNN	94	2100602.52	7348060.22	-3.6
GNN	95	2100416.87	7348114.27	-3.6
GNN	96	2100231.22	7348168.33	-3.6
GNN	97	2100045.57	7348222.38	-3.6
GNN	98	2099859.92	7348276.44	-3.6
GNN	99	2099674.26	7348330.50	-3.6
GNN	100	2099674.26	7348330.50	-3.6
GNN	101	2099674.26	7348330.50	-1.7

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

GNN	102	2099667.63		7348435.25				-3.6
GNN	103	2099661.00		7348540.00				-3.7
GNN	104	2099463.21		7348314.16				-1.6
GNN	105	2099252.79		7348290.83				-1.5
GNN	106	2099163.68		7348114.48				-1.4
GNN	107	2099073.32		7347945.08				-1.3
GNN	108	2099530.41		7348572.60				-3.8
GNN	109	2099399.83		7348605.20				-3.9
GNN	110	2099348.85		7348747.19				-3.9
GNN	111	2099420.53		7348903.36				-4
GNN	112	2099450.93		7349082.83				-4
GNN	113	2099534.69		7349242.57				-4
GNN	114	2099479.57		7349384.24				-4
GNN	115	2099424.46		7349525.90				-4
GNN	116	2099369.35		7349667.57				-4
GNN	117	2099314.23		7349809.23				-4
GNN	118	2099259.12		7349950.90				-4
GNN	119	2099204.01		7350092.56				-4
GNN	120	2099148.90		7350234.23				-3.5
GNN	121	2099093.78		7350375.89				-3.5
GNN	122	2098907.19		7350482.89				-3.5
GNN	123	2098720.59		7350589.88				-3.4
GNN	124	2098533.99		7350696.88				-3.3
GNN	125	2098347.40		7350803.87				-3.2
GNN	126	2098160.80		7350910.87				-3.1
GNN	127	2097974.20		7351017.86				-3
GNN	128	2097787.60		7351124.86				-3
GNN	129	2097601.01		7351231.85				-3
GNN	130	2097414.41		7351338.85				-3
GNN	131	2097227.81		7351445.84				-2.7
GNN	132	2097227.81		7351445.84				-2.6
GNN	133	2097227.81		7351445.84				-1.8
GNN	134	2097032.08		7351489.17				-2.4
GNN	135	2096836.34		7351532.50				-2.2
GNN	136	2097098.58		7351639.00				-1.7
GNN	137	2096969.35		7351832.16				-1.6
GNN	138	2096840.12		7352025.32				-1.5
GNN	139	2096710.88		7352218.48				-1.4
GNN	140	2096581.65		7352411.64				-1.3
GNN	141	2096452.42		7352604.79				-1.3
GNN	142	2096640.61		7351575.82				-2.1
GNN	143	2096444.87		7351619.15				-2
GNN	144	2096221.10		7351772.25				-1.9
GNN	145	2095997.33		7351925.35				-1.8
GNN	146	2095773.56		7352078.45				-1.7
GNN	147	2095549.79		7352231.54				-1.6
GNN	148	2095326.02		7352384.64				-1.5
GNN	149	2095102.25		7352537.74				-1.4
GNN	150	2094878.48		7352690.84				-1.4
GNN	151	2094654.70		7352843.94				-1.35
GNN	152	2094430.93		7352997.04				-1.3
GNN	153	2094207.16		7353150.14				-1.3
GWN	1	43	5	5	0	0	0	0
GWN	2	43	5	5	0	0	0	0
GWN	3	43	5	5	0	0	0	0
GWN	4	43	5	5	0	0	0	0
GWN	5	43	5	5	0	0	0	0
GWN	6	43	5	5	0	0	0	0
GWN	7	43	5	5	0	0	0	0
GWN	8	43	5	5	0	0	0	0
GWN	9	43	5	5	0	0	0	0
GWN	10	43	5	5	0	0	0	0
GWN	11	43	5	5	0	0	0	0

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C*

GWN	12	43	5	5	0	0	0
GWN	13	43	5	5	0	0	0
GWN	14	43	5	5	0	0	0
GWN	15	43	5	5	0	0	0
GWN	16	43	5	5	0	0	0
GWN	17	43	5	5	0	0	0
GWN	18	43	5	5	0	0	0
GWN	19	43	5	5	0	0	0
GWN	20	43	5	5	0	0	0
GWN	21	43	5	5	0	0	0
GWN	22	43	5	5	0	0	0
GWN	23	43	5	5	0	0	0
GWN	24	43	5	5	0	0	0
GWN	25	43	5	5	0	0	0
GWN	26	43	5	5	0	0	0
GWN	27	43	5	5	0	0	0
GWN	28	43	5	5	0	0	0
GWN	29	43	5	5	0	0	0
GWN	30	43	5	5	200	-3	200
GWN	31	43	5	5	200	-2	200
GWN	32	43	5	5	200	-2	200
GWN	33	43	5	5	200	-2	200
GWN	34	35	5	5	100	-2	100
GWN	35	35	5	5	100	-2	100
GWN	36	35	5	5	100	-2	100
GWN	37	30	5	5	100	-2	100
GWN	38	30	5	5	200	-2	200
GWN	39	24	3.9	5.6	200	-2	200
GWN	40	24	3.9	5.6	100	-2	100
GWN	41	6.3	1	1	25	-2.4	25
GWN	42	18	3	3	100	-2	100
GWN	43	18	3	3	100	-2	100
GWN	44	6.3	1	1	25	-2.4	25
GWN	45	6.3	1	1	25	-2.3	25
GWN	46	6.3	1	1	10	-2	5
GWN	47	6.3	0.9	0.9	10	-2	5
GWN	48	6.3	0.8	0.8	0	0	0
GWN	49	6.3	0.7	0.7	0	0	0
GWN	50	6.3	0.6	0.6	0	0	0
GWN	51	6.3	0.5	0.5	0	0	0
GWN	52	6	0.5	0.5	25	-1	25
GWN	53	5.8	0.5	0.5	0	0	0
GWN	54	5.5	0.5	0.5	0	0	0
GWN	55	5	0.5	0.5	25	-1.3	10
GWN	56	18	3	3	50	-2	25
GWN	57	18	3	3	50	-2	25
GWN	58	18	3	3	50	-2	25
GWN	59	18	3	3	50	-2	25
GWN	60	18	3	3	50	-2	25
GWN	61	18	3	3	50	-2	25
GWN	62	18	3	3	50	-2	30
GWN	63	8	5.9	5.9	20	-2	10
GWN	64	12	2.5	2.5	50	-2	30
GWN	65	12	2.5	2.5	200	-2	100
GWN	66	8	5.9	5.9	20	-2	10
GWN	67	8	5.9	5.9	20	-2	10
GWN	68	6.6	0.9	0.9	20	-1.6	0.9
GWN	69	6.6	0.8	0.8	20	-1.5	0.8
GWN	70	6.6	0.7	0.7	20	-1.4	0.7
GWN	71	6.6	0.6	0.6	20	-1.3	0.6
GWN	72	6.6	0.5	0.5	20	-1.3	0.5
GWN	73	6.6	0.5	0.5	40	-1.3	30
GWN	74	10	2.8	2.8	200	-2	100

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C*

GWN	75	10	2.8	2.8	200	-2	100
GWN	76	10	2.8	2.8	100	-2	50
GWN	77	10	2.8	2.8	100	-2	50
GWN	78	10	2.8	2.8	100	-2	50
GWN	79	12	3	3	100	-2	50
GWN	80	15	7.7	6.3	100	-2	50
GWN	81	15	7.7	6.3	100	-2	50
GWN	82	15	7.7	6.3	100	-2	50
GWN	83	10	4	4	100	-2	50
GWN	84	10	4	4	100	-2	50
GWN	85	10	4	4	100	-2	50
GWN	86	10	5	5	50	-2	25
GWN	87	10	8	8	50	-2	25
GWN	88	5	19.7	5.9	0	0	0
GWN	89	5	19.7	5.9	0	0	0
GWN	90	5	5	5	50	-2	25
GWN	91	5	5	5	50	-2	25
GWN	92	5	5	5	50	-2	25
GWN	93	5	5	5	10	-2	5
GWN	94	5	5	5	10	-2	5
GWN	95	5	5	5	10	-2	5
GWN	96	5	5	5	10	-2	5
GWN	97	5	5	5	10	-2	5
GWN	98	5	5	5	10	-2	5
GWN	99	5	5	5	10	-2	5
GWN	100	5	5	5	100	-2	50
GWN	101	5	1	1	5	-1	5
GWN	102	5	4	4	100	-2	50
GWN	103	5	3.6	3.6	100	-2	50
GWN	104	5	0.7	0.7	5	-1	5
GWN	105	5	0.5	0.5	5	-1	5
GWN	106	5	0.5	0.5	10	-1	10
GWN	107	5	0.5	0.5	40	-1.3	30
GWN	108	5	3.6	3.6	100	-2	50
GWN	109	5	3.6	3.6	100	-2	50
GWN	110	5	3.6	3.6	200	-2	100
GWN	111	5	3.6	3.6	200	-2	100
GWN	112	4	5.7	8.5	200	-2	100
GWN	113	4	5.7	8.5	100	-2	50
GWN	114	5	5	5	100	-2	50
GWN	115	5	5	5	100	-2	50
GWN	116	5	2.6	2.6	20	-2	10
GWN	117	5	2.6	2.6	10	-1	10
GWN	118	5	2.6	2.6	10	-1	10
GWN	119	5	2.6	3	10	-1	10
GWN	120	9.8	2.2	3.4	10	-1	10
GWN	121	9.8	2.2	3.4	50	-1	50
GWN	122	5	2.6	2.6	50	-1	50
GWN	123	5	2.6	2.6	10	-1	10
GWN	124	8	2.6	2.6	0	0	0
GWN	125	9.1	2.2	2.2	0	0	0
GWN	126	9.1	2.2	2.2	0	0	0
GWN	127	9.1	2.2	2.2	0	0	0
GWN	128	8.5	2	2	0	0	0
GWN	129	8.5	2	2	0	0	0
GWN	130	8.5	2	2	0	0	0
GWN	131	11.3	2.4	1.1	0	0	0
GWN	132	11.3	2.4	1.1	0	0	0
GWN	133	2	1.4	1.4	10	-1	10
GWN	134	8.5	2	2	10	-1	10
GWN	135	8.5	2	2	10	-1	10
GWN	136	2	1.4	1.4	5	-1	5
GWN	137	2	1.4	1.4	5	-1	5

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C*

GWN	138	2	1.1	1.1	0	0	0
GWN	139	2	0.9	0.9	5	-0.5	5
GWN	140	2	0.7	0.7	0	0	0
GWN	141	2	0.5	0.5	10	-1	10
GWN	142	8.5	2	2	10	-1	10
GWN	143	8.5	2	2	45	-1.5	30
GWN	144	8	2	2	5	-1	5
GWN	145	8	2	2	5	-1	5
GWN	146	8	2	2	5	-1	5
GWN	147	8	2	2	5	-1	5
GWN	148	8	2	2	5	-1	5
GWN	149	8	2	2	5	-1	5
GWN	150	8	2	2	5	-1	5
GWN	151	8	2	2	5	-1	5
GWN	152	6	2	2	5	-1	5
GWN	153	4	2	2	52	-1.3	40

Below is the first day of the Adams Bayou RMA2 boundary condition file.

```

T1 Adams Bayou Long Term Run "B"
T2 Jan 1, 2002 - Jan 1, 2013 at 30 minute (0.5 hour) time step
T3 Fully Permitted PS Flows
$M 1
$L 0 0 1 1 0 1 0 0 0 0
SI 1
DE 0.084 0.183 5
EX 1 5000.00 5000.00
EY 1 5000.00 5000.00
EX 2 5000.00 5000.00
EY 2 5000.00 5000.00
EX 3 5000.00 5000.00
EY 3 5000.00 5000.00
EX 4 5000.00 5000.00
EY 4 5000.00 5000.00
FT 20
IC 0.105 0.3 0.08
RDT 1 1 0.060 2 0.060 1E-14 0 0
RDT 2 1 0.090 2 0.110 1E-14 0 0
RDT 3 1 0.090 2 0.110 1E-14 0 0
CO RSC 10000 0 0
TI 15 15 0.01 0.01
TR 0 0 0 0
TS -1 0 0
TZ 0.5 96431 192863 0 0
CO BAN cards are boundary flow azimuths in radians from x-axis
BAN 1 4.0
BAN 27 4.0
BAN 55 5.9
BAN 73 5.7
BAN 107 1.1
BAN 141 5.3
BAN 153 5.7
CO initial boundary flows in cms
CO BQE 28 is Orange County WCID #2 self-reported flows
CO BQE 36 is City of Pinehurst self-reported flows
CO City of Orange wet weather outfall would be added at element 28 boundary
CO BCN cards are water elevations at downstream boundary in meters amsl
BQE 36 0.00004483
BQE 28 0.00008984
BQN 141 0.02572400
BQE 15 0.00004752
BQN 153 0.16487000

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

BQE 31 0.00007528
BQE 41 0.00003794
BQE 47 0.00005878
BQE 50 0.00004001
BQE 51 0.00004236
BQN 55 0.01708300
BQE 72 0.00003016
BQN 73 0.00910950
BQE 74 0.00003331
BQN 27 464.000000
BCN 1 00200 0 0 0.105
END Simulation at time = 0.0
BCN 1 00200 0 0 0.105
END Simulation at time = 0.5
BQN 141 0.02567800
BQE 15 0.00004687
BQN 153 0.16765000
BQE 31 0.00007421
BQE 41 0.00003740
BQE 47 0.00005796
BQE 50 0.00003945
BQE 51 0.00004248
BQN 55 0.01711200
BQE 72 0.00003052
BQN 73 0.00925050
BQE 74 0.00003286
BCN 1 00200 0 0 0.102
END Simulation at time = 1.0
BCN 1 00200 0 0 0.101
END Simulation at time = 1.5
BQN 141 0.02561800
BQE 15 0.00004623
BQN 153 0.16965000
BQE 31 0.00007316
BQE 41 0.00003687
BQE 47 0.00005714
BQE 50 0.00003891
BQE 51 0.00004256
BQN 55 0.01712700
BQE 72 0.00003073
BQN 73 0.00936530
BQE 74 0.00003241
BCN 1 00200 0 0 0.091
END Simulation at time = 2.0
BCN 1 00200 0 0 0.085
END Simulation at time = 2.5
BQN 141 0.02554700
BQE 15 0.00004560
BQN 153 0.17101000
BQE 31 0.00007213
BQE 41 0.00003635
BQE 47 0.00005634
BQE 50 0.00003837
BQE 51 0.00004260
BQN 55 0.01712700
BQE 72 0.00003083
BQN 73 0.00945660
BQE 74 0.00003196
BCN 1 00200 0 0 0.081
END Simulation at time = 3.0
BCN 1 00200 0 0 0.086
END Simulation at time = 3.5
BQN 141 0.02546300

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

BQE 15 0.00004498
BQN 153 0.17181000
BQE 31 0.00007110
BQE 41 0.00003583
BQE 47 0.00005555
BQE 50 0.00003784
BQE 51 0.00004261
BQN 55 0.01711400
BQE 72 0.00003084
BQN 73 0.00952660
BQE 74 0.00003153
BCN 1 00200 0 0 0.075
END Simulation at time = 4.0
BCN 1 00200 0 0 0.08
END Simulation at time = 4.5
BQN 141 0.02536900
BQE 15 0.00004437
BQN 153 0.17215000
BQE 31 0.00007010
BQE 41 0.00003533
BQE 47 0.00005477
BQE 50 0.00003731
BQE 51 0.00004258
BQN 55 0.01709000
BQE 72 0.00003076
BQN 73 0.00957740
BQE 74 0.00003110
BCN 1 00200 0 0 0.066
END Simulation at time = 5.0
BCN 1 00200 0 0 0.056
END Simulation at time = 5.5
BQN 141 0.02521300
BQE 15 0.00004159
BQN 153 0.17088000
BQE 31 0.00006585
BQE 41 0.00003313
BQE 47 0.00005139
BQE 50 0.00003504
BQE 51 0.00004243
BQN 55 0.01700600
BQE 72 0.00003036
BQN 73 0.00956620
BQE 74 0.00002918
BCN 1 00200 0 0 0.044
END Simulation at time = 6.0
BCN 1 00200 0 0 0.032
END Simulation at time = 6.5
BQN 141 0.02419300
BQE 15 0.00000638
BQN 153 0.14894000
BQE 31 0.00000933
BQE 41 0.00000379
BQE 47 0.00000607
BQE 50 0.00000471
BQE 51 0.00004054
BQN 55 0.01612200
BQE 72 0.00002542
BQN 73 0.00876330
BQE 74 0.00000385
BCN 1 00200 0 0 0.014
END Simulation at time = 7.0
BCN 1 00200 0 0 0.004
END Simulation at time = 7.5

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

```
BQN 141 0.02318500
BQE 15 0.00000265
BQN 153 0.12861000
BQE 31 0.00000627
BQE 41 0.00000325
BQE 47 0.00000527
BQE 50 0.00000402
BQE 51 0.00003850
BQN 55 0.01522500
BQE 72 0.00002120
BQN 73 0.00794300
BQE 74 0.00000359
BCN 1 00200 0 0 -0.024
END Simulation at time = 8.0
BCN 1 00200 0 0 -0.061
END Simulation at time = 8.5
BQN 141 0.02221200
BQE 15 0.00000262
BQN 153 0.11081000
BQE 31 0.00000618
BQE 41 0.00000321
BQE 47 0.00000517
BQE 50 0.00000388
BQE 51 0.00003655
BQN 55 0.01435000
BQE 72 0.00001766
BQN 73 0.00716700
BQE 74 0.00000345
BCN 1 00200 0 0 -0.082
END Simulation at time = 9.0
BCN 1 00200 0 0 -0.118
END Simulation at time = 9.5
BQN 141 0.02128100
BQE 15 0.00000259
BQN 153 0.09554500
BQE 31 0.00000611
BQE 41 0.00000318
BQE 47 0.00000511
BQE 50 0.00000384
BQE 51 0.00003470
BQN 55 0.01352200
BQE 72 0.00001473
BQN 73 0.00645910
BQE 74 0.00000341
BCN 1 00200 0 0 -0.145
END Simulation at time = 10.0
BCN 1 00200 0 0 -0.162
END Simulation at time = 10.5
BQN 141 0.02039200
BQE 15 0.00000256
BQN 153 0.08488900
BQE 31 0.00000603
BQE 41 0.00000314
BQE 47 0.00000505
BQE 50 0.00000379
BQE 51 0.00003294
BQN 55 0.01273700
BQE 72 0.00001232
BQN 73 0.00581340
BQE 74 0.00000336
BCN 1 00200 0 0 -0.191
END Simulation at time = 11.0
BCN 1 00200 0 0 -0.222
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

```
END Simulation at time = 11.5
BQN 141 0.01954200
BQE 15 0.00000253
BQN 153 0.08455600
BQE 31 0.00000596
BQE 41 0.00000310
BQE 47 0.00000499
BQE 50 0.00000374
BQE 51 0.00003128
BQN 55 0.01199500
BQE 72 0.00001033
BQN 73 0.00522420
BQE 74 0.00000332
BCN 1 00200 0 0 -0.256
END Simulation at time = 12.0
BCN 1 00200 0 0 -0.284
END Simulation at time = 12.5
BQN 141 0.01872900
BQE 15 0.00000250
BQN 153 0.08422300
BQE 31 0.00000589
BQE 41 0.00000306
BQE 47 0.00000492
BQE 50 0.00000369
BQE 51 0.00002972
BQN 55 0.01129200
BQE 72 0.00000869
BQN 73 0.00468660
BQE 74 0.00000328
BCN 1 00200 0 0 -0.295
END Simulation at time = 13.0
BCN 1 00200 0 0 -0.297
END Simulation at time = 13.5
BQN 141 0.01796100
BQE 15 0.00000247
BQN 153 0.08390100
BQE 31 0.00000584
BQE 41 0.00000303
BQE 47 0.00000491
BQE 50 0.00000373
BQE 51 0.00002825
BQN 55 0.01065100
BQE 72 0.00000740
BQN 73 0.00422380
BQE 74 0.00000334
BCN 1 00200 0 0 -0.317
END Simulation at time = 14.0
BCN 1 00200 0 0 -0.316
END Simulation at time = 14.5
BQN 141 0.01724800
BQE 15 0.00000310
BQN 153 0.08360500
BQE 31 0.00000631
BQE 41 0.00000308
BQE 47 0.00000504
BQE 50 0.00000396
BQE 51 0.00002694
BQN 55 0.01009900
BQE 72 0.00000648
BQN 73 0.00386090
BQE 74 0.00000351
BCN 1 00200 0 0 -0.353
END Simulation at time = 15.0
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

```
BCN 1 00200 0 0 -0.31
END Simulation at time = 15.5
BQN 141 0.01711900
BQE 15 0.00002510
BQN 153 0.08370100
BQE 31 0.00004299
BQE 41 0.00002151
BQE 47 0.00003341
BQE 50 0.00002304
BQE 51 0.00002693
BQN 55 0.01009400
BQE 72 0.00000861
BQN 73 0.00406750
BQE 74 0.00001914
BCN 1 00200 0 0 -0.305
END Simulation at time = 16.0
BCN 1 00200 0 0 -0.276
END Simulation at time = 16.5
BQN 141 0.01703600
BQE 15 0.00002687
BQN 153 0.08382400
BQE 31 0.00004556
BQE 41 0.00002285
BQE 47 0.00003549
BQE 50 0.00002444
BQE 51 0.00002700
BQN 55 0.01012900
BQE 72 0.00001058
BQN 73 0.00429150
BQE 74 0.00002034
BCN 1 00200 0 0 -0.258
END Simulation at time = 17.0
BCN 1 00200 0 0 -0.241
END Simulation at time = 17.5
BQN 141 0.01694700
BQE 15 0.00002651
BQN 153 0.08394100
BQE 31 0.00004492
BQE 41 0.00002253
BQE 47 0.00003500
BQE 50 0.00002411
BQE 51 0.00002704
BQN 55 0.01015300
BQE 72 0.00001216
BQN 73 0.00448720
BQE 74 0.00002007
BCN 1 00200 0 0 -0.221
END Simulation at time = 18.0
BCN 1 00200 0 0 -0.171
END Simulation at time = 18.5
BQN 141 0.01685400
BQE 15 0.00002615
BQN 153 0.08405000
BQE 31 0.00004429
BQE 41 0.00002221
BQE 47 0.00003452
BQE 50 0.00002378
BQE 51 0.00002705
BQN 55 0.01016800
BQE 72 0.00001341
BQN 73 0.00465740
BQE 74 0.00001981
BCN 1 00200 0 0 -0.133
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

```
END Simulation at time = 19.0
BCN 1 00200 0 0 -0.098
END Simulation at time = 19.5
BQN 141 0.01675600
BQE 15 0.00002580
BQN 153 0.08415300
BQE 31 0.00004367
BQE 41 0.00002190
BQE 47 0.00003404
BQE 50 0.00002346
BQE 51 0.00002705
BQN 55 0.01017400
BQE 72 0.00001439
BQN 73 0.00480430
BQE 74 0.00001955
BCN 1 00200 0 0 -0.061
END Simulation at time = 20.0
BCN 1 00200 0 0 -0.032
END Simulation at time = 20.5
BQN 141 0.01665300
BQE 15 0.00002544
BQN 153 0.08425000
BQE 31 0.00004306
BQE 41 0.00002159
BQE 47 0.00003357
BQE 50 0.00002314
BQE 51 0.00002703
BQN 55 0.01017300
BQE 72 0.00001515
BQN 73 0.00493030
BQE 74 0.00001929
BCN 1 00200 0 0 -0.001
END Simulation at time = 21.0
BCN 1 00200 0 0 0.027
END Simulation at time = 21.5
BQN 141 0.01654600
BQE 15 0.00002509
BQN 153 0.08434000
BQE 31 0.00004245
BQE 41 0.00002129
BQE 47 0.00003310
BQE 50 0.00002283
BQE 51 0.00002699
BQN 55 0.01016400
BQE 72 0.00001573
BQN 73 0.00503730
BQE 74 0.00001903
BCN 1 00200 0 0 0.027
END Simulation at time = 22.0
BCN 1 00200 0 0 0.001
END Simulation at time = 22.5
BQN 141 0.01643500
BQE 15 0.00002475
BQN 153 0.08442300
BQE 31 0.00004186
BQE 41 0.00002099
BQE 47 0.00003264
BQE 50 0.00002252
BQE 51 0.00002693
BQN 55 0.01014700
BQE 72 0.00001616
BQN 73 0.00512700
BQE 74 0.00001878
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix C

```
BCN 1 00200 0 0 -0.01
END Simulation at time = 23.0
BCN 1 00200 0 0 -0.008
END Simulation at time = 23.5
BQN 141 0.01630600
BQE 15 0.00002382
BQN 153 0.08449100
BQE 31 0.00004031
BQE 41 0.00002022
BQE 47 0.00003145
BQE 50 0.00002171
BQE 51 0.00002682
BQN 55 0.01011300
BQE 72 0.00001640
BQN 73 0.00518880
BQE 74 0.00001810
BQN 27 456.000000
BCN 1 00200 0 0 0.031
END Simulation at time = 24.0
STOP
```

Note: The model printout was stopped here, after one day, due to space considerations.

Appendix D Cow Bayou RMA2 Geometry and Boundary Condition Files

T1 Cow Bayou Model B Long Term Run GFGEN input file
 T2 geometry input file

T3

SI 1

\$L 3

GE	1	1	2	3	0	0	0	0	0	1	0.0
GE	2	3	4	5	0	0	0	0	0	1	0.0
GE	3	5	6	7	0	0	0	0	0	901	0.0
GE	4	6	8	9	0	0	0	0	0	1	0.0
GE	5	9	10	11	0	0	0	0	0	1	0.0
GE	6	11	12	13	0	0	0	0	0	901	0.0
GE	7	12	14	15	0	0	0	0	0	1	0.0
GE	8	7	16	17	0	0	0	0	0	1	0.0
GE	9	13	18	19	0	0	0	0	0	2	0.0
GE	10	19	20	21	0	0	0	0	0	2	0.0
GE	11	21	22	23	0	0	0	0	0	2	0.0
GE	12	23	24	25	0	0	0	0	0	2	0.0
GE	13	25	26	27	0	0	0	0	0	2	0.0
GE	14	27	28	29	0	0	0	0	0	2	0.0
GE	15	29	30	31	0	0	0	0	0	2	0.0
GE	16	31	32	33	0	0	0	0	0	2	0.0
GE	17	17	33	34	0	0	0	0	0	901	0.0
GE	18	34	35	36	0	0	0	0	0	1	0.0
GE	19	36	37	38	0	0	0	0	0	1	0.0
GE	20	38	39	40	0	0	0	0	0	1	0.0
GE	21	160	41	42	0	0	0	0	0	1	0.0
GE	22	42	43	44	0	0	0	0	0	1	0.0
GE	23	44	45	46	0	0	0	0	0	901	0.0
GE	24	45	47	48	0	0	0	0	0	1	0.0
GE	25	48	49	50	0	0	0	0	0	901	0.0
GE	26	46	51	52	0	0	0	0	0	2	0.0
GE	27	52	53	54	0	0	0	0	0	2	0.0
GE	28	54	55	56	0	0	0	0	0	901	0.0
GE	29	55	57	58	0	0	0	0	0	2	0.0
GE	30	58	59	50	0	0	0	0	0	2	0.0
GE	31	56	60	61	0	0	0	0	0	2	0.0
GE	32	61	62	63	0	0	0	0	0	3	0.0
GE	33	63	64	65	0	0	0	0	0	3	0.0
GE	34	65	66	67	0	0	0	0	0	4	0.0
GE	35	67	68	69	0	0	0	0	0	4	0.0
GE	36	69	70	71	0	0	0	0	0	4	0.0
GE	37	49	72	73	0	0	0	0	0	1	0.0
GE	38	73	74	75	0	0	0	0	0	1	0.0
GE	39	75	76	77	0	0	0	0	0	1	0.0
GE	40	77	78	79	0	0	0	0	0	1	0.0
GE	41	79	80	81	0	0	0	0	0	1	0.0
GE	42	81	82	83	0	0	0	0	0	1	0.0
GE	43	83	84	85	0	0	0	0	0	1	0.0
GE	44	85	86	87	0	0	0	0	0	2	0.0
GE	45	87	88	89	0	0	0	0	0	2	0.0
GE	46	89	90	91	0	0	0	0	0	901	0.0
GE	47	90	92	93	0	0	0	0	0	3	0.0
GE	48	91	94	95	0	0	0	0	0	4	0.0
GE	49	95	96	97	0	0	0	0	0	4	0.0
GE	50	97	98	99	0	0	0	0	0	4	0.0
GE	51	93	100	101	0	0	0	0	0	3	0.0

*Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D*

GE	52	101	102	103	0	0	0	0	0	3	0.0
GE	53	103	104	105	0	0	0	0	0	901	0.0
GE	54	104	106	107	0	0	0	0	0	3	0.0
GE	55	105	108	109	0	0	0	0	0	4	0.0
GE	56	109	110	111	0	0	0	0	0	4	0.0
GE	57	111	112	113	0	0	0	0	0	4	0.0
GE	58	113	114	115	0	0	0	0	0	4	0.0
GE	59	115	116	117	0	0	0	0	0	4	0.0
GE	60	107	118	119	0	0	0	0	0	2	0.0
GE	61	119	120	121	0	0	0	0	0	2	0.0
GE	62	121	122	123	0	0	0	0	0	2	0.0
GE	63	123	124	125	0	0	0	0	0	2	0.0
GE	64	125	126	127	0	0	0	0	0	2	0.0
GE	65	127	128	129	0	0	0	0	0	2	0.0
GE	66	129	130	131	0	0	0	0	0	901	0.0
GE	67	130	132	133	0	0	0	0	0	2	0.0
GE	68	131	134	135	0	0	0	0	0	4	0.0
GE	69	135	136	137	0	0	0	0	0	4	0.0
GE	70	137	138	139	0	0	0	0	0	4	0.0
GE	71	139	140	141	0	0	0	0	0	4	0.0
GE	72	141	142	143	0	0	0	0	0	4	0.0
GE	73	143	144	145	0	0	0	0	0	4	0.0
GE	74	133	146	147	0	0	0	0	0	2	0.0
GE	75	147	148	149	0	0	0	0	0	2	0.0
GE	76	149	150	151	0	0	0	0	0	2	0.0
GE	77	151	152	153	0	0	0	0	0	2	0.0
GE	78	153	154	155	0	0	0	0	0	2	0.0
GE	79	155	156	157	0	0	0	0	0	2	0.0
GE	80	157	158	159	0	0	0	0	0	2	0.0
GE	81	40	160	161	0	0	0	0	0	901	0.0
GE	82	161	162	163	0	0	0	0	0	4	0.0
GE	83	163	164	165	0	0	0	0	0	4	0.0
GNN	1			2100046.90			7338324.40				-15.00
GNN	2			2100299.70			7338436.60				-15.00
GNN	3			2100552.40			7338548.90				-15.00
GNN	4			2100805.20			7338661.10				-15.00
GNN	5			2101057.90			7338773.40				-15.00
GNN	6			2101057.90			7338773.40				-15.00
GNN	7			2101057.90			7338773.40				-5.00
GNN	8			2101277.30			7338921.60				-15.00
GNN	9			2101496.60			7339069.90				-15.00
GNN	10			2101716.00			7339218.20				-15.00
GNN	11			2101935.30			7339366.50				-15.00
GNN	12			2101935.30			7339366.50				-15.00
GNN	13			2101935.30			7339366.50				-3.60
GNN	14			2102188.10			7339478.50				-15.00
GNN	15			2102440.80			7339591.00				-15.00
GNN	16			2100735.50			7339139.60				-4.85
GNN	17			2100413.00			7339505.80				-4.70
GNN	18			2101827.20			7339601.00				-3.60
GNN	19			2101719.00			7339836.00				-3.60
GNN	20			2101448.00			7339846.00				-3.60
GNN	21			2101225.00			7339697.00				-3.60
GNN	22			2100980.00			7339590.00				-3.60
GNN	23			2100731.00			7339491.00				-3.60
GNN	24			2100788.00			7339753.00				-3.60
GNN	25			2100755.00			7340018.00				-3.60
GNN	26			2100788.00			7340283.00				-3.60
GNN	27			2100652.00			7340512.00				-3.60
GNN	28			2100390.00			7340452.00				-3.60
GNN	29			2100171.00			7340297.00				-3.60
GNN	30			2100290.00			7340058.00				-3.60
GNN	31			2100513.00			7339909.00				-3.60

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

GNN	32	2100625.00	7339667.00	-3.60
GNN	33	2100413.00	7339505.80	-3.60
GNN	34	2100413.00	7339505.80	-4.70
GNN	35	2100167.00	7339821.00	-4.70
GNN	36	2099921.00	7340136.00	-4.70
GNN	37	2099575.00	7340336.00	-4.75
GNN	38	2099189.00	7340440.00	-4.80
GNN	39	2098949.50	7340491.40	-4.90
GNN	40	2098710.00	7340542.90	-5.00
GNN	41	2098165.50	7340646.90	-5.10
GNN	42	2097621.00	7340751.00	-5.20
GNN	43	2097227.00	7340820.00	-5.25
GNN	44	2096833.00	7340889.00	-5.30
GNN	45	2096833.00	7340889.00	-5.00
GNN	46	2096833.00	7340889.00	-2.20
GNN	47	2096439.00	7340958.00	-4.90
GNN	48	2096045.00	7341027.00	-4.80
GNN	49	2096045.00	7341027.00	-4.80
GNN	50	2096045.00	7341027.00	-2.20
GNN	51	2096930.00	7341097.50	-2.20
GNN	52	2097027.00	7341306.00	-2.20
GNN	53	2096838.50	7341438.00	-2.20
GNN	54	2096680.00	7341571.80	-2.20
GNN	55	2096680.00	7341571.80	-2.20
GNN	56	2096680.00	7341571.80	-2.20
GNN	57	2096426.00	7341517.00	-2.20
GNN	58	2096202.00	7341464.00	-2.20
GNN	59	2096123.50	7341245.50	-2.20
GNN	60	2096475.00	7341720.00	-2.15
GNN	61	2096300.00	7341870.00	-2.10
GNN	62	2096300.00	7342100.00	-2.05
GNN	63	2096152.00	7342276.00	-2.00
GNN	64	2096092.00	7342498.00	-1.90
GNN	65	2096052.00	7342725.00	-1.80
GNN	66	2095955.00	7342933.00	-1.70
GNN	67	2095858.00	7343141.00	-1.60
GNN	68	2095695.00	7343304.00	-1.50
GNN	69	2095487.00	7343207.00	-1.40
GNN	70	2095257.00	7343207.00	-1.30
GNN	71	2095049.00	7343110.00	-1.20
GNN	72	2095662.00	7341144.00	-4.70
GNN	73	2095279.00	7341261.00	-4.60
GNN	74	2094896.00	7341378.00	-4.60
GNN	75	2094513.00	7341495.00	-4.60
GNN	76	2094083.60	7341645.10	-4.50
GNN	77	2093774.00	7341801.00	-4.40
GNN	78	2093491.00	7342084.00	-4.35
GNN	79	2093262.00	7342412.00	-4.30
GNN	80	2093033.00	7342740.00	-4.25
GNN	81	2092804.00	7343068.00	-4.20
GNN	82	2092579.00	7343399.00	-4.20
GNN	83	2092354.00	7343730.00	-4.20
GNN	84	2092129.00	7344061.00	-4.20
GNN	85	2091929.00	7344407.00	-4.20
GNN	86	2091894.00	7344805.00	-4.70
GNN	87	2091859.00	7345203.00	-5.20
GNN	88	2091928.00	7345597.00	-4.70
GNN	89	2092128.00	7345943.00	-4.20
GNN	90	2092128.00	7345943.00	-4.00
GNN	91	2092128.00	7345943.00	-1.80
GNN	92	2091845.00	7346226.00	-3.90
GNN	93	2091645.00	7345880.00	-3.80
GNN	94	2092253.00	7346160.00	-1.70

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

GNN	95	2092480.00	7346266.00	-1.60
GNN	96	2092657.00	7346443.00	-1.50
GNN	97	2092782.00	7346660.00	-1.40
GNN	98	2092907.00	7346877.00	-1.30
GNN	99	2092907.00	7347127.00	-1.20
GNN	100	2091476.00	7346243.00	-3.70
GNN	101	2091307.00	7345880.00	-3.60
GNN	102	2090944.00	7346049.00	-3.55
GNN	103	2090647.70	7346224.50	-3.50
GNN	104	2090647.70	7346224.50	-3.50
GNN	105	2090647.70	7346224.50	-2.00
GNN	106	2090216.00	7346277.80	-3.40
GNN	107	2089830.00	7346174.00	-3.30
GNN	108	2090685.00	7346672.00	-1.90
GNN	109	2090685.00	7347072.00	-1.80
GNN	110	2090581.00	7347458.00	-1.70
GNN	111	2090412.00	7347821.00	-1.60
GNN	112	2090026.00	7347925.00	-1.55
GNN	113	2089743.00	7348208.00	-1.50
GNN	114	2090000.00	7348514.00	-1.45
GNN	115	2090169.00	7348877.00	-1.40
GNN	116	2090273.00	7349263.00	-1.35
GNN	117	2090104.00	7349626.00	-1.30
GNN	118	2089639.10	7345951.70	-3.20
GNN	119	2089147.00	7345891.00	-3.10
GNN	120	2089078.00	7346285.00	-3.00
GNN	121	2088678.00	7346285.00	-2.90
GNN	122	2088395.00	7346568.00	-2.80
GNN	123	2088195.00	7346914.00	-2.70
GNN	124	2087832.00	7347083.00	-2.60
GNN	125	2088032.00	7347429.00	-2.50
GNN	126	2088032.00	7347779.00	-2.40
GNN	127	2087831.00	7348066.00	-2.30
GNN	128	2087496.00	7347964.00	-2.25
GNN	129	2087147.00	7347994.80	-2.20
GNN	130	2087147.00	7347994.80	-2.20
GNN	131	2087147.00	7347994.80	-1.80
GNN	132	2086830.00	7348143.00	-2.15
GNN	133	2086583.00	7348390.00	-2.10
GNN	134	2086879.00	7347770.00	-1.70
GNN	135	2086576.00	7347595.00	-1.60
GNN	136	2086241.00	7347493.00	-1.55
GNN	137	2085896.00	7347432.00	-1.50
GNN	138	2085567.00	7347312.00	-1.45
GNN	139	2085250.00	7347164.00	-1.40
GNN	140	2084963.00	7346962.00	-1.35
GNN	141	2084618.00	7346901.00	-1.30
GNN	142	2084283.00	7346799.00	-1.30
GNN	143	2083948.00	7346697.00	-1.30
GNN	144	2083603.00	7346636.00	-1.30
GNN	145	2083286.00	7346784.00	-1.30
GNN	146	2086685.00	7348725.00	-2.00
GNN	147	2086624.00	7349070.00	-1.90
GNN	148	2086608.30	7349424.70	-1.85
GNN	149	2086592.60	7349779.60	-1.80
GNN	150	2086281.30	7349734.20	-1.75
GNN	151	2085970.00	7349689.00	-1.70
GNN	152	2085625.00	7349750.00	-1.60
GNN	153	2085357.00	7349975.00	-1.50
GNN	154	2085089.00	7350200.00	-1.40
GNN	155	2084888.00	7350487.00	-1.30
GNN	156	2084641.00	7350734.00	-1.30
GNN	157	2084440.00	7351021.00	-1.30

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

GNN	158		2084239.00		7351308.00		-1.30	
GNN	159		2084038.00		7351595.00		-1.30	
GNN	160		2098710.00		7340542.90		-5.00	
GNN	161		2098710.00		7340542.90		-1.30	
GNN	162		2098710.00		7340942.90		-1.25	
GNN	163		2098710.00		7341342.90		-1.20	
GNN	164		2098710.00		7341742.90		-1.15	
GNN	165		2098710.00		7342142.90		-1.10	
GWN	1	100	7.5	7.5	120	-10		12
GWN	2	100	7.5	7.5	120	-10		12
GWN	3	100	7.5	7.5	120	-10		12
GWN	4	100	7.5	7.5	120	-10		12
GWN	5	100	7.5	7.5	120	-10		12
GWN	6	100	7.5	7.5	120	-10		12
GWN	7	25	5.5	10	50	-2		50
GWN	8	100	7.5	7.5	120	-10		12
GWN	9	100	7.5	7.5	120	-10		12
GWN	10	100	7.5	7.5	120	-10		12
GWN	11	100	7.5	7.5	120	-10		12
GWN	12	100	7.5	7.5	120	-10		12
GWN	13	25	1.2	5.1	100	-3.6		50
GWN	14	100	7.5	7.5	120	-10		12
GWN	15	100	7.5	7.5	120	-10		12
GWN	16	25	5.5	10	50	-2		50
GWN	17	25	5.5	10	50	-2		50
GWN	18	25	1.2	5.1	100	-2		50
GWN	19	25	1.2	5.1	100	-2		50
GWN	20	25	1.2	5.1	100	-2		50
GWN	21	25	1.2	5.1	50	-2		50
GWN	22	25	1.2	5.1	50	-2		50
GWN	23	25	1.2	5.1	50	-2		50
GWN	24	25	1.2	5.1	50	-2		50
GWN	25	25	1.2	5.1	50	-2		50
GWN	26	25	1.2	5.1	50	-2		50
GWN	27	25	1.2	5.1	200	-2		50
GWN	28	25	1.2	5.1	50	-2		50
GWN	29	25	1.2	5.1	50	-2		50
GWN	30	25	1.2	5.1	100	-2		50
GWN	31	25	1.2	5.1	50	-2		50
GWN	32	25	1.2	5.1	50	-2		50
GWN	33	25	1.2	5.1	50	-2		50
GWN	34	25	5.5	10	50	-2		50
GWN	35	25	5.5	10	50	-2		50
GWN	36	25	5.5	10	200	-3.6		60
GWN	37	25	5.5	10	200	-3.6		60
GWN	38	25	5.5	10	200	-3.6		60
GWN	39	25	5.5	10	200	-3.6		60
GWN	40	25	5.5	10	200	-3.6		60
GWN	41	26	5.25	9.35	200	-3.6		60
GWN	42	27	5	8.7	200	-3.6		60
GWN	43	27	5	8.7	200	-3.6		60
GWN	44	27	5	8.7	200	-3.6		60
GWN	45	27	5	8.7	200	-3.6		200
GWN	46	11	9.1	7.3	20	-2		10
GWN	47	31	5.25	6.85	200	-3.6		200
GWN	48	35	5.5	5	200	-3.6		200
GWN	49	35	4	5	200	-3.6		200
GWN	50	11	9.1	7.3	20	-2		10
GWN	51	11	9.1	7.3	30	-2		15
GWN	52	11	9.1	7.3	30	-2		15
GWN	53	11	9.1	7.3	10	-1		10
GWN	54	11	9.1	7.3	60	-2		30
GWN	55	11	9.1	7.3	60	-2		30

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

GWN	56	10	1.5	1.5	50	-2	25
GWN	57	11	9.1	7.3	60	-2	30
GWN	58	11	9.1	7.3	30	-2	30
GWN	59	11	9.1	7.3	10	-1	10
GWN	60	10	1.5	1.5	50	-2	100
GWN	61	10	1.5	1.5	50	-2	100
GWN	62	10	1.5	1.5	20	-1.5	30
GWN	63	10	1.5	1.5	20	-1.5	30
GWN	64	10	1.5	1.5	20	-1.5	30
GWN	65	10	1.5	1.5	20	-1.5	30
GWN	66	8	1.5	1.5	30	-1.5	45
GWN	67	6	1.5	1.5	30	-1.5	45
GWN	68	5.5	1.5	1.5	30	-1.5	45
GWN	69	5	1.5	1.5	30	-1.5	45
GWN	70	5	1.25	1.25	30	-1.4	45
GWN	71	5	1	1	130	-1.3	100
GWN	72	35	3	5	200	-3	200
GWN	73	35	2	5	200	-3	200
GWN	74	35	1.55	4.3	200	-3	200
GWN	75	35	1	4	200	-3	200
GWN	76	35	2	4	200	-3	200
GWN	77	35	3	4	200	-3	200
GWN	78	35	5	5	200	-3	200
GWN	79	35	7	6	200	-3	200
GWN	80	35	9	7	200	-3	200
GWN	81	35	11	8	200	-3	200
GWN	82	35	11	8	200	-3	200
GWN	83	35	11	8	200	-3	200
GWN	84	33	7	6	200	-3	200
GWN	85	31	5	4	200	-3	200
GWN	86	23	4	3.8	30	-3	10
GWN	87	15	3	3.6	0	0	0
GWN	88	15	4	4.3	0	0	0
GWN	89	15	5	5	0	0	0
GWN	90	12	3	3	10	-2	5
GWN	91	6	1	1	0	0	0
GWN	92	12	3	3	10	-2	5
GWN	93	12	3	3	10	-2	5
GWN	94	5.7	1	1	0	0	0
GWN	95	5.4	1	1	0	0	0
GWN	96	5.1	1	1	0	0	0
GWN	97	4.7	1	1	0	0	0
GWN	98	4.4	1	1	0	0	0
GWN	99	4.1	1	1	20	-1	20
GWN	100	12	3	3	10	-2	5
GWN	101	12	3	3	10	-2	5
GWN	102	12	2.4	2.6	10	-2	5
GWN	103	12	1.8	2.2	10	-2	5
GWN	104	12	1.8	2.2	10	-2	5
GWN	105	2	0.5	1	0	0	0
GWN	106	12	1.8	2.2	40	-2	20
GWN	107	12	1.8	2.2	40	-2	20
GWN	108	1.9	0.5	1	0	0	0
GWN	109	1.8	0.5	1	0	0	0
GWN	110	1.7	0.5	1	0	0	0
GWN	111	1.6	0.5	1	0	0	0
GWN	112	1.5	0.5	1	0	0	0
GWN	113	1.4	0.5	1	0	0	0
GWN	114	1.3	0.5	1	0	0	0
GWN	115	1.2	0.5	1	0	0	0
GWN	116	1.1	0.5	1	0	0	0
GWN	117	1	0.5	1	20	-1	20
GWN	118	12	1.8	2.2	40	-2	20

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

GWN	119	12	1.8	2.2	40	-2	20
GWN	120	12	1.8	2.2	40	-2	20
GWN	121	12	1.8	2.2	20	-2	10
GWN	122	12	1.8	2.2	10	-2	5
GWN	123	12	1.8	2.2	10	-2	5
GWN	124	12	1.8	2.2	10	-2	5
GWN	125	12	1.8	2.2	10	-1	10
GWN	126	12	1.8	2.2	10	-1	10
GWN	127	12	1.8	2.2	10	-1	10
GWN	128	12	1.8	2.2	0	0	0
GWN	129	12	1.8	2.2	0	0	0
GWN	130	8.8	1.5	2	0	0	0
GWN	131	10.5	0.5	1	0	0	0
GWN	132	8.8	1.5	2	0	0	0
GWN	133	8.8	1.5	2	0	0	0
GWN	134	10.5	0.5	1	0	0	0
GWN	135	10.5	0.5	1	0	0	0
GWN	136	10.5	0.5	1	0	0	0
GWN	137	10.5	0.5	1	0	0	0
GWN	138	10	0.5	1	0	0	0
GWN	139	9.5	0.5	1	0	0	0
GWN	140	8.5	0.5	1	0	0	0
GWN	141	7.5	0.5	1	0	0	0
GWN	142	6.5	0.5	1	0	0	0
GWN	143	5.5	0.5	1	0	0	0
GWN	144	4.5	0.5	1	0	0	0
GWN	145	3.5	0.5	1	80	-1.3	80
GWN	146	8.4	1.75	2	10	-1	10
GWN	147	8	2	2	0	0	0
GWN	148	7	2	2	5	-1	5
GWN	149	7	2	2	0	0	0
GWN	150	6.5	2	2	20	-1	20
GWN	151	6	2	2	20	-1	20
GWN	152	5.5	2	2	20	-1	20
GWN	153	5	2	2	20	-1	20
GWN	154	3	4	2.5	20	-1	20
GWN	155	1	6	3	20	-1	20
GWN	156	1	6	3	20	-1	20
GWN	157	1	6	3	20	-1	20
GWN	158	1	6	3	20	-1	20
GWN	159	1	6	3	80	-1.3	80
GWN	160	25	5.5	10	200	-3.6	60
GWN	161	13	1	1	0	0	0
GWN	162	9	1.5	1.5	0	0	0
GWN	163	4.8	1.9	1.9	0	0	0
GWN	164	4.0	1.9	1.9	0	0	0
GWN	165	3.8	1.9	1.9	10	-1.1	10

Below is the first day of the Cow Bayou RMA2 boundary condition file.

```

T1 Cow Bayou Long Term Run B
T2 Jan 1, 2002 - Jan 1, 2013 at 30 min (0.5 hr) time step
T3 Fully Permitted PS Flows
$M 1
$L 0 0 1 1 0 0 0 0 0 0
SI 1
DE 0.084 0.183 5
EX 1 5000.00 5000.00
EY 1 5000.00 5000.00
EX 2 5000.00 5000.00
EY 2 5000.00 5000.00
EX 3 5000.00 5000.00

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

```

EY 3      5000.00      5000.00
EX 4      5000.00      5000.00
EY 4      5000.00      5000.00
FT 20
IC 0.105  0.3  0.08
RDT 1 1 0.030 2 0.040 1E-14 0 0
RDT 2 1 0.040 2 0.045 1E-14 0 0
RDT 3 1 0.045 2 0.050 1E-14 0 0
RDT 4 1 0.060 2 0.070 1E-14 0 0
CO RSC 10000 0 0
TI 25 15 0.0001 0.01
TR 0 0 0 0
TS -1 0 0
TZ 0.5 96431.5 192864 0 0
CO BAN cards are boundary flow azimuths in radians from x-axis
BAN 1 3.58
BAN 15 3.58
BAN 71 0.46
BAN 99 4.71
BAN 117 5.12
BAN 145 5.85
BAN 159 5.32
BAN 165 4.71
CO initial boundary flows in cms
CO BQE 14 is Honeywell WQ0000670-000 self-reported flows
CO BQE 19 is Lanxess WQ0001167-000 self-reported flows
CO BQE 21 is Firestone WQ0000454-000 self-reported flows
CO BQE 36 is City of Bridge City WQ0013691-001 self-reported flows
CO BQE 37 is Gulflander Partners Group WQ0013488-001 self-reported flows
CO BQE 38 is City of Bridge City WQ0010051-001 self-reported flows
CO BQE 44 is Orangefield WSC WQ0014772-001 self-reported flows
CO BQE 50 is Sabine River Authority WQ0012134-001 self-reported flows
CO BQE 78 is TXDOT WQ0011457-001 self-reported flows
CO BQE 79 is PCS Development Group WQ0011916-001 self-reported flows
CO BQE 83 includes Chevron WQ0000359-000 and Printpack ...
CO WQ0002858-000 self-reported flows
BQE 14 0.00002448
BQE 19 0.00020373
BQE 21 0.00002821
BQE 36 0.00000190
BQE 37 0.00000055
BQE 38 0.00005148
BQE 44 0.00000085
BQE 50 0.00000007
BQE 78 0.00000025
BQE 79 0.00000064
BQE 83 0.00005397
BQN 117 0.342150
BQN 145 0.910430
BQN 159 3.332000
BQE 18 0.000116
BQE 22 0.000175
BQE 39 0.000193
BQE 43 0.000147
BQE 58 0.000110
BQE 62 0.000155
BQN 71 0.156670
BQE 75 0.000169
BQN 99 0.227490
BQN 15 464.00000000
BCN 1 00200 0 0 0.105
END Simulation at time = 0.0
BCN 1 00200 0 0 0.105

```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

```
END Simulation at time = 0.5
BQN 117 0.341210
BQN 145 0.907130
BQN 159 3.307000
BQE 18 0.000114
BQE 22 0.000171
BQE 39 0.000189
BQE 43 0.000144
BQE 58 0.000108
BQE 62 0.000152
BQN 71 0.155310
BQE 75 0.000165
BQN 99 0.226020
BCN 1 00200 0 0 0.102
END Simulation at time = 1.0
BCN 1 00200 0 0 0.101
END Simulation at time = 1.5
BQN 117 0.339440
BQN 145 0.903110
BQN 159 3.281000
BQE 18 0.000112
BQE 22 0.000168
BQE 39 0.000185
BQE 43 0.000141
BQE 58 0.000106
BQE 62 0.000149
BQN 71 0.153630
BQE 75 0.000162
BQN 99 0.224060
BCN 1 00200 0 0 0.091
END Simulation at time = 2.0
BCN 1 00200 0 0 0.085
END Simulation at time = 2.5
BQN 117 0.336970
BQN 145 0.898430
BQN 159 3.254400
BQE 18 0.000110
BQE 22 0.000164
BQE 39 0.000181
BQE 43 0.000138
BQE 58 0.000104
BQE 62 0.000146
BQN 71 0.151690
BQE 75 0.000159
BQN 99 0.221710
BCN 1 00200 0 0 0.081
END Simulation at time = 3.0
BCN 1 00200 0 0 0.086
END Simulation at time = 3.5
BQN 117 0.333930
BQN 145 0.893160
BQN 159 3.227500
BQE 18 0.000107
BQE 22 0.000161
BQE 39 0.000178
BQE 43 0.000135
BQE 58 0.000102
BQE 62 0.000143
BQN 71 0.149570
BQE 75 0.000156
BQN 99 0.219060
BCN 1 00200 0 0 0.075
END Simulation at time = 4.0
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

```
BCN 1 00200 0 0 0.08
END Simulation at time = 4.5
BQN 117 0.330430
BQN 145 0.887320
BQN 159 3.200400
BQE 18 0.000105
BQE 22 0.000158
BQE 39 0.000174
BQE 43 0.000133
BQE 58 0.000100
BQE 62 0.000140
BQN 71 0.147320
BQE 75 0.000152
BQN 99 0.216170
BCN 1 00200 0 0 0.066
END Simulation at time = 5.0
BCN 1 00200 0 0 0.056
END Simulation at time = 5.5
BQN 117 0.325820
BQN 145 0.879970
BQN 159 3.171100
BQE 18 0.000101
BQE 22 0.000152
BQE 39 0.000168
BQE 43 0.000128
BQE 58 0.000096
BQE 62 0.000135
BQN 71 0.144500
BQE 75 0.000147
BQN 99 0.212550
BCN 1 00200 0 0 0.044
END Simulation at time = 6.0
BCN 1 00200 0 0 0.032
END Simulation at time = 6.5
BQN 117 0.306920
BQN 145 0.853280
BQN 159 3.101300
BQE 18 0.000066
BQE 22 0.000100
BQE 39 0.000112
BQE 43 0.000084
BQE 58 0.000063
BQE 62 0.000090
BQN 71 0.132810
BQE 75 0.000097
BQN 99 0.198050
BCN 1 00200 0 0 0.014
END Simulation at time = 7.0
BCN 1 00200 0 0 0.004
END Simulation at time = 7.5
BQN 117 0.280070
BQN 145 0.815500
BQN 159 3.010300
BQE 18 0.000039
BQE 22 0.000062
BQE 39 0.000070
BQE 43 0.000052
BQE 58 0.000041
BQE 62 0.000055
BQN 71 0.116630
BQE 75 0.000062
BQN 99 0.177660
BCN 1 00200 0 0 -0.024
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

```
END Simulation at time = 8.0
BCN 1 00200 0 0 -0.061
END Simulation at time = 8.5
BQN 117 0.256740
BQN 145 0.780360
BQN 159 2.928000
BQE 18 0.000038
BQE 22 0.000060
BQE 39 0.000067
BQE 43 0.000051
BQE 58 0.000040
BQE 62 0.000054
BQN 71 0.103250
BQE 75 0.000061
BQN 99 0.160510
BCN 1 00200 0 0 -0.082
END Simulation at time = 9.0
BCN 1 00200 0 0 -0.118
END Simulation at time = 9.5
BQN 117 0.236590
BQN 145 0.748070
BQN 159 2.853700
BQE 18 0.000037
BQE 22 0.000059
BQE 39 0.000067
BQE 43 0.000050
BQE 58 0.000040
BQE 62 0.000054
BQN 71 0.092412
BQE 75 0.000060
BQN 99 0.146230
BCN 1 00200 0 0 -0.145
END Simulation at time = 10.0
BCN 1 00200 0 0 -0.162
END Simulation at time = 10.5
BQN 117 0.219160
BQN 145 0.718170
BQN 159 2.784000
BQE 18 0.000037
BQE 22 0.000058
BQE 39 0.000066
BQE 43 0.000050
BQE 58 0.000039
BQE 62 0.000053
BQN 71 0.083611
BQE 75 0.000059
BQN 99 0.139940
BCN 1 00200 0 0 -0.191
END Simulation at time = 11.0
BCN 1 00200 0 0 -0.222
END Simulation at time = 11.5
BQN 117 0.204060
BQN 145 0.690260
BQN 159 2.719900
BQE 18 0.000036
BQE 22 0.000058
BQE 39 0.000065
BQE 43 0.000049
BQE 58 0.000039
BQE 62 0.000052
BQN 71 0.076440
BQE 75 0.000058
BQN 99 0.137450
```

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

BCN 1 00200 0 0 -0.256
END Simulation at time = 12.0
BCN 1 00200 0 0 -0.284
END Simulation at time = 12.5
BQN 117 0.190950
BQN 145 0.664060
BQN 159 2.661800
BQE 18 0.000036
BQE 22 0.000057
BQE 39 0.000064
BQE 43 0.000048
BQE 58 0.000038
BQE 62 0.000052
BQN 71 0.070576
BQE 75 0.000058
BQN 99 0.135020
BCN 1 00200 0 0 -0.295
END Simulation at time = 13.0
BCN 1 00200 0 0 -0.297
END Simulation at time = 13.5
BQN 117 0.179700
BQN 145 0.639780
BQN 159 2.609300
BQE 18 0.000036
BQE 22 0.000056
BQE 39 0.000064
BQE 43 0.000048
BQE 58 0.000038
BQE 62 0.000051
BQN 71 0.065976
BQE 75 0.000057
BQN 99 0.132680
BCN 1 00200 0 0 -0.317
END Simulation at time = 14.0
BCN 1 00200 0 0 -0.316
END Simulation at time = 14.5
BQN 117 0.173700
BQN 145 0.622320
BQN 159 2.572000
BQE 18 0.000044
BQE 22 0.000069
BQE 39 0.000078
BQE 43 0.000058
BQE 58 0.000045
BQE 62 0.000062
BQN 71 0.064776
BQE 75 0.000069
BQN 99 0.131090
BCN 1 00200 0 0 -0.353
END Simulation at time = 15.0
BCN 1 00200 0 0 -0.31
END Simulation at time = 15.5
BQN 117 0.181570
BQN 145 0.622910
BQN 159 2.575600
BQE 18 0.000076
BQE 22 0.000115
BQE 39 0.000128
BQE 43 0.000097
BQE 58 0.000073
BQE 62 0.000103
BQN 71 0.072099
BQE 75 0.000112

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

BQN 99 0.131860
BCN 1 00200 0 0 -0.305
END Simulation at time = 16.0
BCN 1 00200 0 0 -0.276
END Simulation at time = 16.5
BQN 117 0.188380
BQN 145 0.622630
BQN 159 2.576400
BQE 18 0.000076
BQE 22 0.000115
BQE 39 0.000128
BQE 43 0.000097
BQE 58 0.000074
BQE 62 0.000103
BQN 71 0.078016
BQE 75 0.000112
BQN 99 0.132610
BCN 1 00200 0 0 -0.258
END Simulation at time = 17.0
BCN 1 00200 0 0 -0.241
END Simulation at time = 17.5
BQN 117 0.193560
BQN 145 0.620830
BQN 159 2.572600
BQE 18 0.000074
BQE 22 0.000113
BQE 39 0.000125
BQE 43 0.000095
BQE 58 0.000072
BQE 62 0.000101
BQN 71 0.082362
BQE 75 0.000110
BQN 99 0.133220
BCN 1 00200 0 0 -0.221
END Simulation at time = 18.0
BCN 1 00200 0 0 -0.171
END Simulation at time = 18.5
BQN 117 0.197360
BQN 145 0.617870
BQN 159 2.565200
BQE 18 0.000073
BQE 22 0.000111
BQE 39 0.000123
BQE 43 0.000093
BQE 58 0.000071
BQE 62 0.000099
BQN 71 0.085457
BQE 75 0.000108
BQN 99 0.133700
BCN 1 00200 0 0 -0.133
END Simulation at time = 19.0
BCN 1 00200 0 0 -0.098
END Simulation at time = 19.5
BQN 117 0.200000
BQN 145 0.614030
BQN 159 2.554700
BQE 18 0.000072
BQE 22 0.000109
BQE 39 0.000120
BQE 43 0.000091
BQE 58 0.000069
BQE 62 0.000097
BQN 71 0.087561

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

BQE 75 0.000106
BQN 99 0.134050
BCN 1 00200 0 0 -0.061
END Simulation at time = 20.0
BCN 1 00200 0 0 -0.032
END Simulation at time = 20.5
BQN 117 0.201670
BQN 145 0.609510
BQN 159 2.541800
BQE 18 0.000070
BQE 22 0.000106
BQE 39 0.000118
BQE 43 0.000090
BQE 58 0.000068
BQE 62 0.000095
BQN 71 0.088880
BQE 75 0.000104
BQN 99 0.134290
BCN 1 00200 0 0 -0.001
END Simulation at time = 21.0
BCN 1 00200 0 0 0.027
END Simulation at time = 21.5
BQN 117 0.202510
BQN 145 0.604480
BQN 159 2.526800
BQE 18 0.000069
BQE 22 0.000104
BQE 39 0.000116
BQE 43 0.000088
BQE 58 0.000067
BQE 62 0.000093
BQN 71 0.089579
BQE 75 0.000102
BQN 99 0.134410
BCN 1 00200 0 0 0.027
END Simulation at time = 22.0
BCN 1 00200 0 0 0.001
END Simulation at time = 22.5
BQN 117 0.202660
BQN 145 0.599050
BQN 159 2.510200
BQE 18 0.000068
BQE 22 0.000102
BQE 39 0.000114
BQE 43 0.000086
BQE 58 0.000066
BQE 62 0.000091
BQN 71 0.089789
BQE 75 0.000100
BQN 99 0.134440
BCN 1 00200 0 0 -0.01
END Simulation at time = 23.0
BCN 1 00200 0 0 -0.008
END Simulation at time = 23.5
BQN 117 0.201840
BQN 145 0.592780
BQN 159 2.490900
BQE 18 0.000065
BQE 22 0.000099
BQE 39 0.000110
BQE 43 0.000083
BQE 58 0.000063
BQE 62 0.000088

Technical Support Document for TMDLs for DO and pH in Adams Bayou, Cow Bayou, and Tributaries
Appendix D

```
BQN 71      0.089371
BQE 75      0.000097
BQN 99      0.134290
BQN 15      456.00000000
BCN 1 00200 0 0 0.031
END Simulation at time = 24.0
STOP
```

Note: The model printout was stopped here, after one day, due to space considerations. The complete model input would occupy many hundreds of pages.

Appendix E Goodness-of-fit for the Adams Bayou RMA2 Hydrodynamic Model

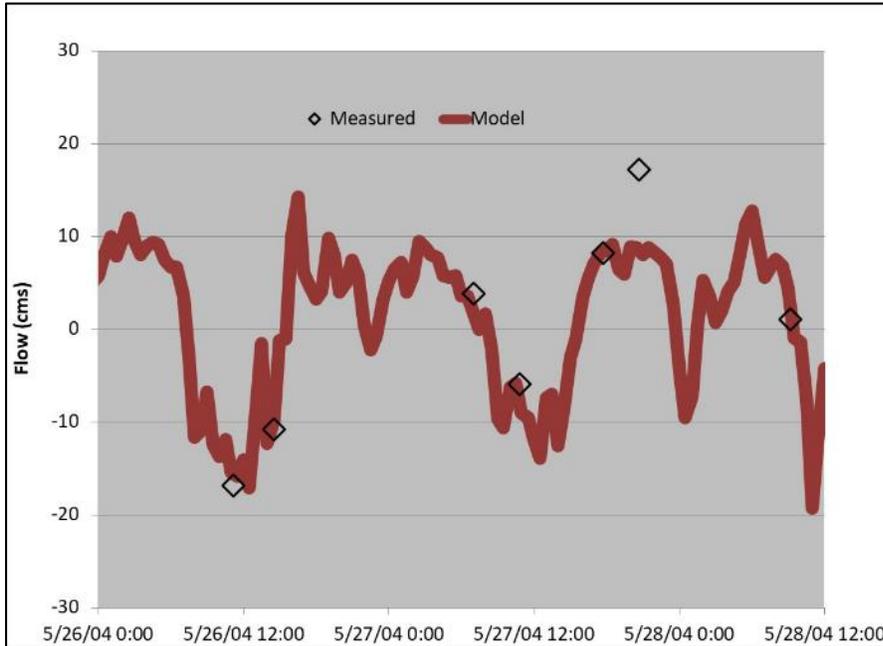


Figure E-1 Flow calibration at station AB2

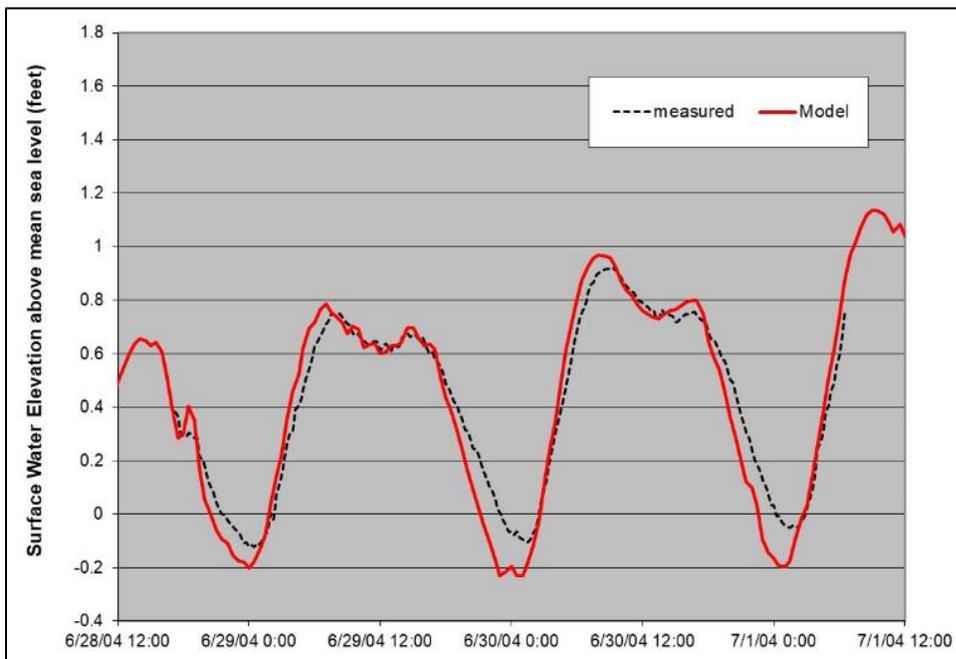


Figure E-2 Water level validation at station AB2

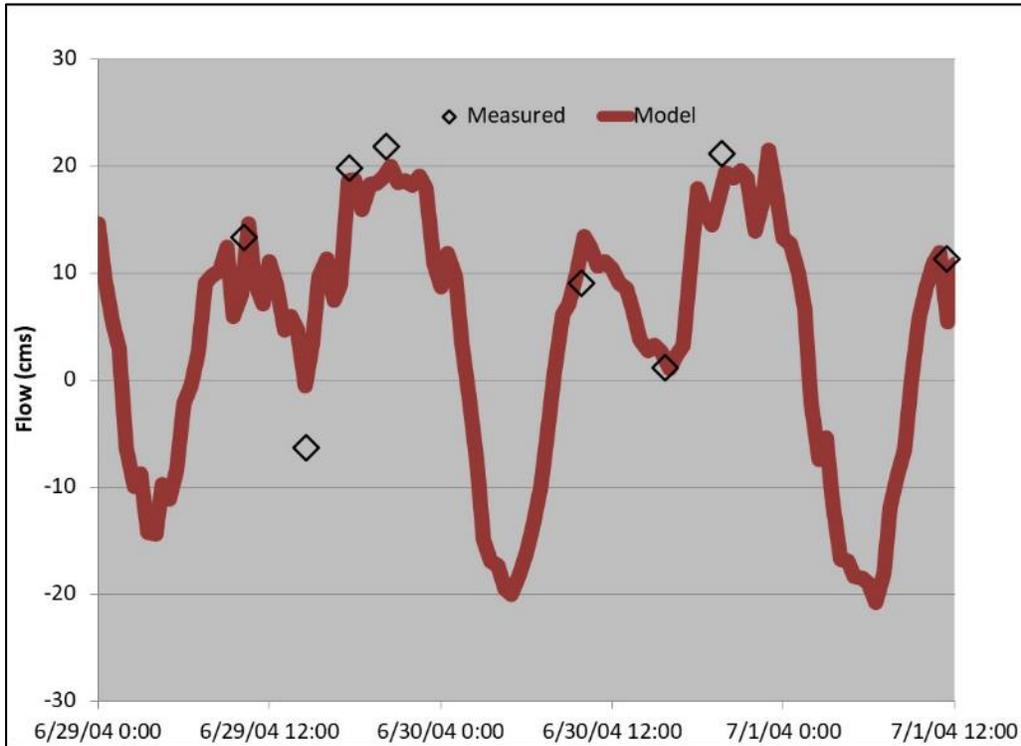


Figure E-3 Flow validation at station AB2

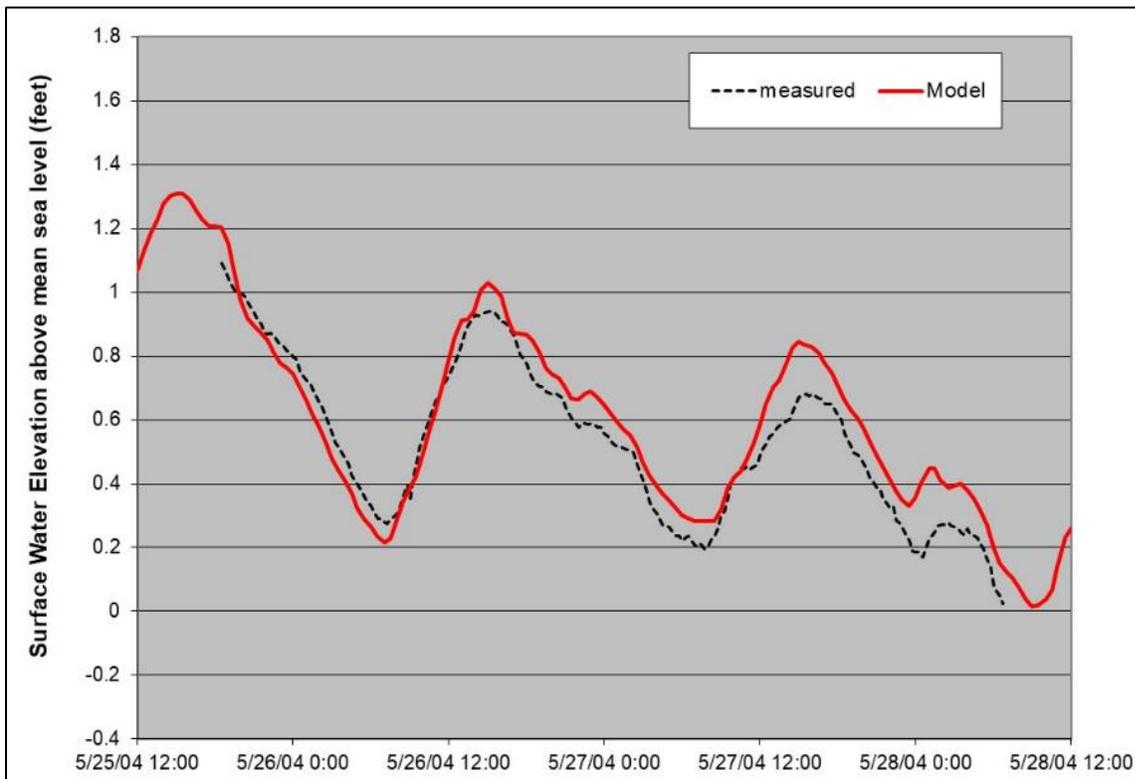


Figure E-4 Water level calibration at station AB3

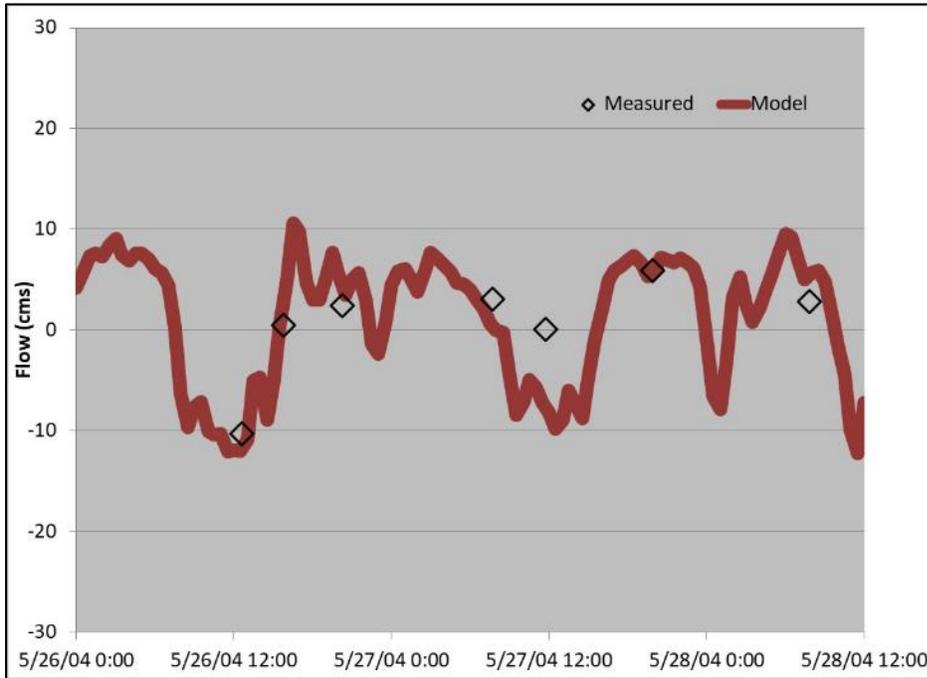


Figure E-5 Flow calibration at station AB3

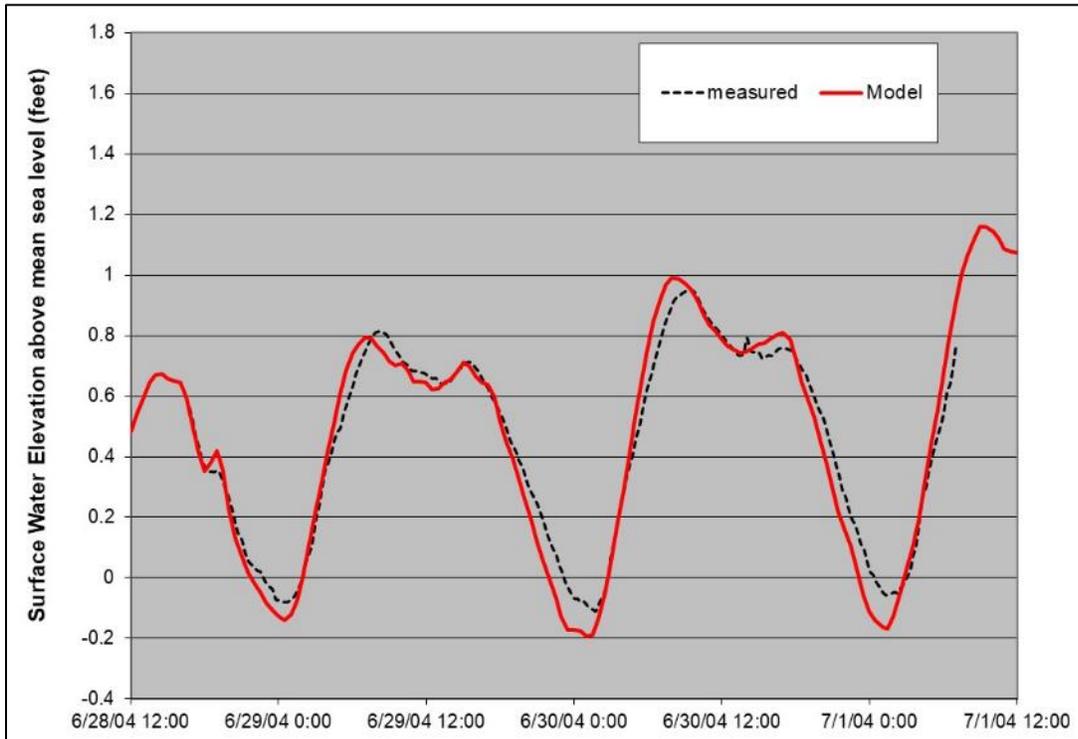


Figure E-6 Water level validation at station AB3

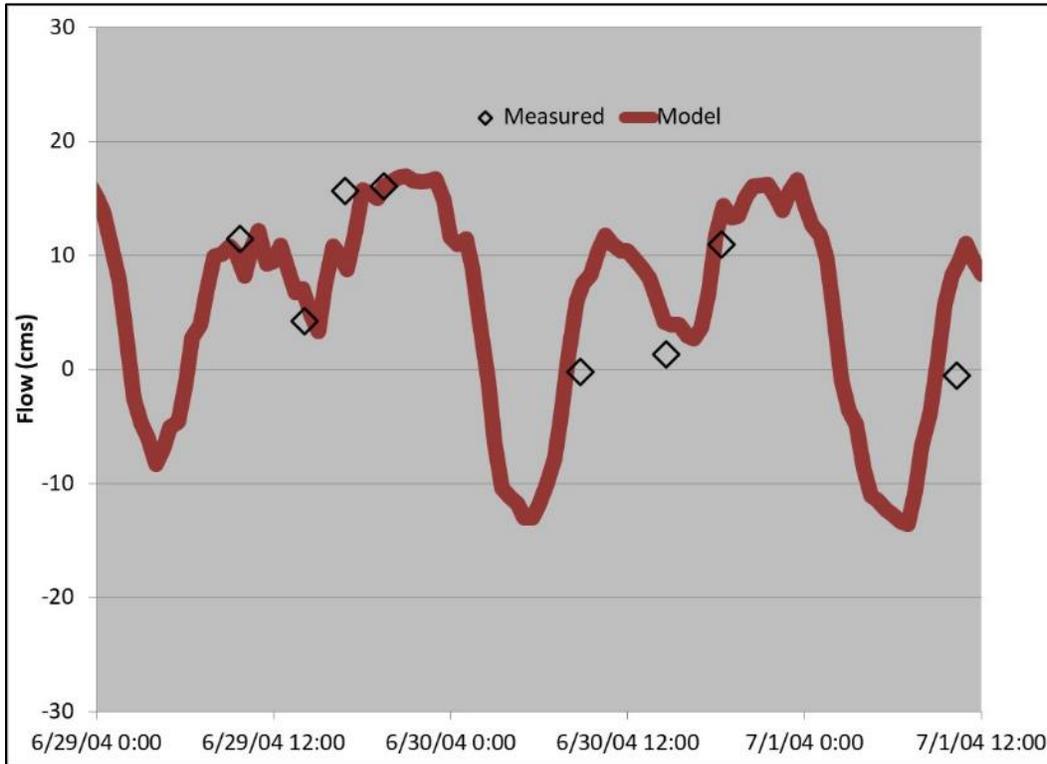


Figure E-7 Flow validation at station AB3

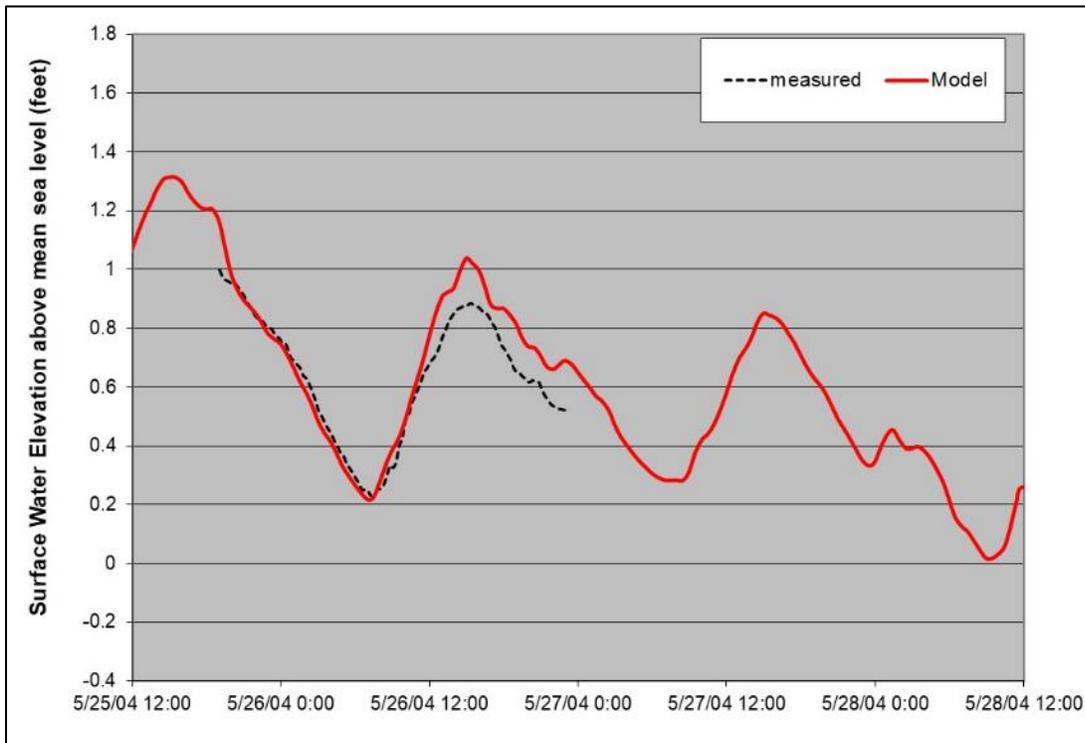


Figure E-8 Water level calibration at station AB4

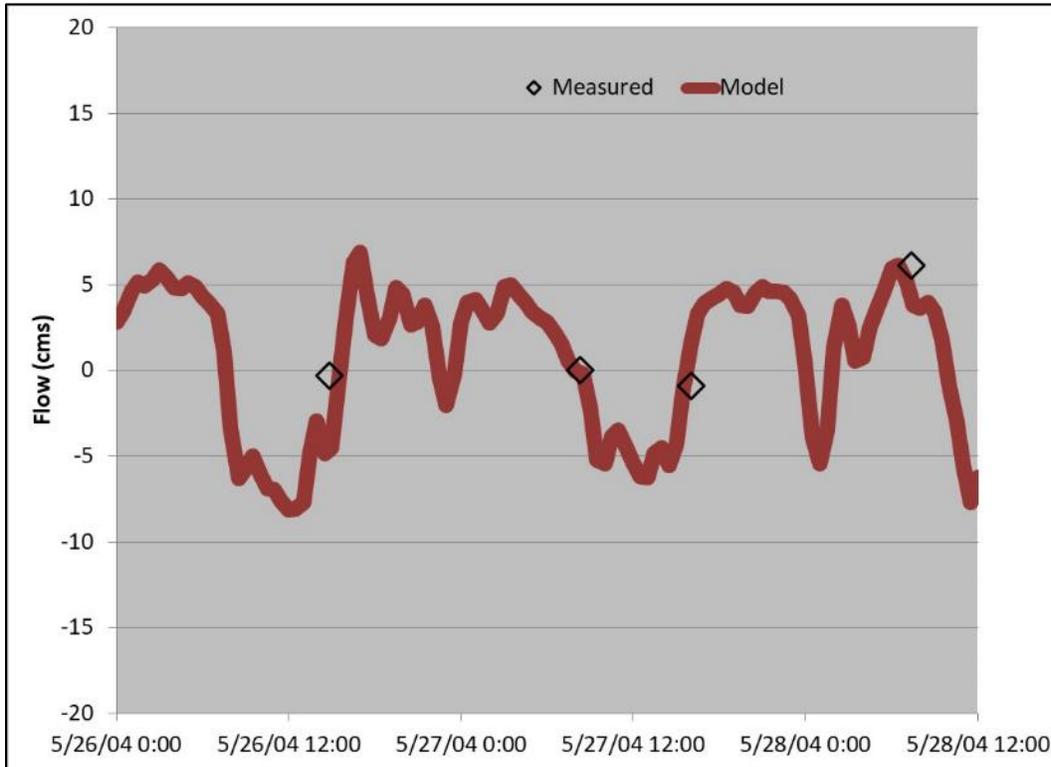


Figure E-9 Flow calibration at station AB4

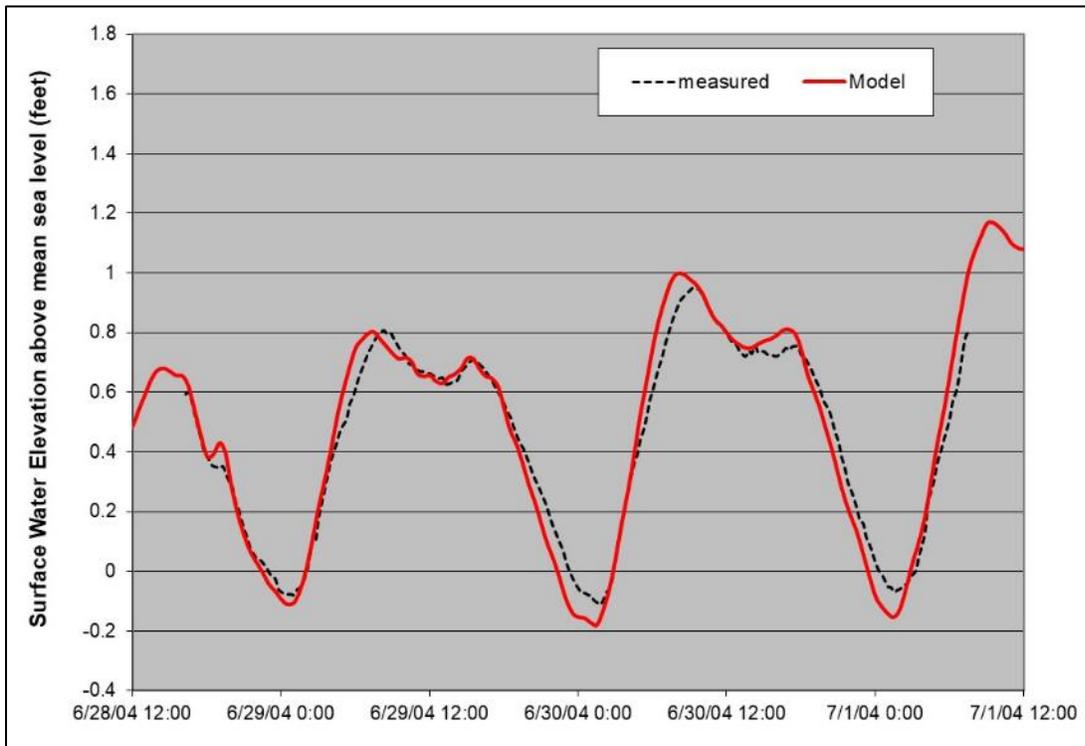


Figure E-10 Water level validation at station AB4

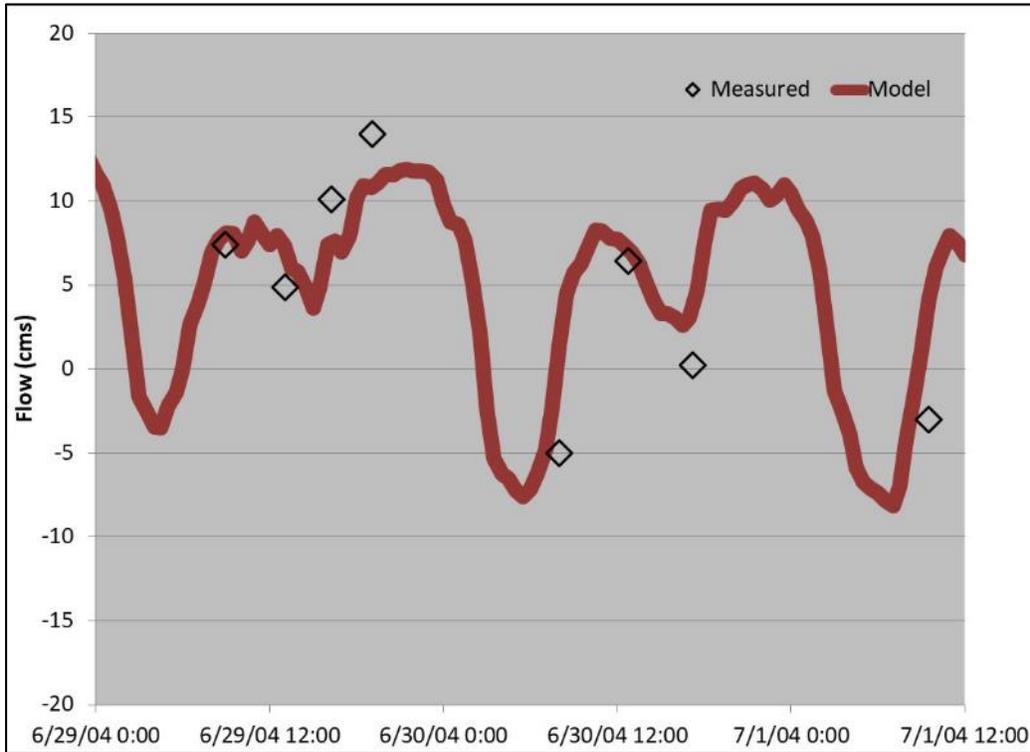


Figure E-11 Flow validation at station AB4

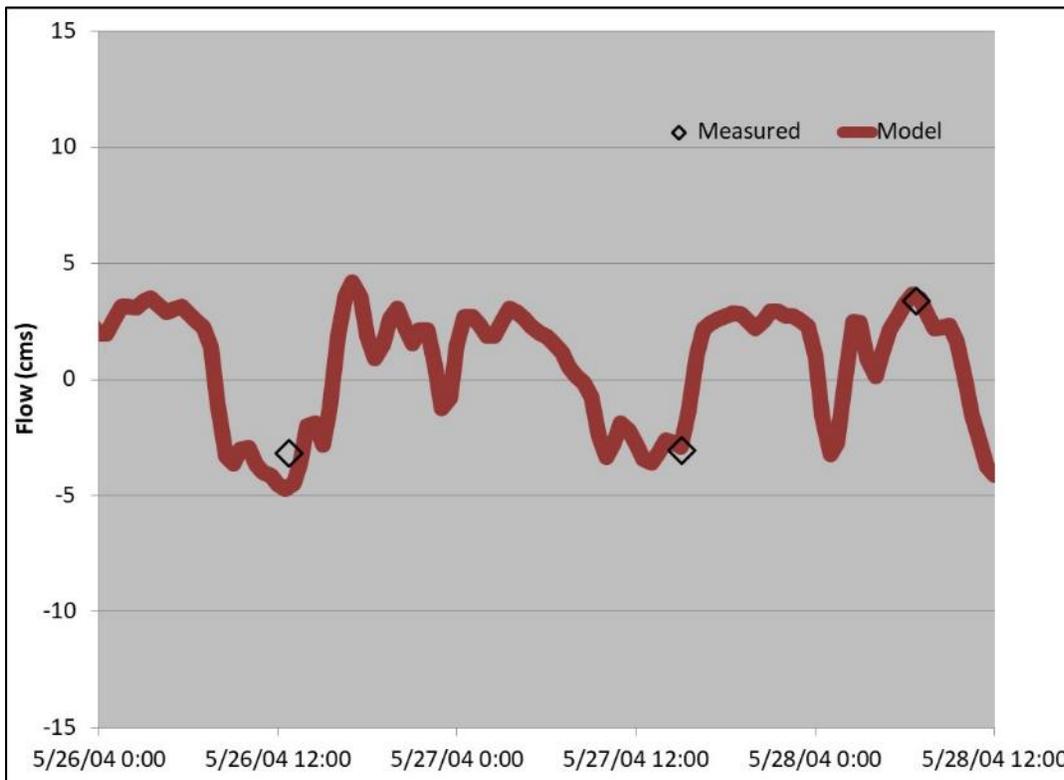


Figure E-12 Flow calibration at station AB5

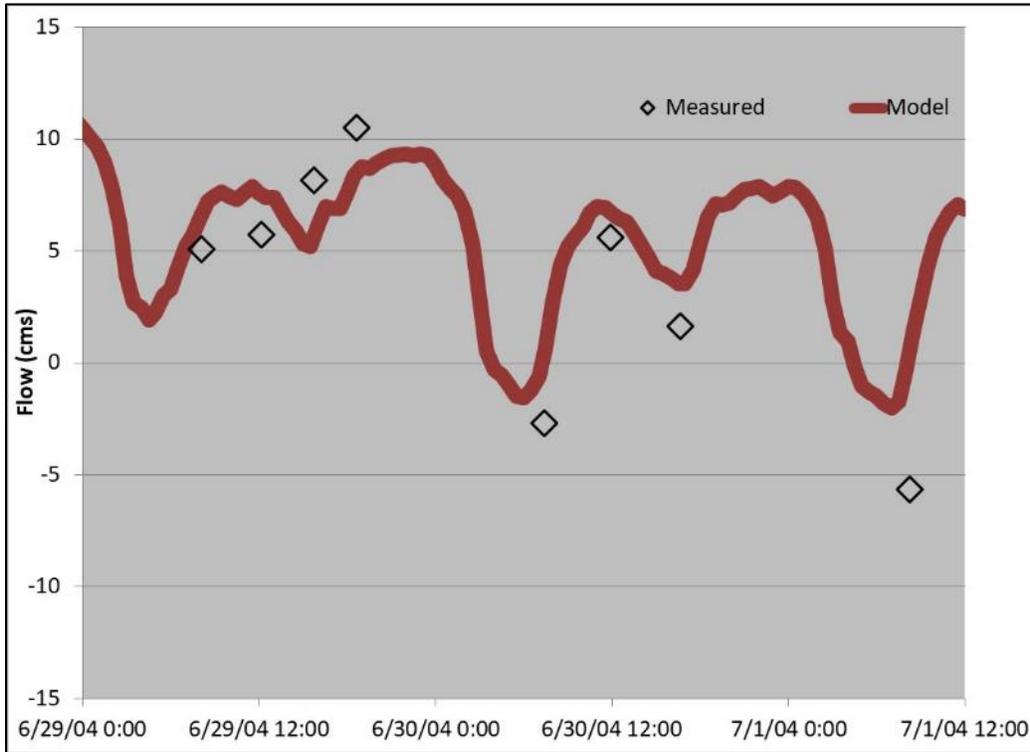


Figure E-13 Flow validation at station AB5

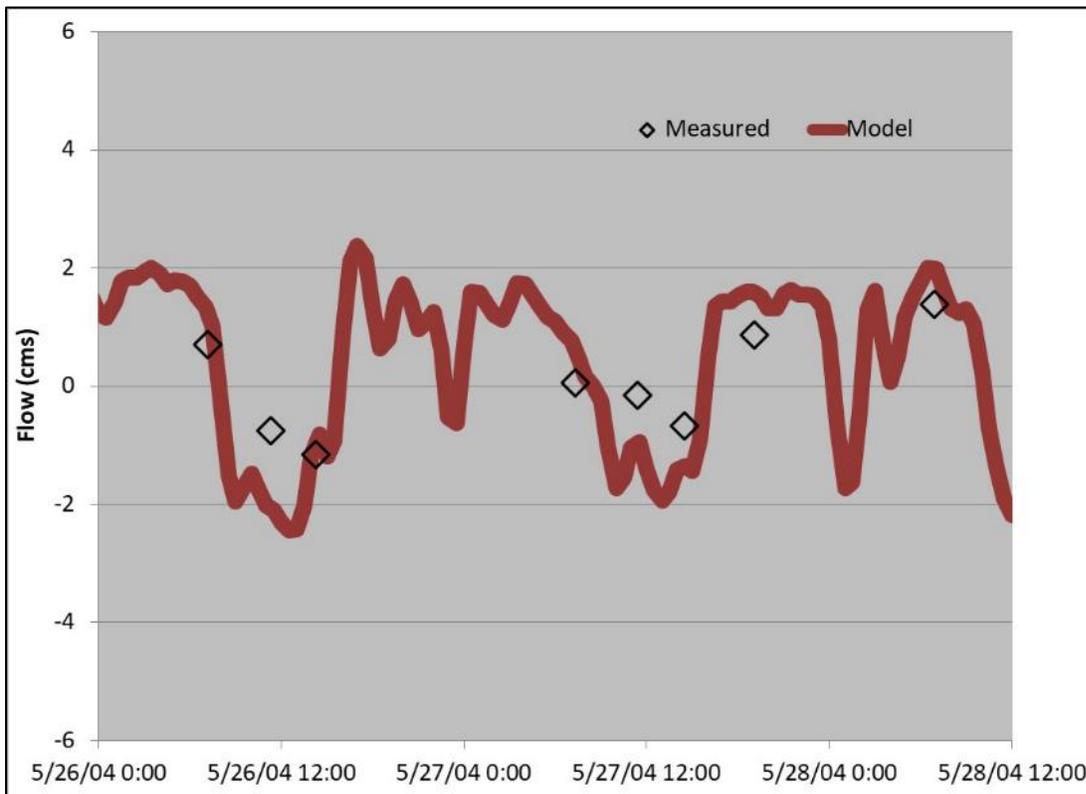


Figure E-14 Flow calibration at station AB6

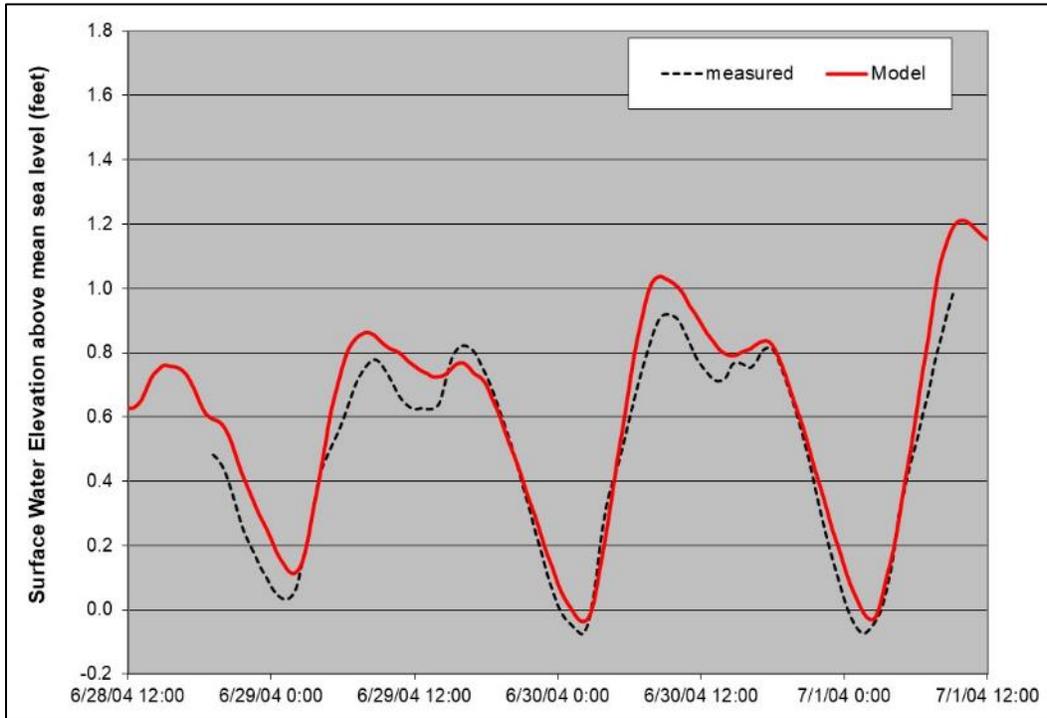


Figure E-15 Water level validation at station AB6

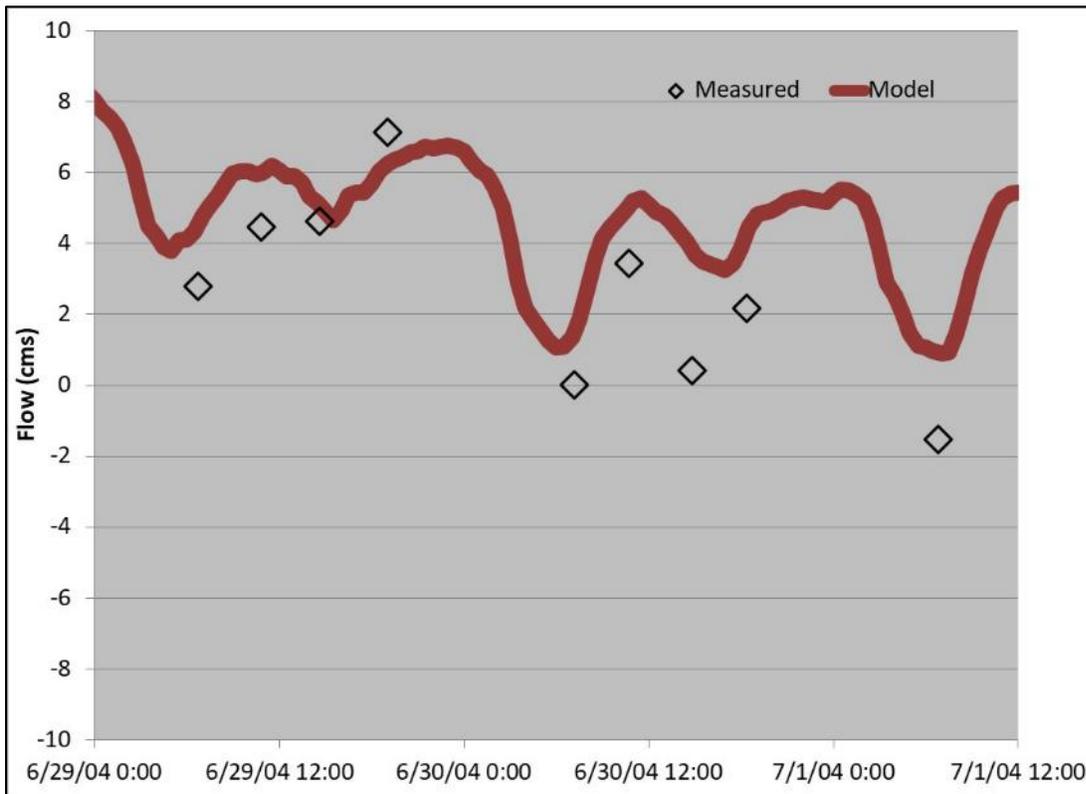


Figure E-16 Flow validation at station AB6

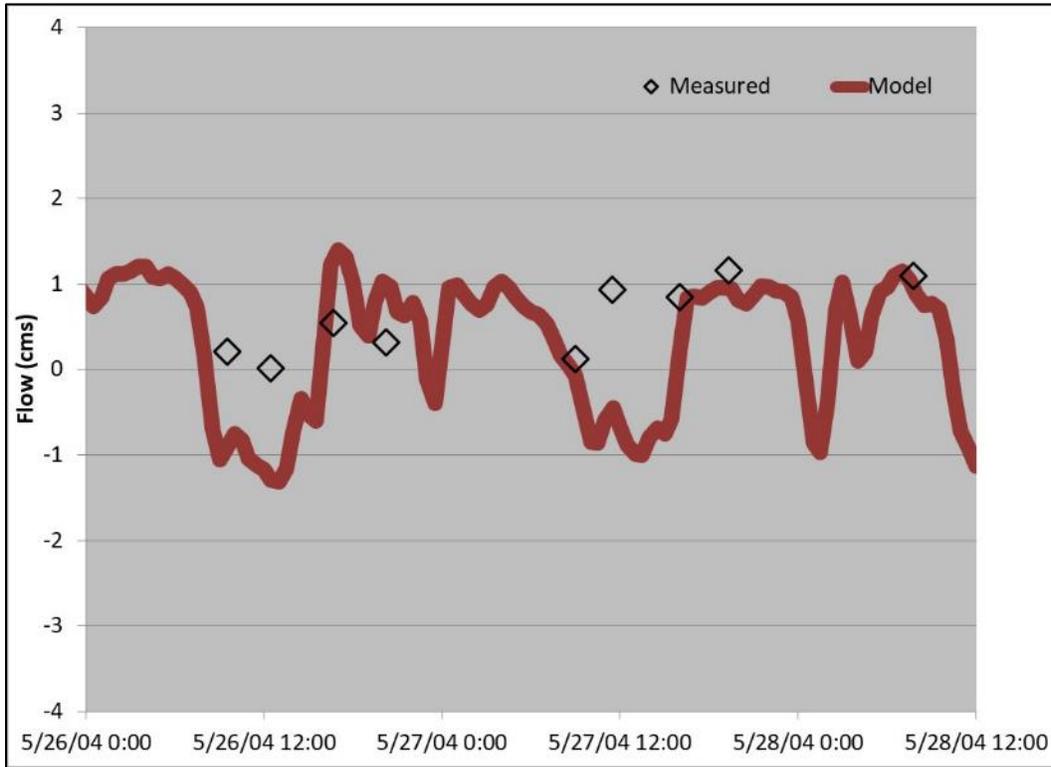


Figure E-17 Flow calibration at station AB7

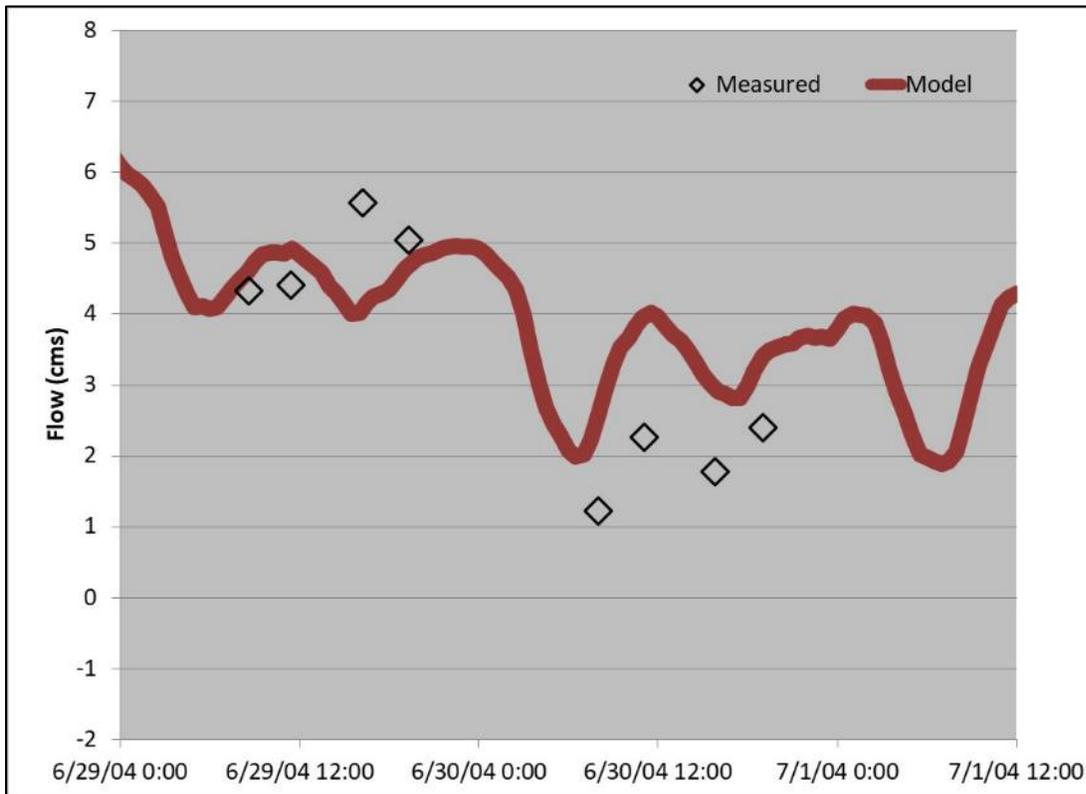


Figure E-18 Flow validation at station AB7

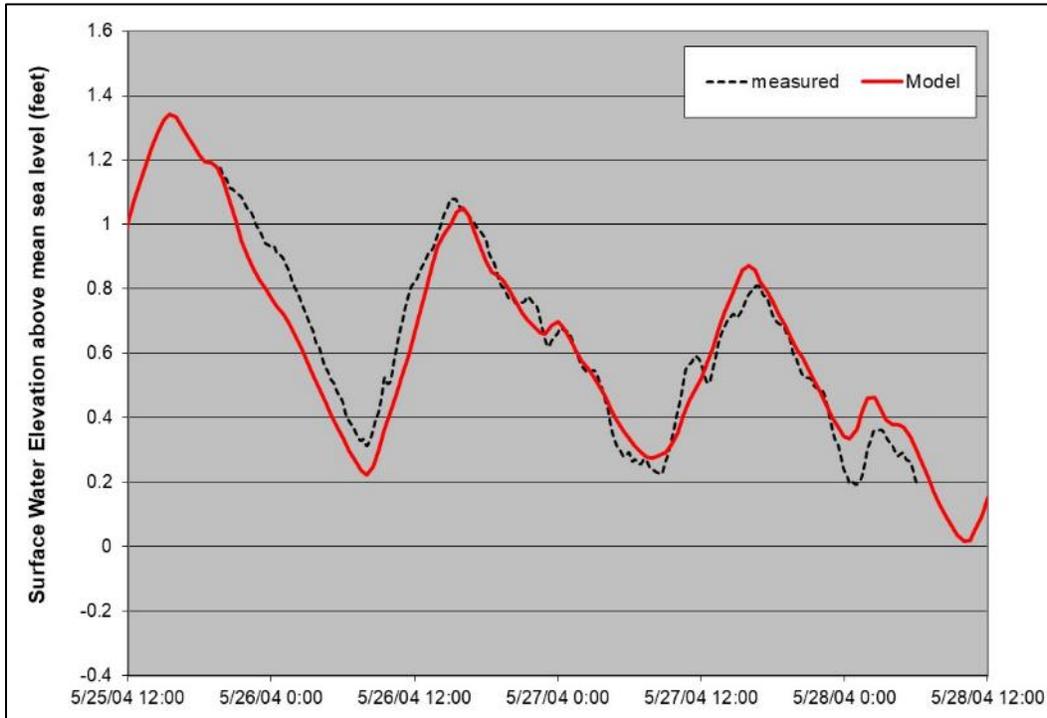


Figure E-19 Water level calibration at station AB8

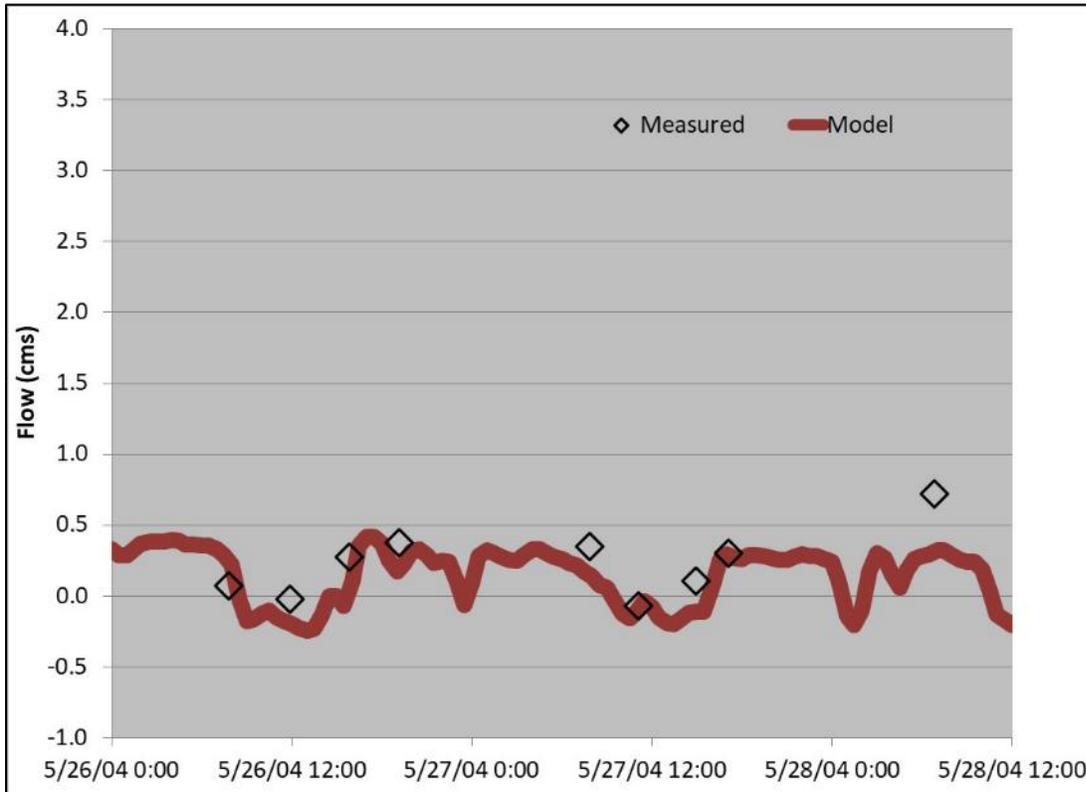


Figure E-20 Flow calibration at station AB8

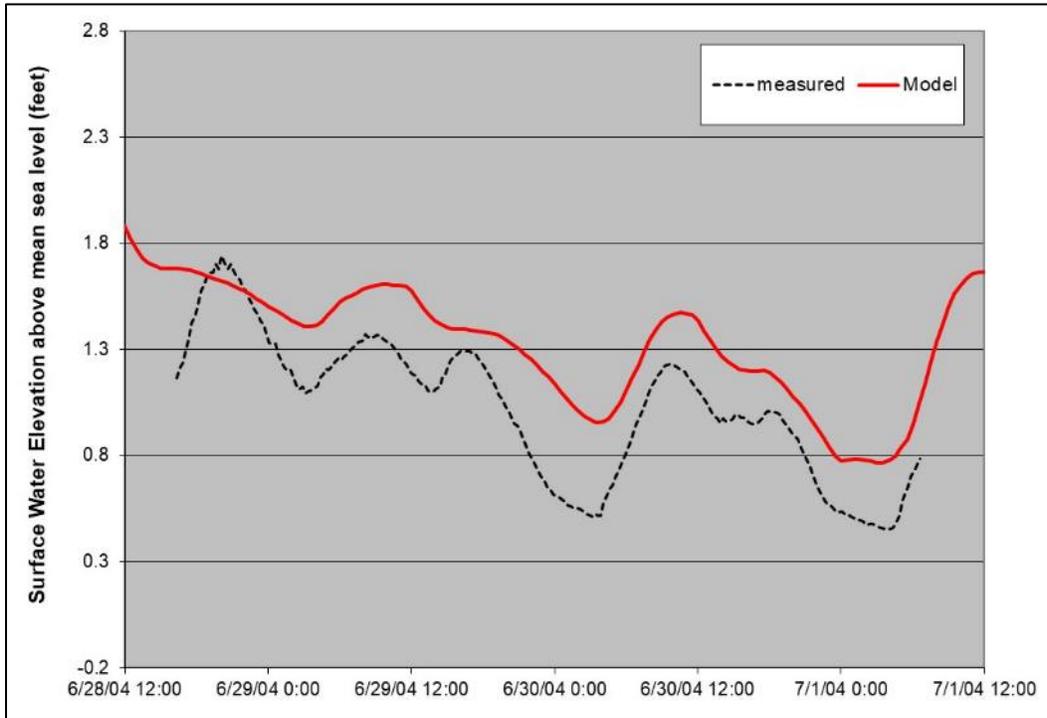


Figure E-21 Water level validation at station AB8

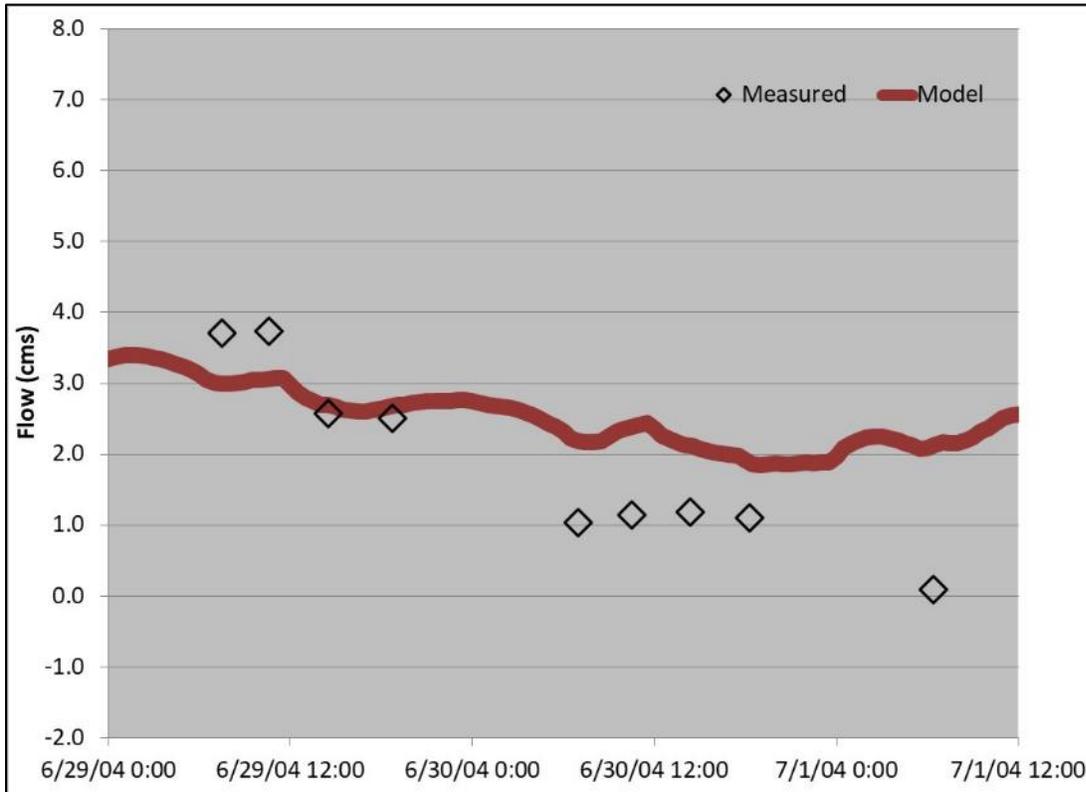


Figure E-22 Flow validation at station AB8

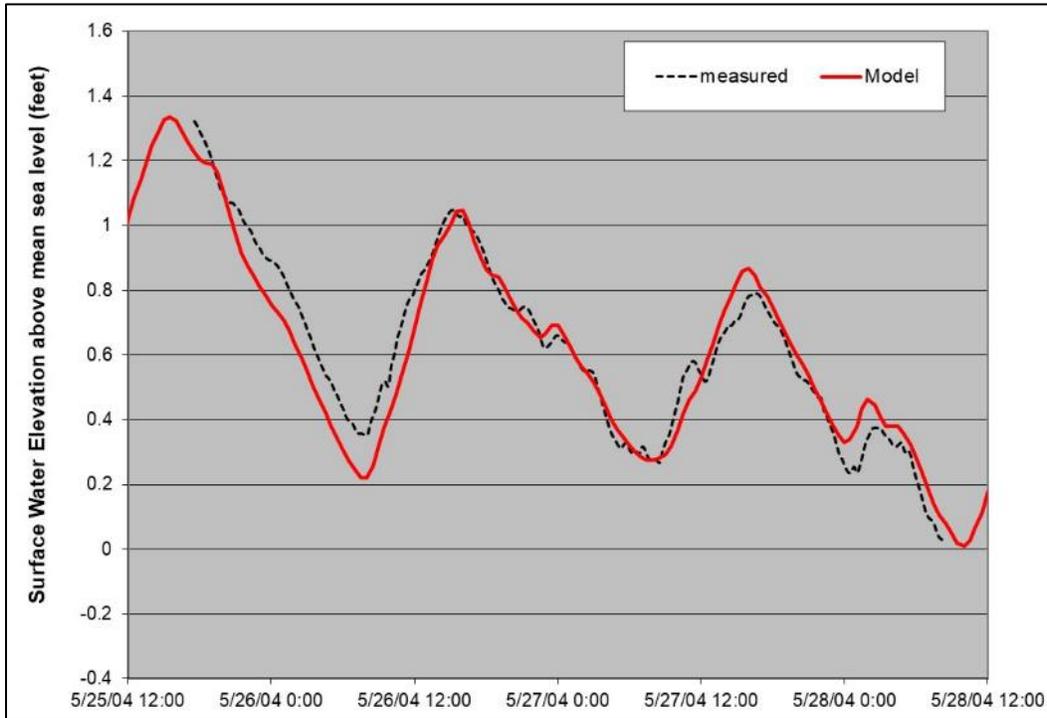


Figure E-23 Water level calibration at station GG (Gum Gully)

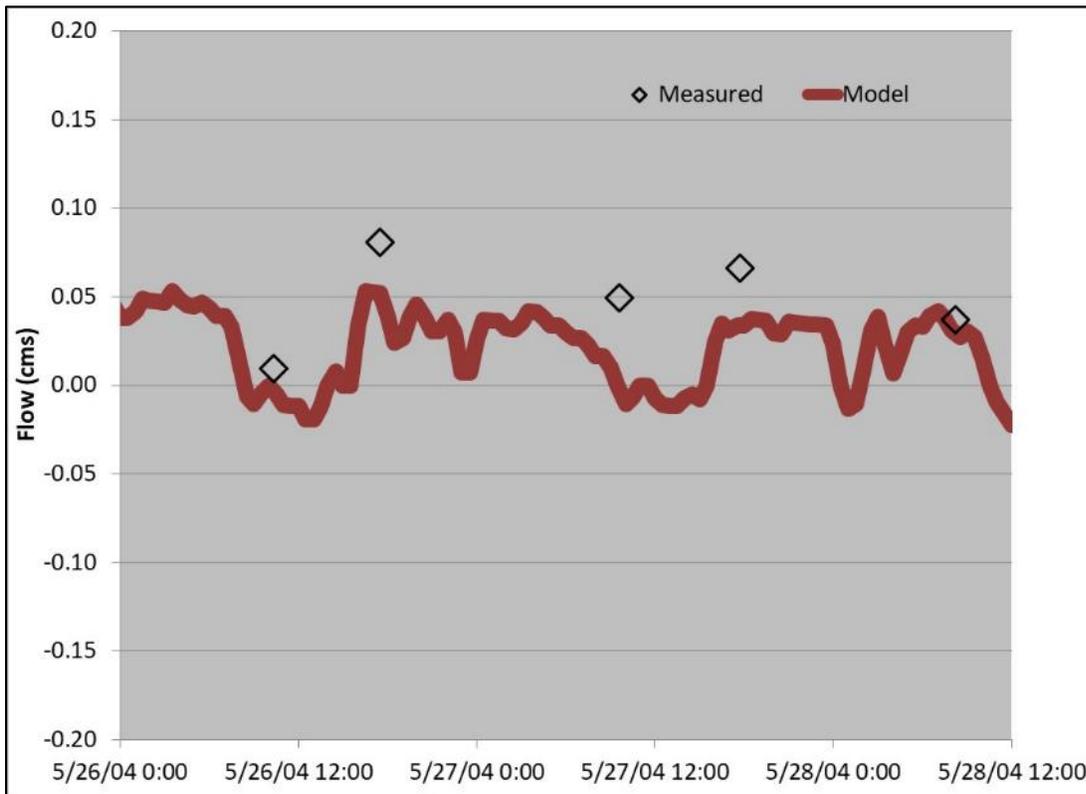


Figure E-24 Flow calibration at station GG (Gum Gully)

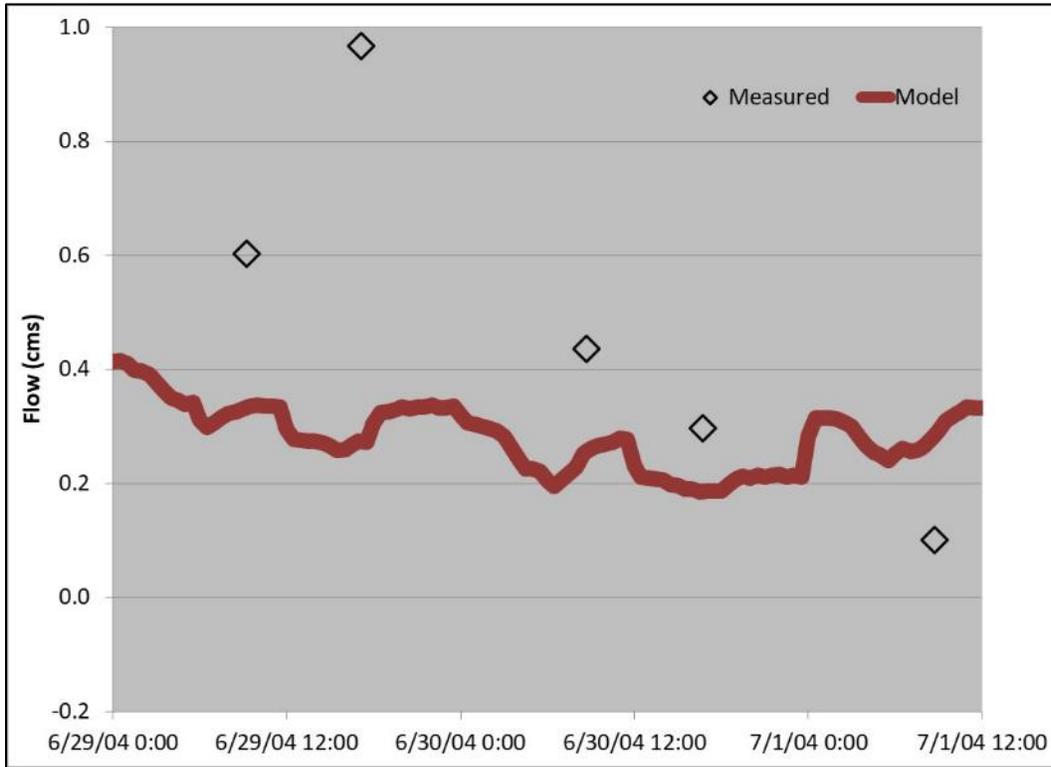


Figure E-25 Flow validation at station GG (Gum Gully)

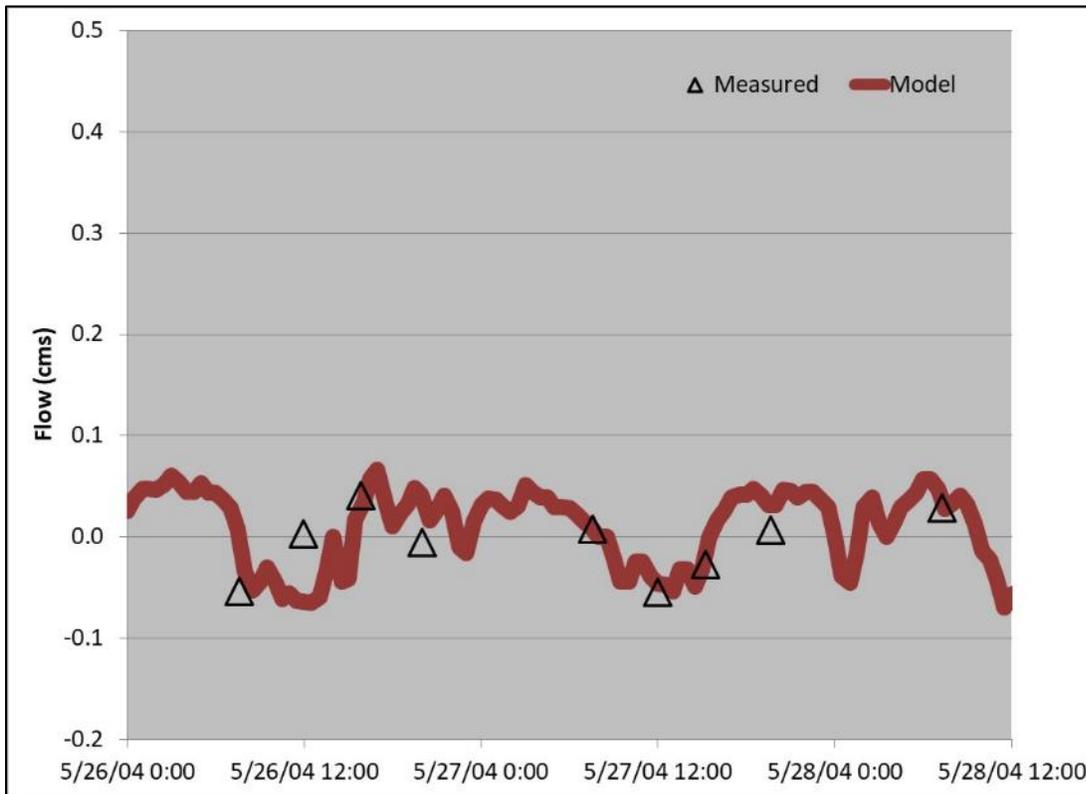


Figure E-26 Flow calibration at station HG (Hudson Gully)

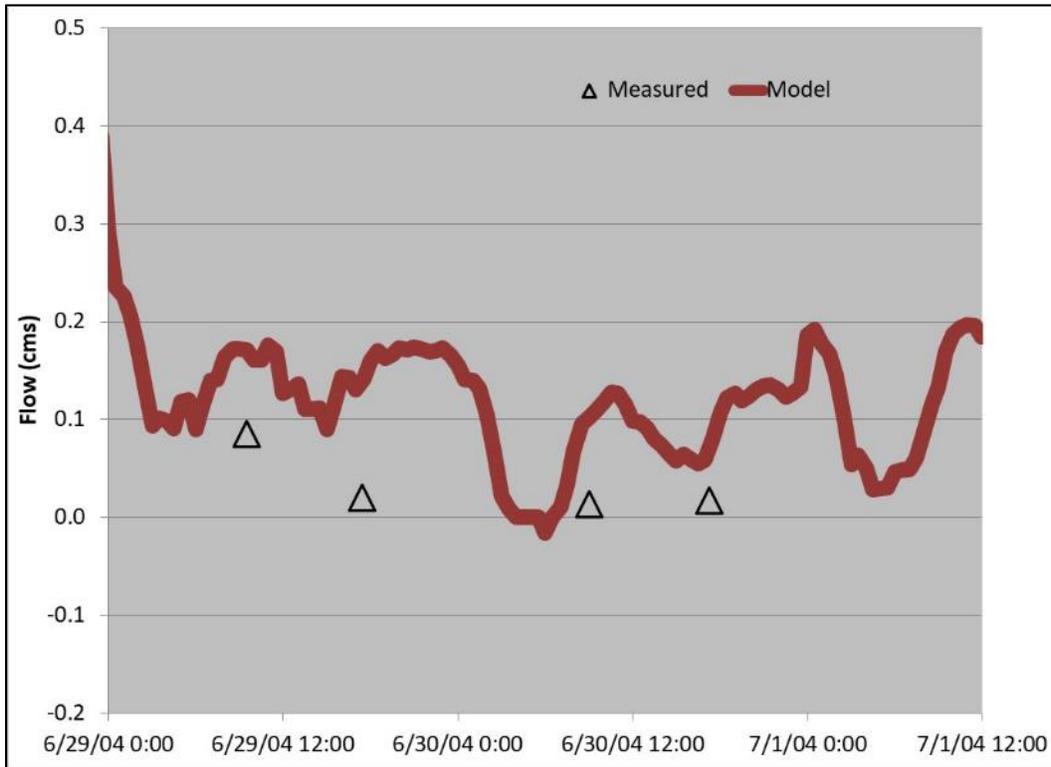


Figure E-27 Flow validation at station HG (Hudson Gully)

Appendix F Goodness-of-fit for the Cow Bayou RMA2 Hydrodynamic Model

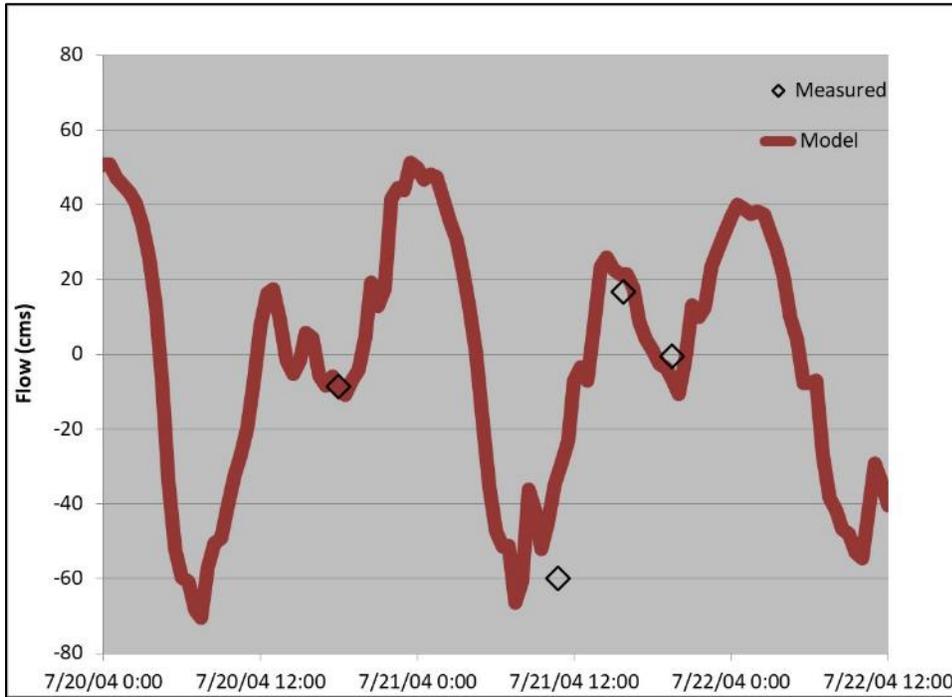


Figure F-1 Flow calibration at Station CB0.5

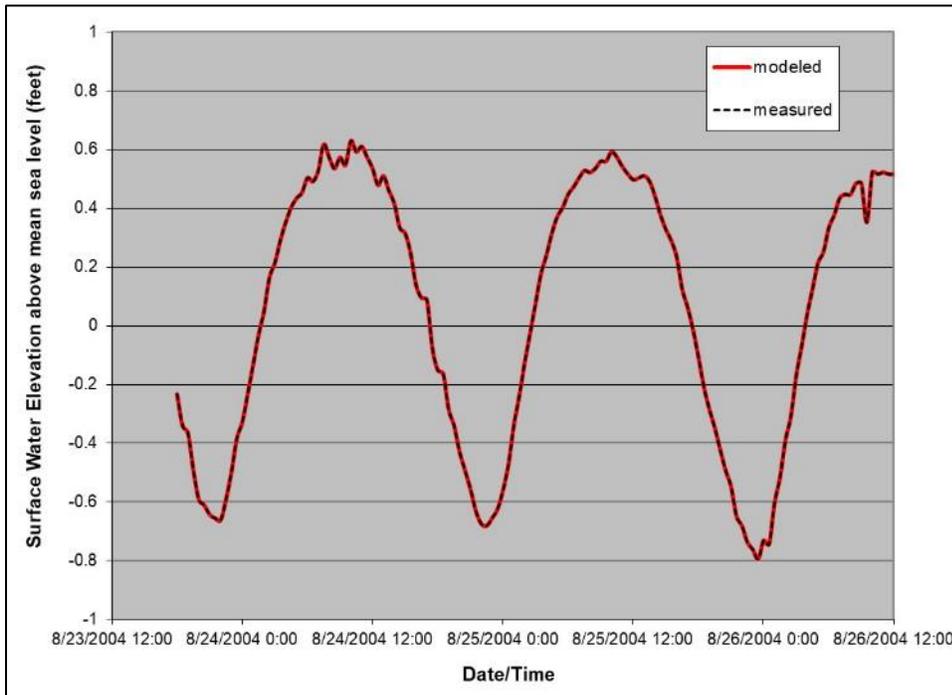


Figure F-2 Water level validation at Station CB0.5

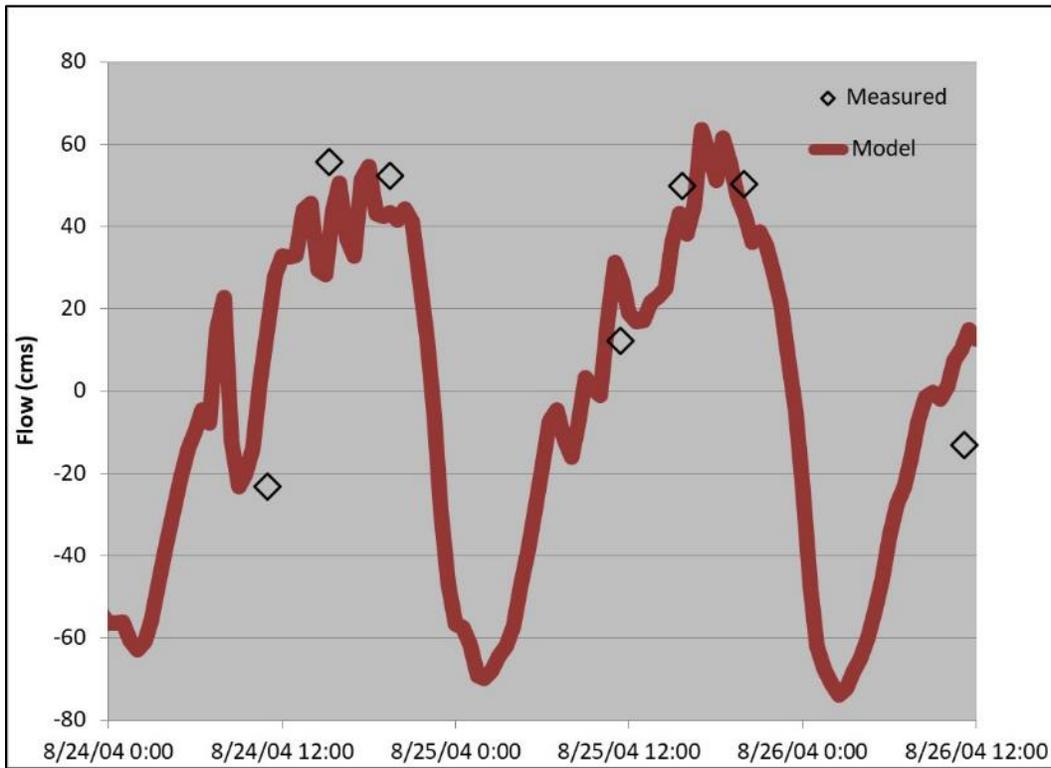


Figure F-3 Flow validation at Station CB0.5

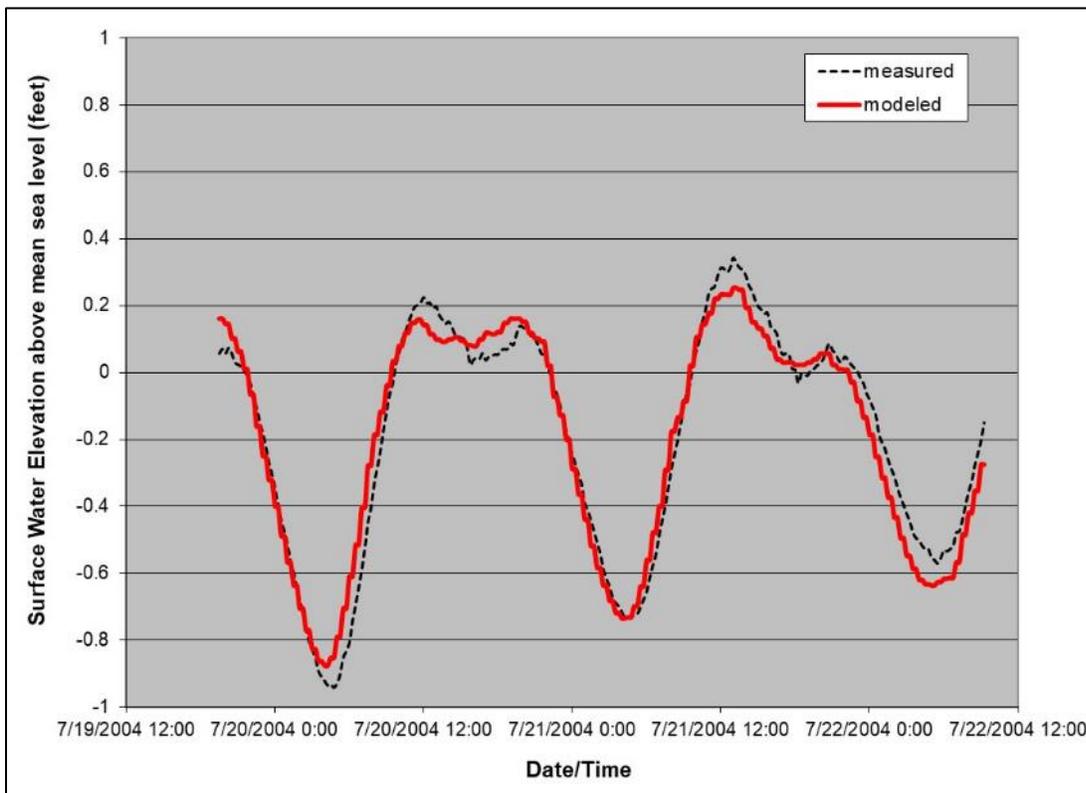


Figure F-4 Water level calibration at Station CB1

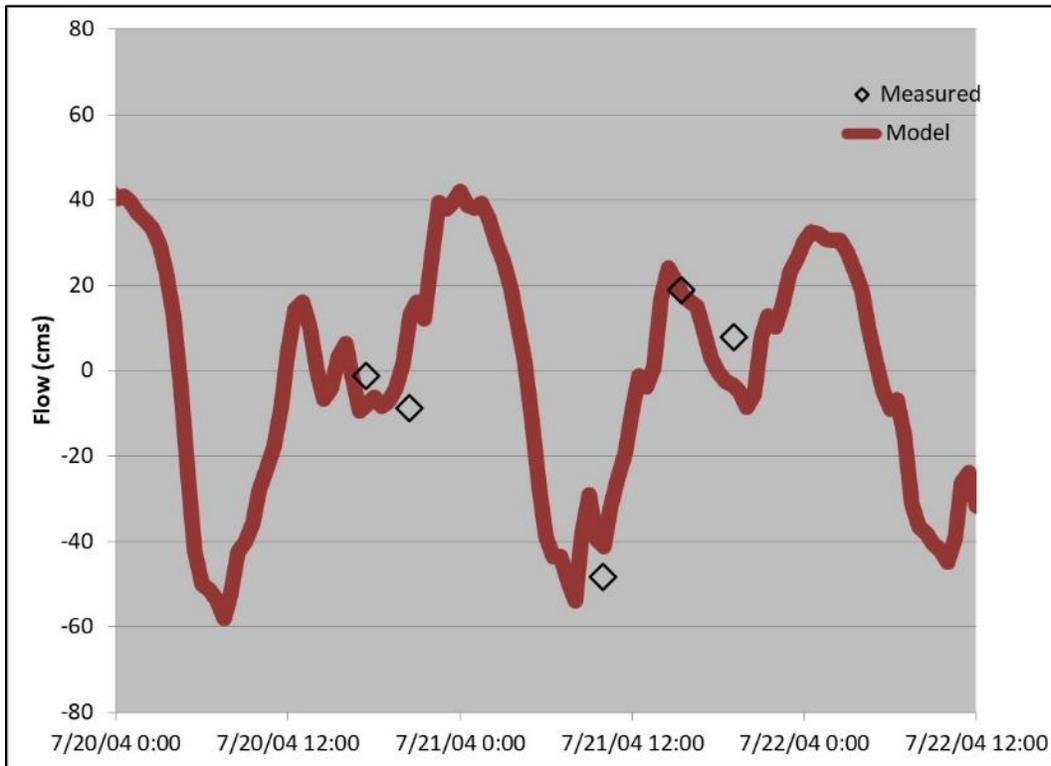


Figure F-5 Flow calibration at station CB1

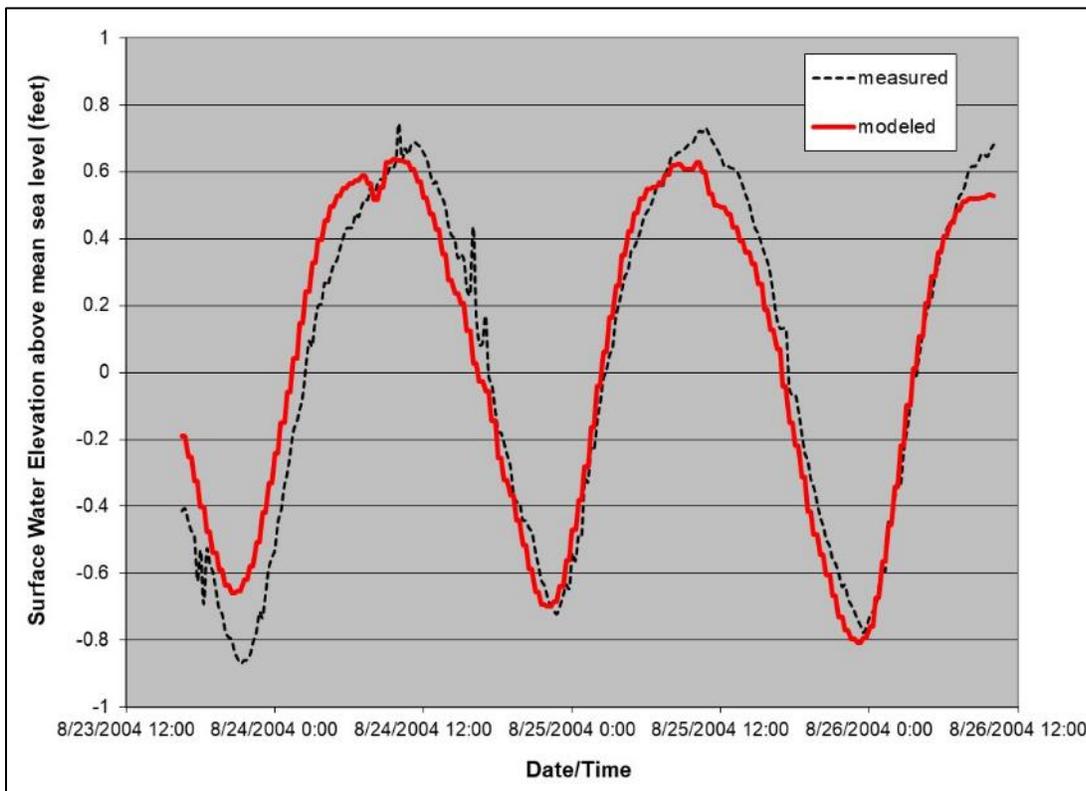


Figure F-6 Water level Validation at station CB1

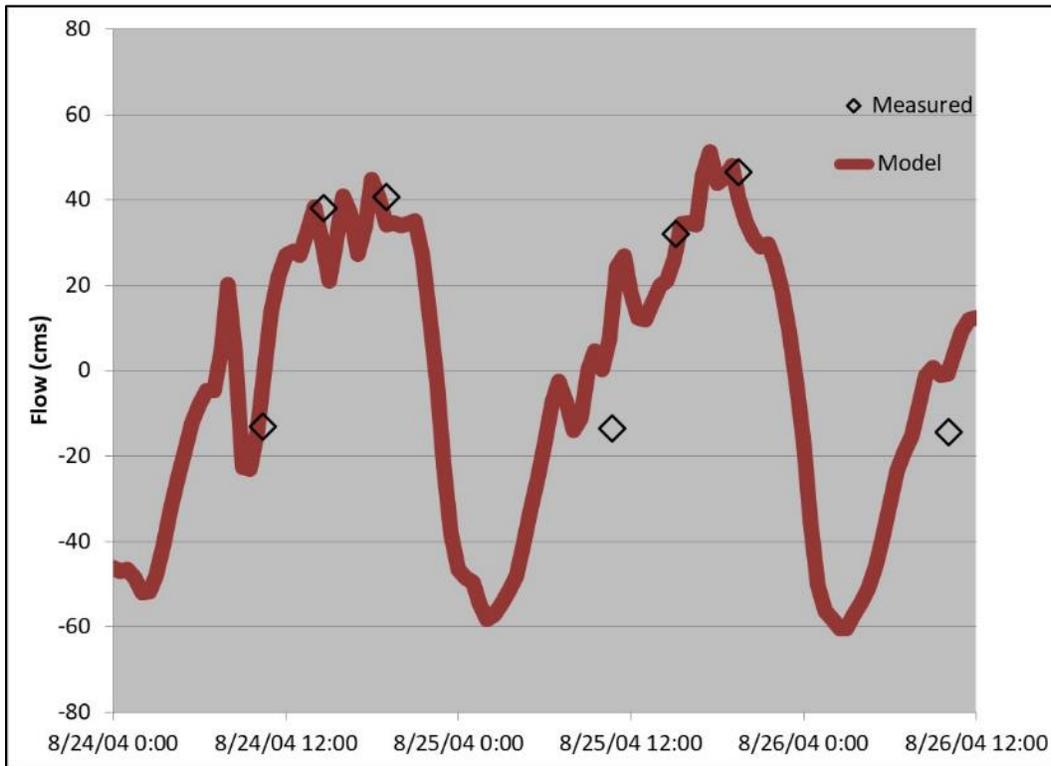


Figure F-7 Flow validation at station CB1

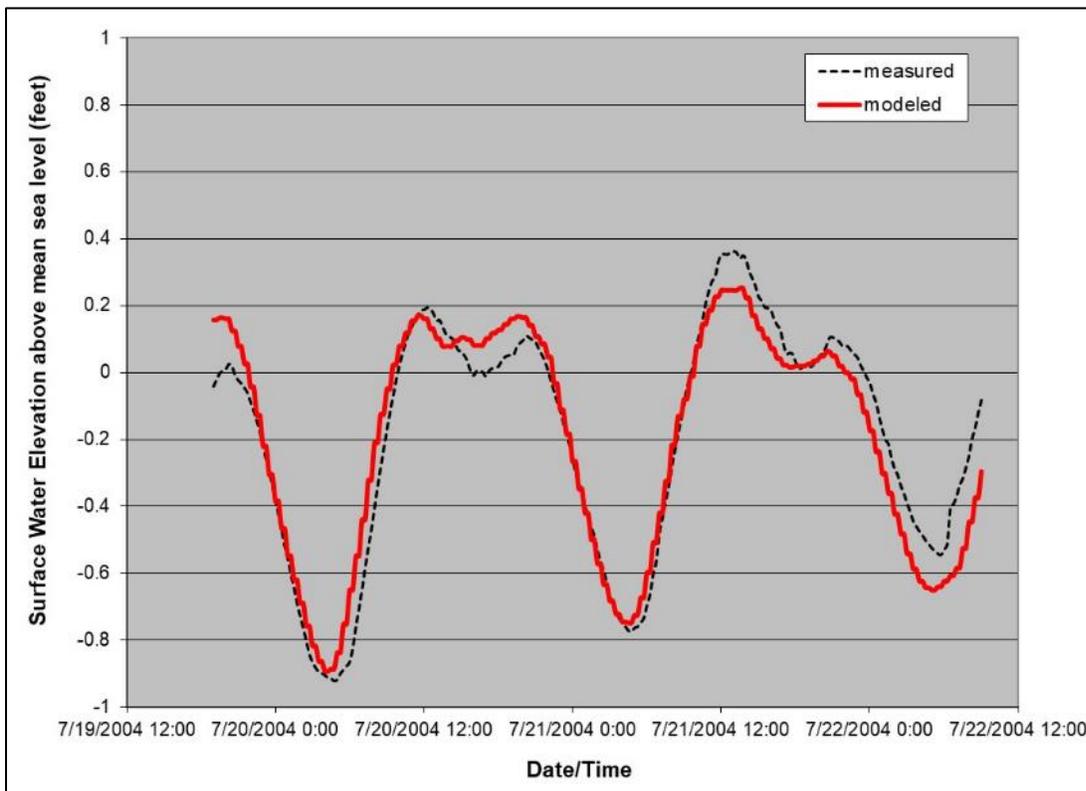


Figure F-8 Water level calibration at station CB2

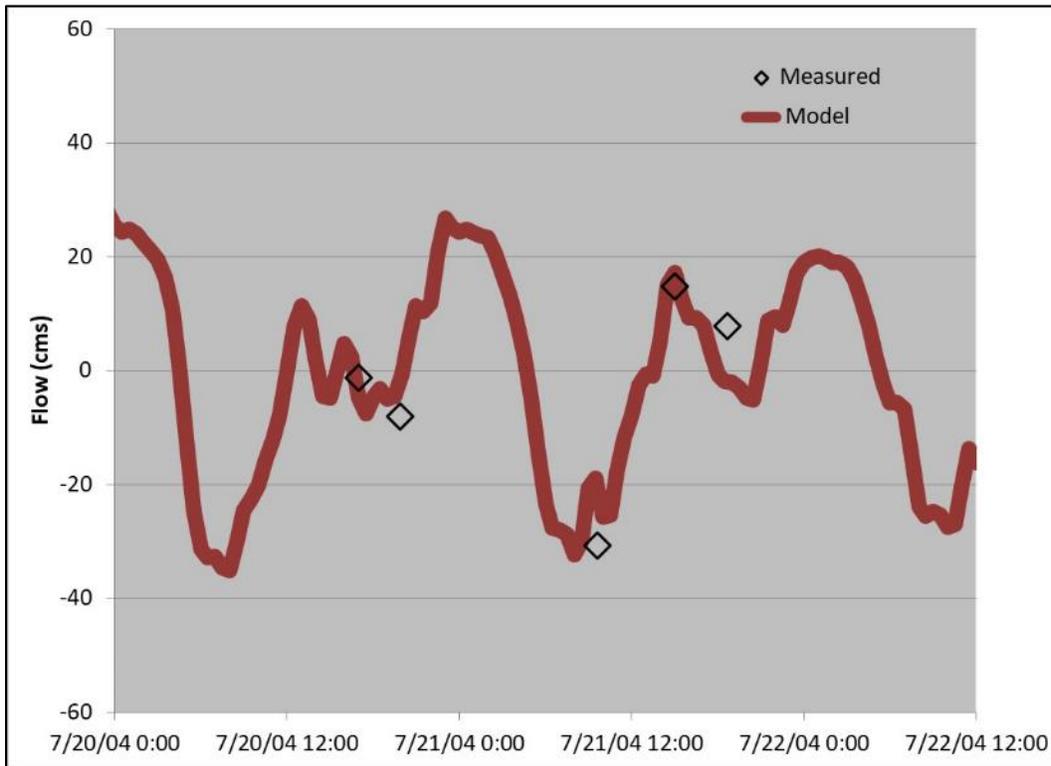


Figure F-9 Flow calibration at station CB2

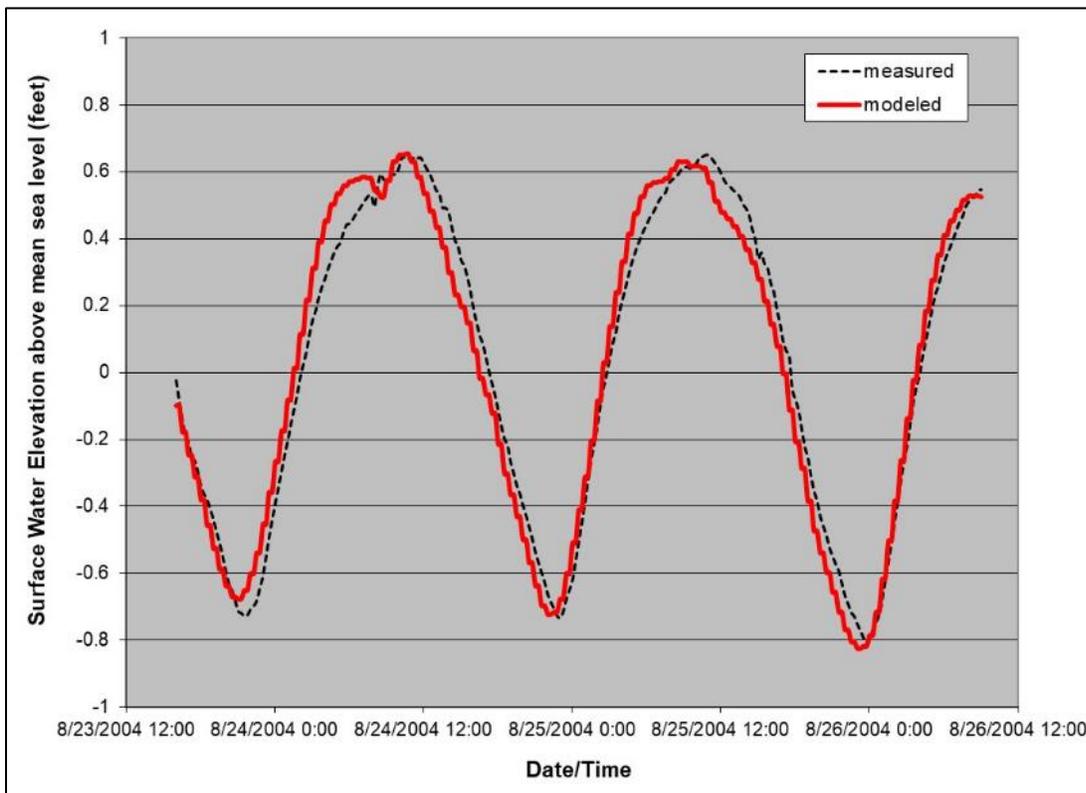


Figure F-10 Water level validation at station CB2

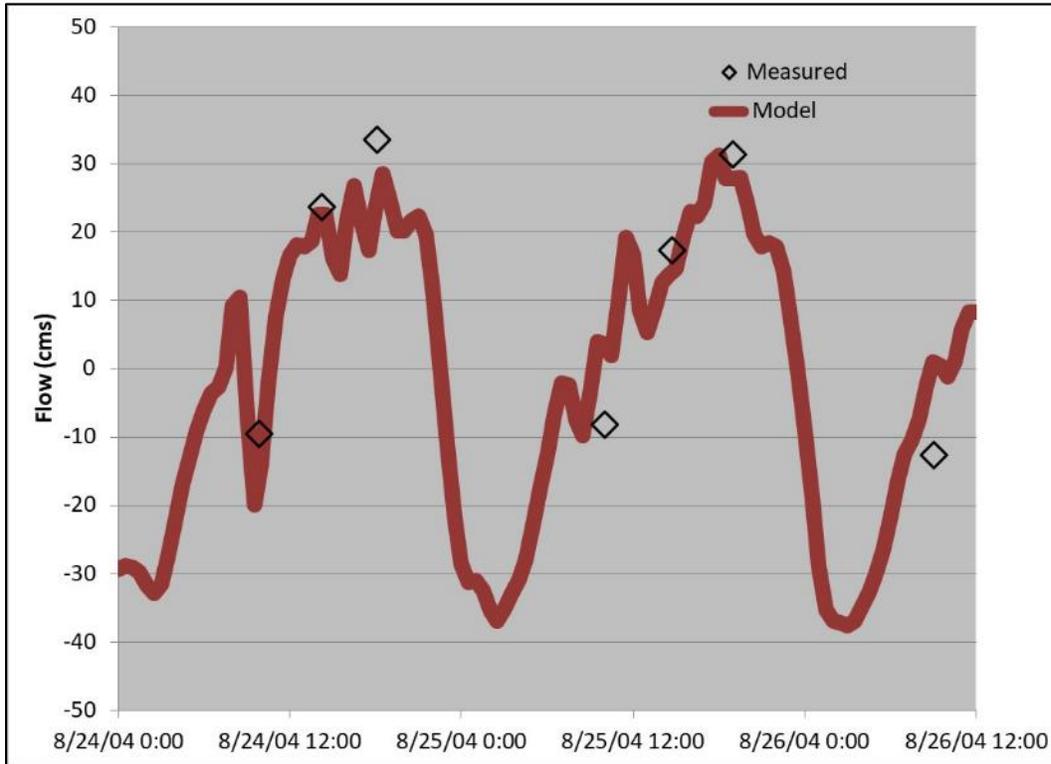


Figure F-11 Flow validation at station CB2

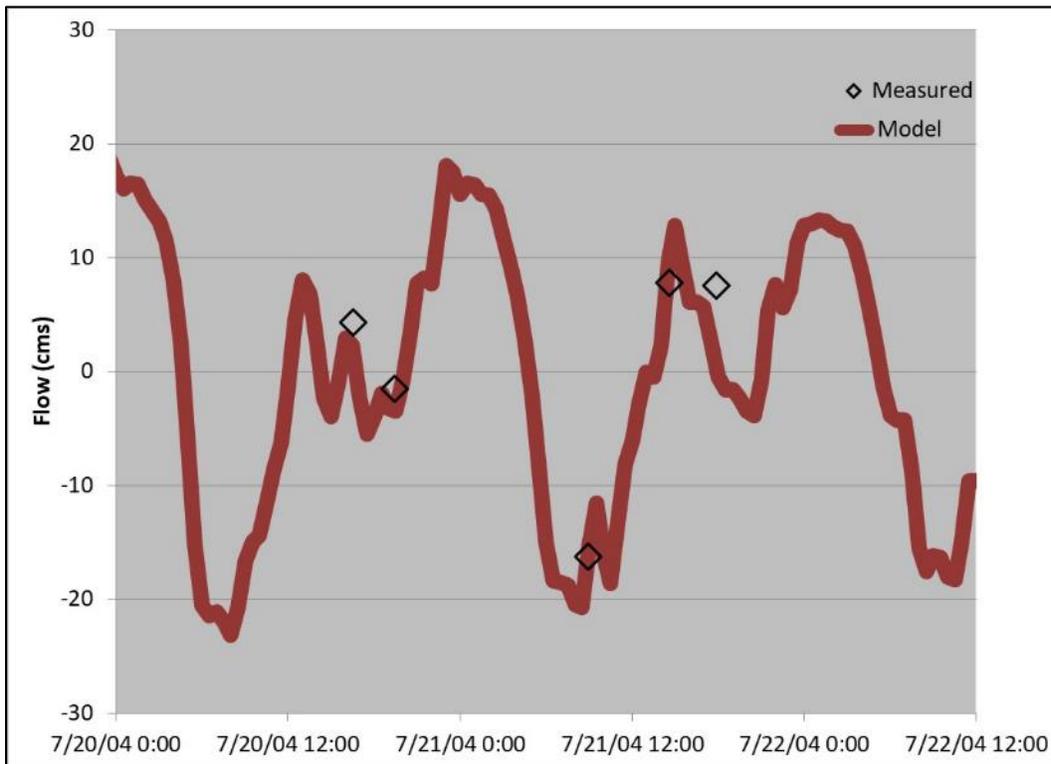


Figure F-12 Flow calibration at station CB2.5

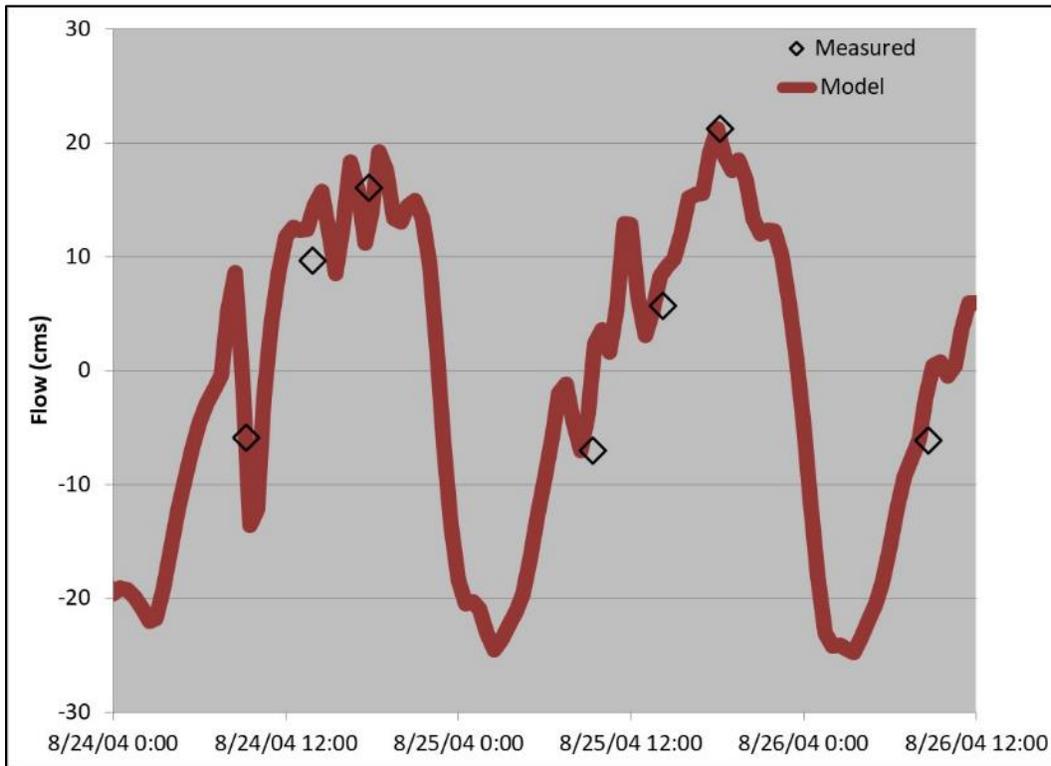


Figure F-13 Flow validation at station CB2.5

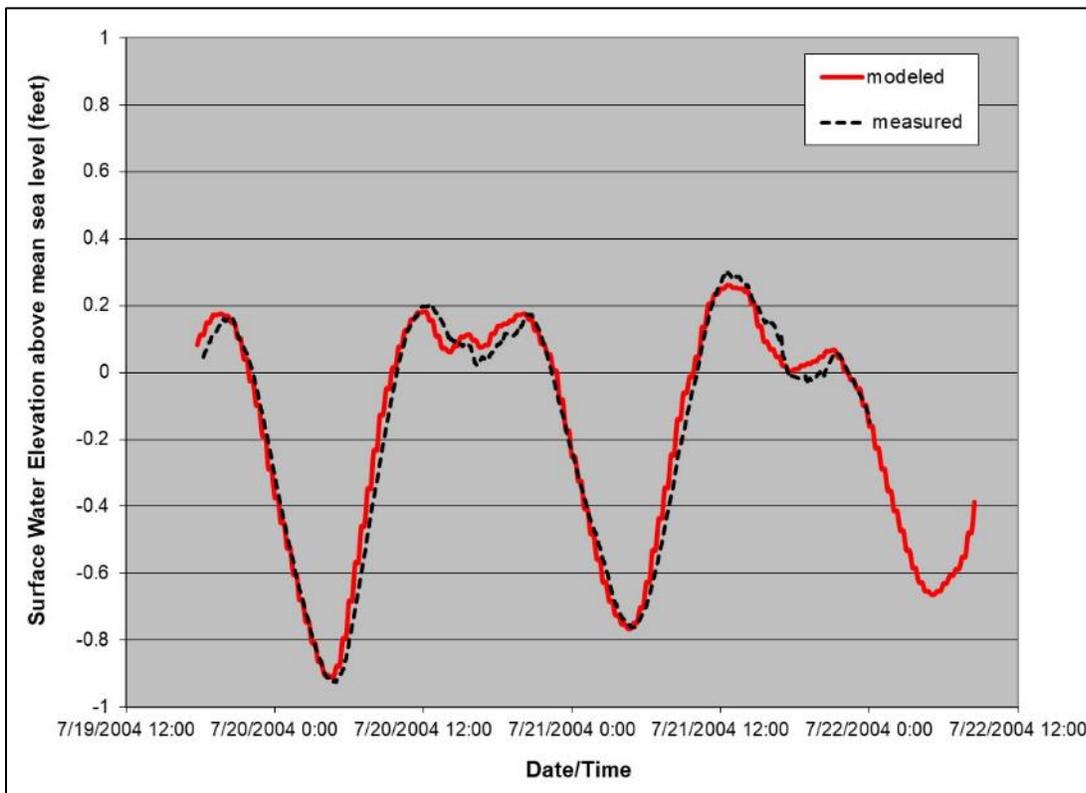


Figure F-14 Water level calibration at station CB3

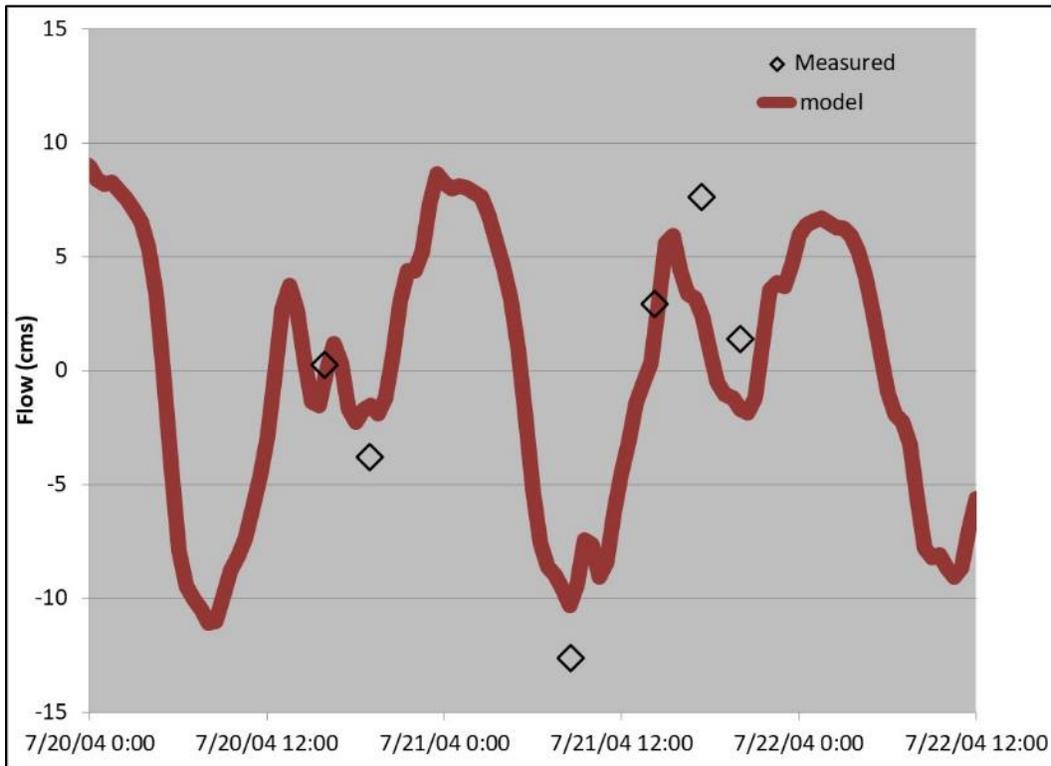


Figure F-15 Flow calibration at station CB3

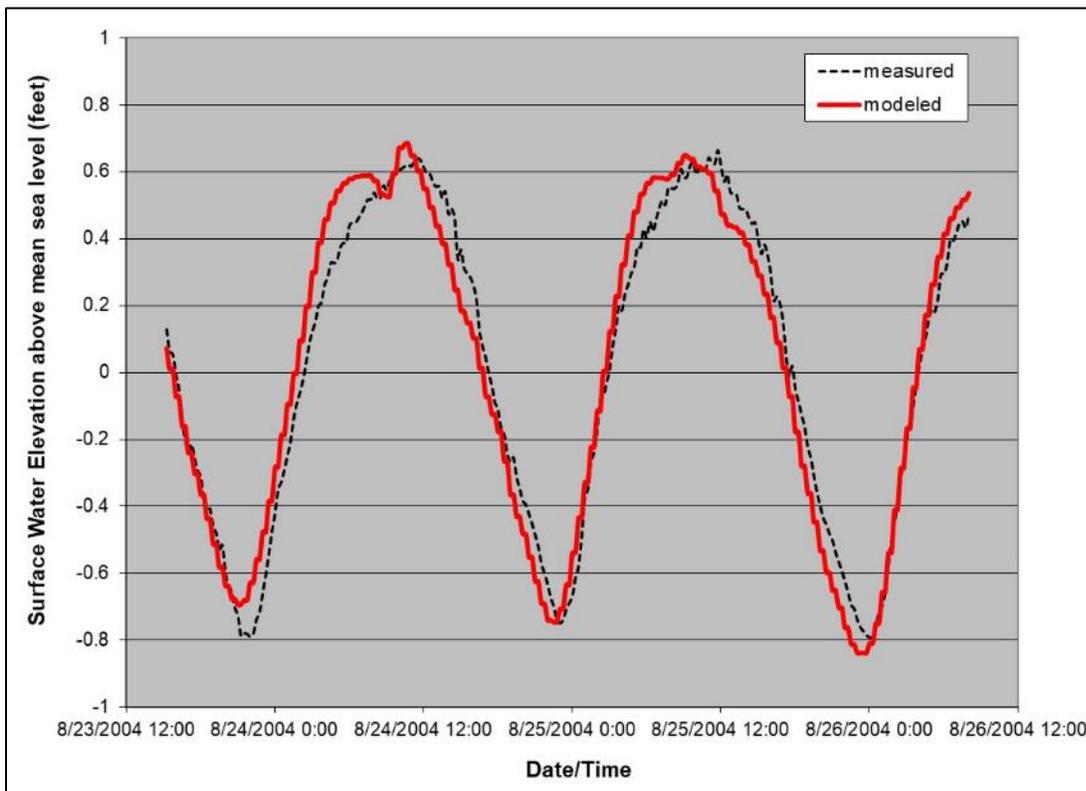


Figure F-16 Water level validation at station CB3

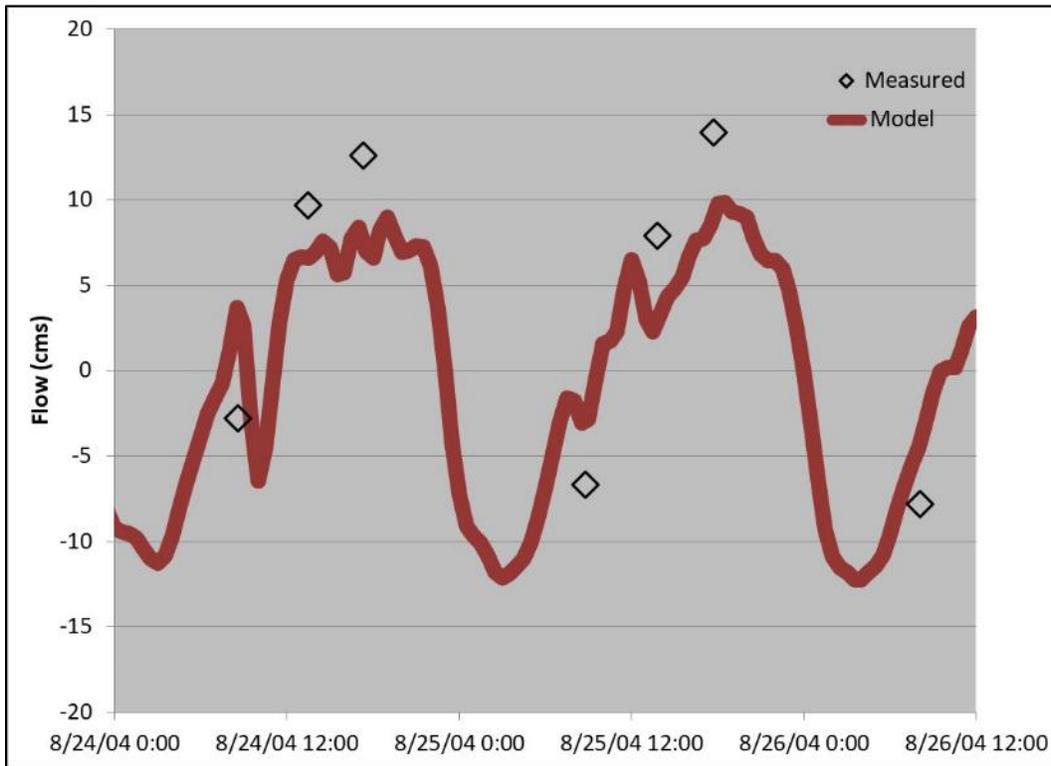


Figure F-17 Flow validation at station CB3

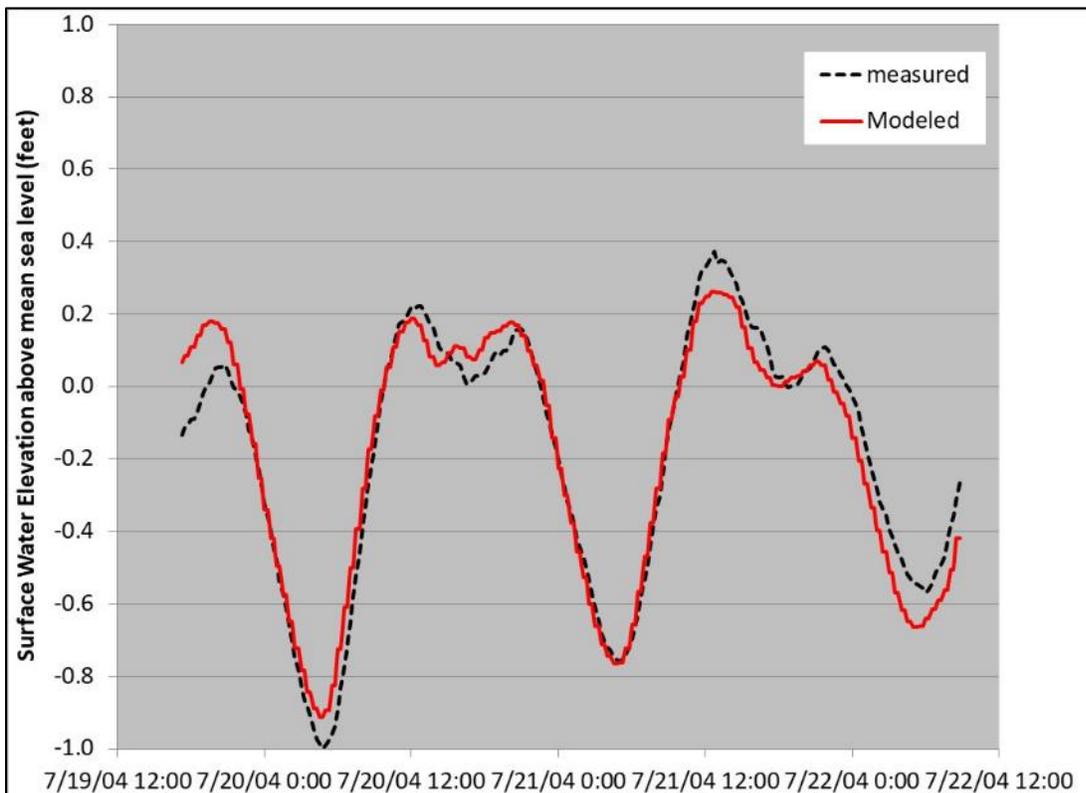


Figure F-18 Water level calibration at station CB3.5

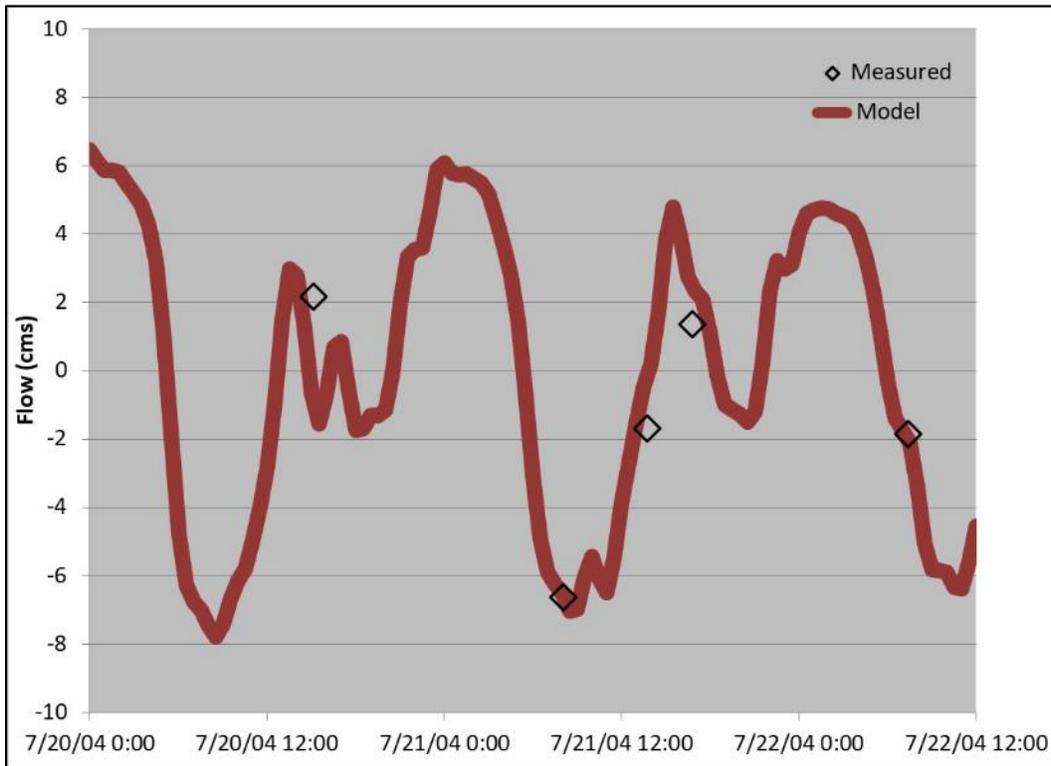


Figure F-19 Flow calibration at station CB3.5

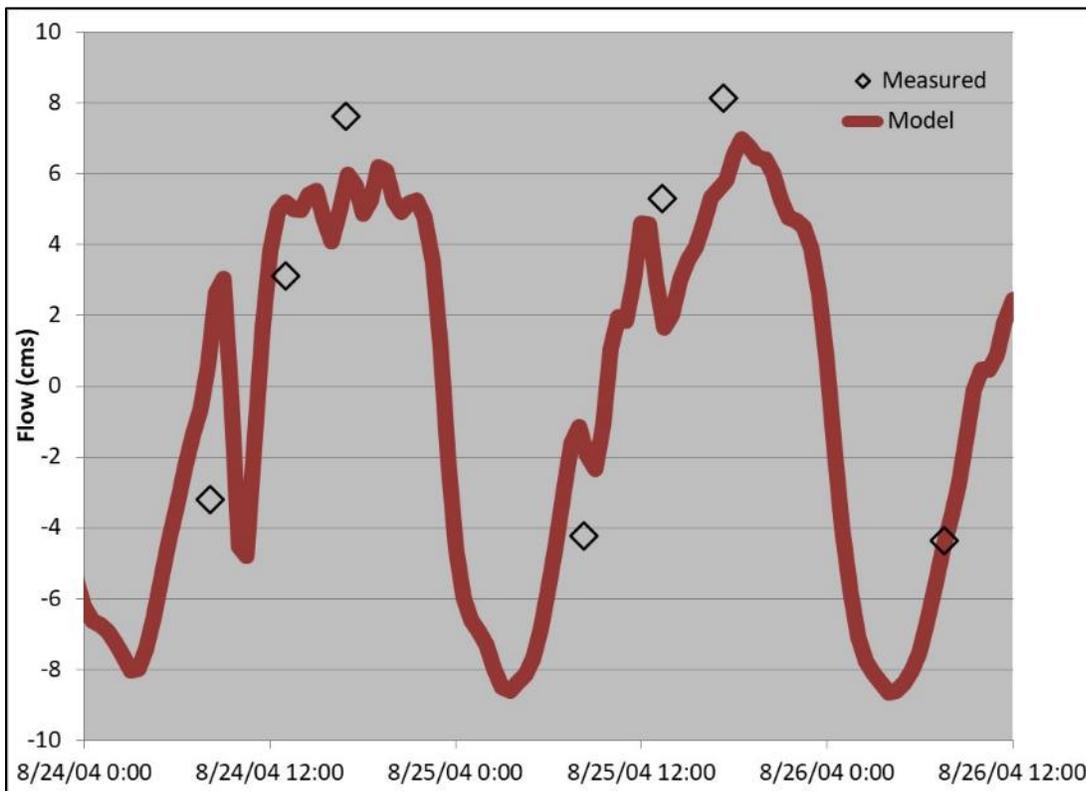


Figure F-20 Flow validation at station CB3.5

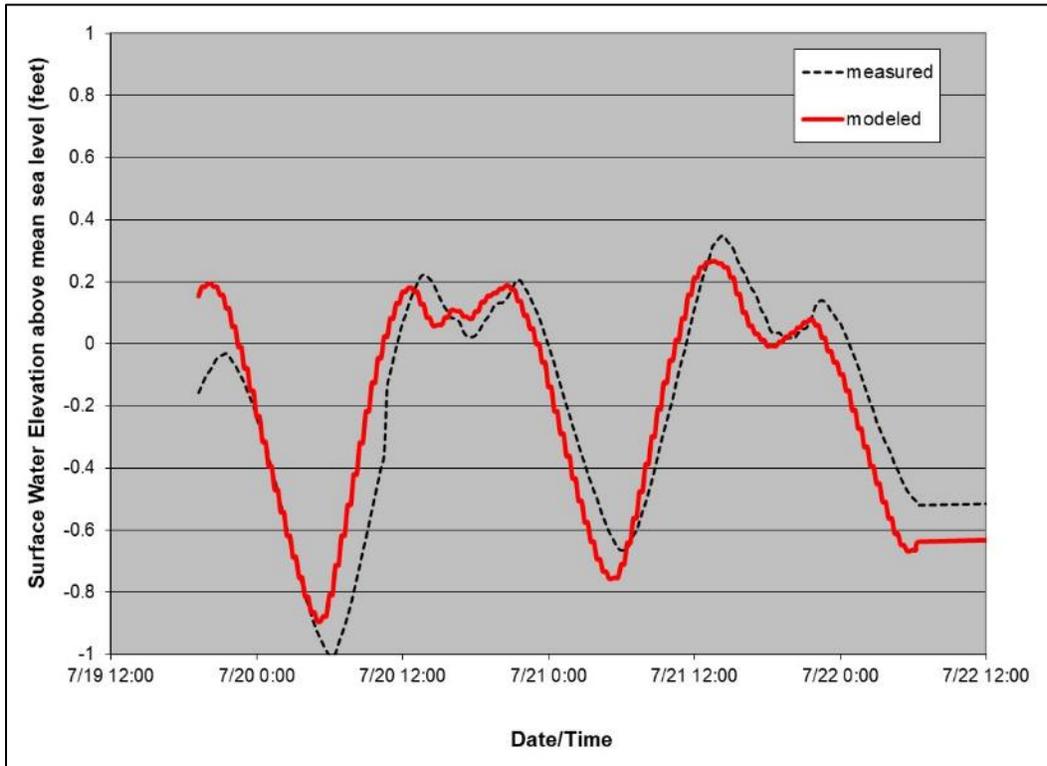


Figure F-21 Water level calibration at station CB4

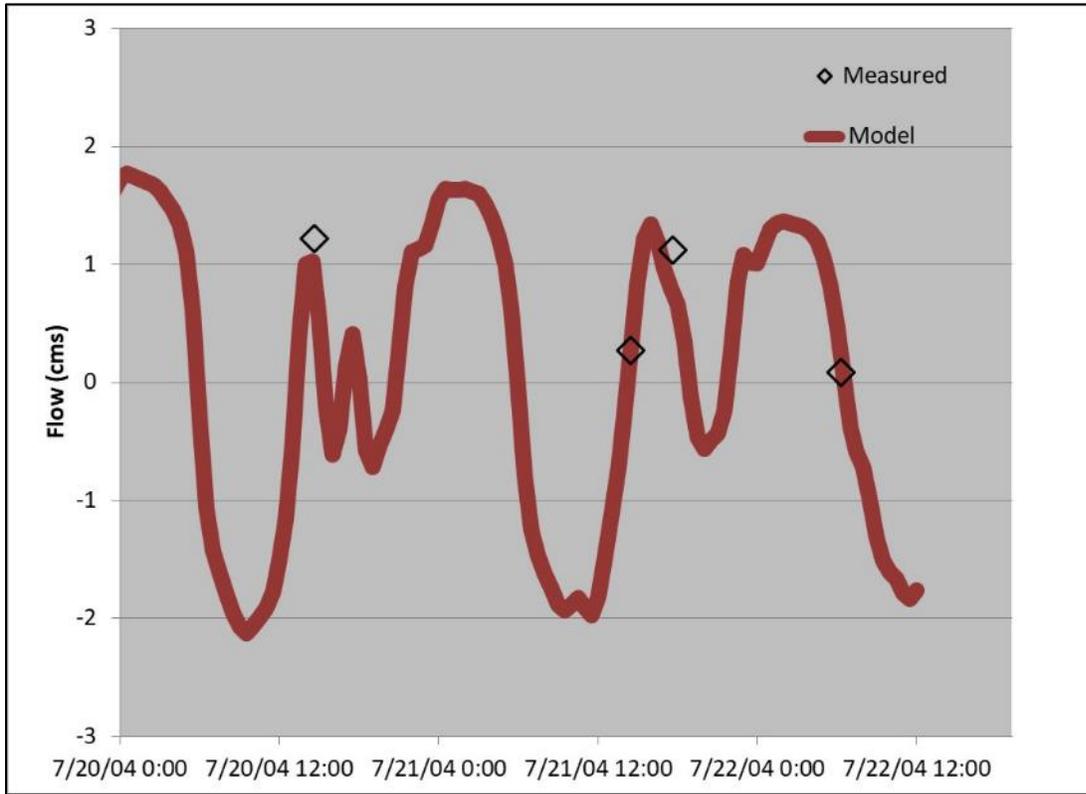


Figure F-22 Flow calibration at station CB4

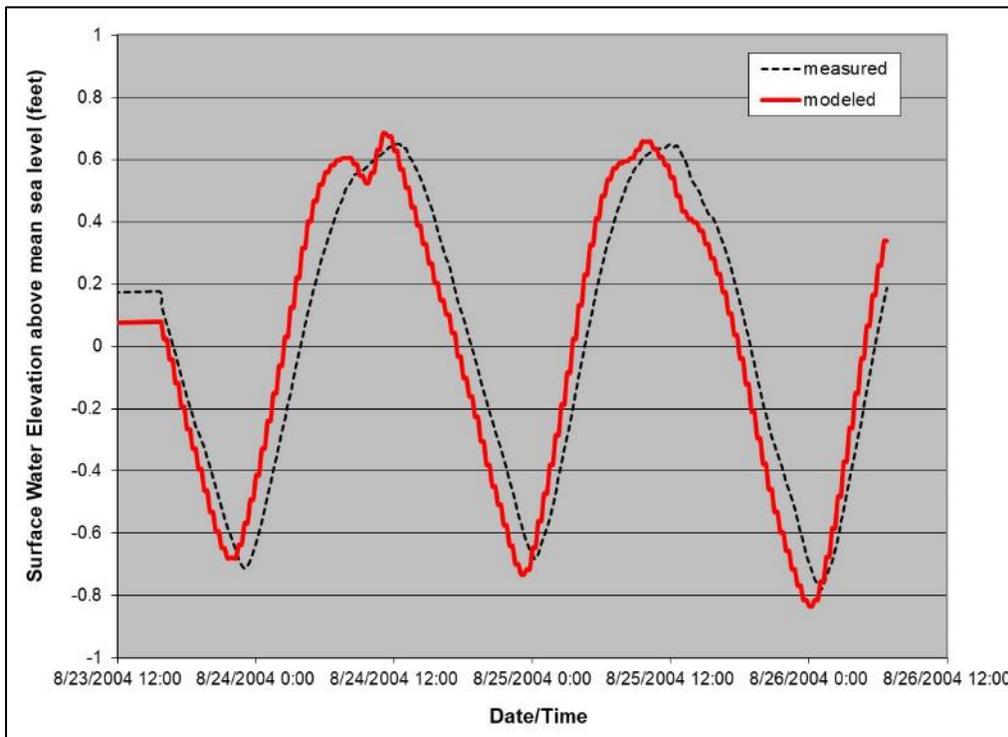


Figure F-23 Water level validation at station CB4

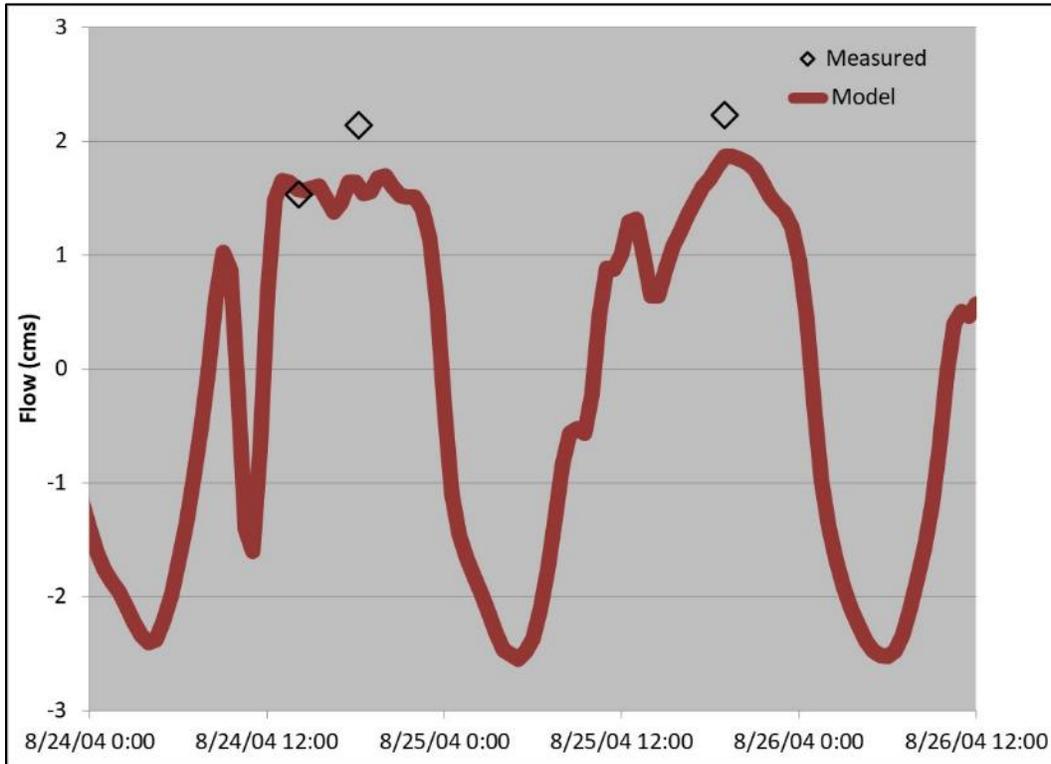


Figure F-24 Flow validation at station CB4

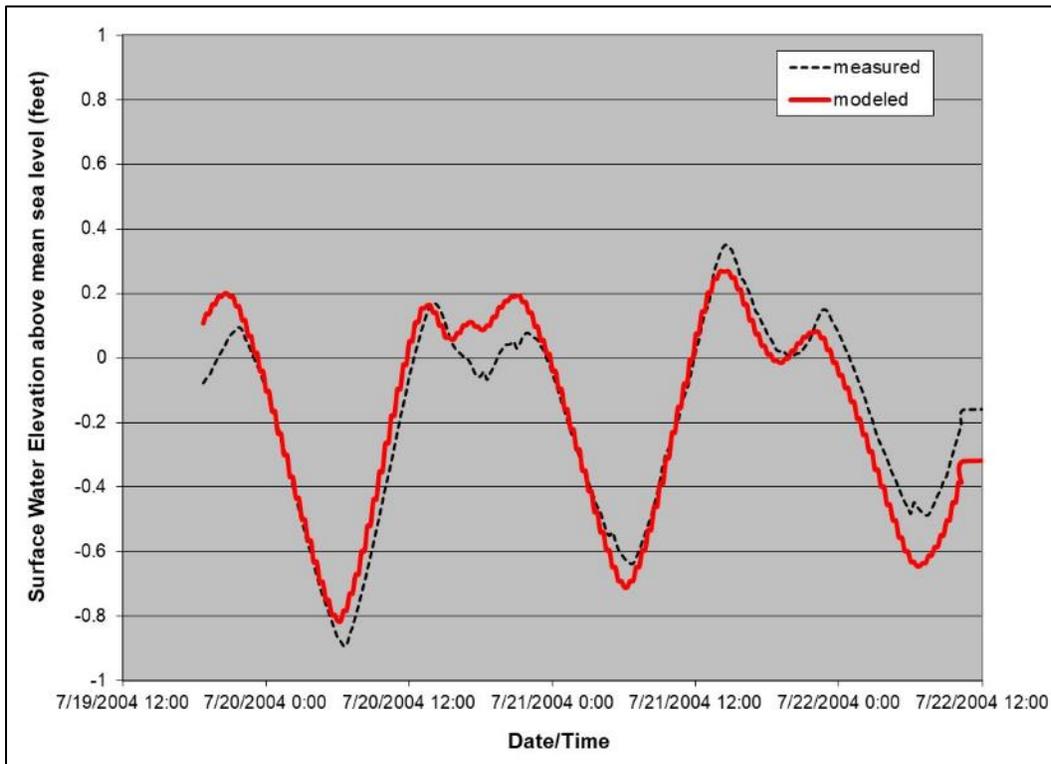


Figure F-25 Water level calibration at station CB5

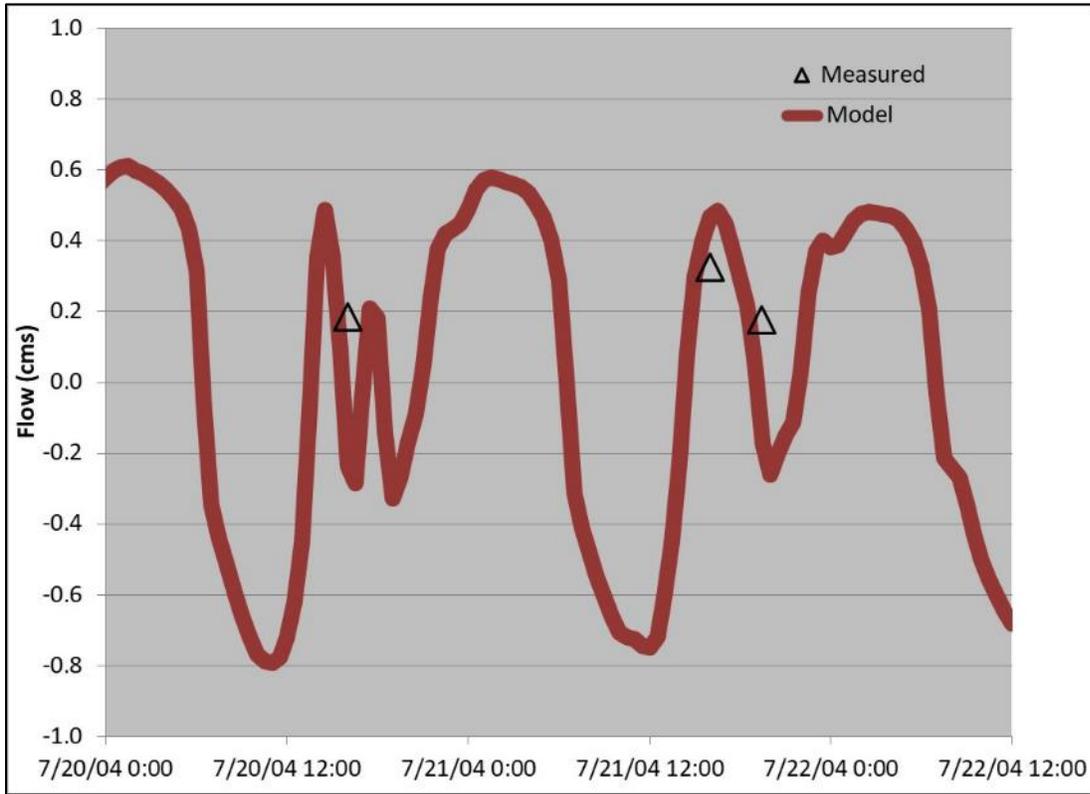


Figure F-26 Flow calibration at station CB5

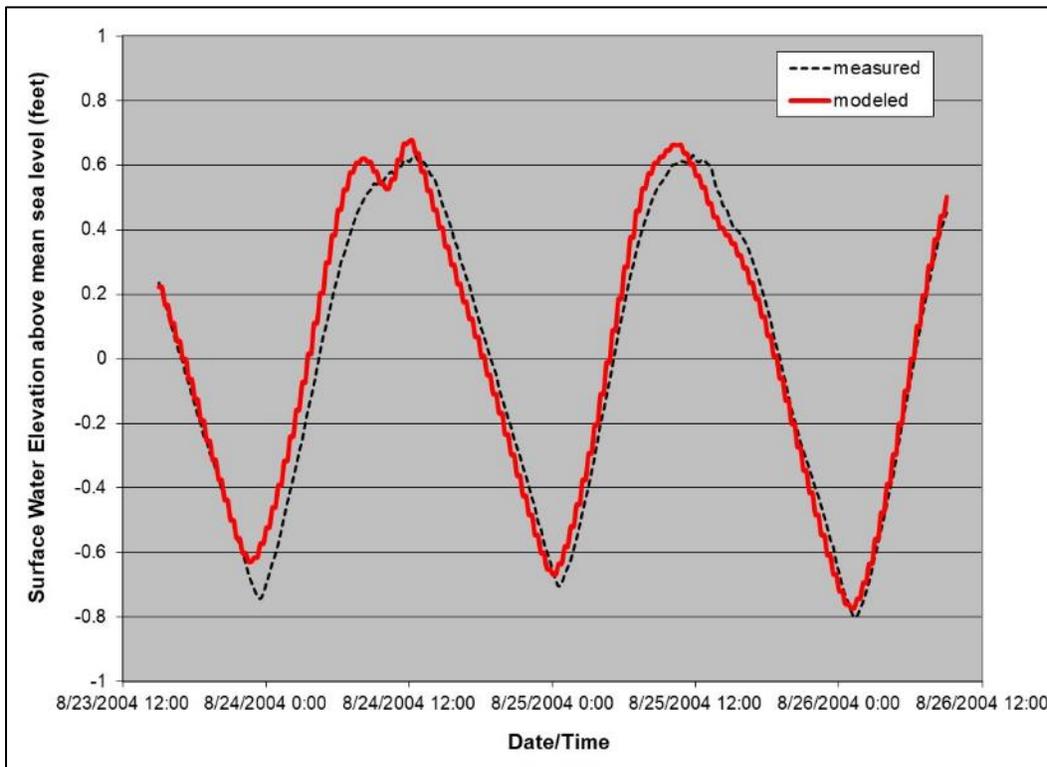


Figure F-27 Water level validation at station CB5

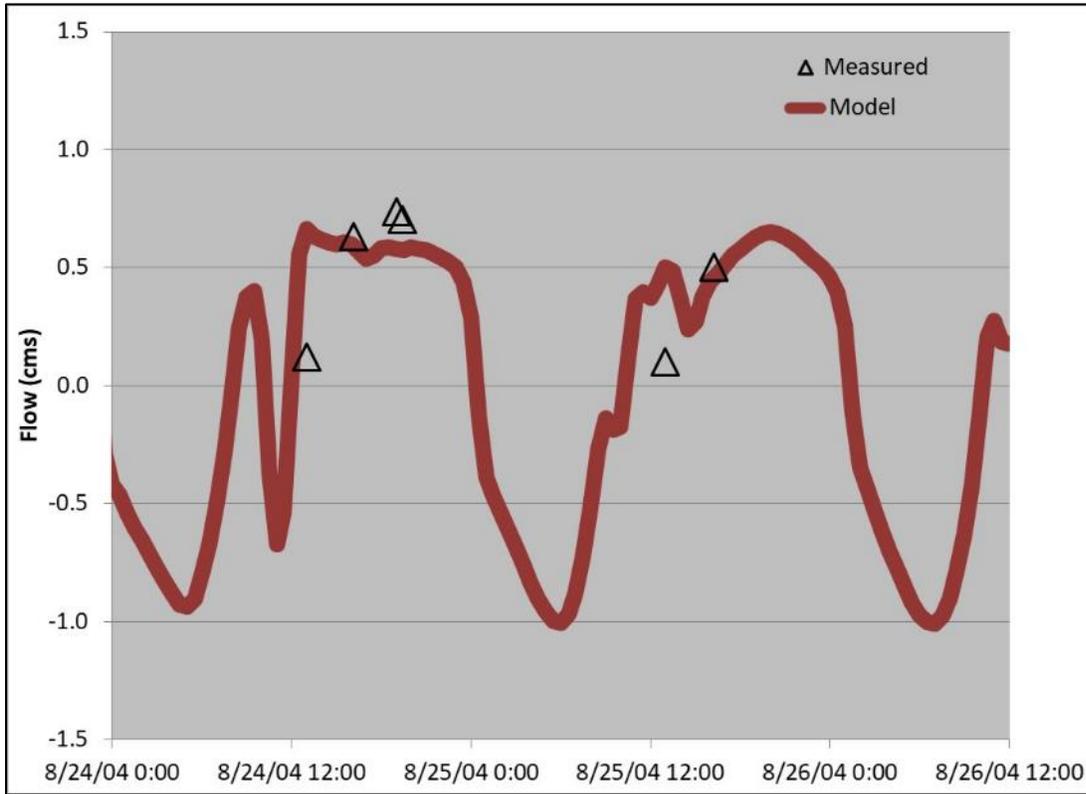


Figure F-28 Flow validation at station CB5

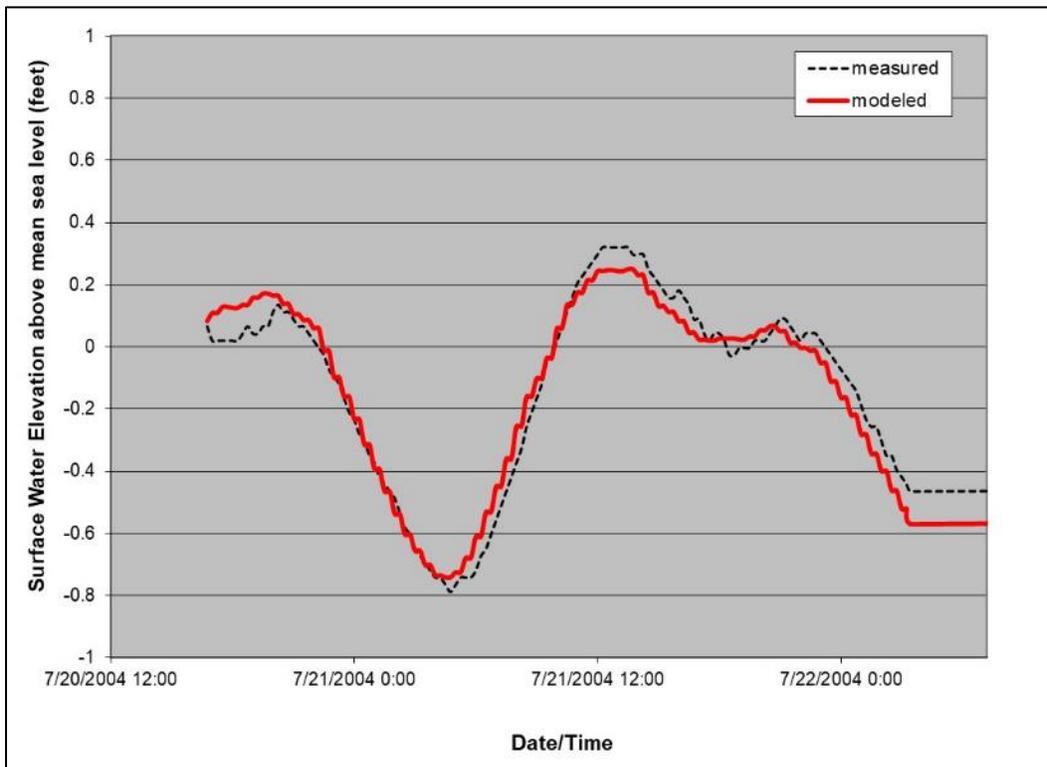


Figure F-29 Water level calibration at station CNB (Coon Bayou)

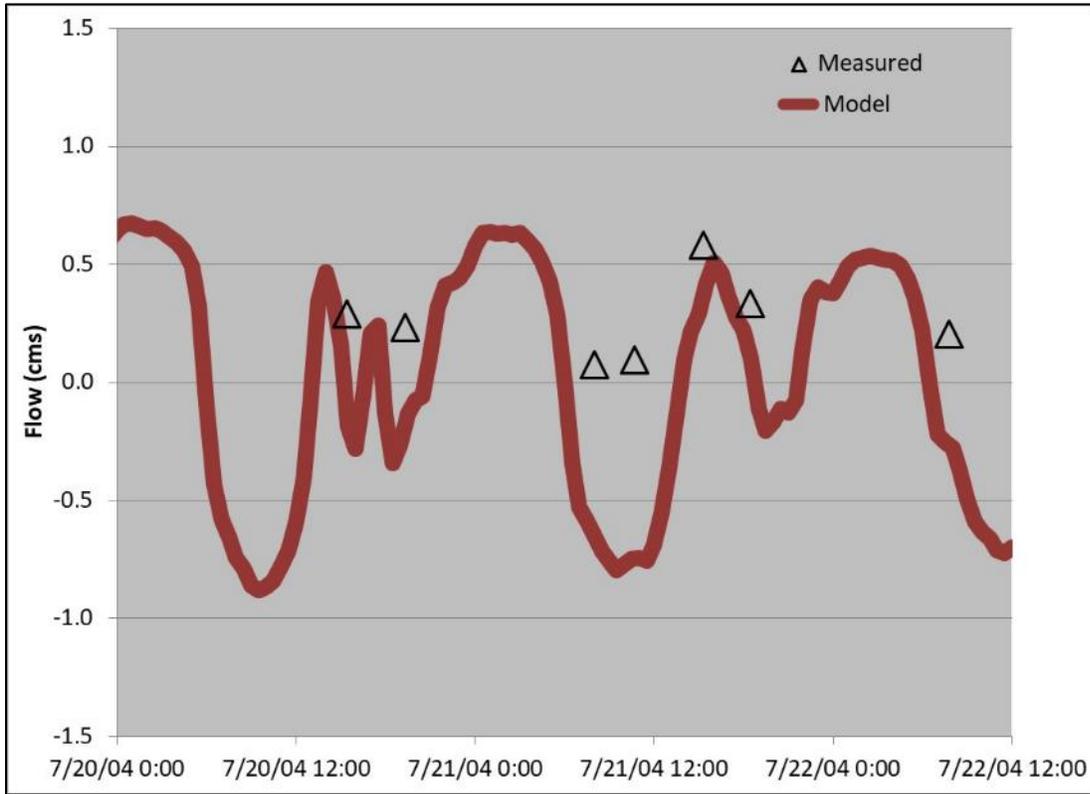


Figure F-30 Flow calibration at station CNB (Coon Bayou)

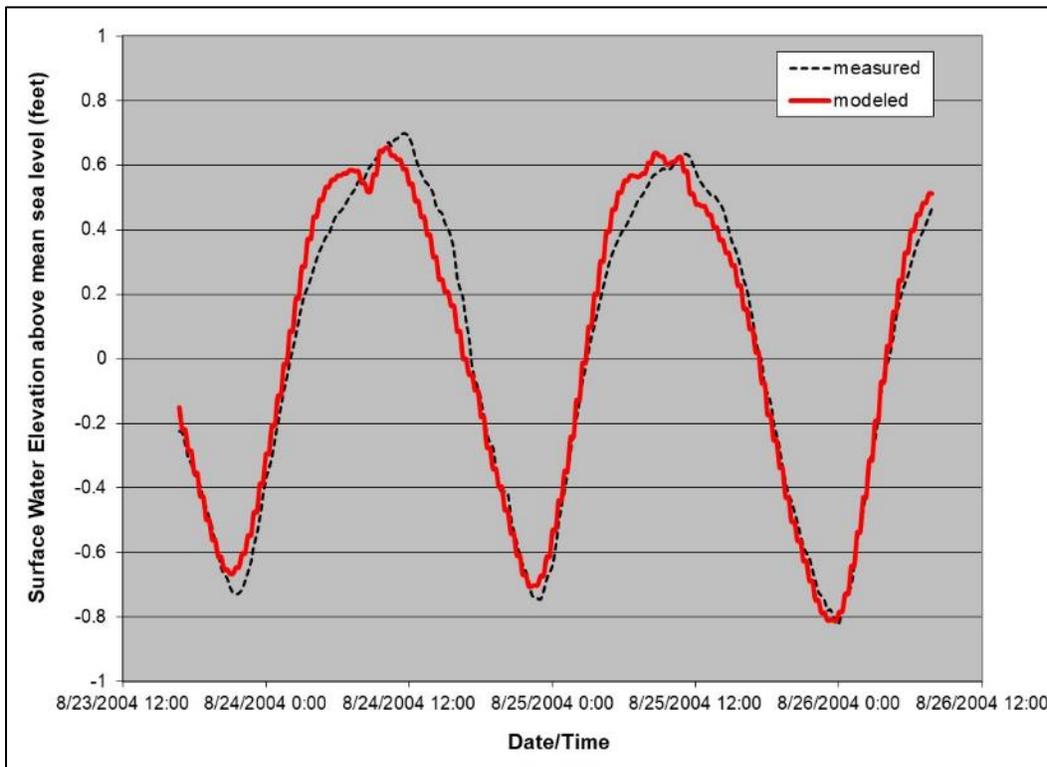


Figure F-31 Water level validation at station CNB (Coon Bayou)

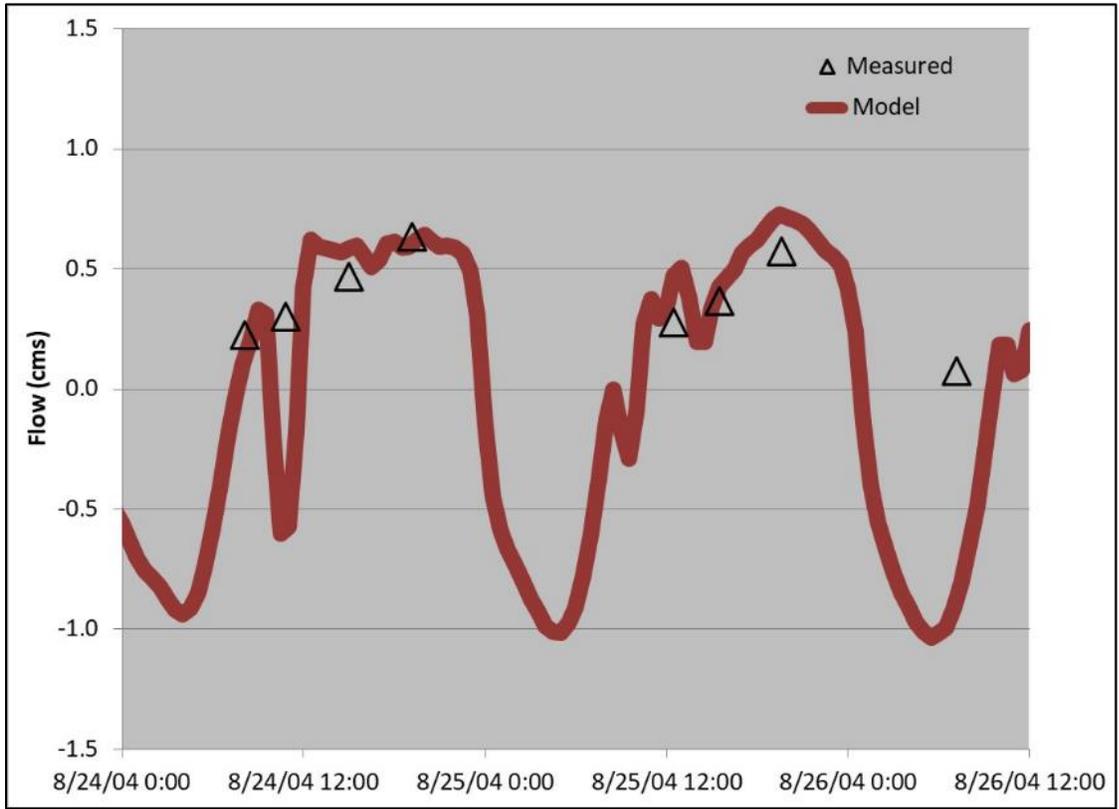


Figure F-32 Flow validation at station CNB (Coon Bayou)

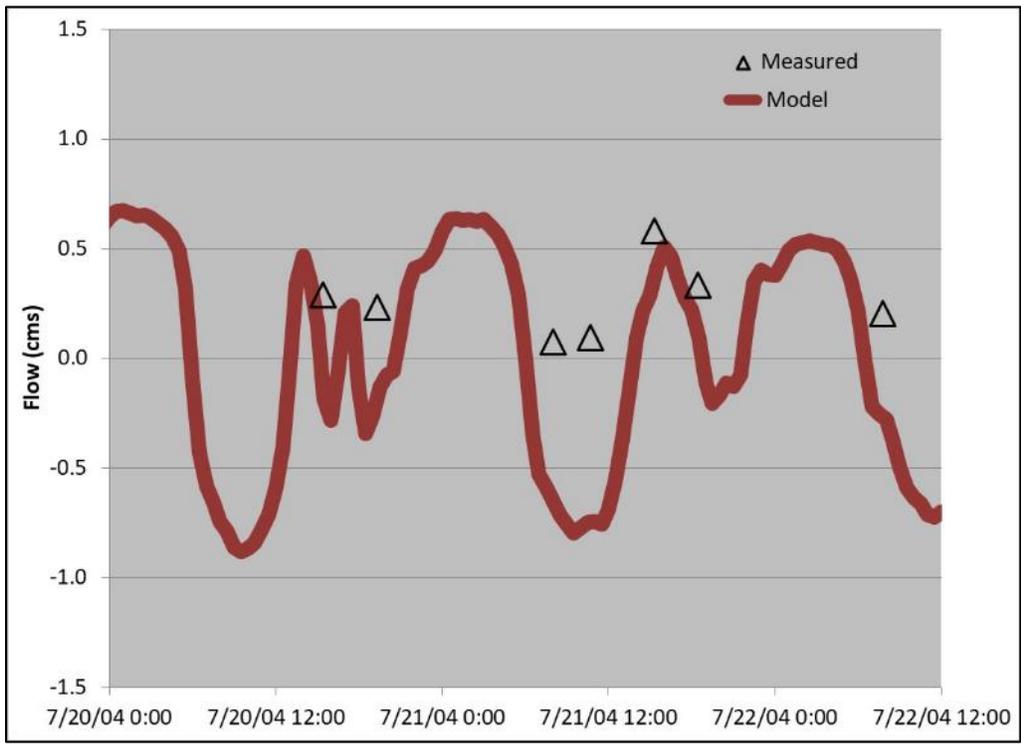


Figure F-33 Flow calibration at station TG2 (Terry Gully)

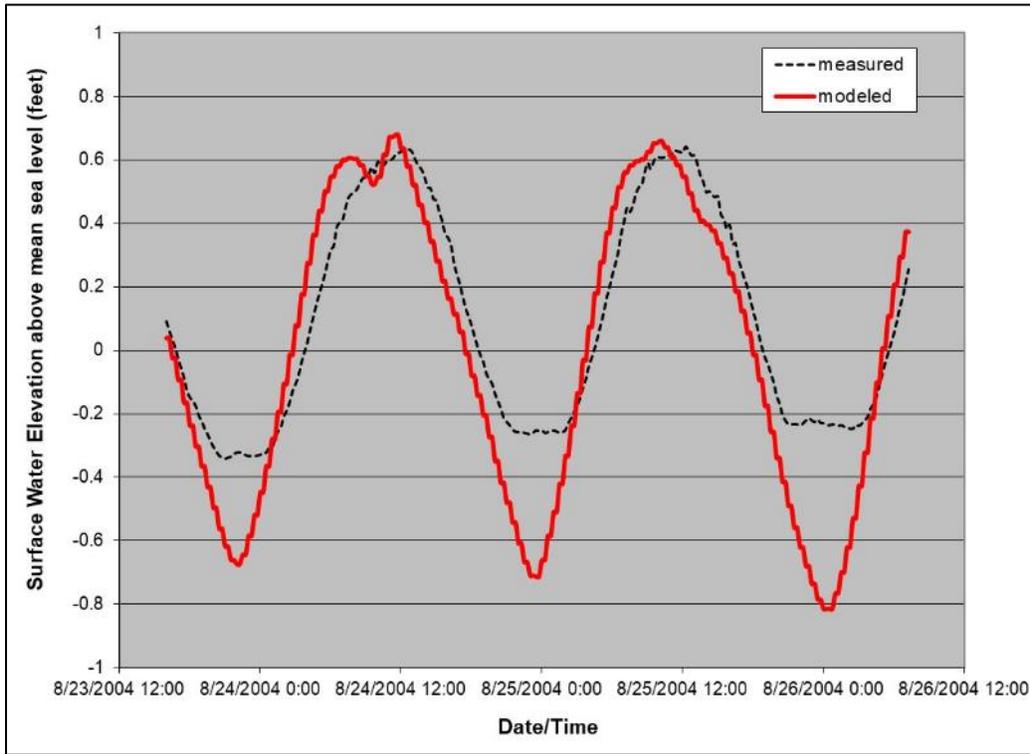


Figure F-34 Water level validation at station TG2 (Terry Gully)

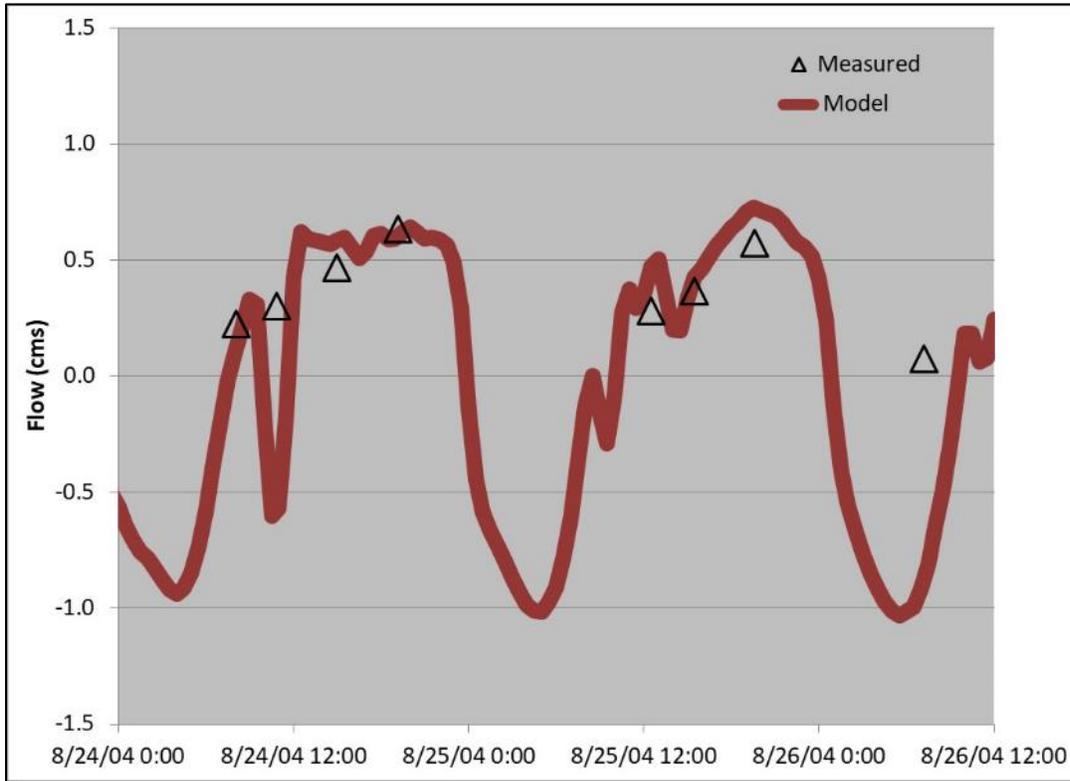


Figure F-35 Flow validation at station TG (Terry Gully)

Appendix G Goodness-of-fit for the Adams Bayou WASP Model

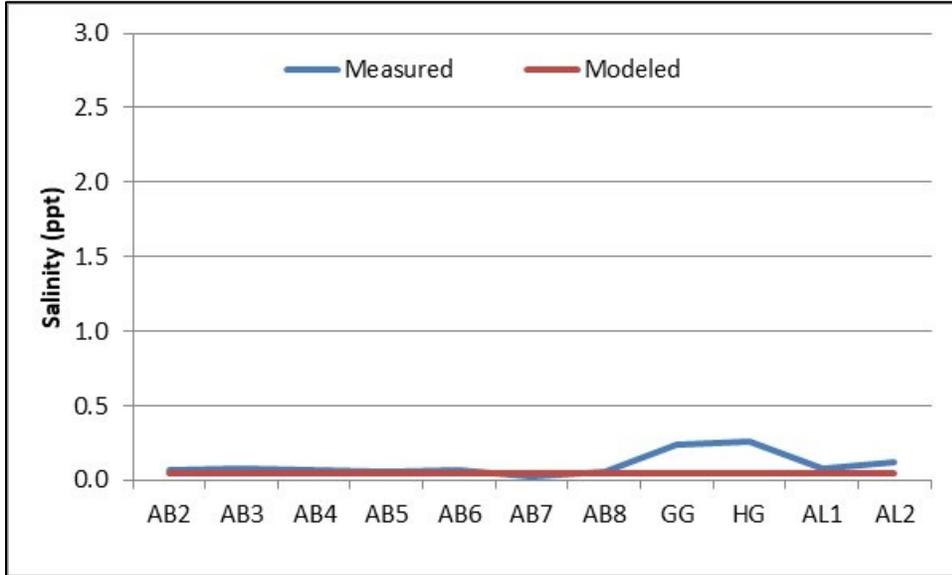


Figure G-1. Calibration of salinity in the Adams Bayou WASP model

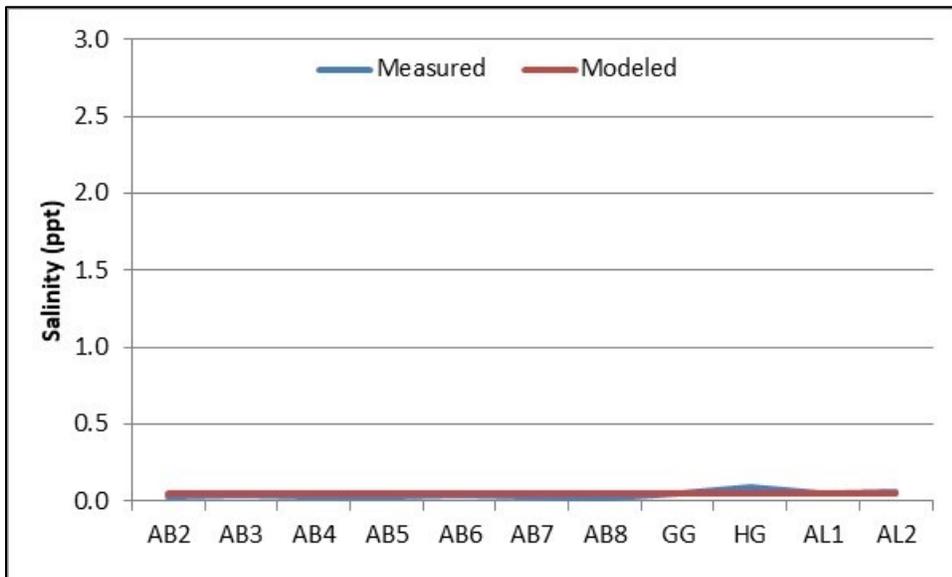


Figure G-2. Validation of salinity in the Adams Bayou WASP model

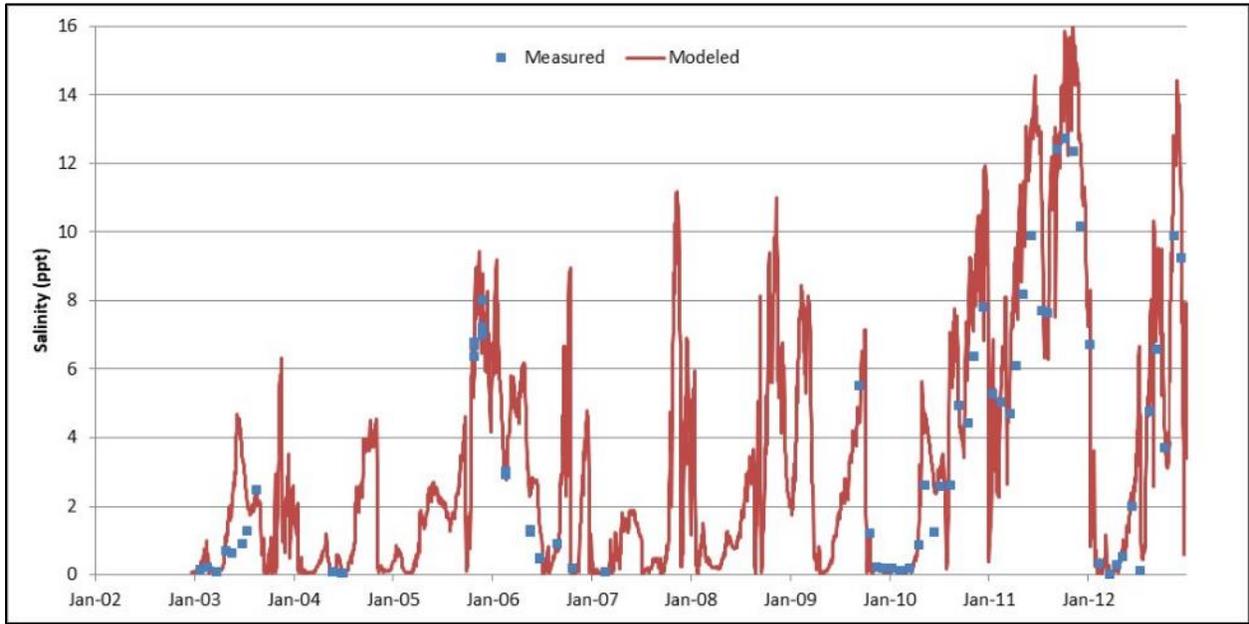


Figure G-3 Long-term validation of salinity calibration at Adams Bayou station AB2

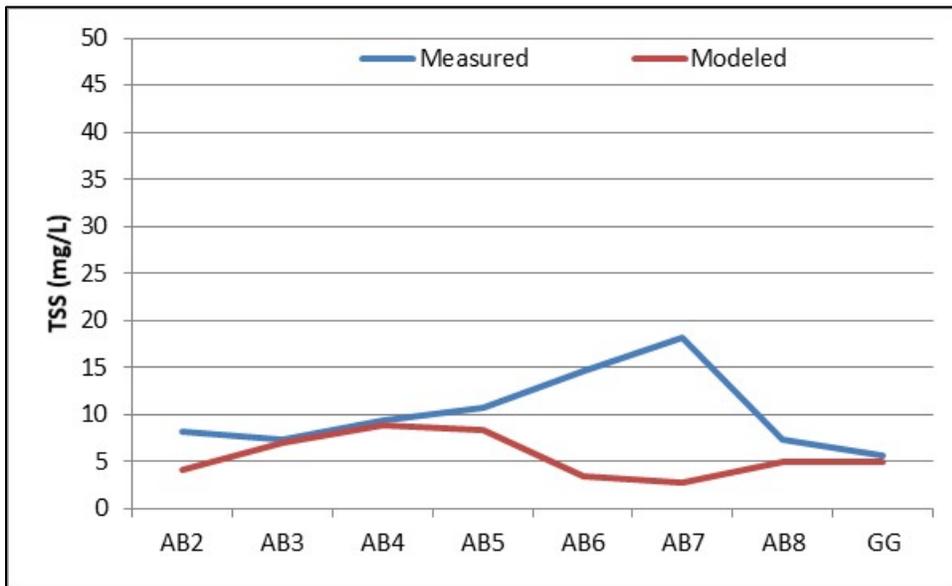


Figure G-4 Calibration of TSS in the Adams Bayou WASP model

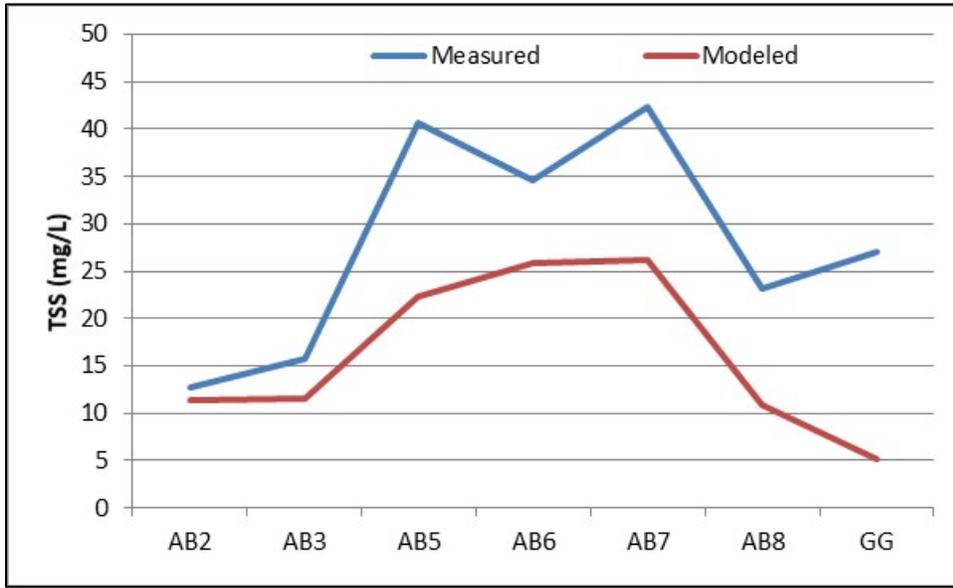


Figure G-5 Validation of TSS in the Adams Bayou WASP model

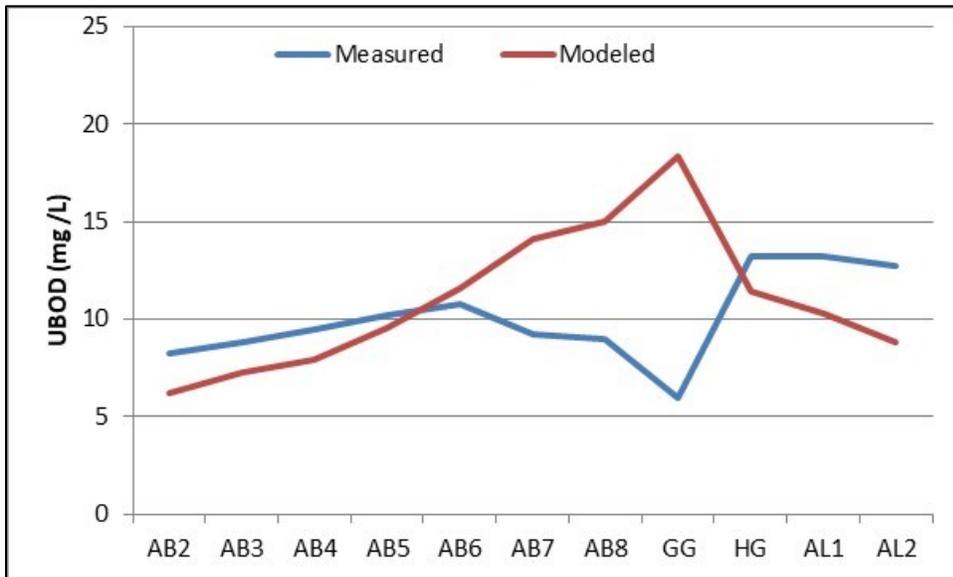


Figure G-6 Calibration of ultimate cBOD in the Adams Bayou WASP model

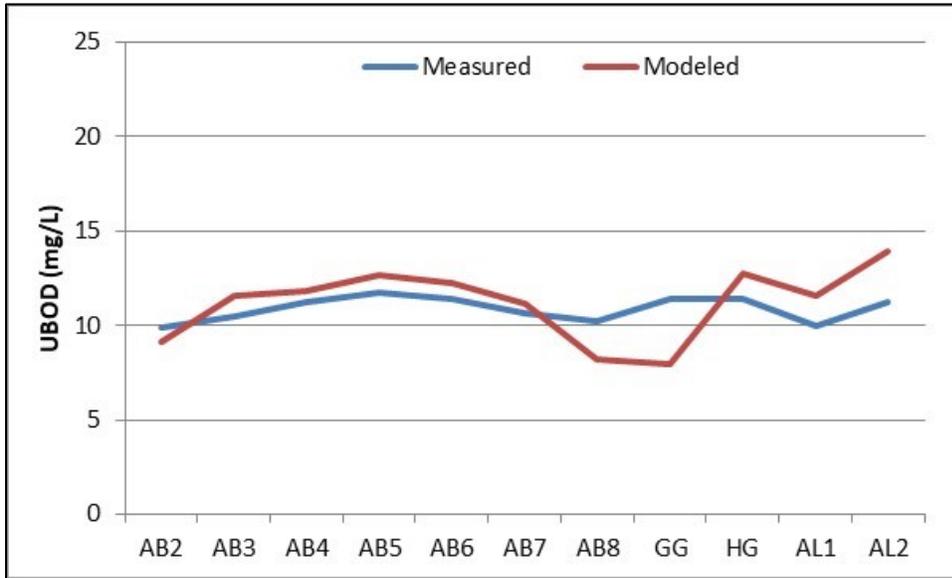


Figure G-7 Validation of ultimate cBOD in the Adams Bayou WASP model

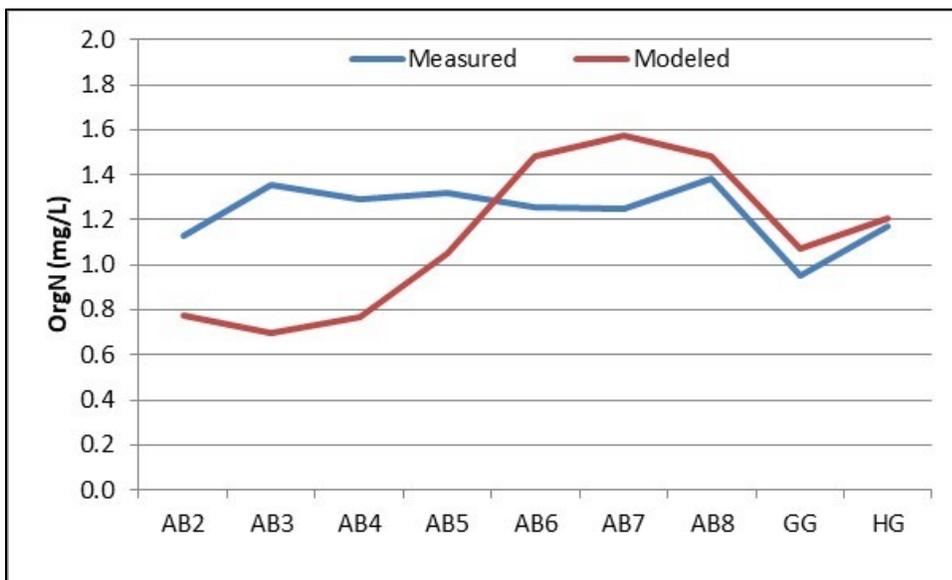


Figure G-8 Calibration of OrgN in the Adams Bayou WASP model

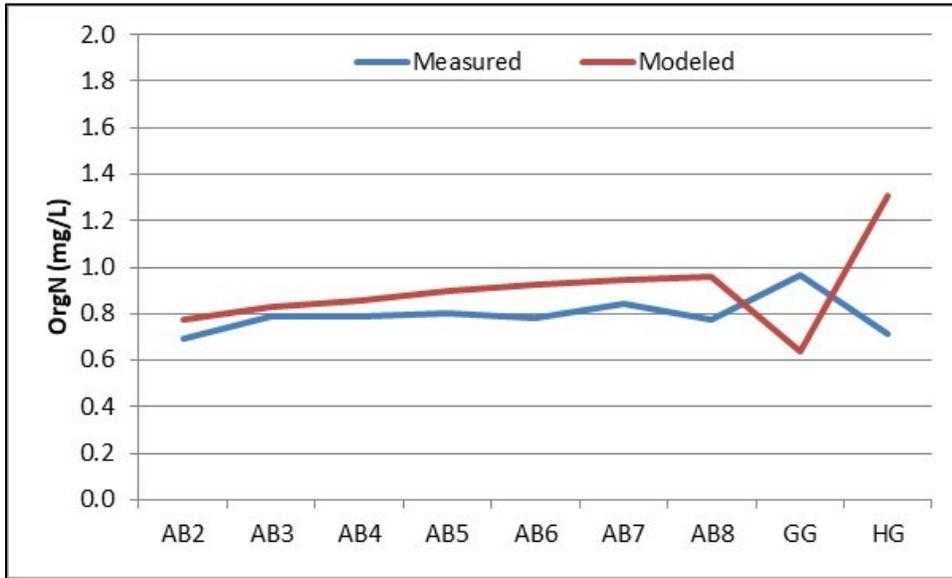


Figure G-9 Validation of OrgN in the Adams Bayou WASP model

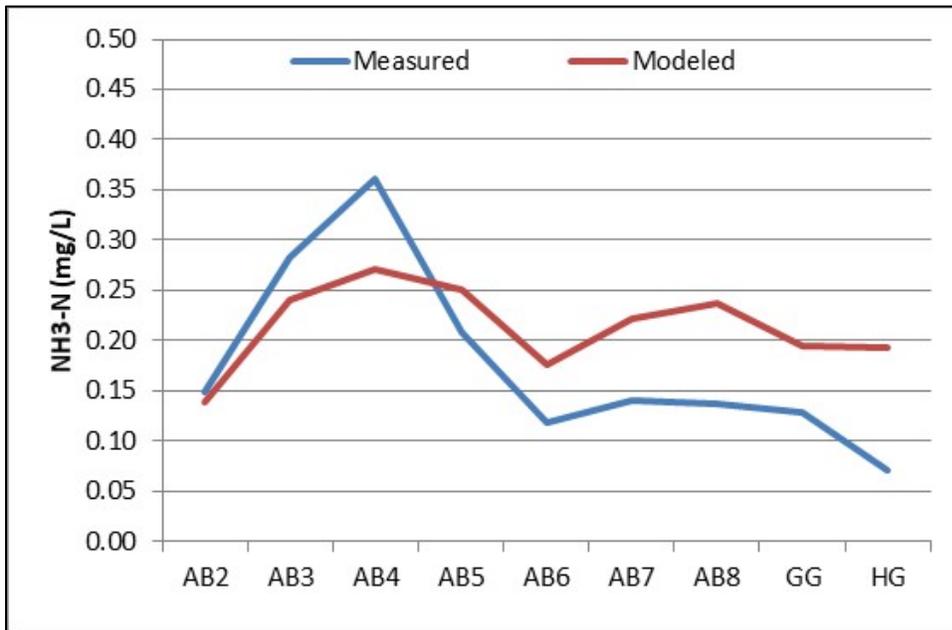


Figure G-10 Calibration of NH₃-N in the Adams Bayou WASP model

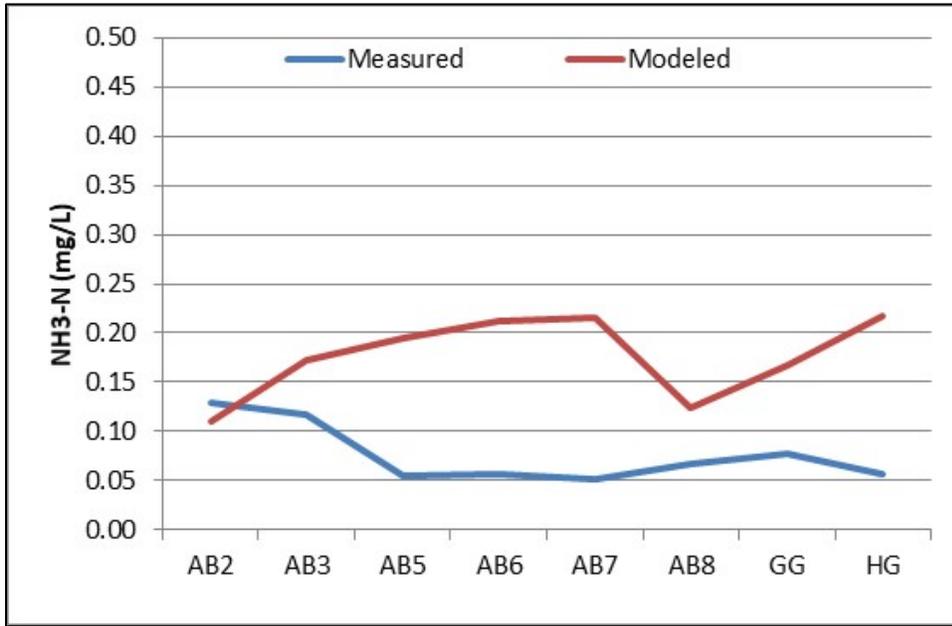


Figure G-11 Validation of NH₃-N in the Adams Bayou WASP model

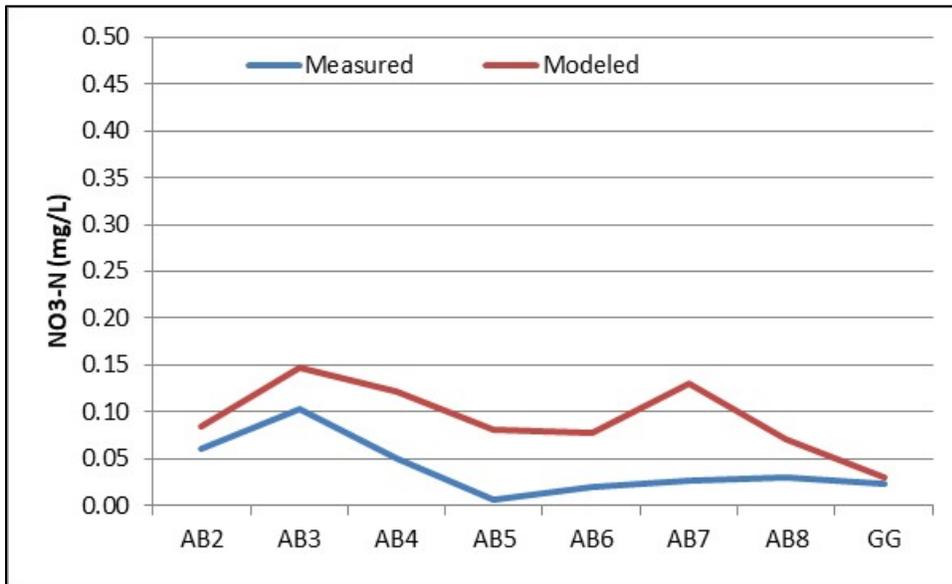


Figure G-12 Calibration of NO₃-N in the Adams Bayou WASP model

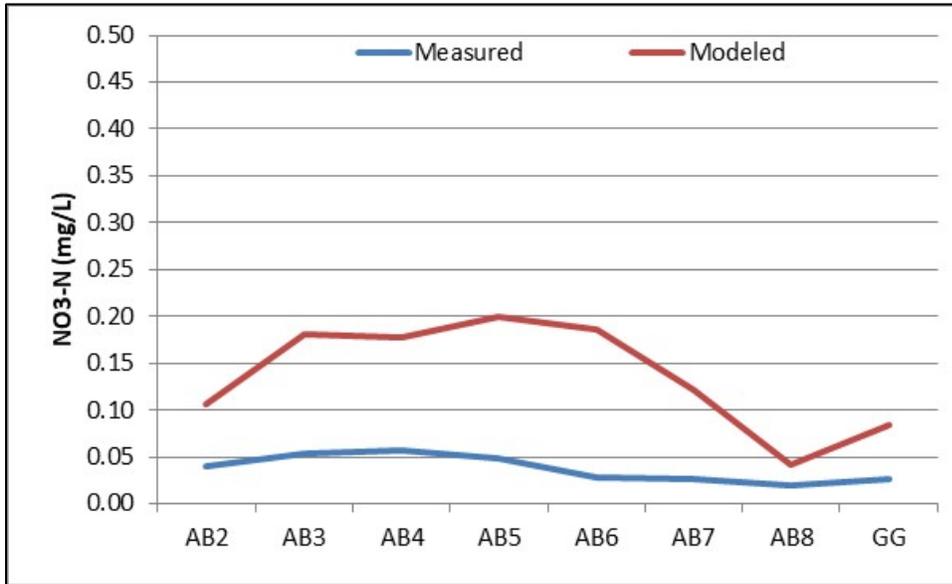


Figure G-13 Validation of NO₃N in the Adams Bayou WASP model

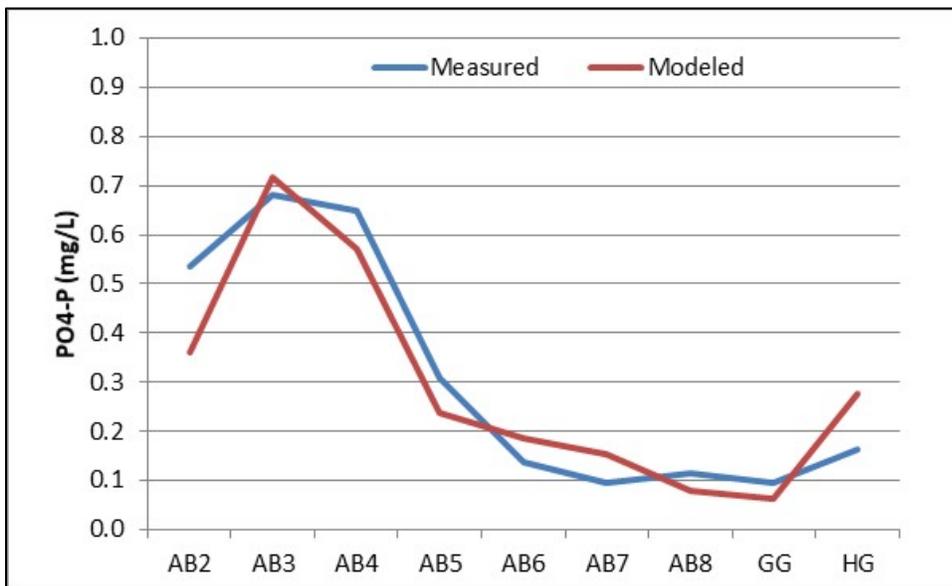


Figure G-14 Calibration of PO₄P in the Adams Bayou WASP model

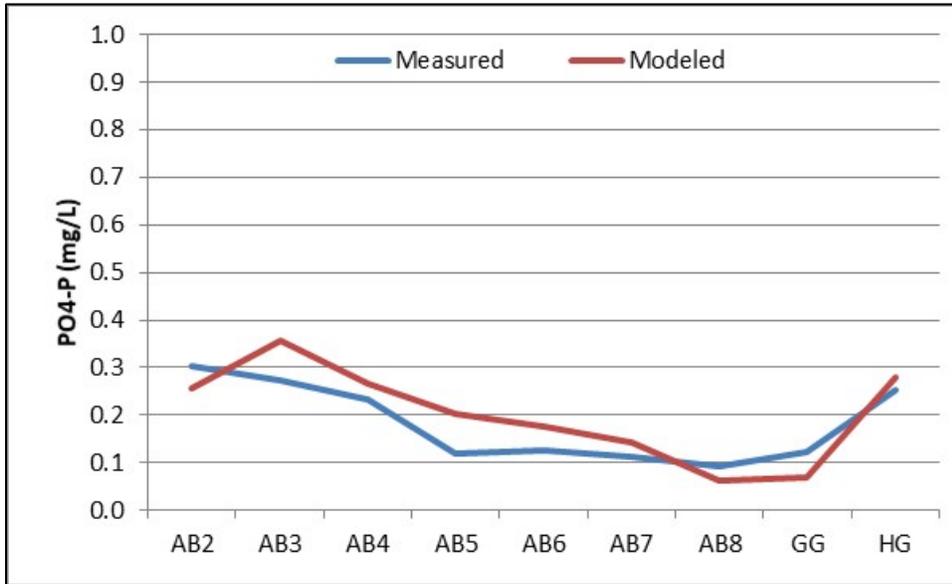


Figure G-15 Validation of PO₄P in the Adams Bayou WASP model

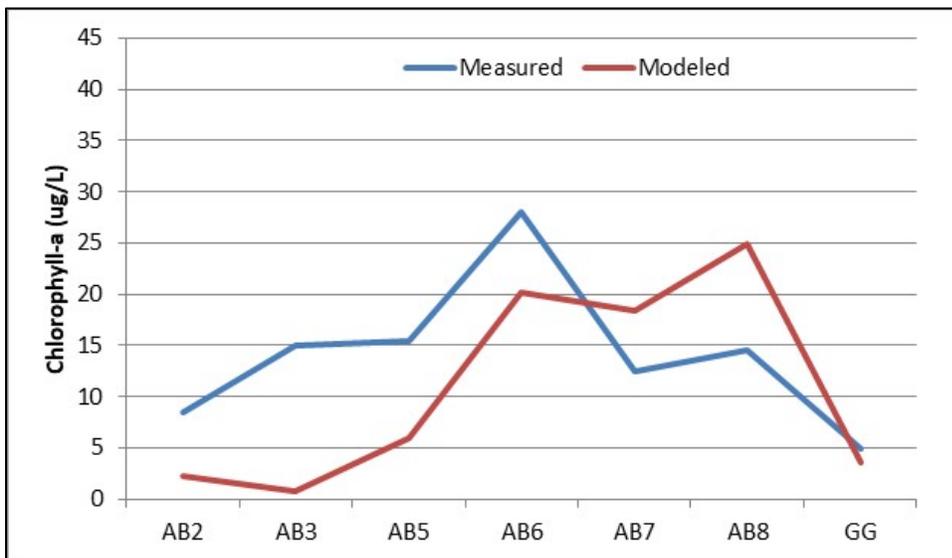


Figure G-16 Calibration of Chlorophyll-a in the Adams Bayou WASP model

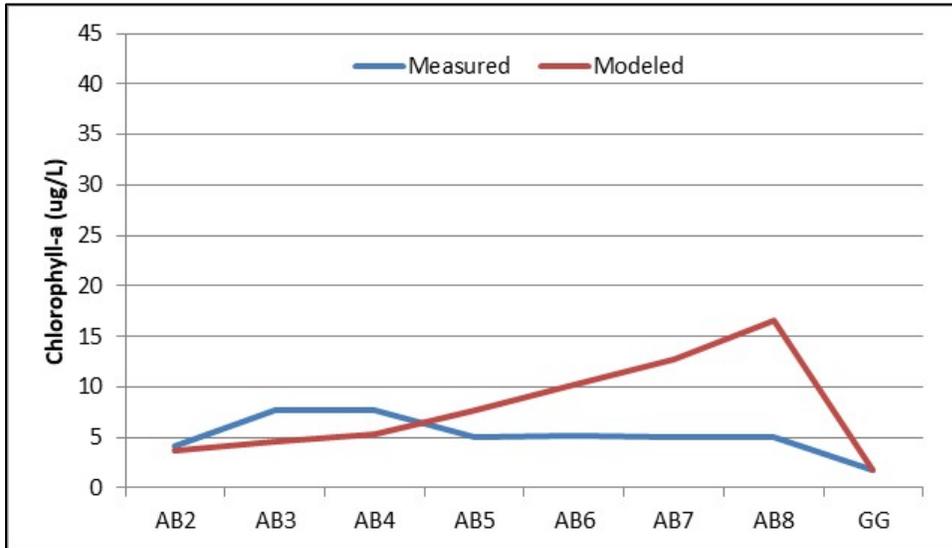


Figure G-17 Validation of Chlorophyll-a in the Adams Bayou WASP model

Appendix H Goodness-of-fit for the Cow Bayou WASP Model

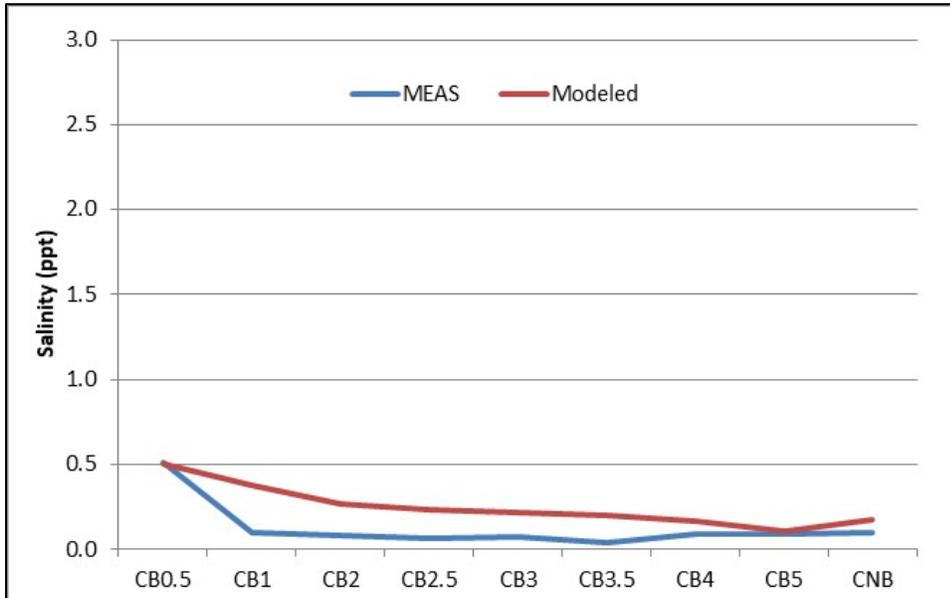


Figure H-1 Calibration of salinity in the Cow Bayou WASP model

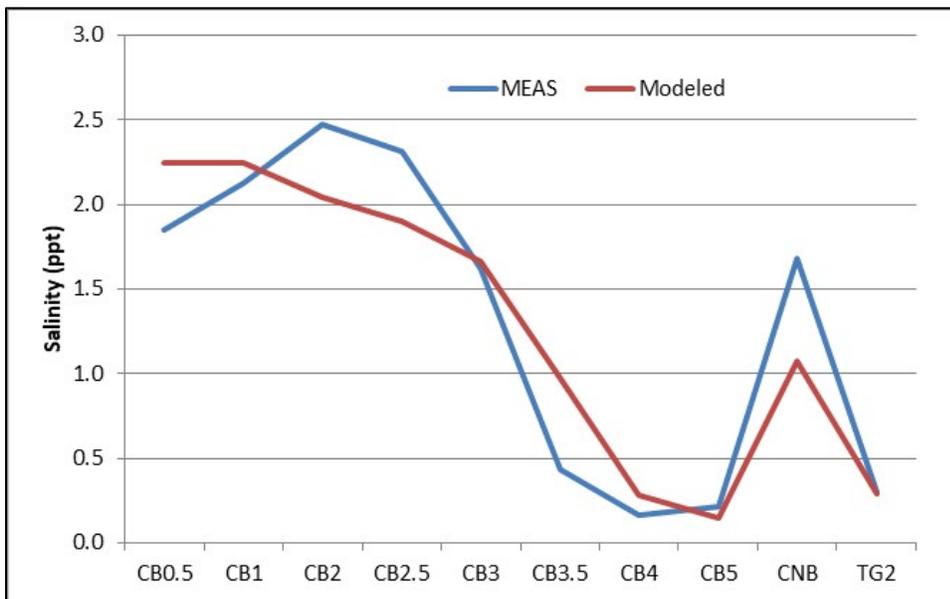


Figure H-2 Validation of salinity in the Cow Bayou WASP model

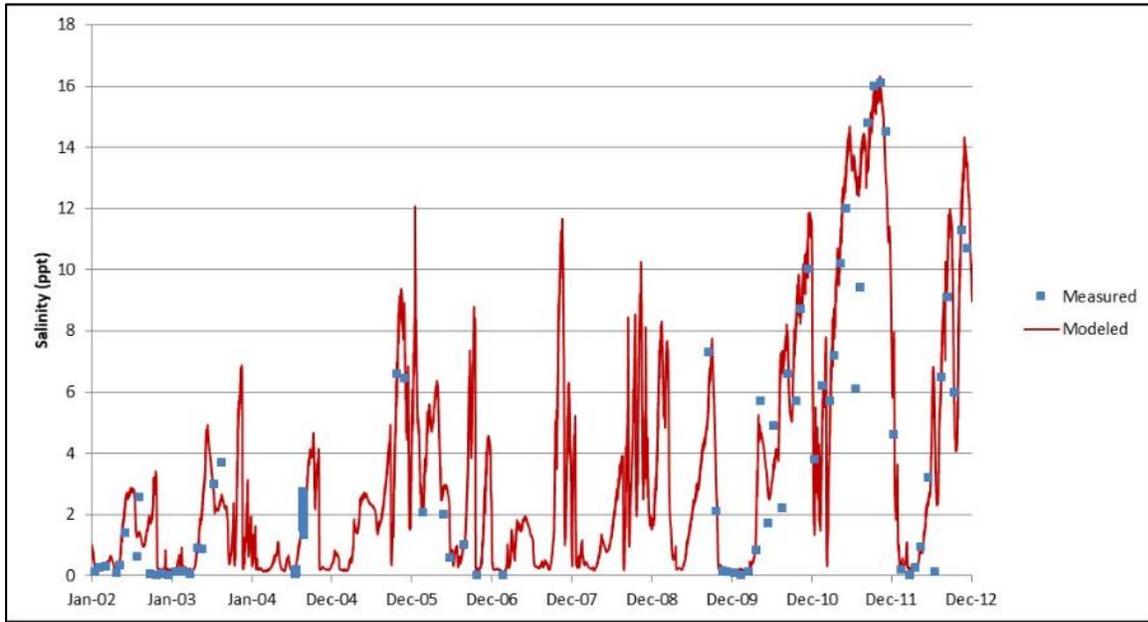


Figure H-3 Long-term validation of salinity calibration at Cow Bayou station CB1

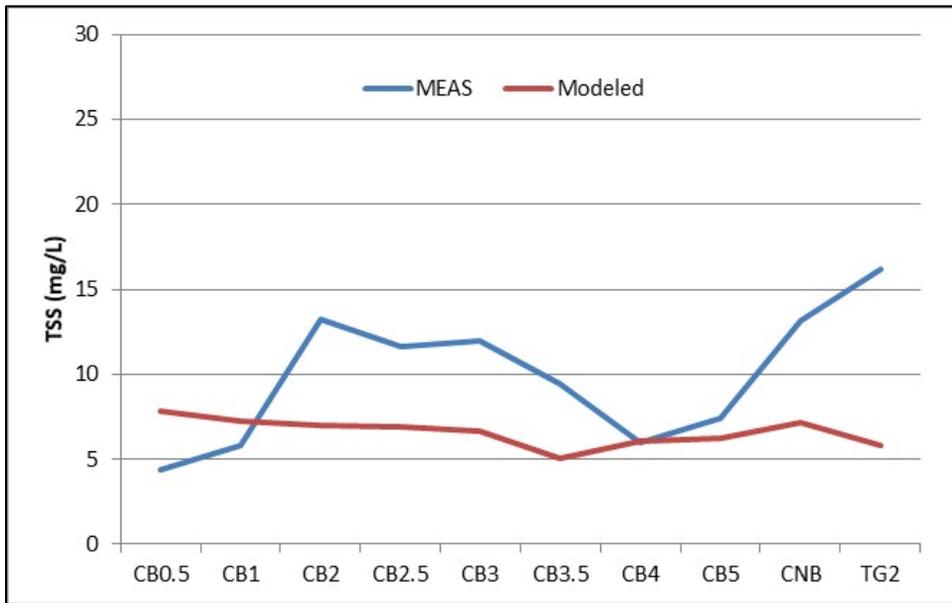


Figure H-4 Calibration of salinity in the Cow Bayou WASP model

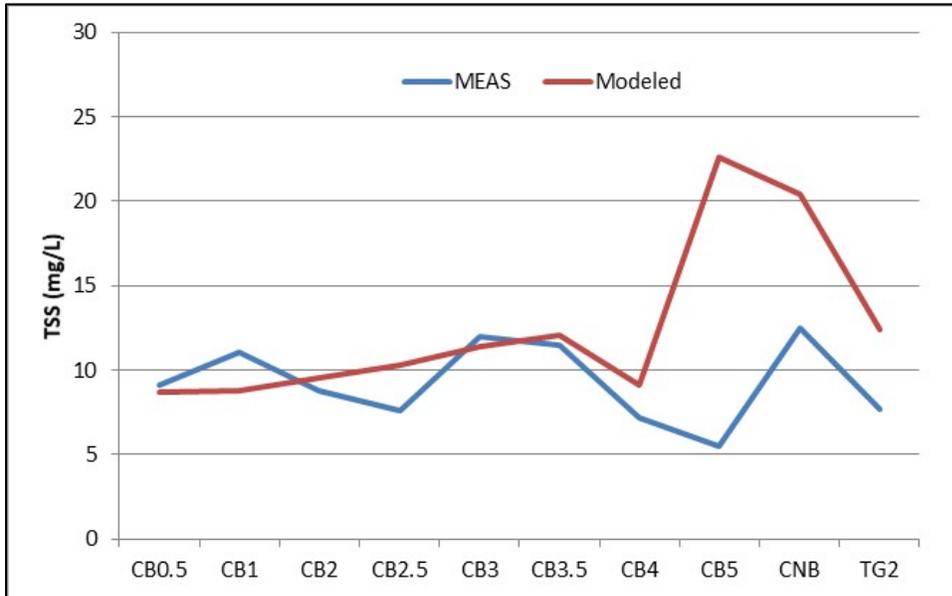


Figure H-5 Validation of TSS in the Cow Bayou WASP model

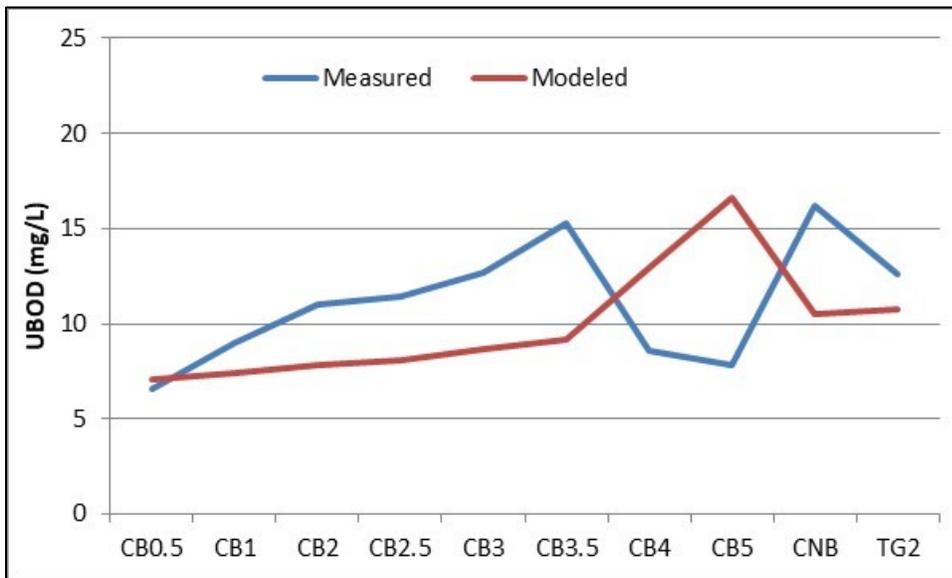


Figure H-6 Calibration of ultimate cBOD in the Cow Bayou WASP model

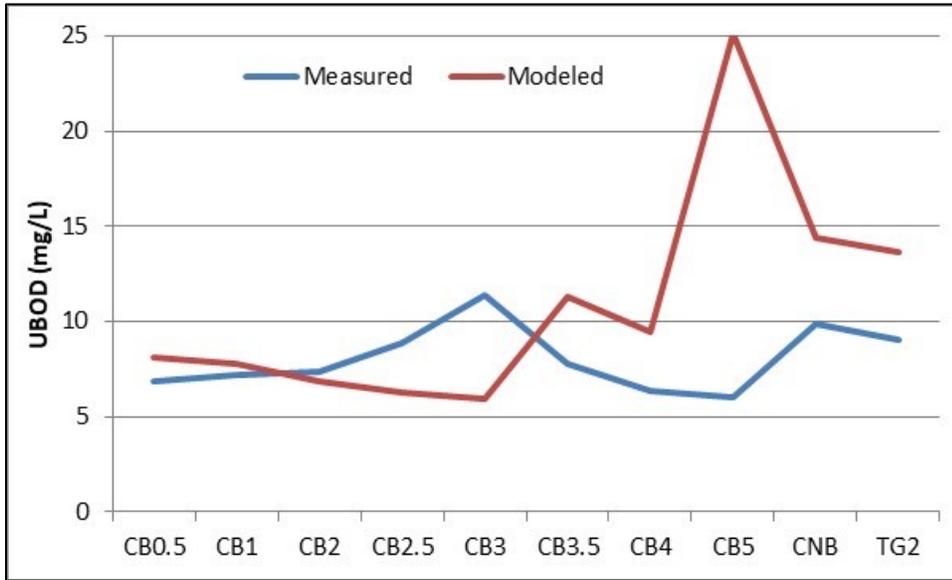


Figure H-7 Validation of ultimate cBOD in the Cow Bayou WASP model

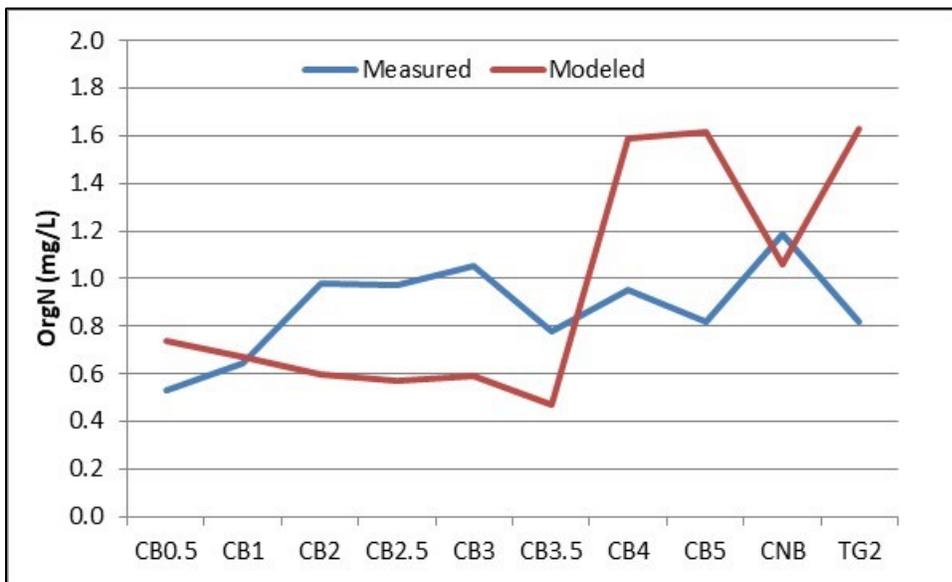


Figure H-8 Calibration of OrgN in the Cow Bayou WASP model

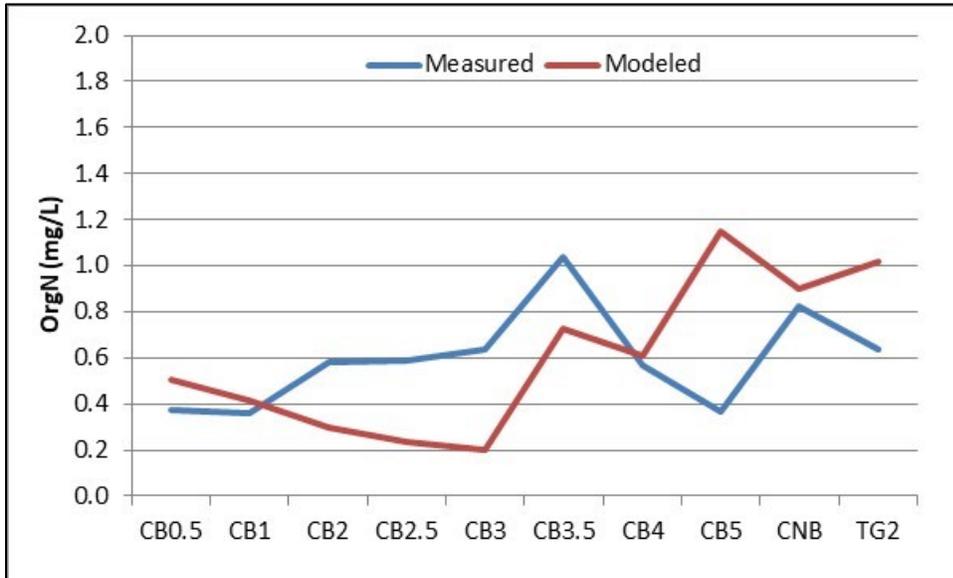


Figure H-9 Validation of OrgN in the Cow Bayou WASP model

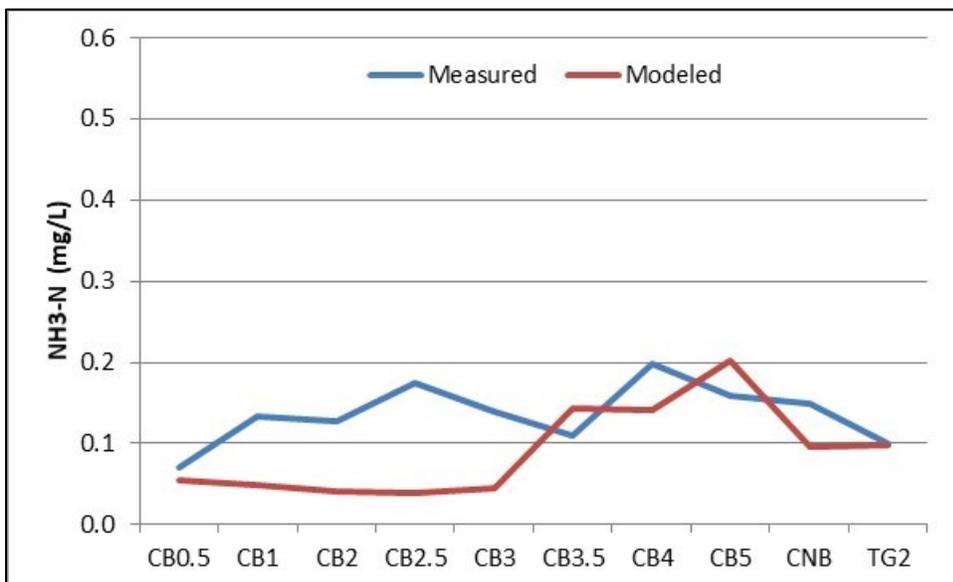


Figure H-10 Calibration of NH₃-N in the Cow Bayou WASP model

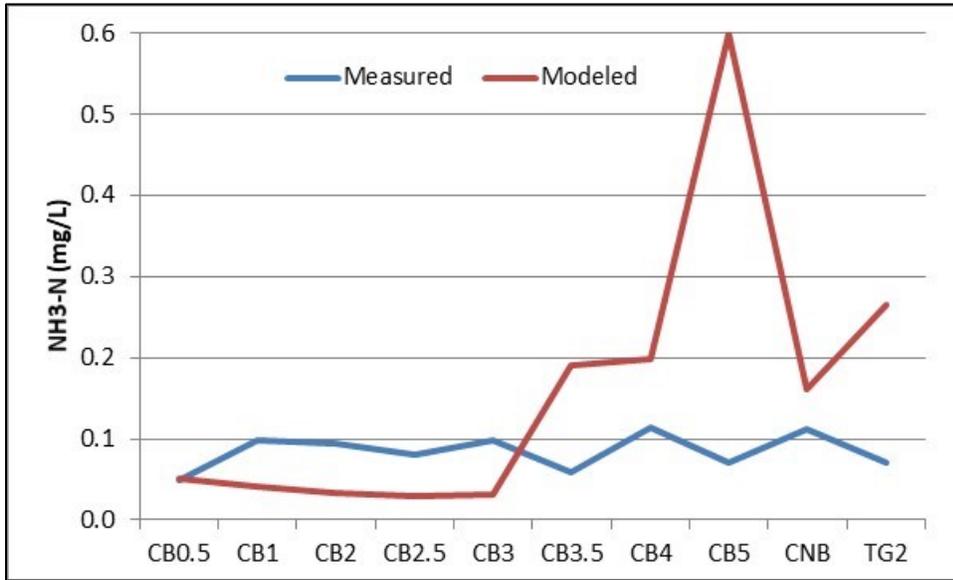


Figure H-11 Validation of NH₃-N in the Cow Bayou WASP model

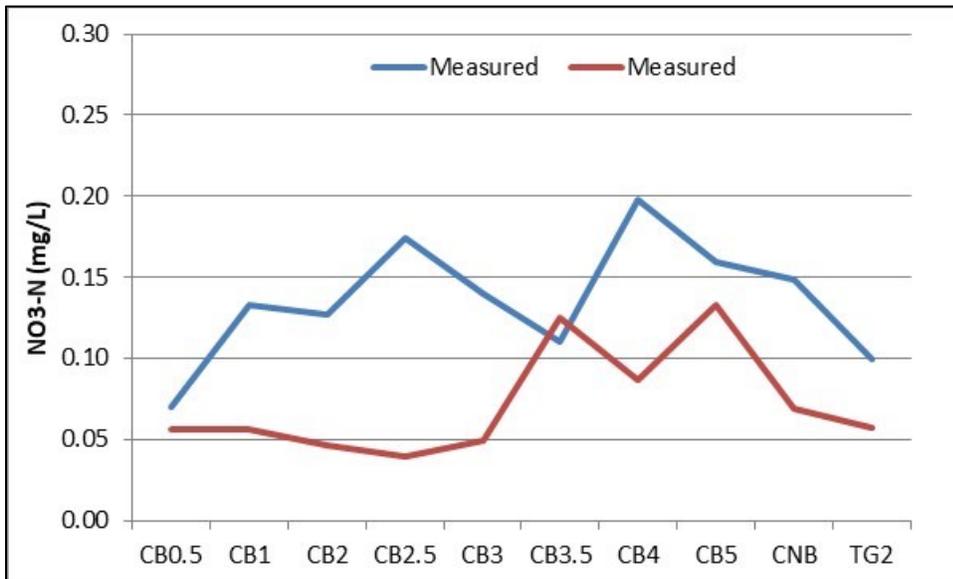


Figure H-12 Calibration of NO₃-N in the Cow Bayou WASP model

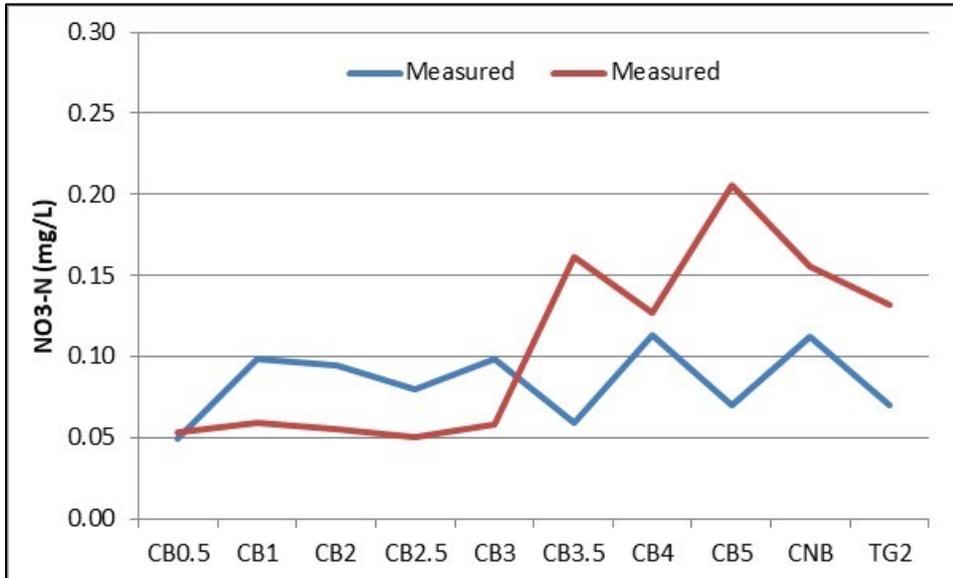


Figure H-13 Validation of NO₃N in the Cow Bayou WASP model

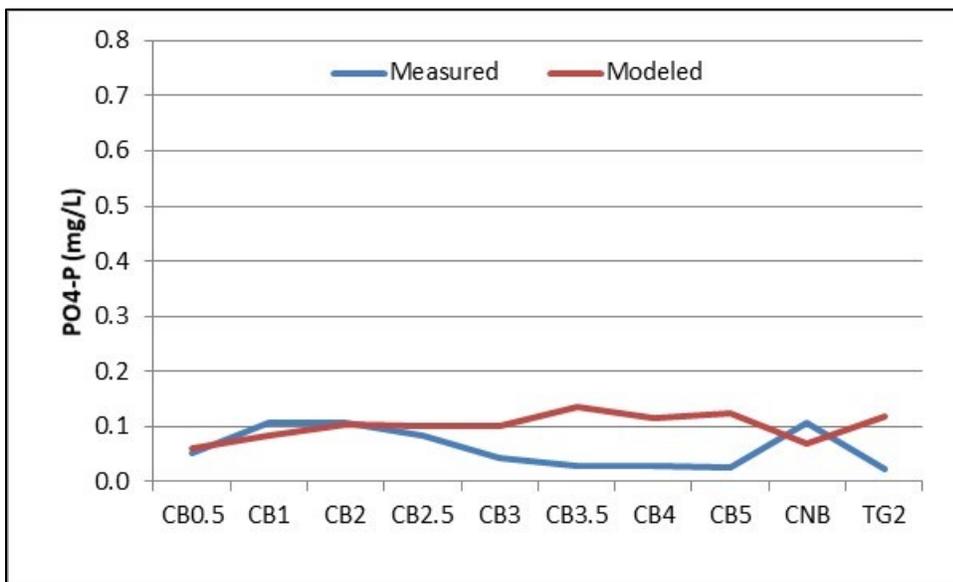


Figure H-14 Calibration of PO₄P in the Cow Bayou WASP model

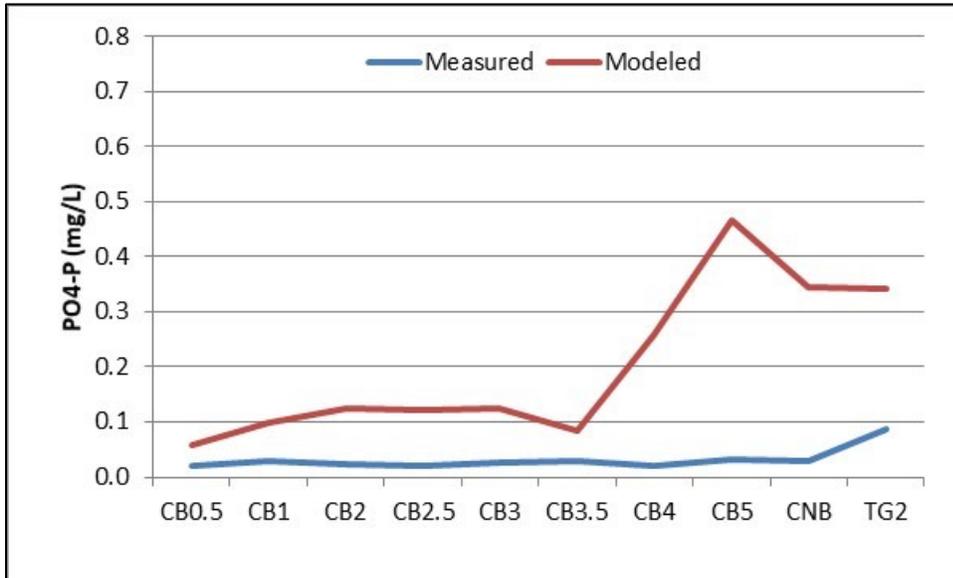


Figure H-15 Validation of PO₄P in the Cow Bayou WASP model

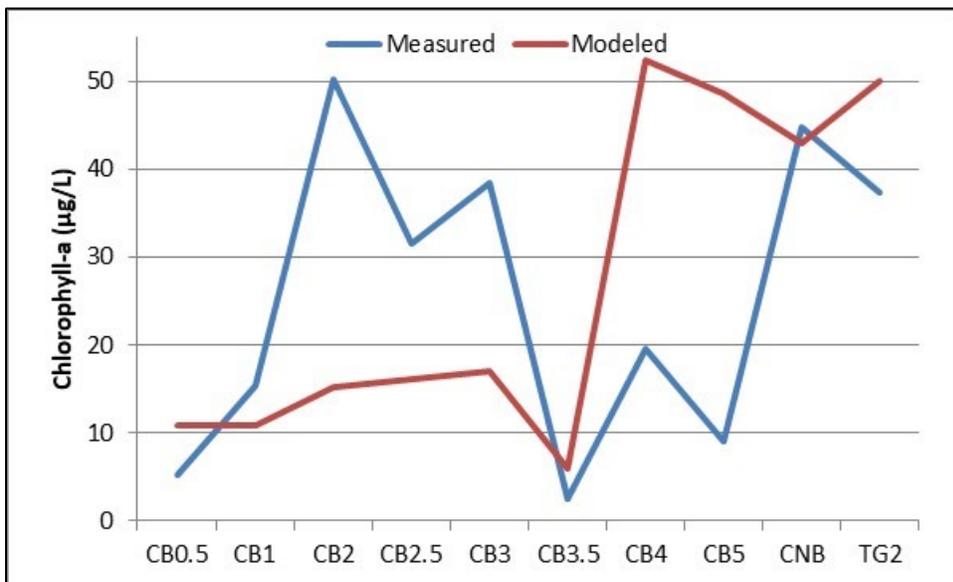


Figure H-16 Calibration of Chlorophyll-a in the Cow Bayou WASP model

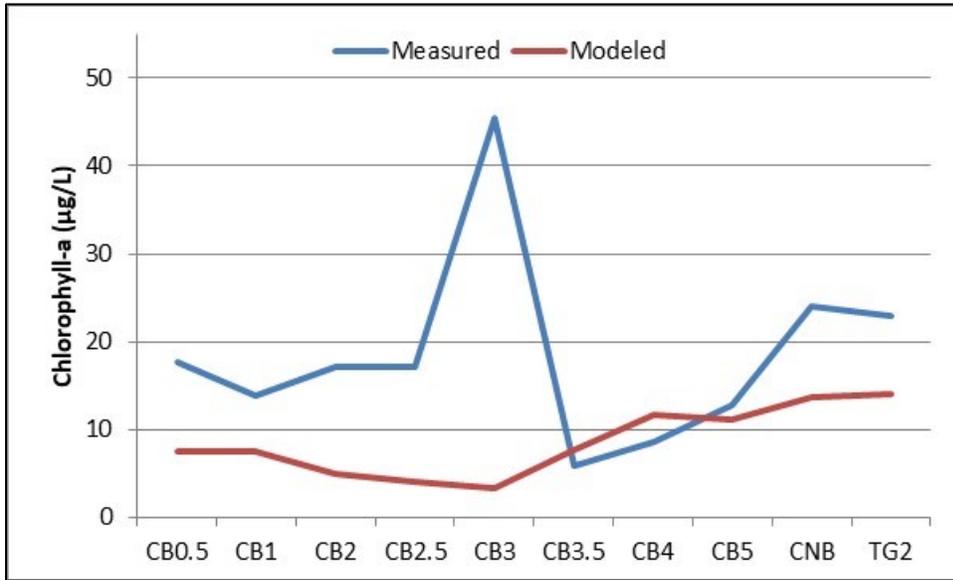


Figure H-17 Validation of Chlorophyll-a in the Cow Bayou WASP model